



NORTH WEST SURVEY CORPORATION INTERNATIONAL LTD.

Land, Aerial And Photogrammetric Surveyors

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REPORT ON
HORIZONTAL AND VERTICAL CONTROL SURVEY
FOR
CYPRUS ANVIL MINING CORPORATION LIMITED
FARO—VANGORDA—SWIM LAKE AREA
MAP SHEET 105 K/1, 2, 3, 4, 5, 6, 7 & 8, Y.T.
1979 001509

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INTRODUCTION

In 1979 North West Survey Corporation Yukon Ltd. was engaged by the Exploration Department, Cyprus Anvil Mines Corporation Limited to perform a control survey in the Faro—Vangorda—Swim Lake Area within Map Sheets 105 K/1, 2, 3, 4, 5, 6, 7 and 8. The purpose of the control survey was threefold:

1. To provide detailed ground control for a photogrammetric mapping program providing 1:5,000, 5 metre contours and 1:2,000, 2⁵ metre contours orthophoto and line mapping.
2. To amalgamate, consolidate and confirm all of the various control surveys existing in the area to a common grid and elevation datum.
3. To provide a monumented and accurate control survey within the area as a framework for future surveys during the various exploration programs.

Considerable work had been done by North West Survey Corp. and its associated company Hosford, Impey and Welter Ltd. for Cyprus Anvil and Kerr Addison Mines Ltd. in the period 1966 to 1978. Several control surveys were performed for Anvil Mining Corporation under instructions from the Surveyor General

of Canada in the Vangorda, Pelly, Blind Creek and Rose Creek areas October, 1966 to March, 1968 by Paul S. White, D.L.S. (see CLSR Plan 55818). At that time astronomic observations and control ties were made to existing Army Survey Monuments 67A24 and 67A55. The field notes were presented to the Surveyor General's office and a compass rule adjustment was performed. Additional control surveys in the immediate mine area were performed between 1970 to 1975. A control survey in the Grum—Vangorda area performed for Kerr Addison Mines Ltd. in 1975 was tied into the Vangorda control traverse. Again at the request of the Exploration Dept. additional control points were established for photogrammetric mapping in 1976. A compass rule adjustment of this network indicated some rather significant discrepancies as compared to the 1966-68 adjustment. The 1976 field returns which included re-measurements on several lines in the 1966-68 traverse were submitted to the Surveyor General's office for a readjustment in the GALS 2 program. That adjustment was designated fourth order because of distortion introduced by Army Survey Monuments 67A24, 67A25 and 67A55.

FIELD PROCEDURES

An area of 1400 sq km required photogrammetric mapping control and was within Map Sheets 105 K/1, 2, 3, 4, 5, 6, 7 and 8. The area has considerable changes in relief from elevations of 600 metres along the Pelly River to ridges of 2000 metres by Mt. Mye. The relief provided excellent visibility between stations for a combined traverse and triangulation control survey framework.

Considerable time was spent in the office in performing a map reconnaissance of the area prior to the field work. All of the available survey information was amassed and plotted on a 1:50,000 topographic map base. This was provided to the photogrammetrists within North West Survey Corp. to provide input as to the additional horizontal and vertical stations required. In addition the GALS 2 adjustment of the 1976 survey program was reviewed to determine weaknesses or observations requiring verification. The location of photogrammetric stations was submitted to Stan Buziak, Cyprus Anvil for establishing and targetting prior to aerial photography. The field work commenced July 16, 1979 at which time all targets were in place. Field observations were made to second or third order specifications according to "Specifications and Recommendations for Control Surveys and Survey Markers"

as published by Geodetic Survey Canada, 1978. Directions were observed for a minimum of 3 sets (forward and reverse) with Wild T2 transits. Lines were measured with either CA1000 Tellurometers (over 6 km), an AGA Model 78 Laser Geodimeter (1 km to 6 km) or a Hewlett Packard 3805A (less than 1 km). Elevations were determined from simultaneous trigonometric levelling techniques. We were also requested to place additional control stations in the vicinity of the Faro Open Pit and establish positions on those on both the Cyprus Anvil Mine Grid and Datum and also the UTM Coordinate Grid and Geodetic datum. In addition detailed control was required in the Dy and Vangorda areas for diamond drill hole surveys.

Monumentation usually consisted of a 1.5 cm x 0.75 m iron bar driven to within 0.1 m of the ground. A 10 cm x 10 cm x 1.2 m red wooden post with hole drilled in the base was placed over the iron bar. In addition at most stations a wooden survey tripod approximately 2.0 m high has been constructed to further identify the survey monument. This was felt particularly important in the Dy—Grum—Vangorda areas where considerable exploration work is underway. In a number of places, where possible, rock posts have been cemented into bedrock. The details of the various monuments and their ancillary monumentation is enclosed in Figure 2. Attached to every monument or tripod was a 1" yellow plastic disc imprinted with the unique station number. Four Army Survey Establishment third-order monuments were integrated into the control survey. Those

monuments are 6785000-67A35, 6785001-67A24, 678566-67A25 and 678567-67A55. In addition a total of 5 first order Geodetic Bench Marks along the Campbell Highway between Faro and Ross River were located and tied by simultaneous trigonometric levelling techniques to the control survey. Those Geodetic Bench Marks are 72Y230, 72Y235, 72Y246, 72Y247 and GSC 758001. The field program went very well with minimal down time due to weather and only some delays due to helicopter availability. The main control survey was finished July 30, 1979 with some detailed control performed later in the Dy area. Aerial photography by our company aircraft at a scale of 1:35,000, 1:20,000 and 1:8,000 was completed of different areas within the survey area depending upon the photogrammetric requirements in August/September, 1979.

PRELIMINARY REDUCTIONS

Preliminary reductions involved the 1979 work plus all of that work performed by our firm in preceding years. The original field notes were reviewed and their results confirmed. All horizontal angles were reduced to a common reference object for input into the adjustment program. All measured distances were corrected for slope and reduced to sea level. Elevation differences were computed utilizing simultaneous trigonometric levelling reduction techniques. Preliminary geographic coordinates were computed from existing UTM coordinates again, for input into the adjustment program.

Considerable time was spent in the preliminary reduction of the pre 1979 data to quantitatively and qualitatively assess it as to its accuracy and reliability prior to final adjustment.

FINAL ADJUSTMENT

The amount of data and complex nature of the control survey necessitated a rigorous adjustment on a large computer. Accordingly the horizontal and vertical data was processed through programs GANET and LEVELOB as developed by the Geodetic Survey of Canada. This work was completed by our associated company A.E. Peterson Consulting Ltd. utilizing computing facilities within our Edmonton office.

Program GANET recently developed by the Geodetic Survey of Canada integrates observed directions and distances into a geodetic adjustment and also provides a rigorous evaluation compatible with present Geodetic Survey techniques. The data is adjusted and evaluated in a least squares process with proper variance-covariance matrices and error modelling. The purpose of program LEVELOB is to give a least squares adjustment for level nets using observation equations. The program provides a least squares adjustment of junction elevations and link differences with their residuals and standard deviations as output. GANET and LEVELOB adjustments are done independently of each other. For both the horizontal and vertical adjustments the input observations and their estimated standard deviations are required.

In GANET the weight for a direction, angle or azimuth is:

$$P = \left[\frac{1.0313}{\sigma} \right]^2$$
 where σ is a priori standard deviation in seconds. Standard deviations for 2, 3, 4 or 6 sets of observations are 4", 2.5", 2.25" and 2.0", respectively. To obtain the weight of lengths: $P = \left[\frac{5}{\sigma} \right]^2$ where σ is the a priori standard deviation in parts per million. The values for the AGA 78, CA1000 and HP3805A were established as follows: 1 cm + 2 ppm, 3 cm + 10 ppm and 0.3 cm + 10 ppm, respectively. All of the data, a total of 110 stations, 487 directions and 229 distances were listed and prepared in GANET format and entered into the GANET program for adjustment. Some difficulty was experienced in isolating some reduction errors and in converting the original station numbers to the 1979 station numbering. Stations 6785000, 6785001, 678566 and 678567 were held fixed in the adjustment. Fixed values were provided by Geodetic Survey of Canada in September, 1979 being the most recent values from the readjustment of existing data of the Yukon framework by introduction of satellite Doppler observations. The fixed adjustment provided an estimated variance factor after adjustment of 2.414. Interstation error ellipses were obtained for each station, as to the relative accuracy between that station and all directly connected stations and all stations within a selected radius.

The interstation elevation differences were prepared for program LEVELOB. All link weights were calculated by an estimated vertical angle error of 7" and a height of instrument error of 0.030 m. Geodetic Bench Marks 758001, 72Y230, 72Y235,

72Y246 and 72Y247 were held fixed at their published values in
the .LEVELOB adjustment.

ANALYSIS OF RESULTS

The constrained adjustment indicated some angular distortion at 1480-BC13A (adjacent to 678566) to 678576 and 1445-HIW 16. In addition the length 1450-HIW 6 to 1462-HIW 9 indicated a 86 ppm correction or 44 cm.

Classification of a control survey is based on a comparison of a computed relative accuracy and the ppm allowed by the specifications for each order of survey. The classes as determined within "Specifications and Recommendations for Control Surveys and Survey Markers - 1978", Geodetic Survey of Canada for lines longer than 5 k are as follows:

first order	relative accuracy < 20 ppm
second order	20 ppm < relative accuracy < 50 ppm
third order	50 ppm < relative accuracy < 120 ppm
fourth order	120 ppm < relative accuracy < 300 ppm

Relative accuracy, computed as 2.45 times the semi major axis divided by distance and expressed in ppm is printed in the righthand column of GANET for use in station classification. As the variance factor after adjustment is 2.414 and the apriori variance factor was 1.000 all of the error ellipses have to be scaled upwards by the square root of 2.41 or 1.55. An inspection of the GANET error ellipses indicates that approximately 75% fall under second order classification with the remainder being of

third order accuracy. Therefore from the relative precisions we can classify the network as third order according to the 1978 Geodetic Publication "Specifications and Recommendations for Control Surveys and Survey Markers".

The adjustment utilizing the readjusted position of the four Army Survey Establishment stations in 1979 indicated good consistency with those values.

The LEVELOB adjusted elevation matrix indicates an average of 0.12 m standard deviation on most of the control stations. Considering the length of the lines, relief involved and the lack of geodetic elevations to the north of the survey area the results are most satisfactory.

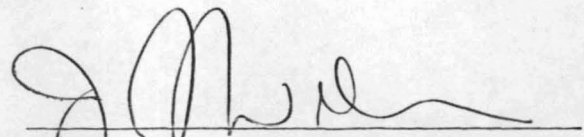
Figure 1 contains the station identifier, station name, geographic coordinates, Universal Transverse Mercator Coordinates, zone, scale factor and geodetic elevation. The scale factor correction is significant and must be applied in performing future survey ties of a precise nature from any control station. All horizontal coordinates, both geographic and UTM are expressed at sea level elevations and accordingly any future survey work again must be reduced to sea level. Appendix A from the Manual of Instructions for the Survey of Canada Lands outlines the procedure in computing coordinates on the Universal Transverse Mercator System.

Figure 2 indicates the monuments placed and ancillary monumentation at the various stations.

Appendix B contains the GANET printout of the control survey.

Appendix C contains the Levelob printout of the control survey.

Target identification and photogrammetric adjustment performed to date on the 1:35,000 and 1:20,000 photo has provided exceptional results.



J.F. Welter, A.L.S., C.L.S.

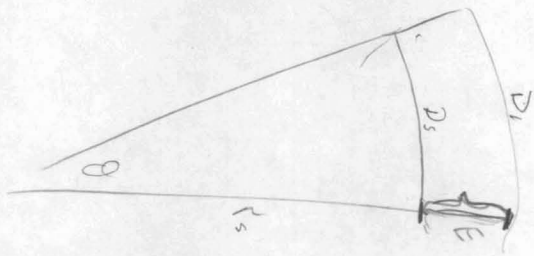
FIGURE 1

FINAL ADJUSTED COORDINATES AND ELEVATIONS

CYPRUS ANVIL MINES CONTROL

MAP SHEET 105 K, Y.T.

1979



$$\frac{r_s}{r_s + E} \times$$

$$D_s = r_s \theta$$

$$r_s = \frac{D_s}{\theta}$$

$$\frac{D_s}{D_1} = \frac{r_s}{r_s + E}$$

$$D_s = \frac{r_s}{r_s + E} \times D_1$$

$$r_s = 20889000 \mu = 6366963 \text{ meters}$$

1300 meters
14000 meters

.99979586
.99978016

DEPARTMENT OF ENERGY, MINES, AND RESOURCES

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GEODETTIC SURVEY OF CANADA--PROGRAM GALS
 MODIFIED BY DR. J. S. ALLMAN...OCTOBER 1975
 ELLIPSOID PARAMETERS USED - CLARKE 1866

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CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

INDEX WITH ADJUSTED CO-ORDINATES

PAGE	NUMBER	NAME	NET NO	GEODETTIC POSITION		UNIVERSAL TRANSVERSE MERCATOR				
				LATITUDE	LONGITUDE	NORTHING	EASTING	ZONE	SCALE	ELEVATION
1	6785000	67A35		62 1 3.46165 N	132 17 15.39127 W	6878910.487	641961.602	8	.9998469	1395.108
2	6785001	67A24		62 14 7.74481 N	132 52 .82460 W	6902038.968	610852.879	8	.9997505	1336.735
3	678566	67A25		62 17 46.57015 N	133 3 39.32790 W	6908491.552	600569.043	8	.9997239	1986.126
4	678567	67A55		62 18 9.46469 N	133 31 10.60857 W	6908571.320	576766.660	8	.9996722	1665.458
5	1470	RC 11		62 20 47.36501 N	133 30 5.90537 W	6913478.353	577585.377	8	.9996737	1682.061
6	1484			62 21 39.05957 N	133 28 2.48002 W	6915119.419	579322.505	8	.9996771	1034.002
7	1463	RC 2		62 19 57.27396 N	133 27 25.27378 W	6911982.826	579932.468	8	.9996783	1515.137
8	1420	WHI 3		62 20 45.04615 N	133 25 33.83900 W	6913499.548	581499.814	8	.9996814	1040.960
9	1481	HIW 2		62 22 48.66667 N	133 23 20.42559 W	6917371.631	583323.197	8	.9996850	1649.105
10	1447			62 24 56.11595 N	133 26 54.46415 W	6921239.806	580153.861	8	.9996787	1888.915
11	1464	HIW 3		62 22 58.80501 N	133 19 32.98327 W	6917768.321	586582.245	8	.9996918	1542.837
12	1494	HIW 4		62 22 1.03173 N	133 15 42.98007 W	6916068.062	589933.887	8	.9996991	1359.219
13	1483	PRI-7		62 21 31.20201 N	133 20 43.78535 W	6915031.721	585634.648	8	.9996898	1421.367
14	1487	PRI 4		62 21 22.74008 N	133 21 17.18750 W	6914757.659	585161.150	8	.9996888	1257.029
15	1485	TRI 18		62 21 42.42985 N	133 22 41.77931 W	6915336.139	583929.754	8	.9996863	1294.534
16	1486	PRI 6		62 20 56.36500 N	133 21 51.23905 W	6913929.197	584692.259	8	.9996879	1190.272
17	1419	VG 19		62 20 28.85785 N	133 23 17.66560 W	6913046.918	583470.671	8	.9996853	1094.794
18	1418	VG 18		62 20 6.83258 N	133 22 57.23545 W	6912372.793	583781.572	8	.9996860	1066.904
19	1417	WHI 1-71		62 20 .61278 N	133 21 47.85762 W	6912205.464	584794.540	8	.9996880	1083.186
20	1416	VG 16		62 19 29.75367 N	133 20 51.02962 W	6911271.486	585626.528	8	.9996898	1088.702
21	1415	VG 15A		62 19 34.18653 N	133 20 37.81880 W	6911413.499	585813.136	8	.9996902	1110.196
22	1475	HIW 8		62 18 38.93608 N	133 21 40.95783 W	6909680.924	584947.828	8	.9996884	1397.164
23	1477			62 18 31.39920 N	133 24 1.27900 W	6909397.164	582933.233	8	.9996842	1445.491
24	1493	HIW 12		62 25 31.48746 N	133 13 58.25227 W	6922620.118	591260.878	8	.9997020	1615.186
25	1492	HIW 13		62 23 5.65864 N	133 4 27.22874 W	6918342.598	599585.104	8	.9997215	1600.957
26	1476	PE 1		62 17 14.13463 N	133 23 6.59801 W	6907026.173	583780.263	8	.9996860	1521.994
27	1478	PE 2		62 15 47.22429 N	133 22 30.00393 W	6904350.400	584375.087	8	.9996872	1360.385
28	1489	HIW 5		62 20 30.99619 N	133 15 5.17338 W	6913296.806	590552.536	8	.9997004	1803.737
29	1450	HIW 6		62 18 29.16551 N	133 15 .02598 W	6909529.832	590728.547	8	.9997008	1738.945
30	1469	HIW 7		62 17 16.46373 N	133 18 12.60128 W	6907206.636	588014.643	8	.9996949	1421.790
31	1409	VG 9		62 16 56.83972 N	133 15 47.57622 W	6906654.938	590120.599	8	.9996995	1207.068
32	1410	VG 10		62 17 33.51492 N	133 16 36.63142 W	6907770.723	589363.394	8	.9996979	1205.178
33	1411	VG 11		62 17 34.05088 N	133 17 28.04395 W	6907767.660	588642.285	8	.9996962	1187.423
34	1412	VG 12		62 18 6.74816 N	133 18 16.92056 W	6908760.760	587911.640	8	.9996947	1172.242
35	1413	VG 13A		62 18 26.15748 N	133 19 2.47135 W	6909344.143	587239.993	8	.9996932	1151.568
36	1414	VG 14		62 18 33.84717 N	133 19 37.97487 W	6909568.798	586722.605	8	.9996921	1134.332
37	1407	VG 7		62 16 45.28092 N	133 13 51.50330 W	6906342.645	591803.078	8	.9997032	1331.654
38	1424	HIW 6KA		62 16 4.38474 N	133 13 34.71626 W	6905084.011	592079.705	8	.9997039	1308.019
39	1423	HIW 5KA		62 15 41.75696 N	133 13 28.38392 W	6904386.451	592190.211	8	.9997041	1276.447
40	1405	VG 5		62 16 2.81464 N	133 12 50.89938 W	6905052.811	592712.796	8	.9997053	1300.253
41	1422	HIW 4KA		62 16 1.94845 N	133 13 10.75466 W	6905018.124	592427.256	8	.9997066	1302.274
42	1461	HIW 1KA		62 15 27.03994 N	133 14 2.96382 W	6903917.487	591703.958	8	.9997030	1324.705
43	1495	HIW 15		62 21 11.82179 N	132 58 54.66078 W	6914966.630	604471.086	8	.9997337	1404.395
44	1453	HIW 10		62 15 18.92988 N	133 7 19.71470 W	6903830.314	597527.197	8	.9997165	1284.126

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 GEODETIC SURVEY OF CANADA—PROGRAM GALS
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CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

INDEX WITH ADJUSTED CO-ORDINATES

PAGE	NUMBER	NAME	NET NO	GEODETIC POSITION		UNIVERSAL TRANSVERSE MERCATOR				
				LATITUDE	LONGITUDE	NORTHING	EASTING	ZONE	SCALE	ELEVATION
45	1402	VG 2		62 14 51.78881 N	133 9 3.19097 W	6902947.662	596058.684	8	.9997130	1227.661
46	1403	VG 3		62 14 55.41990 N	133 9 54.74591 W	6903038.830	595311.699	8	.9997113	1214.248
47	1457	HIW 3KA		62 15 7.24264 N	133 10 20.82339 W	6903393.954	594925.154	8	.9997104	1220.405
48	14571	JK1		62 15 6.05187 N	133 10 16.50913 W	6903358.872	594988.429	8	.9997105	1222.825
49	1454	JK 4		62 15 15.13006 N	133 11 28.44826 W	6903610.569	593942.818	8	.9997081	1172.687
50	1452	HIW 2KA		62 15 5.12503 N	133 11 31.73301 W	6903299.710	593904.084	8	.9997080	1142.213
51	1459	JK 3		62 15 .78060 N	133 11 9.55580 W	6903174.255	594227.774	8	.9997088	1166.198
52	1460	IN 4		62 15 5.37079 N	133 11 20.64764 W	6903311.784	594063.786	8	.9997084	1150.246
53	1458	IN 1		62 15 3.23061 N	133 10 50.27274 W	6903257.861	594503.825	8	.9997094	1186.118
54	1456	IN 2		62 14 55.13679 N	133 10 54.75557 W	6903005.639	594446.191	8	.9997093	1161.114
55	1455	IN 3		62 14 44.53416 N	133 10 46.00311 W	6902681.167	594581.689	8	.9997096	1162.649
56	1451	JK 2		62 14 41.21131 N	133 11 3.59864 W	6902571.235	594330.698	8	.9997090	1163.629
57	1488	HIW 11		62 13 50.32688 N	133 9 10.26284 W	6901043.273	596010.921	8	.9997129	1195.614
58	1446	U+U 611		62 12 56.75509 N	133 11 38.09160 W	6899325.664	593923.169	8	.9997081	1390.257
59	1479	DY 1		62 13 59.54907 N	133 8 11.06300 W	6901353.077	596857.282	8	.9997149	1190.464
60	1471	DP 1		62 13 54.25466 N	133 7 40.92420 W	6901201.836	597297.047	8	.9997160	1131.941
61	1472	IB 751		62 13 48.47587 N	133 7 26.33675 W	6901029.193	597512.796	8	.9997165	1094.303
62	1473	IB 756		62 14 15.53238 N	133 7 26.60035 W	6901866.094	597484.731	8	.9997164	1147.940
63	1474	DP 2		62 13 52.59043 N	133 6 51.43413 W	6901171.085	598012.926	8	.9997177	1040.608
64	1443	BC 5		62 13 11.47555 N	133 6 22.96986 W	6899911.113	598461.016	8	.9997187	880.126
65	1449	BC 3		62 12 54.70737 N	133 7 43.07620 W	6899358.382	597307.685	8	.9997160	935.430
66	1439			62 11 52.48854 N	133 5 18.91853 W	6897494.701	599458.084	8	.9997212	1266.526
67	1440			62 11 37.84364 N	133 5 10.41581 W	6897045.267	599594.346	8	.9997215	1272.020
68	14401	1440 ECC		62 11 50.22474 N	133 5 21.26817 W	6897423.664	599426.197	8	.9997211	1268.308
69	1468	BC 7		62 13 47.46881 N	133 3 38.81585 W	6901094.790	600798.092	8	.9997244	785.463
70	1442			62 13 26.81359 N	133 0 46.83576 W	6900531.094	603300.292	8	.9997307	955.698
71	1448			62 12 36.49374 N	133 1 57.36924 W	6898943.288	602329.241	8	.9997283	1096.962
72	1444	SL 7		62 12 7.14119 N	133 0 13.08250 W	6898081.359	603863.625	8	.9997321	911.008
73	1467	BC 16		62 14 58.18988 N	133 1 9.46223 W	6903347.906	602887.105	8	.9997297	891.373
74	1438			62 16 39.52786 N	132 59 33.99491 W	6906525.317	604167.046	8	.9997329	1425.048
75	1466			62 16 25.32403 N	132 56 12.34680 W	6906177.337	607087.230	8	.9997405	866.848
76	1465	BC 20		62 16 57.27472 N	132 52 26.03098 W	6907271.331	610316.791	8	.9997491	858.193
77	1432	BC 17		62 14 50.64473 N	132 52 53.17233 W	6903341.244	610053.965	8	.9997484	1307.723
78	1441			62 10 44.75274 N	133 0 59.84336 W	6895511.837	603266.071	8	.9997306	1125.057
79	1429			62 8 26.70893 N	132 56 29.38229 W	6891363.508	607312.466	8	.9997411	963.003
80	1430	SL 12		62 10 28.66494 N	132 54 10.09305 W	6895200.836	609206.839	8	.9997461	961.825
81	1425			62 6 40.47308 N	132 50 45.66003 W	6888239.036	612397.846	8	.9997547	1069.259
82	1429			62 9 18.71490 N	132 45 57.54272 W	6893275.275	616404.080	8	.9997660	1113.342
83	1431			62 11 27.65971 N	132 42 33.36441 W	6897367.033	619217.317	8	.9997741	1110.953
84	1436			62 13 18.28917 N	132 45 34.96353 W	6900697.299	616474.368	8	.9997662	939.631
85	1433			62 14 1.61534 N	132 37 22.64477 W	6902284.784	623533.145	8	.9997869	1311.570
86	1435			62 17 55.69451 N	132 48 48.81881 W	6909182.809	613385.540	8	.9997575	885.537
87	1426	SL 13		62 3 50.36124 N	132 34 54.45288 W	6883463.751	626377.432	8	.9997956	1406.842
88	1404	VG 4		62 15 47.92032 N	133 11 33.05893 W	6904623.172	593847.979	8	.9997079	1300.062

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GEODETTIC SURVEY OF CANADA—PROGRAM GALS PAGE 113
 MODIFIED BY DR. J. S. ALLMAN...OCTOBER 1975
 ELLIPSOID PARAMETERS USED - CLARKE 1866

CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

INDEX WITH ADJUSTED CO-ORDINATES

PAGE	NUMBER	NAME	NET NO	GEODETTIC POSITION		UNIVERSAL TRANSVERSE MERCATOR				
				LATITUDE	LONGITUDE	NORTHING	EASTING	ZONE	SCALE	ELEVATION
89	1462	HIW 9		62 16 29.81194 N	133 10 55.11200 W	6905934.536	594358.750	8	.9997091	1581.978
90	678756	MT. MYE		62 10 43.22560 N	133 5 55.62771 W	6910186.037	598554.299	8	.9997190	2061.185
91	1482	HIW 1		62 24 23.96263 N	133 29 41.29280 W	6920188.336	577783.316	8	.9996741	1788.171
92	1499			62 13 45.42010 N	133 8 8.01805 W	6900917.232	596913.824	8	.9997150	1170.997
93	1498			62 13 40.38365 N	133 8 7.72167 W	6900761.541	596922.590	8	.9997151	1153.615
94	1496			62 13 35.26997 N	133 7 54.40957 W	6900608.800	597119.339	8	.9997155	1127.214
95	1500	DY 2		62 14 .78056 N	133 7 51.69345 W	6901399.237	597135.765	8	.9997156	1160.767
96	1434	HIW 17		62 15 50.86984 N	132 42 57.83015 W	6905496.308	618576.420	8	.9997722	1173.795
97	1491	HIW 14		62 19 32.22694 N	133 0 38.06200 W	6911839.456	603079.377	8	.9997301	1801.704
98	1497			62 13 37.80199 N	133 8 .29098 W	6900684.764	597032.168	8	.9997153	1138.770
99	1480	QC 13A		62 17 50.10108 N	133 3 40.49650 W	6908600.282	600548.938	8	.9997238	2014.147
100	1408	VG 8		62 16 34.67073 N	133 14 37.56044 W	6905996.299	591148.184	8	.9997018	1288.260
101	1490	HIW 7KA		62 16 26.71365 N	133 14 14.05326 W	6905759.334	591493.724	8	.9997025	1301.997
102	1406	VG 6		62 16 11.59433 N	133 13 40.75505 W	6905304.678	591986.529	8	.9997036	1319.143
103	1421	RC 4		62 20 48.01729 N	133 25 40.21038 W	6913589.247	581405.949	8	.9996812	1040.080
104	1401	VG 1		62 14 17.65568 N	133 7 43.69486 W	6901924.642	597236.124	8	.9997158	1200.912
105	1445	HIW 16		62 16 17.44804 N	133 6 42.70027 W	6905656.256	598008.252	8	.9997177	1725.839
106	1437	BC 21		62 18 58.78112 N	132 50 56.68040 W	6911072.621	611479.269	8	.9997522	1768.000
107	1427			62 15 37.52034 N	132 38 34.11993 W	6905219.750	622393.376	8	.9997835	1689.032
108	107	GRAVITY 107		62 22 3.52190 N	133 8 31.89488 W	6916317.381	596126.584	8	.9997132	1936.785
109	108	GRAVITY 108		62 21 9.46673 N	133 2 26.56486 W	6914800.069	601426.931	8	.9997260	1994.775
110	111	GRAVITY 111		62 20 33.95159 N	132 57 .62610 W	6913846.661	606147.581	8	.9997380	1673.227

FIGURE 2

MONUMENTS PLACED AND ANCILLARY MONUMENTATION

CYPRUS ANVIL MINES CONTROL

MAP SHEET 105 K, Y.T.

1979

FIGURE 2

IDENTIFICATION NUMBER	STATION NUMBER	MONUMENT	NOTES
6785000	67A35	Mag plug, tripod	
6785001	67A24	Mag plug, tripod	
678566	67A25	Aluminum post	
678567	67A55	Mag plug - 4x4 cairn	
1401	VG1	IP, 4x4, tripod	
1402	VG2	IP, 4x4, tripod	
1403	VG3	IP, 4x4, tripod	
1404	VG4	IP, 4x4, tripod	
1405	VG5	IP, 4x4, tripod	
1406	VG6	IP, 4x4, tripod	
1407	VG7	IP, 4x4, tripod	
1408	VG8	IP, 4x4, tripod	
1409	VG9	IP, 4x4, tripod	
1410	VG10	IP, 4x4, tripod	
1411	VG11	IP, 4x4, tripod	
1412	VG12	IP, 4x4, tripod	
1413	VG13A	IP, 4x4, tripod	
1414	VG14	IP, 4x4, tripod	
1415	VG15A	IP, 4x4	
1416	VG16	IP, 4x4, tripod	
1417	WHI 1-71	IP, 4x4, tripod	
1418	VG18	IP, 4x4, tripod	
1419	VG19	IP, 4x4, tripod	
1420	WHI 3	IB, 4x4, tripod	

IDENTIFICATION NUMBER	STATION NUMBER	MONUMENT	NOTES
1421	RC 4	IP, 4x4, rock cairn	
1422	HIW 4KA	IB, 4x4, tripod	
1423	HIW 5KA	IB, 4x4 in concrete, tripod	
1424	HIW 6KA	IB, 4x4 in concrete, tripod	
1425		IB, 4x4, tripod	
1426	SL 13	IP, 4x4, tripod	
1427		Rock post, 4x4, cairn	
1428		Rock post, tripod	
1429		Rock post, tripod	
1430	SL 12	IP, 4x4, tripod	
1431		IB, 4x4, tripod	
1432	BC 17	IP, 4x4, tripod	0.33 m above ground level
1433		Rock post, tripod	
1434	HIW 17	IB, 4x4, tripod	
1435		IB, 4x4, tripod	
1436		IB, 4x4, tripod	
1437	BC 21	IP, 4x4, rock cairn	0.70 m above ground level
1438		IB, 4x4, tripod	0.33 m above ground level
1439		IB, 4x4, tripod	
1440		Rock post, tripod	0.05 m below ground level
1441		IB, 4x4, tripod	
1442		IB, 4x4, tripod	
1443	BC 5	IP, 4x4, tripod	0.32 m above ground level
1444	SL 7	IP, 4x4, tripod	
1445	HIW 16	IB, 4x4, cairn	

IDENTIFICATION NUMBER	STATION NUMBER	MONUMENT	NOTES
1446	U&U 611	IB, tripod	0.36 m above ground level
1447		IB, 4x4, tripod	
1448		IB, 4x4, tripod	IB, 0.002 above ground level HI to ground level
1449	BC 3	IP, 4x4, tripod	
1450	HIW 6	IB, 4x4, tripod	
1451	JK 2	IB, tripod	
1452	HIW 2KA	IB, 4x4, tripod	
1453	HIW 10	IB, 4x4	
1454	JK 4	IB, tripod	
1455	IN 3	IB, tripod	
1456	IN 2	IB, tripod	
1457	HIW 3KA	IB, 4x4, tripod	
1458	IN 1	IB, tripod	
1459	JK 3	IB, tripod	
1460	IN 4	IB, tripod	
1461	HIW 1KA	IB, 4x4, tripod	
1462	HIW 9	IB, 4x4, tripod	
1463	RC 2	IB, 4x4, rock cairn	0.24 m above ground level
1464	HIW 3	IB, 4x4	0.32 m above ground level
1465	BC 20	IP, 4x4, tripod	0.17 m above ground level
1466		IB, 4x4, tripod	
1467	BC 16	IP, 4x4, tripod	0.15 m above ground level
1468	BC 7	IP, 4x4, tripod	
1469	HIW 7	IP, 4x4, tripod	

IDENTIFICATION NUMBER	STATION NUMBER	MONUMENT	NOTES
1470	RC 11	IP, 4x4, barber pole tripod	
1471	DP 1	IB, tripod	
1472	IB 751	IB, tripod	
1473	IB 756	IB, tripod	
1474	DP 2	IB, tripod	
1475	HIW 8	IP, 4x4, tripod	
1476	PE 1	4x4, rock cairn	
1477		IB, 4x4, tripod	0.305 m above ground level
1478	PE 2	Rock post, 4x4, tripod	
1479	DY 1	Rock post, tripod	
1480	BC 13A	IB, 4x4, tripod	
1481	HIW 2	IB, 4x4, tripod	
1482	HIW 1	IB, 4x4, tripod	0.62 m above ground level
1483		Rock post, tripod, sighting pole	
1484		IB, tripod	
1485	TRI 18	IB, bedrock	0.56 m above ground level
1486	PRI 6	IP, 4x4, tripod	0.460 m above ground level
1487	PRI 4	IB in bedrock	0.710 m above ground level
1488	HIW 11	IB, 4x4	
1489	HIW 5	IB, 4x4	
1490	HIW 7KA	IB, 4x4, tripod	
1491	HIW 14	IB, 4x4	
1492	HIW 13	IB, 4x4	
1493	HIW 12	IB, 4x4	
1494	HIW 4	IB, 4x4	

IDENTIFICATION NUMBER	STATION NUMBER	MONUMENT	NOTES
1495	HIW 15	IB, 4x4	
1496		Rock post, tripod	
1497		Rock post, tripod	
1498		Rock post, tripod	
1499		IB, tripod	
1500	DY 2	IB, tripod	
14571	JK 1	IB, tripod	
14401	1440ECC	IB	
678756	MT. MYE	Rock Cairn	

LEGEND

- Rock Posts - CLS rock post 8.0 cm diameter bronze cap with shaft grouted in bedrock.
- IB - Approximately 1.5 cm x 0.80 m iron bar
- IP - CLS old pattern iron post, 1.0 m iron pipe 1.5 cm diameter with top 0.13 m squared
- 4x4 - 10.0 cm x 10.0 cm x 1.3 m red wood post
- Tripod - 2.0 m high, approximately 2.5 m a round base - 3 legs of native timber

APPENDIX A

UTM COORDINATE SYSTEM COMPUTATION

MANUAL OF INSTRUCTIONS

FOR THE SURVEY OF CANADA LANDS

SECOND EDITION

1979

Chapter E2

UTM Coordinate System

1. (1) The Universal Transverse Mercator (UTM) system is a plane rectangular coordinate system derived by using a Gauss-Kruger transverse Mercator projection within narrow zones of the spheroid bounded by meridians. The projection is conformal and has a constant scale factor along the central meridian of the zone of 0.9996. The spheroid is divided into 6° zones with central meridian at west longitudes, $\lambda = 3^\circ \dots 51^\circ, 57^\circ, 63^\circ \dots 135^\circ, 141^\circ \dots$. Zones are numbered eastward from longitude 180°; the number 'n' of a zone is given by the formula: $n = (183 - \lambda)/6$.

(2) The Clarke spheroid of 1866 is used to represent the shape of the earth for the UTM projection in North America. It has a and b axes of 6 378 206.4 metres and 6 356 583.8 metres respectively.

(3) UTM coordinates are expressed in metres. The coordinate axes of a zone are the central meridian and the Equator, but the central meridian is given a false easting of 500 000 metres to avoid negative eastings.

(4) Basic formulae for conversions between UTM and geographical coordinates can be found in the following references:

Lee, L.P. "Conformal Projections Based on Elliptic Functions". *Cartographica*, Monograph 16, Dept. of Geography, York University, Toronto, 1976;

Lee, L.P. "The Transverse Mercator Projection of the Spheroid". *Empire Survey Review*, Vol. VIII, No. 45, Oct. 1945;

Redfean, J.C.B. "Transverse Mercator Formulae". *Empire Survey Review*, Vol. IX, No. 69, July 1948;

Schmid, Erwin. "The General Term in the Expansion for Meridian Length". *The Canadian Surveyor*, Vol. 25, No. 2, June 1971;

Thomas, Paul D. "Conformal Projections in Geodesy and Cartography". *Special Publication 251*, United States Department of Commerce, National Geodetic Survey, Washington, 1952;

United States Department of the Army. "Universal Transverse Mercator Grid". *Technical Manual TM 5-241-8*, U.S. Government Printing Office, Washington, April 1973.

(5) Tables of official UTM coordinates for COGLR grid area corners between Latitudes 40° and 85° are available, on request, from the Surveyor General.

2. Before plane coordinate computations can be made the measured quantities must be reduced to equivalent measurements on the projection plane. Distances may be reduced from the mean elevation of measurement to the projection plane by using the combined factor obtained from the preceding graph.

3. Measured angles, bearings or directions do not normally require any reduction to equivalent plane surface measurements before using them for plane coordinate computations because the curved spheroidal surface of the earth is only slightly tilted with respect to the UTM plane. However, whenever long sight lines are involved there may be a significant difference between an observed direction or bearing T (the azimuth, corrected for convergence between the central meridian and the observation point) and the grid bearing t. The difference is always less than 6" for sight lines less than 10 km but may be as much as a minute on a 100 km sight line. For a sight line between instrument station 1 and target station 2, with coordinates (N_1, E_1) and (N_2, E_2) respectively, the following formula gives the value of $(t - T)$ to a small fraction of a second:

$$(t - T)'' = 0.85'' \times 10^{-9} (N_1 - N_2) (2E_1 + E_2 - 1\ 500\ 000)$$

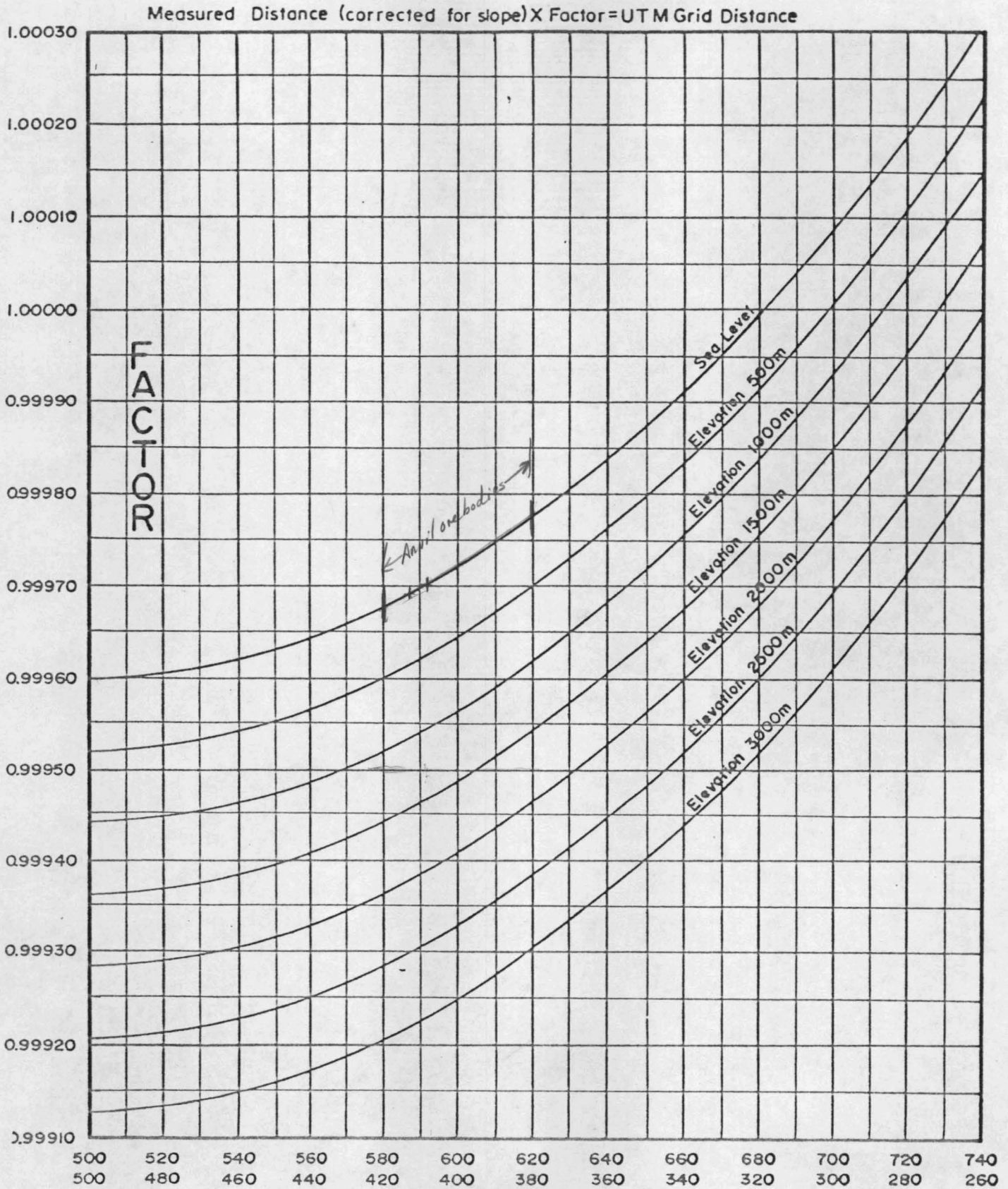
$$\text{where } t \text{ is defined by the equation } \tan t = \frac{E_2 - E_1}{N_2 - N_1}$$

4. If a survey has many long lines or crosses zone boundaries it is advisable to use a computer program such as GALS, MANOR, or COSMOS which computes in geographic coordinates directly and provides UTM coordinates as a final output.

5. The east and west boundaries of a grid area are defined in COGLR as meridians. The north and south boundaries are defined not as parallels of latitude but as straight lines being chords to parallels of latitude. Coordinates of points on any of the boundaries may be found directly by interpolation between the official UTM coordinates of the corners and areas are computed on the UTM plane from the coordinates. If the geographic coordinates of a point are given it may be easily and precisely located within a COGLR subdivision by first converting its geographic coordinates to UTM coordinates.

FACTOR FOR REDUCING HORIZONTAL DISTANCES TO UTM GRID DISTANCES

(AT DIFFERENT ELEVATIONS AND UTM EASTINGS)



UTM EASTING (Km)

FIG. E 1

APPENDIX B

LEVELOB VERTICAL ADJUSTMENT

CYPRUS ANVIL MINES CONTROL

MAP SHEET 105 K, Y.T.

1979

PROGRAM LEVELOB--A.E. PETERSON CONSULTING LTD.
EDMONTON, ALTA.

DATE 15 11 1979 TIME 15 19 15

CYPUVERT

247 115 5

NOTE LINK WEIGHTS CALCULATED BY ANGLE ERROR OF 7 SECONDS
AND HI ERROR OF .010 HEIGHT UNITS

INPUT DATA

1	1496	1127.400
2	1497	1138.970
3	1498	1153.800
4	1500	1160.770
5	1499	1171.200
6	5000	1395.100
7	5001	1336.500
8	8566	1985.900
9	8567	1665.100
10	1401	1200.900
11	1402	1227.600
12	1403	1214.200
13	1404	1300.000
14	1405	1300.100
15	1406	1318.900
16	1407	1331.500
17	1408	1288.100
18	1409	1206.900
19	1410	1204.900
20	1411	1187.100
21	1412	1171.900
22	1413	1151.200
23	1414	1133.900
24	1415	1109.700
25	1416	1088.300
26	1417	1082.700
27	1418	1066.400
28	1419	1094.300
29	1420	1040.500
30	1421	1039.600
31	1422	1302.500
32	1423	1276.700
33	1424	1307.900

34	1425	1069.200
35	1426	1407.700
36	1427	1689.000
37	1428	963.000
38	1429	1113.500
39	1430	961.800
40	1431	1110.500
41	1432	1307.400
42	1433	1311.700
43	1434	1172.800
44	1435	885.700
45	1436	939.800
46	1437	1768.200
47	1438	1425.300
48	1439	1266.100
49	1440	1272.000
50	4401	1268.000
51	1441	1125.100
52	1442	955.900
53	1443	880.100
54	1444	912.000
55	1445	1725.800
56	1446	1389.900
57	1447	1888.600
58	1448	1097.000
59	1449	935.200
60	1450	1738.800
61	1451	1163.600
62	1452	1142.200
63	1453	1284.100
64	1454	1172.600
65	1455	1162.500
66	1456	1161.000
67	1457	1220.300
68	4571	1220.300
69	1458	1186.000
70	1459	1166.100
71	1460	1150.200
72	1461	1324.700
73	1462	1581.900
74	1463	1514.600
75	1464	1542.500
76	1465	857.800
77	1466	867.100
78	1467	891.200
79	1468	786.100
80	1469	1421.600
81	1470	1681.600
82	1471	1132.100
83	1472	1094.500
84	1473	1147.600
85	1474	1040.400
86	1475	1396.700
87	1476	1522.000
88	1477	1445.500
89	1478	1360.300

90	1479		1190.700	
91	1480		2014.100	
92	1481		1648.700	
93	1482		1787.900	
94	1483		1420.800	
95	1484		1033.800	
96	1485		1294.300	
97	1486		1190.000	
98	1487		1256.800	
99	1488		1195.600	
100	1489		1803.600	
101	1490		1302.400	
102	1491		1801.300	
103	1492		1600.600	
104	1493		1614.800	
105	1494		1358.900	
106	1495		1404.000	
107	8756		2060.800	
108	111		1673.220	
109	108		1994.770	
110	107		1936.800	
111	8001		698.445	
112	4230		756.480	
113	4235		766.077	
114	4246		648.508	
115	4247		716.383	
1	5001	5000	58.5970	.8656
2	5001	1401	-135.6430	.1070
3	5001	1425	-267.3379	.1112
4	5001	1426	71.1570	.3377
5	5001	1427	352.5481	.0826
6	5001	1431	-226.0030	.0560
7	5001	1439	-70.3770	.0868
8	5001	1446	53.3730	.1695
9	5000	8001	-696.6650	.0496
10	5000	1426	11.6770	.1520
11	5000	1427	294.3330	.6194
12	1401	1442	-245.1970	.0224
13	1401	1448	-104.0770	.0201
14	1401	1471	-68.9660	.0004
15	1401	1472	-106.6120	.0006
16	1401	1479	-10.4460	.0003
17	1403	1457	6.1550	.0002
18	1406	1424	-11.1430	.0001
19	1417	1463	431.8821	.0136
20	1417	1483	338.1101	.0051
21	1426	1427	282.9629	.2822
22	1428	5001	373.7759	.0730
23	1428	1425	106.2710	.0206
24	1428	1430	-1.2050	.0134
25	1429	1425	-44.2020	.0239
26	1429	1430	-151.4540	.0320
27	1429	1431	-2.3460	.0143
28	1433	1427	377.4609	.0058
29	1433	1431	-200.5950	.0247
30	1434	1427	515.1750	.0085

31	1435	1427	803.9771	.0559
32	1435	1437	882.4260	.0042
33	1436	1427	749.3779	.0320
34	1436	1433	371.9609	.0302
35	1437	1427	-79.2210	.0885
36	1437	1432	-460.1760	.0357
37	1437	1439	-501.6631	.1896
38	1437	1443	-888.0740	.1695
39	1437	1468	-982.0801	.1232
40	1438	1432	-117.2790	.0259
41	1438	1437	342.9929	.0428
42	1438	1439	-158.7790	.0598
43	1439	4401	1.7820	.0001
44	1439	1442	-310.8789	.0139
45	1439	1443	-386.4021	.0040
46	1439	1449	-331.0879	.0047
47	1440	5001	64.6290	.0875
48	1440	1428	-309.0500	.0530
49	1440	4401	-3.7110	.0001
50	1440	1441	-146.9700	.0092
51	1441	5001	211.6360	.0578
52	1442	1439	310.7510	.0139
53	1442	1444	-44.6890	.0037
54	1442	1448	141.2770	.0020
55	1443	1449	55.3030	.0010
56	1445	1401	-524.9089	.0084
57	1446	1401	-189.2970	.0103
58	1446	1404	-90.1700	.0162
59	1446	1439	-123.9220	.0196
60	1446	1440	-118.1040	.0216
61	1446	1461	-65.4810	.0150
62	1447	1470	-207.0190	.0386
63	1447	1481	-239.8410	.0145
64	1447	1482	-100.7090	.0039
65	1450	1483	-317.4280	.0325
66	1459	1446	224.0780	.0086
67	1463	1484	-481.0339	.0059
68	1464	1447	346.1541	.0308
69	4235	1446	624.1001	.0394
70	4230	1425	312.8201	.0135
71	1464	1450	195.7250	.0491
72	1464	1482	245.4660	.0481
73	1465	1437	909.8201	.0092
74	1465	1432	449.5161	.0090
75	1466	1438	558.1919	.0050
76	1466	1432	440.8911	.0098
77	1467	1432	416.2271	.0296
78	1467	1439	375.2629	.0266
79	1468	1439	481.0950	.0086
80	1469	1461	-96.9340	.0141
81	1470	1484	-648.1160	.0033
82	1470	1482	106.1230	.0260
83	1471	1445	593.9080	.0118
84	1471	1442	-176.1910	.0206
85	1471	1439	134.7550	.0107
86	1471	1474	-91.3300	.0003

87	1471	1473	15.9320	.0003
88	1472	1474	-53.6970	.0002
89	1472	1442	-138.6000	.0195
90	1472	1439	172.2790	.0094
91	1472	1445	631.4919	.0125
92	1472	1473	53.6400	.0005
93	1473	1439	118.5540	.0133
94	1473	1442	-192.2070	.0206
95	1473	1445	577.8450	.0085
96	1474	1439	225.8720	.0090
97	1475	1417	-313.9719	.0037
98	1475	1477	48.3150	.0024
99	1477	1476	76.5110	.0037
100	1477	1463	69.6270	.0091
101	1477	1483	-24.2300	.0226
102	1478	4246	-711.8491	.0128
103	1478	1476	161.6000	.0044
104	1479	1446	199.7470	.0074
105	1479	1445	535.5229	.0115
106	1479	1442	-234.7890	.0244
107	1480	1445	-288.3201	.0088
108	1480	8756	46.9040	.0035
109	1481	1463	-133.8810	.0234
110	1481	1464	-106.2450	.0063
111	1481	1482	139.0790	.0223
112	1481	1483	-227.7560	.0063
113	1485	1463	220.5240	.0157
114	1485	1483	126.8580	.0018
115	1486	1463	324.8010	.0153
116	1486	1481	458.8000	.0080
117	1486	1483	231.1010	.0013
118	1487	1463	258.0149	.0202
119	1487	1481	392.0820	.0059
120	1487	1483	164.3380	.0002
121	1485	1487	-37.5170	.0011
122	1486	1487	66.7300	.0006
123	1485	1486	-104.2920	.0015
124	1485	1487	-37.4720	.0011
125	1485	1486	-104.2730	.0015
126	1486	1487	66.7700	.0006
127	1404	1451	-136.4320	.0026
128	1460	1454	22.4510	.0001
129	1460	1452	-8.0350	.0001
130	1459	1460	-15.9470	.0001
131	1459	1404	133.8840	.0013
132	1459	1454	6.5020	.0002
133	1459	1451	-2.6050	.0003
134	1458	1451	-22.4920	.0003
135	1458	1454	-13.4490	.0003
136	1458	1404	113.9240	.0014
137	1458	1455	-23.4560	.0002
138	1458	1456	-25.0010	.0001
139	1457	1404	79.7280	.0016
140	1457	1452	-78.1490	.0007
141	1456	1451	2.5210	.0002
142	1455	1404	137.4040	.0025

143	1455	1457	57.7780	.0004
144	1451	1454	8.9500	.0008
145	1451	1457	56.7940	.0006
146	1452	1454	30.4780	.0001
147	4247	1461	608.4199	.0153
148	1461	1452	-182.4210	.0031
149	1452	1457	78.1970	.0007
150	1457	1404	79.6310	.0016
151	1404	1422	2.2570	.0013
152	1422	1423	-25.8260	.0003
153	1423	1461	48.2460	.0003
154	1461	1405	-24.4800	.0014
155	1422	1490	-2.2770	.0001
156	1422	1424	5.7530	.0001
157	1424	1423	-31.5850	.0003
158	1457	1404	79.6310	.0016
159	1422	1404	-2.2570	.0013
160	1401	1402	26.7260	.0015
161	1402	1403	-13.4190	.0004
162	1403	1404	85.7970	.0027
163	1404	1405	.1360	.0009
164	1405	1406	18.8320	.0004
165	1406	1407	12.5340	.0007
166	1407	1408	-43.3820	.0004
167	1408	1409	-81.1630	.0009
168	1409	1410	-1.8820	.0011
169	1410	1411	-17.7520	.0004
170	1411	1412	-15.1740	.0009
171	1412	1413	-20.6900	.0005
172	1413	1414	-17.2150	.0002
173	1414	1415	-24.1170	.0025
174	1415	1417	-27.0030	.0010
175	1417	1418	-16.2630	.0006
176	1418	1419	27.9000	.0004
177	1419	1421	-54.6340	.0027
178	1401	1406	118.3590	.0225
179	1408	1419	-193.3530	.0627
180	1401	1480	813.2529	.0321
181	1480	1491	-212.4570	.0098
182	1480	8566	-28.0210	.0001
183	4247	8567	948.6580	.0788
184	8567	1470	16.5200	.0143
185	1470	1482	106.0390	.0260
186	1482	1481	-138.8370	.0223
187	1481	1464	-106.2540	.0063
188	1464	1494	-183.6060	.0082
189	1464	1489	261.0669	.0207
190	1489	1450	-64.7250	.0082
191	1463	1420	-474.2429	.0028
192	1450	1469	-317.1941	.0074
193	1469	1475	-24.6960	.0090
194	1475	1463	117.9810	.0176
195	1463	1470	166.8540	.0045
196	1481	1494	-289.9221	.0262
197	1470	1420	-641.1560	.0089
198	1469	1409	-214.7910	.0028

199	1450	1462	-156.9530	.0151
200	1462	1453	-297.8979	.0084
201	1453	1401	-83.2260	.0022
202	1401	1488	-5.2980	.0014
203	1488	1461	129.0910	.0155
204	1461	1469	96.8550	.0141
205	1481	1493	-33.9840	.0522
206	1493	1492	-14.2920	.0505
207	1492	8756	460.1790	.0390
208	8756	1495	-656.8860	.0334
209	1495	1491	397.2900	.0068
210	1491	1434	-628.6101	.1617
211	1434	1445	552.7681	.2439
212	1445	1401	-524.9651	.0084
213	1421	1420	.8820	.0001
214	1401	5001	135.6800	.1070
215	5001	1480	677.3301	.0861
216	8566	5001	-649.4250	.0850
217	1432	5001	29.0130	.0014
218	1415	1416	-21.4940	.0001
219	1437	1480	245.8210	.0726
220	1480	8567	-348.8369	.3261
221	1405	1462	281.8611	.0020
222	1427	5001	-351.9680	.0825
223	1457	4571	2.4200	.0001
224	1475	1463	117.8780	.0176
225	1480	1437	-245.8590	.0724
226	1480	1440	-742.4199	.0772
227	1482	8756	272.9451	.3062
228	1496	1498	26.3960	.0001
229	1497	1439	127.8100	.0093
230	1497	1445	586.9570	.0146
231	1497	1446	251.5610	.0066
232	1497	1496	-11.5610	.0001
233	1497	1498	14.8460	.0001
234	1499	1439	95.3950	.0105
235	1499	1446	219.2840	.0066
236	1499	1496	-43.7780	.0001
237	1499	1497	-32.2330	.0001
238	1499	1498	-17.3790	.0001
239	1500	1473	-12.7780	.0002
240	1500	1471	-28.8430	.0001
241	8756	1480	-47.1760	.0038
242	1437	111	-94.7550	.0209
243	111	108	321.5591	.0134
244	108	107	-57.9750	.0176
245	107	1464	-393.9041	.0538
246	1462	1406	-262.5769	.0035
247	1406	1424	-11.1130	.0001

SOLUTION TO NORMALS

-.186E 00	-.200E 00	-.185E 00	-.373E-02	-.203E 00	.852E-02
.235E 00	.226E 00	.358E 00	.117E-01	.609E-01	.481E-01
.609E-01	.152E 00	.243E 00	.153E 00	.159E 00	.167E 00
.277E 00	.322E 00	.342E 00	.348E 00	.431E 00	.496E 00
.402E 00	.485E 00	.504E 00	.494E 00	.460E 00	.479E 00
-.226E 00	-.253E 00	.119E 00	.590E-01	-.858E 00	.318E-01
.292E-02	-.159E 00	.243E-01	.452E 00	.323E 00	-.130E 00
.995E 00	-.163E 00	-.169E 00	-.201E 00	-.253E 00	.425E 00
.197E-01	.308E 00	-.438E-01	-.203E 00	.252E-01	-.992E 00
.390E-01	.357E 00	.314E 00	-.389E-01	.230E 00	.145E 00
.285E-01	.129E-01	.254E-01	.863E-01	.149E 00	.114E 00
.105E 00	.253E 01	.118E 00	.974E-01	.458E-01	.416E-02
.776E-01	.536E 00	.336E 00	.393E 00	-.253E 00	.173E 00
-.638E 00	.190E 00	.460E 00	-.160E 00	-.198E 00	.340E 00
.208E 00	.464E 00	-.662E-02	-.972E-02	.841E-01	-.236E 00
.464E-01	.405E 00	.270E 00	.567E 00	.201E 00	.233E 00
.272E 00	.228E 00	.135E-01	.136E 00	-.403E 00	.404E 00
.356E 00	.386E 00	.319E 00	.394E 00	.384E 00	.678E-02
.484E-02	-.150E-01				

SOLUTION TO NORMALS

.797E-03	.595E-03	.250E-03	.675E-03	.534E-03	.236E-03
.811E-03	.682E-03	.628E-03	.757E-03	.683E-03	.459E-03
.811E-03	.755E-03	.688E-03	.709E-03	.620E-03	.565E-03
.563E-03	.597E-03	.743E-03	.504E-03	.772E-03	.620E-03
.620E-03	.805E-03	.729E-03	.654E-03	.643E-03	.721E-03
.812E-03	.676E-03	.484E-03	.516E-03	.703E-03	.635E-03
.776E-03	.678E-03	.605E-03	.735E-03	.793E-03	.533E-03
.639E-03	.690E-03	.659E-03	.565E-03	.743E-03	.858E-03
.596E-03	.623E-03	.547E-03	.708E-03	.510E-03	.708E-03
.527E-03	.381E-03	.691E-03	.765E-03	.677E-03	.663E-03
.798E-03	.961E-03	.919E-03	.527E-03	.687E-03	.288E-03
.416E-03	.416E-03	.577E-03	.544E-03	.744E-03	.502E-03
.453E-03	.697E-03	.648E-03	.680E-03	.513E-03	.616E-03
.610E-03	.600E-03	.539E-03	.698E-03	.554E-03	.813E-03
.642E-03	.649E-03	.722E-03	.592E-03	.624E-03	.647E-03
.904E-03	.562E-03	.628E-03	.690E-03	.603E-03	.729E-03
.472E-03	.588E-03	.493E-03	.588E-03	.812E-03	.715E-03
.812E-03	.651E-03	.584E-03	.640E-03	.533E-03	.793E-03
.645E-03	.684E-03				

ADJUSTED ELEVATION MATRIX

S.D.

1	1496	1127.214	.116
2	1497	1138.770	.116
3	1498	1153.615	.116
4	1500	1160.767	.106
5	1499	1170.997	.116
6	5000	1395.108	.246

7	5001	1336.735	.131
8	8566	1986.126	.133
9	8567	1665.458	.170
10	1401	1200.912	.104
11	1402	1227.661	.104
12	1403	1214.248	.102
13	1404	1300.062	.101
14	1405	1300.253	.101
15	1406	1319.143	.100
16	1407	1331.654	.103
17	1408	1288.260	.104
18	1409	1207.068	.106
19	1410	1205.178	.110
20	1411	1187.423	.112
21	1412	1172.242	.114
22	1413	1151.548	.115
23	1414	1134.332	.115
24	1415	1110.196	.115
25	1416	1088.702	.115
26	1417	1083.186	.113
27	1418	1066.904	.115
28	1419	1094.794	.117
29	1420	1040.960	.120
30	1421	1040.080	.120
31	1422	1302.274	.100
32	1423	1276.447	.100
33	1424	1308.019	.100
34	1425	1069.259	.123
35	1426	1406.842	.376
36	1427	1689.032	.174
37	1428	963.003	.160
38	1429	1113.342	.169
39	1430	961.825	.189
40	1431	1110.953	.178
41	1432	1307.723	.134
42	1433	1311.570	.182
43	1434	1173.795	.198
44	1435	885.537	.164
45	1436	939.631	.233
46	1437	1768.000	.147
47	1438	1425.048	.162
48	1439	1266.526	.110
49	1440	1272.020	.111
50	4401	1268.308	.110
51	1441	1125.057	.155
52	1442	955.698	.120
53	1443	880.126	.125
54	1444	911.008	.142
55	1445	1725.839	.113
56	1446	1390.257	.107
57	1447	1888.915	.142
58	1448	1096.962	.129
59	1449	935.430	.125
60	1450	1738.945	.126
61	1451	1163.629	.102
62	1452	1142.213	.102

63	1453	1284.126	.115
64	1454	1172.687	.102
65	1455	1162.649	.103
66	1456	1161.114	.103
67	1457	1220.405	.102
68	4571	1222.825	.102
69	1458	1186.118	.102
70	1459	1166.198	.102
71	1460	1150.246	.102
72	1461	1324.705	.100
73	1462	1581.978	.107
74	1463	1515.137	.116
75	1464	1542.837	.131
76	1465	858.193	.156
77	1466	866.848	.161
78	1467	891.373	.185
79	1468	785.463	.156
80	1469	1421.790	.110
81	1470	1682.061	.124
82	1471	1131.941	.105
83	1472	1094.303	.106
84	1473	1147.940	.106
85	1474	1040.608	.106
86	1475	1397.164	.113
87	1476	1521.994	.116
88	1477	1445.491	.113
89	1478	1360.385	.112
90	1479	1190.464	.106
91	1480	2014.147	.132
92	1481	1649.105	.123
93	1482	1788.171	.138
94	1483	1421.367	.119
95	1484	1034.002	.131
96	1485	1294.534	.120
97	1486	1190.272	.120
98	1487	1257.029	.119
99	1488	1195.614	.112
100	1489	1803.737	.152
101	1490	1301.997	.101
102	1491	1801.704	.169
103	1492	1600.957	.243
104	1493	1615.186	.253
105	1494	1359.219	.161
106	1495	1404.395	.185
107	8756	2061.185	.141
108	111	1673.227	.208
109	108	1994.775	.226
110	107	1936.785	.234
111	8001	698.445	.000
112	4230	756.480	.000
113	4235	766.077	.000
114	4246	648.508	.000
115	4247	716.383	.000

LINE NO.	FROM STA.	TO STA.	ADJ. ELEV. DIFF.	OBS. ELEV. DIFF.	RESIDUAL (OBS-ADJ)	SIGMA (INPUT)	LINK S.D.
1	5001	5000	58.373	58.597	.224	.9304	.266
2	5001	1401	-135.823	-135.643	.180	.3271	.101
3	5001	1425	-267.476	-267.338	.138	.3334	.146
4	5001	1426	70.106	71.157	1.051	.5811	.375
5	5001	1427	352.297	352.548	.251	.2874	.145
6	5001	1431	-225.783	-226.003	-.220	.2366	.161
7	5001	1439	-70.209	-70.377	-.168	.2946	.099
8	5001	1446	53.522	53.373	-.149	.4117	.107
9	5000	8001	-696.663	-696.665	-.002	.2228	.246
10	5000	1426	11.733	11.677	-.056	.3898	.370
11	5000	1427	293.924	294.333	.409	.7870	.284
12	1401	1442	-245.215	-245.197	.018	.1495	.064
13	1401	1448	-103.950	-104.077	-.127	.1419	.079
14	1401	1471	-68.971	-68.966	.005	.0188	.019
15	1401	1472	-106.609	-106.612	-.003	.0236	.021
16	1401	1479	-10.448	-10.446	.002	.0179	.022
17	1403	1457	6.157	6.155	-.002	.0144	.017
18	1406	1424	-11.124	-11.143	-.019**	.0091	.008
19	1417	1463	431.951	431.882	-.069	.1168	.057
20	1417	1483	338.181	338.110	-.071	.0712	.062
21	1426	1427	282.190	282.963	.772	.5312	.380
22	1428	5001	373.732	373.776	.044	.2701	.160
23	1428	1425	106.256	106.271	.015	.1435	.137
24	1428	1430	-1.179	-1.205	-.026	.1159	.131
25	1429	1425	-44.083	-44.202	-.119	.1546	.146
26	1429	1430	-151.517	-151.454	.063	.1790	.168
27	1429	1431	-2.389	-2.346	.043	.1194	.133
28	1433	1427	377.462	377.461	-.001	.0759	.087
29	1433	1431	-200.618	-200.595	.023	.1572	.158
30	1434	1427	515.237	515.175	-.062	.0921	.111
31	1435	1427	803.495	803.977	.482**	.2364	.161
32	1435	1437	882.462	882.426	-.036	.0648	.079
33	1436	1427	749.401	749.378	-.023	.1790	.162
34	1436	1433	371.939	371.961	.022	.1738	.162
35	1437	1427	-78.968	-79.221	-.253	.2974	.152
36	1437	1432	-460.277	-460.176	.101	.1889	.101

37	1437	1439	-501.474	-501.663	-.189	.4354	.118
38	1437	1443	-887.874	-888.074	-.200	.4117	.131
39	1437	1468	-982.537	-982.080	.457	.3510	.157
40	1438	1432	-117.325	-117.279	.045	.1608	.106
41	1438	1437	342.952	342.993	.041	.2068	.132
42	1438	1439	-158.522	-158.779	-.257	.2446	.135
43	1439	4401	1.782	1.782	-.000	.0073	.009
44	1439	1442	-310.828	-310.879	-.051	.1178	.068
45	1439	1443	-386.400	-386.402	-.002	.0631	.060
46	1439	1449	-331.096	-331.088	.008	.0687	.061
47	1440	5001	64.715	64.629	-.086	.2958	.100
48	1440	1428	-309.017	-309.050	-.033	.2302	.156
49	1440	4401	-3.712	-3.711	.001	.0122	.015
50	1440	1441	-146.963	-146.970	-.007	.0958	.112
51	1441	5001	211.679	211.636	-.043	.2404	.141
52	1442	1439	310.828	310.751	-.077	.1178	.068
53	1442	1444	-44.689	-44.689	.000	.0608	.076
54	1442	1448	141.264	141.277	.013	.0452	.054
55	1443	1449	55.304	55.303	-.001	.0315	.037
56	1445	1401	-524.927	-524.909	.018	.0917	.048
57	1446	1401	-189.345	-189.297	.048	.1013	.051
58	1446	1404	-90.196	-90.170	.026	.1274	.056
59	1446	1439	-123.731	-123.922	-.191	.1401	.059
60	1446	1440	-118.237	-118.104	.133	.1469	.060
61	1446	1461	-65.553	-65.481	.072	.1226	.059
62	1447	1470	-206.854	-207.019	-.165	.1964	.099
63	1447	1481	-239.810	-239.841	-.031	.1203	.086
64	1447	1482	-100.744	-100.709	.035	.0627	.069
65	1450	1483	-317.578	-317.428	.150	.1802	.098
66	1459	1446	224.060	224.078	.018	.0930	.057
67	1463	1484	-481.135	-481.034	.101	.0770	.068
68	1464	1447	346.078	346.154	.076	.1756	.097
69	4235	1446	624.180	624.100	-.080	.1985	.107
70	4230	1425	312.779	312.820	.041	.1162	.123
71	1464	1450	196.108	195.725	-.383	.2215	.104
72	1464	1482	245.334	245.466	.132	.2192	.093
73	1465	1437	909.806	909.820	.014	.0957	.098
74	1465	1432	449.530	449.516	-.014	.0948	.098
75	1466	1438	558.200	558.192	-.008	.0709	.081
76	1466	1432	440.876	440.891	.016	.0988	.100
77	1467	1432	416.350	416.227	-.123	.1719	.157
78	1467	1439	375.153	375.263	.110	.1630	.156
79	1468	1439	481.063	481.095	.032	.0925	.112
80	1469	1461	-97.086	-96.934	.152	.1189	.062
81	1470	1484	-648.059	-648.116	-.057	.0578	.061
82	1470	1482	106.110	106.123	.013	.1613	.092
83	1471	1445	593.899	593.908	.009	.1085	.049
84	1471	1442	-176.243	-176.191	.052	.1434	.064
85	1471	1439	134.585	134.755	.170	.1033	.049
86	1471	1474	-91.333	-91.330	.003	.0186	.018
87	1471	1473	16.000	15.932	-.068**	.0180	.014
88	1472	1474	-53.695	-53.697	-.002	.0143	.016
89	1472	1442	-138.605	-138.600	.005	.1396	.064
90	1472	1439	172.223	172.279	.056	.0971	.049
91	1472	1445	631.537	631.492	-.045	.1120	.049
92	1472	1473	53.638	53.640	.002	.0213	.019

93	1473	1439	118.585	118.554	-.031	.1154	.049
94	1473	1442	-192.243	-192.207	.036	.1434	.064
95	1473	1445	577.899	577.845	-.054	.0921	.049
96	1474	1439	225.918	225.872	-.046	.0951	.049
97	1475	1417	-313.979	-313.972	.007	.0611	.057
98	1475	1477	48.326	48.315	-.011	.0494	.054
99	1477	1476	76.503	76.511	.008	.0609	.072
100	1477	1463	69.646	69.627	-.019	.0954	.069
101	1477	1483	-24.124	-24.230	-.106	.1502	.078
102	1478	4246	-711.877	-711.849	.027	.1133	.112
103	1478	1476	161.609	161.600	-.009	.0662	.077
104	1479	1446	199.793	199.747	-.046	.0859	.054
105	1479	1445	535.375	535.523	.148	.1072	.051
106	1479	1442	-234.767	-234.789	-.022	.1561	.066
107	1480	1445	-288.308	-288.320	-.012	.0936	.089
108	1480	8756	47.037	46.904	-.133**	.0592	.052
109	1481	1463	-133.969	-133.881	.088	.1530	.070
110	1481	1464	-106.269	-106.245	.024	.0792	.060
111	1481	1482	139.065	139.079	.014	.1494	.081
112	1481	1483	-227.738	-227.756	-.018	.0793	.054
113	1485	1463	220.603	220.524	-.079	.1255	.063
114	1485	1483	126.833	126.858	.025	.0422	.025
115	1486	1463	324.865	324.801	-.064	.1237	.062
116	1486	1481	458.833	458.800	-.033	.0892	.054
117	1486	1483	231.095	231.101	.006	.0355	.022
118	1487	1463	258.108	258.015	-.093	.1423	.061
119	1487	1481	392.076	392.082	.006	.0770	.053
120	1487	1483	164.338	164.338	-.000	.0149	.017
121	1485	1487	-37.505	-37.517	-.012	.0334	.022
122	1486	1487	66.757	66.730	-.027	.0239	.018
123	1485	1486	-104.262	-104.292	-.030	.0391	.023
124	1485	1487	-37.505	-37.472	.033	.0334	.022
125	1485	1486	-104.262	-104.273	-.011	.0391	.023
126	1486	1487	66.757	66.770	.013	.0239	.018
127	1404	1451	-136.432	-136.432	.000	.0511	.021
128	1460	1454	22.440	22.451	.011	.0105	.009
129	1460	1452	-8.033	-8.035	-.002	.0080	.008
130	1459	1460	-15.951	-15.947	.004	.0087	.009
131	1459	1404	133.864	133.884	.020	.0366	.021
132	1459	1454	6.489	6.502	.013	.0144	.011
133	1459	1451	-2.569	-2.605	-.036**	.0163	.014
134	1458	1451	-22.489	-22.492	-.003	.0184	.013
135	1458	1454	-13.431	-13.449	-.018	.0174	.015
136	1458	1404	113.944	113.924	-.020	.0371	.021
137	1458	1455	-23.469	-23.456	.013	.0157	.017
138	1458	1456	-25.004	-25.001	.003	.0094	.010
139	1457	1404	79.656	79.728	.072	.0399	.019
140	1457	1452	-78.192	-78.149	.043	.0256	.016
141	1456	1451	2.515	2.521	.006	.0129	.013
142	1455	1404	137.412	137.404	-.008	.0504	.023
143	1455	1457	57.756	57.778	.022	.0203	.018
144	1451	1454	9.058	8.950	-.108**	.0276	.014
145	1451	1457	56.776	56.794	.018	.0254	.017
146	1452	1454	30.473	30.478	.005	.0103	.009
147	4247	1461	608.322	608.420	.098	.1236	.100
148	1461	1452	-182.491	-182.421	.070	.0553	.034

49	1452	1457	78.192	78.197	.005	.0256	.016
50	1457	1404	79.656	79.631	-.025	.0399	.019
151	1404	1422	2.213	2.257	.044	.0361	.024
152	1422	1423	-25.827	-25.826	.001	.0177	.016
153	1423	1461	48.257	48.246	-.011	.0177	.020
154	1461	1405	-24.452	-24.480	-.028	.0371	.027
155	1422	1490	-.277	-.277	.000	.0072	.009
156	1422	1424	5.745	5.753	.008	.0110	.012
157	1424	1423	-31.572	-31.585	-.013	.0184	.016
158	1457	1404	79.656	79.631	-.025	.0399	.019
159	1422	1404	-2.213	-2.257	-.044	.0361	.024
160	1401	1402	26.749	26.726	-.023	.0381	.040
161	1402	1403	-13.413	-13.419	-.006	.0194	.023
162	1403	1404	85.813	85.797	-.016	.0522	.024
163	1404	1405	.191	.136	-.055	.0300	.026
164	1405	1406	18.890	18.832	-.058**	.0198	.020
165	1406	1407	12.511	12.534	.023	.0263	.031
166	1407	1408	-43.394	-43.382	.012	.0191	.023
167	1408	1409	-81.192	-81.163	.029	.0301	.035
168	1409	1410	-1.890	-1.882	.008	.0329	.039
169	1410	1411	-17.755	-17.752	.003	.0192	.024
170	1411	1412	-15.181	-15.174	.007	.0304	.037
171	1412	1413	-20.694	-20.690	.004	.0225	.028
172	1413	1414	-17.217	-17.215	.002	.0153	.019
173	1414	1415	-24.135	-24.117	.018	.0499	.056
174	1415	1417	-27.011	-27.003	.007	.0320	.038
175	1417	1418	-16.281	-16.263	.018	.0254	.031
176	1418	1419	27.890	27.900	.010	.0192	.023
177	1419	1421	-54.714	-54.634	.080	.0517	.054
178	1401	1406	118.231	118.359	.128	.1500	.048
179	1408	1419	-193.466	-193.353	.113	.2503	.082
180	1401	1480	813.235	813.253	.018	.1791	.091
181	1480	1491	-212.443	-212.457	-.014	.0989	.109
182	1480	8566	-28.021	-28.021	.000	.0075	.009
183	4247	8567	949.075	948.658	-.417	.2806	.170
184	8567	1470	16.602	16.520	-.082	.1197	.137
185	1470	1482	106.110	106.039	-.071	.1613	.092
186	1482	1481	-139.065	-138.837	.228	.1494	.081
187	1481	1464	-106.269	-106.254	.015	.0791	.060
188	1464	1494	-183.617	-183.606	.011	.0905	.100
189	1464	1489	260.900	261.067	.167	.1437	.122
190	1489	1450	-64.792	-64.725	.067	.0908	.101
191	1463	1420	-474.177	-474.243	-.066	.0528	.052
192	1450	1469	-317.155	-317.194	-.039	.0861	.082
193	1469	1475	-24.626	-24.696	-.070	.0949	.078
194	1475	1463	117.972	117.981	.009	.1327	.063
195	1463	1470	166.924	166.854	-.070	.0672	.057
196	1481	1494	-289.886	-289.922	-.036	.1619	.109
197	1470	1420	-641.101	-641.156	-.055	.0942	.068
198	1469	1409	-214.723	-214.791	-.068	.0527	.053
199	1450	1462	-156.967	-156.953	.014	.1229	.091
200	1462	1453	-297.852	-297.898	-.046	.0916	.070
201	1453	1401	-83.214	-83.226	-.012	.0468	.054
202	1401	1488	-5.298	-5.298	.000	.0369	.044
203	1488	1461	129.091	129.091	.000	.1245	.063
204	1461	1469	97.086	96.855	-.231	.1189	.062

205	1481	1493	-33.919	-33.984	-.065	.2286	.233
206	1493	1492	-14.229	-14.292	-.063	.2248	.231
207	1492	8756	460.228	460.179	-.049	.1975	.214
208	8756	1495	-656.790	-656.886	-.096	.1828	.135
209	1495	1491	397.310	397.290	-.020	.0825	.096
210	1491	1434	-627.909	-628.610	-.701	.4021	.211
211	1434	1445	552.044	552.768	.724	.4939	.185
212	1445	1401	-524.927	-524.965	-.038	.0917	.048
213	1421	1420	.880	.882	.002	.0077	.010
214	1401	5001	135.823	135.680	-.143	.3271	.101
215	5001	1480	677.412	677.330	-.082	.2934	.117
216	8566	5001	-649.391	-649.425	-.034	.2916	.117
217	1432	5001	29.012	29.013	.001	.0373	.045
218	1415	1416	-21.494	-21.494	.000	.0090	.011
219	1437	1480	246.148	245.821	-.326	.2694	.128
220	1480	8567	-348.689	-348.837	-.148	.5710	.181
221	1405	1462	281.725	281.861	.136**	.0448	.042
222	1427	5001	-352.297	-351.968	.329	.2872	.145
223	1457	4571	2.420	2.420	.000	.0073	.009
224	1475	1463	117.972	117.878	-.094	.1326	.063
225	1480	1437	-246.148	-245.859	.288	.2690	.128
226	1480	1440	-742.127	-742.420	-.293	.2778	.098
227	1482	8756	273.014	272.945	-.069	.5534	.151
228	1496	1498	26.401	26.396	-.005	.0092	.008
229	1497	1439	127.756	127.810	.054	.0964	.063
30	1497	1445	587.069	586.957	-.112	.1210	.074
231	1497	1446	251.487	251.561	.074	.0815	.058
232	1497	1496	-11.556	-11.561	-.005	.0076	.007
233	1497	1498	14.845	14.846	.001	.0078	.007
234	1499	1439	95.529	95.395	-.134	.1026	.063
235	1499	1446	219.260	219.284	.024	.0815	.058
236	1499	1496	-43.783	-43.778	.005	.0113	.009
237	1499	1497	-32.227	-32.233	-.006	.0094	.008
238	1499	1498	-17.382	-17.379	.003	.0080	.008
239	1500	1473	-12.826	-12.778	.048**	.0157	.015
240	1500	1471	-28.826	-28.843	-.017	.0093	.011
241	8756	1480	-47.037	-47.176	-.139**	.0615	.052
242	1437	111	-94.772	-94.755	.017	.1444	.165
243	111	108	321.548	321.559	.011	.1157	.137
244	108	107	-57.990	-57.975	.015	.1325	.153
245	107	1464	-393.949	-393.904	.045	.2319	.217
246	1462	1406	-262.835	-262.577	.258**	.0590	.043
247	1406	1424	-11.124	-11.113	.011	.0091	.008

MEAN RESIDUAL

-.0007

STD. ERROR OF OBS. OF UNIT WT.

1.2505

**INDICATES RESIDUALS > 2*SIGMA SET BY A-PRIORI INPUT FACTORS

TIME USED= 194.00 SECONDS

APPENDIX C

GANET HORIZONTAL ADJUSTMENT

CYPRUS ANVIL MINES CONTROL

MAP SHEET 105 K, Y.T.

1979

CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

SPACE REQUIREMENTS

THE PROGRAM REQUIRES = 35673
 SPACE REQUESTED = 60673
 WORKING SPACE = 25000
 MAX NUMBER OF STATIONS = 999
 SPACE FOR DATA EDIT = 10989

THE FOLLOWING OPTIONS HAVE BEEN CHOSEN FROM THE CONTROL CARD

CARD PUNCHED..	0-00	3 0-00	0	0	0	1 0.1	0	0	0	1	0.	0.0WEIG
	10	15 20	25	30	35	40 45	50	55	60	65	70	75 80
COL 2-10	CONVERGENCE CRITERION		.000005 SECONDS									
COL 14-15	NO OF ITERATIONS (DESIGN MODE=-1)		3									
	(DATA CHECK=99)											
COL 16-20	APRIORI VARIANCE FACTOR		1.00									
COL 24-25	PRINT FULL INVERSE MATRIX		NO									
COL 29-30	PRINT NDRMAL EQUATIONS		NO									
COL 31	INTEGRATION STATUS(DEFAULT A)		NO									
COL 34-35	PRODUCE CODE 34 CARDS		NO									
COL 39-40	STORE ADJUSTED COORDINATES (=1)		YES									
	FORM POSITION EQUATIONS (=2)		NO									
	DO BOTH THE ABOVE (=3)		NO									
COL 41-44	RADIUS FOR ERROR ELLIPSES		5000.0 M									
COL 45	INCLUDE ALL CONNECTED LINES		YES									
COL 50	INPUT LISTING COMPLETE (=1)		NO									
COL 55	PRINT ADJUSTED COORDS FOR EACH PASS		NO									
COL 60	GEOID CORRECTIONS		NO									
	(1=CORRECTION APPLIED, PRINT SUPPRESSED)											
	(2=PRINT REDUCED OBSERVATIONS)											
COL 64-65	ELLIPSOID NUMBER		1									
COL 66-70	CONSTRAINT DEFAULT		1.000									
COL 71-74	PRINT PARAMETRIC EQUATIONS OVER		600.0									
COL 75	PRINT ALL PARAMETRIC EQUATIONS		NO									
COL 76-79	PRECISION TYPE		WEIGHT									
	NEW VARI		STAN OLD WEIG									
COL 80	NO BANDWIDTH MINIMUM (N)											

CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

PROCESSING POSITIONS
 PROCESSING OBSERVATIONS

SUMMARY OF INPUT

NUM OF ERRORS DETECTED	=	0		
NUM OF STATIONS INPUT	=	110	-28065519.92	
NUM OF UNKNOWNNS	=	212		
NUM OF ASTRO STATIONS	=	0	0.	
NUM OF DIRECTIONS AND SUM	=	487	241208909.5	83.22900000
NUM OF DISTANCES AND SUM	=	229	1112519.916	104.68600000
NUM OF AZIMUTHS AND SUM	=	0	0.	0.
NUM OF PDS EQUAT AND SUM	=	0	0.	0.
SUM OF OBSERVATIONS	=	2423214	29.466	
SUM OF PRECISIONS	=		187.915	
THERE ARE 96 OBSERVATIONS TO FIXITY				
INPUT COMPLETE				

CHOOSING A PARTITION SIZE OF	106
PARTITIONS IN FIRST ROW	2
TOTAL NUMBER OF PARTITIONS	8

THIS ADJUSTMENT REQUIRES 24476 WORDS OF WORKING SPACE

GOING INTO OVERLAY	7	NRP=	110	NPEI=	2	
INPUT SPAN	29					MINIMUM SPAN 39
GOING INTO OVERLAY	2	NRP=	110	NPEI=	2	

NOTE-ELLIPSOID PARAMETERS

CLARKE 1866

A = 6378206.4000

F = 294.9786982

DEPARTMENT OF ENERGY, MINES, AND RESOURCES
 GEODETIC SURVEY OF CANADA PROGRAM GANET

DATE = 79/11/19

CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

INPUT COORDINATES

INPUT GEOD SPHEROID COMPONENTS

STA INDX	NORM UNK	STATION NUMBER	NAME	LATITUDE D M S			LONGITUDE D M S			ELEVATION (METERS)	GEOD HEIGHT (METERS)	MERIDIAN COMP. (SECS)	PRIME VERTICAL (SECS)
1		6785000	67A35	62	1	3.46165N	132	17	15.39127W	1395.108			
2		6785001	67A24	62	14	7.74481N	132	52	.82460W	1336.735			
3		678566	67A25	62	17	46.57015N	133	3	39.32790W	1986.126			
4		678567	67A55	62	10	9.46469N	133	31	10.60857W	1665.458			
5	125	1470	RC 11	62	20	47.36413N	133	30	5.90605W	1602.061			
6	141	1484		62	21	39.05866N	133	28	2.48085W	1034.002			
7	99	1463	RC 2	62	19	57.27306N	133	27	25.27454W	1515.137			
8	139	1420	NHI 3	62	20	45.04533N	133	25	33.83973W	1040.960			
9	123	1481	HIW 2	62	22	48.66588N	133	23	20.42669W	1649.105			
10	133	1447		62	24	56.11510N	133	26	54.46559W	1888.915			
11	107	1464	HIW 3	62	22	58.80454N	133	19	32.98452W	1542.837			
12	135	1494	HIW 4	62	22	1.03139N	133	15	42.98100W	1359.219			
13	101	1483		62	21	31.20138N	133	20	43.78588W	1421.367			
14	127	1487	PR1 4	62	21	22.73926N	133	21	17.18870W	1257.029			
15	131	1485	TR1 18	62	21	42.42906N	133	22	41.78033W	1294.534			
16	129	1486	PR1 6	62	20	56.36423N	133	21	51.24002W	1190.272			
17	137	1419	VG 19	62	20	28.85708N	133	23	17.66630W	1094.794			
18	147	1418	VG 18	62	20	6.83183N	133	22	57.23610W	1066.904			
19	105	1417	NHI 1-71	62	20	-61208N	133	21	47.85823W	1083.186			
20	153	1416	VG 16	62	19	29.75296N	133	20	51.03015W	1088.702			
21	145	1415	VG 15A	62	19	34.18582N	133	20	37.81934W	1110.196			
22	103	1475	HIW 8	62	18	38.93539N	133	21	40.95836W	1397.164			
23	109	1477		62	18	31.39845N	133	24	1.27951W	1445.491			
24	143	1493	HIW 12	62	25	31.48473N	133	13	58.25400W	1615.186			
25	161	1492	HIW 13	62	23	5.65663N	133	4	27.22881W	1600.957			
26	149	1476	PE 1	62	17	14.13390N	133	23	6.59837W	1521.994			
27	155	1478	PE 2	62	15	47.22357N	133	22	30.00412W	1360.385			
28	111	1489	HIW 5	62	20	30.98602N	133	15	5.17350W	1803.737			
29	93	1450	HIW 6	62	18	29.16538N	133	15	.02522W	1738.945			
30	45	1469	HIW 7	62	17	16.46327N	133	18	12.60274W	1421.790			
31	113	1409	VG 9	62	16	56.83870N	133	15	47.57697W	1207.068			
32	115	1410	VG 10	62	17	33.51397N	133	16	36.63201W	1205.178			
33	157	1411	VG 11	62	17	34.04999N	133	17	28.04456W	1187.423			
34	159	1412	VG 12	62	18	6.74734N	133	18	16.92107W	1172.242			
35	163	1413	VG 13A	62	18	26.15670N	133	19	2.47183W	1151.548			
36	151	1414	VG 14	62	18	33.84640N	133	19	37.97535W	1134.332			
37	97	1407	VG 7	62	16	45.27994N	133	13	51.50378W	1331.654			
38	95	1424	HIW 6KA	62	16	4.38387N	133	13	34.71771W	1308.019			
39	85	1423	HIW 5KA	62	15	41.75566N	133	13	28.38780W	1276.447			
40	43	1405	VG 5	62	16	2.81403N	133	12	50.89790W	1300.253			
41	83	1422	HIW 4KA	62	16	1.94682N	133	13	10.75655W	1302.274			
42	55	1461	HIW 1KA	62	15	27.03933N	133	14	2.96698W	1324.705			
43	165	1495	HIW 15	62	21	11.82117N	132	58	54.66016W	1404.395			
44	73	1453	HIW 10	62	15	18.93010N	133	7	19.71493W	1284.126			
45	77	1402	VG 2	62	14	51.78812N	133	9	3.19188W	1227.661			
46	71	1403	VG 3	62	14	55.41865N	133	9	54.74691W	1214.248			
47	59	1457	HIW 3KA	62	15	7.24121N	133	10	20.82477W	1220.405			
48	121	14571	JK1	62	15	6.05046N	133	10	16.51049W	1222.825			
49	79	1454	JK 4	62	15	15.12816N	133	11	28.44971W	1172.687			
				62	15	5.12313N	133	11	31.73393W	1142.213			

DEPARTMENT OF ENERGY, MINES, AND RESOURCES
 GEODETIC SURVEY OF CANADA PROGRAM GANET

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CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

INPUT COORDINATES

INPUT GEOD SPHEROID COMPONENTS

STA INDX	NDRM UNK	STATION NUMBER	NAME	LATITUDE D M S	LONGITUDE D M S	ELEVATION (METERS)	GEOD HEIGHT (METERS)	MERIDIAN COMP. (SECS)	PRIME VERTICAL (SECS)
51	47	1459	JK 3	62 15 .77829N	133 11 9.55689W	1166.198			
52	87	1460	IN 4	62 15 5.36867N	133 11 20.64897W	1150.246			
53	81	1458	IN 1	62 15 3.22878N	133 10 50.27397W	1186.118			
54	117	1456	IN 2	62 14 55.13496N	133 10 54.75680W	1161.114			
55	119	1455	IN 3	62 14 44.53247N	133 10 46.00429W	1162.649			
56	65	1451	JK 2	62 14 41.20947N	133 11 3.59991W	1163.629			
57	61	1488	HIW 11	62 13 50.32678N	133 9 10.26517W	1195.614			
58	11	1446	U+U 611	62 12 56.75613N	133 11 38.09115W	1390.257			
59	63	1479	DY 1	62 13 59.54954N	133 8 11.06381W	1190.464			
60	37	1471	DP 1	62 13 54.25555N	133 7 40.92485W	1131.941			
61	41	1472	IB 751	62 13 48.47665N	133 7 26.33823W	1094.303			
62	51	1473	IB 756	62 14 15.53292N	133 7 26.60220W	1147.940			
63	69	1474	DP 2	62 13 52.59126N	133 6 51.43526W	1040.608			
64	31	1443	BC 5	62 13 11.47708N	133 6 22.97176W	880.126			
65	67	1449	BC 3	62 12 54.70906N	133 7 43.87828W	935.430			
66	13	1439		62 11 52.48993N	133 5 18.92120W	1266.526			
67	19	1440		62 11 37.84477N	133 5 10.41829W	1272.020			
68	49	14401	1440 ECC	62 11 50.22611N	133 5 21.27088W	1268.308			
69	33	1468	BC 7	62 13 47.46999N	133 3 38.81737W	785.463			
70	39	1442		62 13 26.81411N	133 0 46.83719W	955.698			
71	75	1448		62 12 36.49431N	133 1 57.37079W	1096.962			
72	89	1444	SL 7	62 12 7.14170N	133 0 13.08419W	911.008			
73	53	1467	BC 16	62 14 58.19079N	133 1 9.46379W	891.373			
74	15	1438		62 16 39.52869N	132 59 33.99396W	1425.048			
75	91	1466		62 16 25.32442N	132 56 12.34598W	866.848			
76	35	1465	BC 20	62 16 57.27464N	132 52 26.02961W	858.193			
77	17	1432	BC 17	62 14 50.64469N	132 52 53.17242W	1307.723			
78	25	1441		62 10 44.75357N	133 0 59.84607W	1125.057			
79	21	1420		62 8 26.70926N	132 56 29.38430W	963.003			
80	29	1430	SL 12	62 10 28.66512N	132 54 10.09438W	961.825			
81	27	1425		62 6 40.47299N	132 50 45.66260W	1069.259			
82	23	1429		62 9 18.71442N	132 45 57.54430W	1113.342			
83	3	1431		62 11 27.65892N	132 42 33.36513W	1110.953			
84	1	1436		62 13 18.28845N	132 45 34.96335W	939.631			
85	5	1433		62 14 1.41403N	132 37 22.64447W	1311.570			
86	9	1435		62 17 55.69395N	132 48 48.81661W	885.537			
87	7	1426	SL 13	62 3 50.36139N	132 34 54.45409W	1406.842			
88	167	1404	VG 4	62 15 47.91858N	133 11 33.05958W	1300.062			4265-24
89	169	1462	HIW 9	62 16 29.81121N	133 10 55.10855W	1581.978			
90	171	678756	MT MYE	62 18 43.22419N	133 5 55.62465W	2061.185			
91	173	1482	HIW 1	62 24 23.96169N	133 29 41.29423W	1788.171			
92	175	1499		62 13 45.41752N	133 8 8.01213W	1170.997			
93	177	1498		62 13 40.38064N	133 8 7.71584W	1153.615			
94	179	1496		62 13 35.26701N	133 7 54.40405W	1127.214			
95	181	1500	DY 2	62 14 .78234N	133 7 51.69498W	1160.767			
96	183	1434	HIW 17	62 15 50.86883N	132 42 57.82929W	1173.795			
97	185	1491	HIW 14	62 19 32.22643N	133 0 38.06144W	1801.704			
98	187	1497		62 13 37.79868N	133 8 .28450W	1138.770			
99	189	1480	BC 13A	62 17 50.10108N	133 3 40.49649W	2014.147			

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INPUT COORDINATES

INPUT GEOID SPHEROID COMPONENTS

STA INDX	NORM YK	STATION		LATITUDE			LONGITUDE			ELEVATION (METERS)	GEOID HEIGHT (METERS)	MERIDIAN COMP. (SECS)	PRIME VERTICAL (SECS)
		NUMBER	NAME	D	M	S	D	M	S				
101	193	1490	HIW 7KA	62	16	26.71258N	133	14	14.05325W	1301.997			
102	195	1406	VG 6	62	16	11.59333N	133	13	40.75256W	1319.143			
103	197	1421	RC 4	62	20	48.01646N	133	25	40.21111W	1040.080			
104	199	1401	VG 1	62	14	17.65622N	133	7	43.69553W	1200.912			
105	201	1445	HIW 16	62	16	17.44886N	133	6	42.70010W	1725.839			
106	203	1437	BC 21	62	18	58.78083N	132	50	56.67757W	1768.000			
107	205	1427		62	15	37.51911N	132	38	34.11911W	1689.032			
108	207	107	GRAVITY 107	62	22	3.54500N	133	8	31.88500W	1936.785			
109	209	108	GRAVITY 108	62	21	9.52700N	133	2	26.53000W	1994.775			
110	211	111	GRAVITY 111	62	20	34.04500N	132	57	.57600W	1673.227			

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ELAPSED TIME 24.768 24.768

POSITION CORRECTIONS - PASS 1

MAXIMUM LATITUDE CORRECTION= .09342
MAXIMUM LONGITUDE CORRECTION= .05012
PASS TIME= 115.329 115.329 ELAPSED TIMES= 140.097 140.097

POSITION CORRECTIONS - PASS 2

MAXIMUM LATITUDE CORRECTION= .00001
MAXIMUM LONGITUDE CORRECTION= .00002
PASS TIME= 111.384 111.384 ELAPSED TIMES= 251.481 251.481

POSITION CORRECTIONS - PASS 3

MAXIMUM LATITUDE CORRECTION= .00000
MAXIMUM LONGITUDE CORRECTION= .00000

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THE ESTIMATE OF THE VARIANCE FACTOR AFTER ADJUSTMENT IS 2.414
THE APRIORI VARIANCE FACTOR WAS 1.000
THIS GIVES A VARIANCE RATIO OF 2.41

397 DEGREES OF FREEDOM
716 OBSERVATIONS
0 POSITION EQUATIONS
55.4 PER CENT REDUNDANCY
106 FREE STATIONS
3.7 DEGREES OF FREEDOM PER FREE STATION

3 ITERATIONS REQUIRED FOR CONVERGENCE

THE VARIANCE RATIO TEST IS NOT SATISFIED AT THE 99 (CONFIDENCE LEVEL

CARE SHOULD BE TAKEN IN USING SUBSEQUENT RESULTS

F TEST FACTOR = 1.93

IT SHOULD BE LESS THAN UNITY

THE TAU REJECTION VALUE IS 4.300 BASED ON A CONFIDENCE LEVEL OF 99. PER CENT
STANDARDISED CORRECTIONS GREATER THAN THIS VALUE WILL BE MARKED

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			LATITUDE	LONGITUDE	SEMI- MAJOR (M)	SEMI- MINOR (M)	ORIENT					
ERROR ELLIPSES ARE SCALED BY THE A PRIORI VARIANCE FACTOR OF 1.0000												
4	6785000	67A35	62 1 3.46165 N	132 17 15.39127 W							1395.108	
4	6785001	67A24	62 14 7.74481 N	132 52 .82460 W							1336.735	
4	678566	67A25	62 17 46.57015 N	133 3 39.32790 W							1986.126	
4	678567	67A55	62 18 9.46469 N	133 31 10.60857 W							1665.458	
4	1470	RC 11	62 20 47.36500 N	133 30 5.90537 W	.071	.034	25.5				1682.061	
4	1484		62 21 39.05957 N	133 28 2.48002 W	.073	.041	38.7				1034.002	
4	1463	RC 2	62 19 57.27396 N	133 27 25.27378 W	.063	.034	23.3				1515.137	
4	1420	WHI 3	62 20 45.04615 N	133 25 33.83900 W	.063	.038	34.0				1040.960	
4	1481	HIW 2	62 22 48.66667 N	133 23 20.42559 W	.065	.041	51.8				1649.109	
4	1447		62 24 56.11595 N	133 26 54.46415 W	.085	.044	56.8				1888.915	
4	1464	HIW 3	62 22 50.80501 N	133 19 32.98327 W	.062	.050	63.0				1542.837	
4	1494	HIW 4	62 22 1.03173 N	133 15 42.98007 W	.085	.069	116.5				1359.219	
4	1483		62 21 31.20200 N	133 20 43.78535 W	.055	.041	44.8				1421.367	
4	1487	PR1 4	62 21 22.74008 N	133 21 17.18750 W	.055	.040	42.5				1257.029	
4	1485	TR1 18	62 21 42.42985 N	133 22 41.77931 W	.059	.039	43.9				1294.534	
4	1486	PR1 6	62 20 56.36500 N	133 21 51.23905 W	.055	.038	38.0				1190.272	
4	1419	VG 19	62 20 28.85785 N	133 23 17.66560 W	.058	.038	33.5				1094.794	
4	1418	VG 18	62 20 6.83258 N	133 22 57.23545 W	.056	.037	31.0				1066.904	
4	1417	WHI I-71	62 20 .61278 N	133 21 47.85762 W	.053	.036	31.2				1083.186	
4	1416	VG 16	62 19 29.75367 N	133 20 51.02961 W	.053	.037	28.9				1088.702	
4	1415	VG 15A	62 19 34.18653 N	133 20 37.81880 W	.053	.037	28.5				1110.198	
4	1475	HIW 8	62 18 38.93608 N	133 21 40.95783 W	.052	.036	25.1				1397.164	
4	1477		62 18 31.39920 N	133 24 1.27900 W	.057	.040	16.2				1445.491	
4	1493	HIW 12	62 25 31.48746 N	133 13 58.25227 W	.100	.079	70.0				1615.186	
4	1492	HIW 13	62 23 5.65864 N	133 4 27.22874 W	.100	.081	168.3				1600.957	
4	1476	PE 1	62 17 14.13463 N	133 23 6.59801 W	.062	.053	50.6				1521.994	
4	1478	PE 2	62 15 47.22429 N	133 22 30.00393 W	.105	.057	77.6				1360.385	
4	1489	HIW 5	62 20 30.98619 N	133 15 5.17337 W	.071	.055	172.0				1803.737	
4	1450	HIW 6	62 18 29.16551 N	133 15 .02598 W	.049	.040	22.3				1738.945	
4	1469	HIW 7	62 17 16.46373 N	133 18 12.60128 W	.048	.032	15.6				1421.790	
4	1409	VG 9	62 16 56.83972 N	133 15 47.57622 W	.042	.032	13.6				1207.068	
4	1410	VG 10	62 17 33.51492 N	133 16 36.63142 W	.046	.036	22.3				1205.178	
4	1411	VG 11	62 17 34.05087 N	133 17 28.04395 W	.049	.036	23.3				1187.423	
4	1412	VG 12	62 18 6.74816 N	133 18 16.92056 W	.054	.037	29.0				1172.242	
4	1413	VG 13A	62 18 26.15748 N	133 19 2.47135 W	.056	.038	31.0				1151.548	
4	1414	VG 14	62 18 33.84716 N	133 19 37.97487 W	.056	.038	30.3				1134.332	
4	1407	VG 7	62 16 45.28092 N	133 13 51.50330 W	.039	.032	14.1				1331.654	
4	1424	HIW 6KA	62 16 4.38474 N	133 13 34.71626 W	.036	.029	178.5				1308.019	
4	1423	HIW 5KA	62 15 41.75696 N	133 13 28.38392 W	.036	.028	171.6				1276.447	

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			LATITUDE	LONGITUDE	SEMI- MAJOR (M)	SEMI- MINOR (M)	ORIENT					
ERROR ELLIPSES ARE SCALED BY THE A PRIORI VARIANCE FACTOR OF 1.0000												
4	1405	VG 5	62 16 2.81464 N	133 12 50.89938 W	.034	.029	172.4	1300.253				
4	1422	HIW 4KA	62 16 1.94845 N	133 13 10.75466 W	.035	.029	175.7	1302.274				
4	1461	HIW 1KA	62 15 27.03994 N	133 14 2.96381 W	.037	.028	169.1	1324.705				
4	1495	HIW 15	62 21 11.82179 N	132 58 54.66078 W	.070	.064	65.5	1404.395				
4	1453	HIW 10	62 15 18.92988 N	133 7 19.71470 W	.043	.028	170.2	1284.126				
4	1402	VG 2	62 14 51.78881 N	133 9 3.19097 W	.031	.022	139.9	1227.661				
4	1403	VG 3	62 14 55.41990 N	133 9 54.74591 W	.032	.024	144.7	1214.248				
4	1457	HIW 3KA	62 15 7.24264 N	133 10 20.82339 W	.032	.024	146.8	1220.405				
4	14571	JK1	62 15 6.05187 N	133 10 16.50913 W	.034	.024	141.4	1222.825				
4	1454	JK 4	62 15 15.13006 N	133 11 28.44826 W	.034	.025	153.4	1172.687				
4	1452	HIW 2KA	62 15 5.12503 N	133 11 31.73301 W	.034	.025	152.5	1142.213				
4	1459	JK 3	62 15 .78060 N	133 11 9.55580 W	.034	.024	150.0	1166.198				
4	1460	IN 4	62 15 5.37079 N	133 11 20.64764 W	.034	.025	150.8	1150.246				
4	1458	IN 1	62 15 3.23061 N	133 10 50.27274 W	.033	.025	149.2	1186.118				
4	1456	IN 2	62 14 55.13679 N	133 10 54.75557 W	.033	.025	149.1	1161.114				
4	1455	IN 3	62 14 44.53416 N	133 10 46.00311 W	.034	.025	145.9	1162.649				
4	1451	JK 2	62 14 41.21131 N	133 11 3.59863 W	.034	.024	146.0	1163.629				
4	1488	HIW 11	62 13 50.32687 N	133 9 10.26284 W	.043	.033	76.4	1195.614				
4	1446	U+U 611	62 12 56.75509 N	133 11 38.09160 W	.038	.021	136.7	1390.257				
4	1479	DY 1	62 13 59.54907 N	133 8 11.06300 W	.030	.020	130.5	1190.464				
4	1471	DP 1	62 13 54.25466 N	133 7 40.92419 W	.030	.019	127.9	1131.941				
4	1472	IB 751	62 13 48.47587 N	133 7 26.33675 W	.030	.019	126.0	1094.303				
4	1473	IB 756	62 14 15.53238 N	133 7 26.60035 W	.029	.019	130.2	1147.940				
4	1474	DP 2	62 13 52.59043 N	133 6 51.43413 W	.029	.020	122.6	1040.608				
4	1443	BC 5	62 13 11.47555 N	133 6 22.96986 W	.035	.027	100.3	880.126				
4	1449	BC 3	62 12 54.70737 N	133 7 43.87620 W	.035	.031	112.4	935.430				
4	1439		62 11 52.48854 N	133 5 18.91853 W	.035	.022	103.6	1266.526				
4	1440		62 11 37.84364 N	133 5 10.41580 W	.036	.025	104.2	1272.020				
4	14401	1440 ECC	62 11 50.22474 N	133 5 21.26817 W	.035	.024	103.3	1268.308				
4	1468	BC 7	62 13 47.46881 N	133 3 38.81585 W	.043	.028	108.7	785.463				
4	1442		62 13 26.81359 N	133 0 46.83576 W	.033	.029	5.6	955.698				
4	1448		62 12 36.49374 N	133 1 57.36924 W	.037	.032	85.8	1096.962				
4	1444	SL 7	62 12 7.14119 N	133 0 13.08250 W	.050	.035	64.6	911.008				
4	1467	BC 16	62 14 58.18988 N	133 1 9.46223 W	.056	.027	6.8	891.373				
4	1438		62 16 39.52786 N	132 59 33.99491 W	.048	.028	33.4	1425.048				
4	1466		62 16 25.32403 N	132 56 12.34680 W	.038	.024	49.7	866.848				
4	1465	BC 20	62 16 57.27472 N	132 52 26.03098 W	.036	.022	99.2	858.193				
4	1432	BC 17	62 14 50.64473 N	132 52 53.17233 W	.017	.013	146.5	1307.723				
4	1441		62 10 44.75274 N	133 0 59.84336 W	.048	.036	54.2	1125.057				

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			LATITUDE	LONGITUDE	SEMI- MAJOR [M]	SEMI- MINOR [M]	ORIENT				
ERROR ELLIPSES ARE SCALED BY THE A PRIORI			VARIANCE FACTOR OF		1.0000						
4	1428		62 8 26.70893 N	132 56 29.38229 W	.074	.055	126.3			963.003	
4	1430	SL 12	62 10 28.66494 N	132 54 10.09305 W	.073	.072	58.1			961.825	
4	1425		62 6 40.47307 N	132 50 45.66003 W	.079	.055	97.3			1069.259	
4	1429		62 9 18.71490 N	132 45 57.54272 W	.064	.059	96.5			1113.342	
4	1431		62 11 27.65271 N	132 42 33.36441 W	.063	.056	173.9			1110.953	
4	1436		62 13 18.28917 N	132 45 34.96353 W	.114	.084	80.2			939.631	
4	1433		62 14 1.41534 N	132 37 22.64477 W	.069	.061	158.6			1311.570	
4	1435		62 17 55.69450 N	132 48 48.81881 W	.046	.034	107.4			885.537	
4	1426	SL 13	62 3 50.36124 N	132 34 54.45288 W	.136	.112	126.5			1406.842	
4	1404	VG 4	62 15 47.92032 N	133 11 33.05893 W	.032	.027	155.7			1300.062	
4	1462	H1W 9	62 16 29.81194 N	133 10 55.11200 W	.034	.030	141.5			1581.978	
4	670756	MT MYE	62 18 43.22560 N	133 5 55.62771 W	.024	.015	38.3			2061.185	
4	1482	H1W 1	62 24 23.96263 N	133 29 41.29280 W	.089	.044	46.1			1788.171	
4	1499		62 13 45.42010 N	133 8 8.01805 W	.032	.021	127.4			1170.997	
4	1498		62 13 40.38365 N	133 8 7.72167 W	.032	.021	126.6			1153.615	
4	1496		62 13 35.26997 N	133 7 54.40957 W	.032	.021	125.8			1127.214	
4	1500	DY 2	62 14 78.056 N	133 7 51.69345 W	.030	.019	131.1			1160.767	
4	1434	H1W 17	62 15 50.86983 N	132 42 57.83015 W	.070	.052	128.8			1173.795	
4	1491	H1W 14	62 19 32.22694 N	133 0 38.06200 W	.055	.035	52.4			1801.704	
4	1497		62 13 37.80199 N	133 8 29.098 W	.032	.021	125.9			1138.770	
4	1480	BC 13A	62 17 50.10108 N	133 3 40.49650 W	.004	.001	171.3			2014.147	
4	1408	VG 8	62 16 34.67073 N	133 14 37.56044 W	.040	.032	12.7			1288.260	
4	1490	H1W 7KA	62 16 26.71365 N	133 14 14.05326 W	.040	.032	11.8			1301.997	
4	1406	VG 6	62 16 11.59432 N	133 13 40.75505 W	.037	.029	1.6			1319.143	
4	1421	RC 4	62 20 48.01728 N	133 25 40.21038 W	.064	.038	34.2			1040.080	
4	1401	VG 1	62 14 17.65568 N	133 7 43.69486 W	.028	.018	131.4			1200.912	
4	1445	H1W 16	62 16 17.44884 N	133 6 42.70026 W	.025	.017	137.9			1725.839	
4	1437	BC 21	62 18 58.78112 N	132 50 56.68040 W	.045	.026	105.5			1768.000	
4	1427		62 15 37.52034 N	132 38 34.11923 W	.071	.054	136.7			1689.032	
4	107	GRAVITY 107	62 22 3.52190 N	133 8 31.89488 W	.087	.072	76.2			1936.789	
4	108	GRAVITY 108	62 21 9.46672 N	133 2 26.56485 W	.077	.056	54.8			1994.775	
4	111	GRAVITY 111	62 20 33.95159 N	132 57 6.2610 W	.075	.053	98.8			1673.227	

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THE STANDARDISED CORRECTIONS HAVE BEEN SCALED BY THE CALCULATED SECOND MOMENT. FACTOR = .8643
 VALUES GREATER THAN THE VALUE OF TAU (4.3001) WILL BE MARKED

OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FOR. AZ.	DISTANCE
6785001	67A24	1401 VG 1	0.000	.170	-.789	0 0 0.000	-.273	271 24 23.958	13620.8740
		1445 HIW 16	16 12 30.500	.170	3.057	16 12 34.346	1.056	287 36 58.304	13347.8114
		678566 67A25	32 35 18.800	.170	-3.794	32 35 15.795	-1.311	303 59 39.753	12143.7500
		1480 BC 13A	32 58 12.800	.170	-3.022	32 58 10.567	-1.044	304 22 34.525	12218.8618
		1438	34 20 35.200	.170	2.137	34 20 38.126	.738	305 45 2.084	8053.6448
		1432 BC 17	58 57 21.500	.170	-11.222	58 57 11.066	-3.878	330 21 35.024	1528.1876
		1437 BC 21	94 26 55.500	.170	-2.484	94 26 53.804	-.858	5 51 17.762	9057.5955
		1427	165 4 20.550	.170	-1.823	165 4 19.516	-.630	76 28 43.474	11973.6101
		1433	179 22 9.900	.170	3.098	179 22 13.787	1.070	90 46 37.744	12685.5870
		1431	209 39 55.200	.170	1.997	209 39 57.986	.690	121 4 21.944	9583.0312
		6785000 67A35	217 6 25.200	.170	5.962	217 6 31.951	2.060	128 30 55.909	38772.2904
		1426 SL 13	230 35 34.500	.170	-4.890	230 35 30.399	-1.690	141 59 54.357	24213.9853
		1429	238 7 43.200	.170	.032	238 7 44.021	.011	149 32 7.979	10376.4265
		1425	264 5 30.200	.170	.363	264 5 31.352	.125	175 29 55.310	13889.5817
		1428	288 49 37.200	.170	2.213	288 49 40.202	.765	200 14 4.159	11250.0811
		1441	319 46 25.200	.170	1.413	319 46 27.401	.488	231 10 51.359	10010.7490
		1440	336 33 34.400	.170	4.719	336 33 39.908	1.631	247 58 3.866	12319.5699
		1439	338 44 15.000	.170	2.799	338 44 18.587	.967	250 8 42.545	12270.7507
		1446 U+U 611	351 22 31.000	.170	-.234	351 22 32.023	.081	262 46 55.981	17150.4134
6785000	67A35	1426 SL 13	0.000	.170	-1.226	0 0 0.000	-.424	288 40 58.906	16238.6305
		6785001 67A24	20 20 39.000	.170	.269	20 20 40.496	.093	309 1 39.402	38772.2904
		1427	37 4 24.700	.170	.957	37 4 26.883	.331	325 45 25.789	32794.6946
107	GRAVITY 107	1464 HIW 3	0.000	.170	1.948	0 0 0.000	.673	280 17 24.398	9656.8704
		1493 HIW 12	43 41 21.200	.170	-1.571	43 41 17.681	-.543	323 58 42.079	7964.7154
		108 GRAVITY 108	187 19 52.000	.170	-.377	187 19 49.675	-.130	107 37 14.073	5514.7960
108	GRAVITY 108	107 GRAVITY 107	0.000	.170	-.284	0 0 0.000	-.098	287 42 37.712	5514.7960
		111 GRAVITY 111	175 26 35.500	.170	.267	175 26 36.051	.092	103 9 13.763	4817.2569
		1400 BC 13A	262 5 7.000	.170	-.386	262 5 6.898	-.133	189 47 44.610	6263.3697
		678756 HT MYE	285 55 50.000	.170	.404	285 55 50.688	.139	213 38 28.400	5436.7001
111	GRAVITY 111	108 GRAVITY 108	0.000	.170	-.623	0 0 0.000	-.215	283 14 2.473	4817.2569
		1437 BC 21	196 4 6.200	.170	2.281	196 4 9.104	.788	119 18 11.577	6011.7065
		678756 HT MYE	322 50 37.200	.170	-1.657	322 50 36.166	-.573	246 4 38.639	8431.8874
1401	VG 1	6785001 67A24	0.000	.170	-.611	0 0 0.000	-.211	91 10 29.630	13620.8740
		1442	13 25 20.500	.170	1.111	13 25 22.222	.384	104 35 51.852	6223.9496
		1448	30 49 25.300	.170	1.294	30 49 27.206	.447	121 59 56.835	5903.1927
		1439	63 50 38.300	.170	-2.652	63 50 36.259	-.916	155 1 5.889	4957.3500
		1472 IB 751	73 18 43.500	.170	-1.511	73 18 42.600	-.522	164 29 12.230	937.5207
		1471 DP 1	85 39 47.400	.170	-.832	85 39 47.180	-.287	176 50 16.809	725.5744
		1479 DY 1	124 1 2.700	.170	1.775	124 1 5.086	.613	215 11 34.716	685.9115
		1446 U+U 611	142 22 7.000	.170	-6.167	142 22 1.444	-2.131	233 32 31.074	4211.9566
		1488 HIW 11	144 45 1.000	.170	2.248	144 45 3.859	.777	235 55 33.489	1509.7135
		1406 VG 6	213 15 24.900	.170	1.048	213 15 26.559	.362	304 25 56.189	6245.4416

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR.	FOR. AZ.	DISTANCE
		1402 VG 2	221 27 58.800	.170	1.408	221 28 .819	-.486	312 38 30.448	1560.2323
		1453 HIW 10	279 9 52.500	.170	2.411	279 9 55.523	.833	10 20 25.152	1928.3206
		1445 HIW 16	282 10 21.200	.170	-3.749	282 10 18.062	-1.295	13 20 47.692	3811.7396
		1480 DC 13A	296 52 27.100	.170	.800	296 52 28.511	.276	28 2 58.141	7454.5323
1402	VG 2	1437 DC 21	327 46 8.600	.170	3.427	327 46 12.638	1.184	58 56 42.267	16932.3782
		1403 VG 3	0.000	.170	.365	0 0 0.000	-.126	278 35 42.029	752.7448
		1401 VG 1	214 1 38.800	.170	-.365	214 1 38.070	-.126	132 37 20.100	1560.2323
1403	VG 3	1404 VG 4	0.000	.170	-1.114	0 0 0.000	-.385	318 53 24.581	2157.6193
		1402 VG 2	139 41 30.500	.170	-.210	139 41 31.823	.072	98 34 56.405	752.7448
		1457 HIW 3KA	355 18 25.800	.170	.904	355 18 27.818	.312	314 11 52.399	525.0616
1405	VG 5	1406 VG 6	0.000	.170	-3.446	0 0 0.000	-1.191	290 42 26.112	768.9277
		1462 HIW 9	132 41 42.000	.170	.143	132 41 45.589	.049	63 24 11.701	1867.7920
		1404 VG 4	181 36 10.800	.170	.018	181 36 14.264	.006	112 18 40.376	1214.1228
		1461 HIW 1KA	292 29 44.300	.170	3.286	292 29 51.032	1.135	223 12 17.144	1519.2363
1406	VG 6	1407 VG 7	0.000	.170	-4.470	0 0 0.000	-1.545	351 32 44.445	1054.3671
		1405 VG 5	119 8 50.000	.170	3.067	119 8 57.537	1.060	110 41 41.983	768.9277
		1401 VG 1	132 47 48.000	.170	3.267	132 47 55.738	1.129	124 20 40.183	6245.4416
		1424 HIW 6KA	167 7 50.000	.170	-1.864	167 7 52.606	-.644	158 40 37.052	239.6029
1404	VG 4	1405 VG 5	0.000	.170	-5.268	0 0 0.000	-1.820	292 19 49.273	1214.1228
		1403 VG 3	206 32 9.000	.170	-5.970	206 32 8.298	-2.063	138 51 57.571	2157.6193
		1457 HIW 3KA	208 2 22.000	.170	.714	208 2 27.982	.247	140 22 17.255	1634.8819
		1458 IN 1	223 36 38.800	.170	-2.655	223 36 41.413	-.917	155 56 30.686	1515.1061
		1459 JK 3	234 34 43.800	.170	3.794	234 34 52.862	1.311	166 54 42.135	1498.3042
		1451 JK 2	236 1 47.000	.170	.332	236 1 52.600	.115	168 21 41.873	2108.5677
		1446 U+U 611	248 27 10.800	.170	5.670	248 27 21.737	1.959	180 47 11.010	5299.5892
		1422 HIW 4KA	354 48 10.000	.170	3.381	354 48 18.649	1.168	287 8 7.922	1475.0311
1407	VG 7	1406 VG 6	0.000	.170	5.370	0 0 0.000	1.855	171 32 34.931	1054.3671
		1420 HIW 7KA	37 57 52.600	.066	-4.474	37 57 42.756	-.963	209 30 17.687	660.4633
		1408 VG 8	72 9 11.000	.170	-3.633	72 9 1.998	-1.255	243 41 36.929	741.0592
1408	VG 8	1409 VG 9	0.000	.170	-1.031	0 0 0.000	-.356	304 12 42.940	1220.9461
		1412 VG 12	9 54 25.000	.170	-4.623	9 54 21.408	-1.598	314 7 4.348	10426.9882
		1407 VG 7	119 28 7.300	.170	4.887	119 28 13.219	1.689	63 40 56.159	741.0592
		1490 HIW 7KA	181 47 2.300	.170	.768	181 47 4.099	-.265	125 59 47.039	419.1124
1409	VG 9	1410 VG 10	0.000	.170	-.542	0 0 0.000	-.187	328 5 10.070	1337.7102
		1408 VG 8	156 6 27.300	.170	3.048	156 6 30.890	1.053	124 11 40.960	1220.9461
		1469 HIW 7	318 7 56.000	.170	-2.507	318 7 54.035	-.866	286 13 4.105	2177.6425
1410	VG 10	1411 VG 11	0.000	.170	-.228	0 0 0.000	-.079	271 17 19.798	741.3391
		1409 VG 9	236 47 7.300	.170	-.228	236 47 6.844	-.079	148 4 26.642	1337.7102
1411	VG 11	1412 VG 12	0.000	.170	-.323	0 0 0.000	-.112	325 10 13.335	1233.2950
		1410 VG 10	126 6 20.300	.170	.323	126 6 20.246	.112	91 16 34.281	741.3391
1412	VG 12	1413 VG 13A	0.000	.170	.307	0 0 0.000	-.106	312 28 41.675	889.9044
		1411 VG 11	192 40 49.000	.170	-.307	192 40 48.386	-.106	145 9 30.061	1233.2950

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR.	FOR. AZ.	DISTANCE	
1413	VG 13A	1414	VG 14	0.000	.170	-498	0 0 0.000	.172	294 57 39.539	564.2304
		1412	VG 12	197 30 22.800	.170	-498	197 30 21.804	-.172	132 28 1.343	889.9044
1414	VG 14	1415	VG 15A	0.000	.170	.380	0 0 0.000	.131	335 14 14.363	2057.3457
		1413	VG 13A	139 42 54.500	.170	-380	139 42 53.739	-.131	114 57 8.102	564.2304
1415	VG 15A	1417	WHI 1-71	0.000	.170	1.881	0 0 0.000	.650	309 3 40.432	1298.5637
		1414	VG 14	206 9 44.700	.170	-1.881	206 9 40.937	-.650	155 13 21.369	2057.3457
		1416	VG 16	285 8 2.300	.170	.000	285 8 .419	.000	234 11 40.851	234.5730
1417	WHI 1-71	1415	VG 15A	0.000	.170	-2.054	0 0 0.000	-.710	129 2 38.603	1298.5637
		1475	HIW 8	48 42 16.300	.170	-1.273	48 42 17.081	-.440	177 44 55.485	2530.6048
		1463	RC 2	139 46 43.300	.170	-2.897	139 46 42.458	-1.001	268 42 20.861	4858.7170
		1418	VG 18	151 52 33.800	.170	2.446	151 52 38.300	.845	280 55 16.703	1017.1486
		1483	VG 18	249 8 41.800	.170	3.778	249 8 47.633	1.306	18 11 26.036	2952.2589
1418	VG 18	1419	VG 19	0.000	.170	1.010	0 0 0.000	.349	336 40 25.977	742.5970
		1417	WHI 1-71	124 13 51.300	.170	-1.010	124 13 49.280	-.349	100 54 15.257	1017.1486
1419	VG 19	1420	WHI 3	0.000	.170	2.577	0 0 0.000	.890	284 21 43.312	2022.8054
		1421	RC 4	1 47 1.000	.170	-.401	1 46 58.022	-.139	286 8 41.334	2135.4359
		1408	VG 8	209 37 45.200	.170	-2.122	209 37 40.501	-.733	133 59 23.813	10426.9882
		1418	VG 18	232 18 27.200	.170	-.053	232 18 24.570	-.018	156 40 7.882	742.5970
1420	WHI 3	1419	VG 19	0.000	.170	-.551	0 0 0.000	-.190	104 19 42.697	2022.8054
		1463	RC 2	123 0 21.500	.170	-.398	123 0 21.652	-.138	227 20 4.349	2181.7579
		1470	RC 11	166 45 21.900	.170	-2.840	166 45 19.611	-.981	271 5 2.308	3915.7569
		1421	RC 4	210 45 51.900	.170	3.789	210 45 56.240	1.309	315 5 38.936	129.8744
1421	RC 4	1470	RC 11	0.000	.170	3.484	0 0 0.000	1.204	269 43 48.235	3823.4140
		1419	VG 19	196 22 49.800	.170	.524	196 22 46.840	.181	106 6 35.075	2135.4359
		1420	WHI 3	225 21 52.200	.170	-3.659	225 21 45.057	-1.264	135 5 33.293	129.8744
		1463	RC 2	314 11 31.200	.170	-.349	314 11 27.367	-.121	223 55 15.602	2180.5460
1422	HIW 4KA	1404	VG 4	0.000	.170	-1.453	0 0 0.000	-.502	107 6 41.451	1475.0311
		1423	HIW 5KA	95 2 .800	.170	-.607	95 2 1.646	-.210	202 8 43.097	674.8853
		1424	HIW 6KA	175 11 52.500	.170	2.060	175 11 56.014	.712	282 18 37.465	353.8466
1423	HIW 5KA	1422	HIW 4KA	0.000	.170	-2.158	0 0 0.000	-.746	22 8 27.493	674.8853
		1461	HIW 1KA	205 28 2.000	.170	-1.253	205 28 2.904	-.433	227 36 30.398	675.7515
		1424	HIW 6KA	330 25 37.700	.170	3.411	330 25 43.268	1.179	352 34 10.762	706.4679
1424	HIW 6KA	1422	HIW 4KA	0.000	.170	-1.114	0 0 0.000	-.385	102 18 16.255	353.8466
		1423	HIW 5KA	70 15 49.000	.170	-1.213	70 15 48.902	-.419	172 34 5.157	706.4679
		1406	VG 6	236 22 22.700	.170	2.327	236 22 26.141	.804	338 40 42.397	239.6029
1425		1428		0.000	.170	-.834	0 0 0.000	-.288	303 28 15.355	5970.0409
		6785001	67A24	52 2 46.000	.170	-.407	52 2 46.427	-.140	355 31 1.783	13889.5817
		1429		96 56 4.200	.170	1.240	96 56 6.274	.429	40 24 21.630	6436.8832
1426	SL 13	6785001	67A24	0.000	.170	1.786	0 0 0.000	.617	322 15 1.847	24213.9853
		1427		29 30 40.900	.170	-.181	29 30 38.933	-.062	351 45 40.780	22122.4355
		6785000	67A35	146 10 25.000	.170	-1.605	146 10 21.609	-.555	108 25 23.456	16238.6305
1427		6785000	67A35	0.000	.170	-4.564	0 0 0.000	-1.577	145 26 35.282	32794.6946

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR.	FOR. AZ.	DISTANCE
		1433	15 25 7.800	.170	-.720	15 25 11.643	-.249	160 51 46.925	3149.1836
		1426 SL 13	26 15 48.000	.170	-1.311	26 15 51.252	-.453	171 42 26.534	22122.4355
		1436	89 15 33.800	.170	1.909	89 15 40.272	.660	234 42 15.554	7450.6525
		6785001 67A24	111 13 56.000	.170	1.538	111 14 2.102	.532	256 40 37.384	11973.6101
		1434 HIW 17	130 47 7.600	.170	3.069	130 47 15.232	1.060	276 13 50.514	3827.8128
		1435	150 23 24.200	.170	-.593	150 23 28.171	-.205	295 50 3.453	9843.3460
		1437 BC 21	154 50 44.200	.170	.672	154 50 49.436	.232	300 17 24.718	12387.2981
1428		6785001 67A24	0.000	.170	-.518	0 0 0.000	-.179	20 10 6.624	11250.0811
		1430 SL 12	7 55 34.000	.170	-.792	7 55 33.726	-.274	28 5 40.350	4280.5532
		1425	103 13 2.200	.170	2.170	103 13 4.888	.750	123 23 11.513	5970.0409
		1440	288 0 39.800	.170	-.860	288 0 39.458	-.297	308 10 46.082	9586.5091
1429		6785001 67A24	0.000	.170	-1.614	0 0 0.000	-.558	329 37 29.318	10376.4265
		1431	66 51 38.300	.170	-.030	66 51 39.884	-.010	36 29 9.201	4966.7029
		1425	250 51 8.300	.170	-2.896	250 51 7.018	-1.001	220 28 36.336	6436.8832
		1430 SL 12	317 19 38.700	.170	4.540	317 19 44.854	1.569	286 57 14.171	7452.1927
1430	SL 12	1429	0.000	.170	-2.352	0 0 0.000	-.813	106 49 58.611	7452.1927
		1428	101 17 40.200	.170	2.352	101 17 44.903	.813	208 7 43.515	4280.5532
1431		6785001 67A24	0.000	.170	-2.070	0 0 0.000	-.715	301 12 43.969	9583.0312
		1433	102 5 2.300	.170	1.142	102 5 5.512	-.395	43 17 49.482	6544.4206
		1429	275 19 22.800	.170	.929	275 19 25.799	.321	216 32 9.769	4966.7029
1432	BC 17	1401 VG 1	0.000	.170	.100	0 0 0.000	.035	265 34 5.929	12899.3431
		1467 BC 16	6 21 39.300	.170	-3.295	6 21 35.905	-1.139	271 55 41.833	7168.7346
		1438	34 42 56.300	.170	-3.245	34 42 52.954	-1.121	300 16 58.883	6694.5782
		1466	50 1 4.000	.170	-1.856	50 1 2.043	-.641	315 35 7.972	4105.3077
		1465 BC 20	100 7 55.800	.170	3.153	100 7 58.853	1.089	5 42 4.782	3939.8547
		1437 BC 21	106 45 15.300	.170	-5.428	106 45 9.772	-1.876	12 19 15.700	7863.6222
		6785001 67A24	244 46 32.300	.170	10.572	244 46 42.772	3.653	150 20 48.701	1528.1876
1433		1436	0.000	.170	-1.929	0 0 0.000	-.667	259 25 43.682	7236.7016
		6785001 67A24	11 33 50.200	.170	-.998	11 33 51.131	-.345	270 59 34.813	12685.5870
		1427	81 27 3.700	.170	.868	81 27 6.497	.300	340 52 50.178	3149.1836
		1431	323 56 36.700	.170	2.059	323 56 40.688	.711	223 22 24.370	6544.4206
1434	HIW 17	1491 HIW 14	0.000	.170	3.008	0 0 0.000	1.039	294 16 55.920	16749.1409
		1437 BC 21	15 53 52.800	.170	-.119	15 53 49.673	-.041	310 10 45.594	9027.9339
		1427	161 53 8.000	.170	-3.805	161 53 1.188	-1.315	96 9 57.108	3827.8128
		1445 HIW 16	338 11 8.500	.170	.916	338 11 6.409	.317	272 28 2.329	20574.0555
1435		1437 BC 21	0.000	.170	4.190	0 0 0.000	1.448	316 41 15.985	2684.9196
		1427	158 59 51.700	.170	-4.190	158 59 43.319	-1.448	115 40 59.304	9843.3460
1436		1427	0.000	.170	-1.616	0 0 0.000	-.558	54 36 3.144	7450.6525
		1433	24 42 21.700	.170	1.616	24 42 24.931	.558	79 18 28.075	7236.7016
1437	BC 21	1427	0.000	.170	-.548	0 0 0.000	-.189	120 6 27.330	12387.2981
		1434 HIW 17	9 57 14.500	.170	-.717	9 57 14.331	-.248	130 3 41.660	9027.9339
		1435	16 33 .300	.170	-5.408	16 32 55.440	-1.869	136 39 22.769	2684.9196

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		6785001	67A24	65 45 47.300	.170	-0.635	65 45 47.213	-0.219	185 52 14.543	9057.5955
		1432	BC 17	72 14 28.500	.170	2.447	72 14 31.495	.845	192 20 58.824	7863.6222
		1465	BC 20	78 48 5.600	.170	-1.687	78 48 4.461	-.583	198 54 31.791	3976.0592
		1439		103 18 56.300	.170	1.773	103 18 58.621	.612	223 25 25.950	18139.5217
		1468	BC 7	108 44 49.100	.170	-2.415	108 44 47.233	-.835	228 51 14.562	14620.4167
		1443	BC 5	111 11 17.800	.170	-3.199	111 11 15.150	-1.105	231 17 42.479	17152.5507
		1401	VG 1	119 5 2.300	.170	3.509	119 5 6.357	1.212	239 11 33.686	16932.3782
		1438		119 55 5.500	.170	7.453	119 55 13.501	2.575	240 1 40.830	8613.0589
		1445	HIW 16	129 53 35.200	.170	-0.781	129 53 34.967	-.270	250 0 2.296	14522.9908
		1480	BC 13A	139 3 2.000	.170	3.989	139 3 6.537	1.378	259 9 33.867	11209.3929
		111	GRAVITY 111	179 17 9.800	.170	-3.778	179 17 6.570	-1.306	299 23 33.899	6011.7065
1438		1437	BC 21	0.000	.170	-3.453	0 0 0.000	-1.193	59 54 2.816	8613.0589
		1466		38 40 13.800	.170	0.870	38 40 18.122	.300	98 34 20.938	2941.6184
		1432	BC 17	60 16 56.300	.170	1.551	60 17 1.303	.536	120 11 4.119	6694.5782
		6785001	67A24	65 44 15.300	.170	-0.559	65 44 18.193	-.193	125 38 21.009	8053.6448
		1439		149 24 49.200	.170	1.591	149 24 54.744	.550	209 18 57.060	10187.3947
1439		1401	VG 1	0.000	.170	-2.017	0 0 0.000	-.697	335 3 13.976	4957.3500
		1473	IB 756	2 20 24.200	.170	4.084	2 20 30.302	1.411	337 23 44.278	4797.5145
		1443	BC 5	4 12 51.600	.170	.383	4 12 54.000	.132	339 16 7.976	2614.7702
		1474	DP 2	5 10 36.700	.170	1.643	5 10 40.360	.568	340 13 54.336	3951.3350
		1445	HIW 16	16 33 48.700	.170	1.655	16 33 52.373	.572	351 37 6.349	8291.6573
		1468	BC 7	47 3 12.300	.170	-2.426	47 3 11.822	-.838	22 6 25.860	3842.4539
		1438		54 10 38.600	.170	-2.753	54 10 37.865	-.951	29 13 51.841	10187.3947
		1467	BC 16	57 0 1.000	.170	-.271	57 0 2.746	-.094	32 3 16.723	6785.5331
		1437	BC 21	68 9 26.600	.170	-.236	68 9 28.853	.082	43 12 42.830	18139.5217
		1442		78 19 3.500	.170	2.403	78 19 7.920	.830	53 22 21.897	4898.5094
		6785001	67A24	94 53 39.100	.170	1.364	94 53 42.481	.471	69 56 56.458	12270.7507
		14401	1440 ECC	230 48 40.800	.170	-.134	230 48 42.684	-.046	205 51 56.660	77.8869
		1446	U+U 611	314 56 27.500	.170	-.163	314 56 29.354	-.056	289 59 43.331	5831.5635
		1449	BC 3	337 33 5.500	.170	-1.928	337 33 5.589	-.666	312 36 19.565	2846.4165
		1496		349 43 54.000	.170	-5.419	349 43 50.599	-1.872	324 47 4.575	3895.6886
		1499		350 0 41.300	.170	-4.896	350 0 38.422	-1.692	325 3 52.398	4265.8224
		1471	DP 1	356 23 46.700	.170	2.867	356 23 51.584	.991	331 27 5.561	4292.2379
		1472	IB 751	357 48 27.900	.170	5.371	357 48 35.289	1.856	332 51 49.265	4035.5498
1440		6785001	67A24	0.000	.170	-3.428	0 0 0.000	-1.184	67 46 25.314	12319.5699
		1441		46 35 8.700	.170	-2.200	46 35 9.927	-.760	114 21 35.241	3980.1567
		1428		60 16 34.300	.170	2.283	60 16 40.010	.789	128 3 5.324	9586.5091
		1446	U+U 611	225 49 24.000	.170	1.110	225 49 28.537	.383	293 35 53.851	6114.2293
		1404	VG 4	256 44 43.600	.170	-.393	256 44 47.421	-.136	324 31 12.735	9512.9932
		14401	1440 ECC	269 57 32.800	.170	.436	269 57 36.664	.151	337 44 1.978	414.1915
		1480	BC 13A	298 38 28.800	.170	1.406	298 38 33.634	.486	6 24 58.947	11597.5959
14401	1440 ECC	1440		0.000	.170	-.202	0 0 0.000	-.070	157 43 52.378	414.1915

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR.	FOR. AZ.	DISTANCE	
		1439	228 8 1.800	.170	.202	228 8 2.203	.070	25 51 54.582	77.8869	
1441		1440	0.000	.170	1.172	0 0 0.000	.405	294 25 16.865	3980.1567	
		6785001	67A24	116 37 40.000	.170	-1.172	116 37 37.656	-.405	51 2 54.521	10010.7490
1442		1401	VG 1	0.000	.170	2.322	0 0 0.000	.802	284 42 .703	6223.9496
		1445	HIW 16	31 8 31.500	.170	-3.020	31 8 28.159	-1.043	315 50 26.862	7369.0525
		1444	SL 7	244 6 29.000	.170	-0.000	244 6 26.678	-.000	168 48 27.381	2514.3470
		1448		288 30 22.000	.170	3.694	288 30 23.373	1.077	213 12 24.076	1861.7043
		1439		308 44 22.500	.170	1.719	308 44 21.897	.594	233 26 22.600	4898.5094
		1472	IB 751	351 58 40.000	.170	-1.658	351 58 36.020	-.573	276 40 36.724	5810.4941
		1471	DP 1	353 26 2.000	.170	.079	353 25 59.757	.027	278 8 .460	6042.2718
		1479	DY 1	354 19 47.500	.170	-2.780	354 19 42.398	-.961	279 1 43.102	6497.0330
		1473	IB 756	359 59 14.900	.170	-.356	359 59 12.222	-.123	284 41 12.925	5968.4729
1443	BC 5	1439		0.000	.170	-.161	0 0 0.000	-.056	159 15 11.313	2614.7702
		1449	BC 3	86 48 57.200	.170	1.547	86 48 58.908	.535	246 4 10.221	1279.3008
		1437	BC 21	251 48 52.500	.170	-1.386	251 48 51.275	-.479	51 4 2.588	17152.5507
1445	HIW 16	1401	VG 1	0.000	.170	.638	0 0 0.000	.220	193 21 41.674	3011.2396
		1479	DY 1	3 17 1.500	.170	1.296	3 17 2.158	.448	196 38 43.832	4455.7088
		1446	U+U 611	21 8 36.300	.170	-.161	21 8 35.823	.056	214 30 17.496	7536.3729
		1462	HIW 9	82 40 15.900	.170	-2.039	82 40 13.223	-.704	276 1 54.897	3661.1461
		1480	BC 13A	209 6 10.000	.170	5.616	209 6 14.978	1.941	42 27 56.652	3889.8361
		1437	BC 21	236 24 19.300	.170	4.407	236 24 23.069	1.523	69 46 4.743	14522.9908
		1434	HIW 17	258 45 23.000	.170	-2.907	258 45 19.455	-1.004	92 7 1.129	20574.0555
		6785001	67A24	274 2 11.100	.170	5.693	274 2 16.155	1.967	107 23 57.829	13347.8114
		1442		302 23 35.700	.170	-4.803	302 23 30.259	-1.660	135 45 11.933	7369.0525
		1439		338 14 11.300	.170	-.122	338 14 10.540	-.042	171 35 52.214	8291.6573
		1472	IB 751	354 25 16.900	.170	.484	354 25 16.746	.167	187 46 58.420	4654.8701
		1473	IB 756	356 10 28.200	.170	-1.558	356 10 26.003	-.539	189 32 7.677	3827.2304
		1471	DP 1	357 22 53.300	.170	-1.090	357 22 51.572	-.377	190 44 33.246	4512.1168
		1497		359 25 9.300	.170	-5.776	359 25 2.886	-1.996	192 46 44.560	5067.8434
1446	U+U 611	1401	VG 1	0.000	.170	.450	0 0 0.000	.155	53 29 3.679	4211.9566
		1479	DY 1	3 28 4.800	.170	7.883	3 28 12.233	2.724	56 57 15.912	3567.4599
		1499		10 5 43.100	.170	-8.924	10 5 33.726	-3.084	63 34 37.405	3388.7652
		1497		14 30 3.800	.170	.829	14 30 4.180	.287	67 59 7.859	3394.0640
		6785001	67A24	29 0 32.500	.170	-1.383	29 0 30.667	-.478	82 29 34.357	17150.4134
		1439		56 25 5.300	.170	-.629	56 25 4.221	-.217	109 54 7.900	5831.5635
		1440		60 1 9.000	.170	-1.324	60 1 7.226	-.458	113 30 10.905	6114.2293
		1461	HIW 1KA	282 19 16.200	.170	-5.126	282 19 10.624	-1.771	335 48 14.303	5101.4765
		1404	VG 4	307 18 5.000	.170	-1.673	307 18 2.878	-.578	0 47 6.557	5299.5892
		1459	JK 3	312 38 17.600	.170	4.116	312 38 21.267	1.422	6 7 24.946	3861.7521
		1445	HIW 16	340 56 51.800	.170	1.064	340 56 52.415	.368	34 25 56.094	7536.3729
		1480	BC 13A	343 39 18.000	.170	4.716	343 39 22.266	1.630	37 8 25.946	11401.4570
1447		1470	RC 11	0.000	.170	.644	0 0 0.000	.222	199 41 8.342	8178.0546

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FOR. AZ.	DISTANCE	
		1482	HIW 1	47 46 11.700	.170	-6.85	47 46 10.371	-.237	247 27 18.713	2594.1143
		1464	HIW 3	280 3 34.700	.170	.248	280 3 34.304	.086	119 44 42.646	7308.1426
		1481	HIW 2	302 21 38.200	.170	-.207	302 21 37.350	-.071	142 2 45.691	5002.3383
1448		1401	VG 1	0.000	.170	3.191	0 0 0.000	1.103	302 5 3.256	5903.1927
		1442		91 6 24.800	.170	-3.191	91 6 18.417	-1.103	33 11 21.673	1861.7043
1449	BC 3	1443	BC 5	0.000	.170	-4.194	0 0 0.000	-1.449	66 2 58.642	1279.3008
		1439		66 31 4.300	.170	4.194	66 31 12.689	1.449	132 34 11.331	2846.4165
1450	HIW 6	1489	HIW 5	0.000	.170	-.256	0 0 0.000	-.089	358 52 28.893	3772.2124
		1462	HIW 9	137 23 55.300	.170	-2.986	137 23 52.570	-1.032	136 16 21.463	5110.7665
		1469	HIW 7	232 6 36.000	.066	.270	232 6 36.526	.058	230 59 5.420	3573.5466
		1483		319 52 47.200	.170	1.910	319 52 49.366	.660	318 45 18.259	7500.1912
		1464	HIW 3	335 57 34.800	.170	1.229	335 57 36.285	.425	334 50 5.178	9225.8451
1451	JK 2	1457	HIW 3KA	0.000	.170	-.614	0 0 0.000	-.212	37 27 24.993	1015.3044
		1454	JK 4	303 41 7.100	.170	-3.711	303 41 4.003	-1.282	341 8 28.996	1109.6770
		1404	VG 4	310 54 40.000	.170	2.339	310 54 42.953	.808	348 22 7.946	2108.5677
		1459	JK 3	314 27 52.000	.170	-2.129	314 27 50.485	-.735	351 55 15.478	611.9189
		1458	IN 1	338 18 4.000	.170	1.459	338 18 6.072	.504	15 45 31.066	708.3226
1452	HIW 2KA	1456	IN 2	339 2 15.300	.170	2.655	339 2 18.569	.917	16 29 43.562	449.6261
		1454	JK 4	0.000	.170	.135	0 0 0.000	.047	8 42 9.760	313.3538
		1460	IN 4	78 34 48.700	.001	-22.992	78 34 25.572	-.609	87 16 35.333	160.2041
1453	HIW 10	1462	HIW 9	0.000	.170	1.358	0 0 0.000	.469	305 15 3.890	3804.6193
		1401	VG 1	245 5 45.200	.170	-1.358	245 5 42.484	-.469	190 20 46.374	1928.3206
1454	JK 4	1457	HIW 3KA	0.000	.170	-2.864	0 0 0.000	-.990	104 2 10.294	1006.2272
		1459	JK 3	44 24 57.500	.170	-1.831	44 24 58.532	-.633	148 27 8.826	521.2750
		1460	IN 4	55 31 15.500	.170	5.639	55 31 24.003	1.949	159 33 34.297	322.4374
		1451	JK 2	57 5 56.500	.170	-2.653	57 5 56.711	-.917	161 8 7.004	1109.6770
		1452	HIW 2KA	84 39 57.800	.170	1.710	84 40 2.374	.591	188 42 12.667	313.3538
1455	IN 3	1404	VG 4	0.000	.170	-1.109	0 0 0.000	-.383	340 54 51.265	2076.5898
		1457	HIW 3KA	46 25 26.600	.170	1.109	46 25 28.818	.383	27 20 20.084	791.4514
1456	IN 2	1451	JK 2	0.000	.170	-.851	0 0 0.000	-.294	196 29 51.388	449.6261
		1458	IN 1	177 58 57.200	.170	.851	177 58 58.903	.294	14 28 50.291	258.7983
1457	HIW 3KA	1404	VG 4	0.000	.170	3.063	0 0 0.000	1.058	320 23 21.187	1634.8819
		14571	JK1	160 14 3.500	.170	-.000	160 14 .437	-.000	120 37 21.624	72.3710
		1403	VG 3	173 48 10.300	.170	.896	173 48 8.133	.310	134 11 29.321	525.0616
		1455	IN 3	246 57 27.200	.170	-2.957	246 57 21.180	-1.022	207 20 42.367	791.4514
		1451	JK 2	257 4 44.300	.170	.424	257 4 41.661	.147	217 28 2.848	1015.3044
		1452	HIW 2KA	305 57 20.800	.170	-.144	305 57 17.593	-.050	266 20 38.780	1025.7075
		1454	JK 4	323 39 53.300	.170	-1.282	323 39 48.955	-.443	284 3 10.143	1006.2272
1458	IN 1	1451	JK 2	0.000	.170	-1.062	0 0 0.000	-.367	195 45 42.859	708.3226
		1454	JK 4	108 0 20.800	.170	.189	108 0 22.050	.065	303 46 4.909	662.8627
		1404	VG 4	140 11 25.000	.170	-.366	140 11 25.695	-.127	335 57 8.554	1515.1061
		1455	IN 3	338 9 29.700	.170	1.102	338 9 31.864	.381	173 55 14.722	582.0956

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FOR. AZ.	DISTANCE		
1459	JK 3	1456	IN 2	358 43	10.200	.170	.138	358 43 11.399	.048	194 28 54.258	258.7983
		1451	JK 2		0.000	.170	4.889	0 0 0.000	1.689	171 55 10.207	611.9189
		1446	U+U 611	14 12	49.200	.170	-4.321	14 12 39.989	-1.493	186 7 50.196	3861.7521
		1460	IN 4	139 40	20.500	.170	.584	139 40 16.195	.202	311 35 26.401	214.0864
1460	IN 4	1454	JK 4	156 32	23.500	.170	-3.271	156 32 15.340	-1.130	328 27 25.546	521.2750
		1404	VG 4	174 59	55.500	.170	2.119	174 59 52.730	.732	346 55 2.937	1498.3042
		1459	JK 3		0.000	.170	2.742	0 0 0.000	.948	131 35 16.585	214.0864
		1452	HIW 2KA	135 41	29.700	.170	1.600	135 41 28.558	.553	267 16 45.143	160.2041
1461	HIW IKA	1454	JK 4	207 58	31.700	.170	-4.343	207 58 24.615	-1.501	339 33 41.200	322.4374
		1405	VG 5		0.000	.170	-.694	0 0 0.000	-.240	43 11 13.361	1519.2363
		1423	HIW 5KA	4 24	46.300	.170	-.563	4 24 46.431	-.194	47 35 59.792	675.7515
		1452	HIW 2KA	64 3	29.500	.170	6.456	64 3 36.650	2.231	107 14 50.011	2285.8880
1462	HIW 9	1488	HIW 11	82 5	35.300	.170	-2.822	82 5 33.172	-.975	125 16 46.533	5179.4504
		1446	U+U 611	112 34	49.500	.170	2.554	112 34 52.748	.883	155 46 6.109	5101.4765
		1469	HIW 7	270 5	43.400	.170	-4.931	270 5 39.164	-1.704	313 16 52.524	4944.1140
		1450	HIW 6		0.000	.170	3.694	0 0 0.000	1.276	316 19 58.291	5110.7665
1463	RC 2	1445	HIW 16	139 38	20.500	.170	-3.629	139 38 13.176	-1.254	95 58 11.467	3661.1461
		1453	HIW 10	168 51	57.300	.170	1.342	168 51 54.947	.464	125 11 53.239	3804.6193
		1405	VG 5	287 6	1.000	.170	-1.406	287 5 55.900	-.486	243 25 54.191	1867.7920
		1475	HIW 8		0.000	.170	7.867	0 0 0.000	2.718	116 1 12.778	5520.1355
1464	HIW 3	1477		16 5	49.800	.170	6.087	16 5 48.020	2.103	132 7 .799	3962.3542
		1470	RC 11	187 51	12.300	.170	-.510	187 51 3.923	-.176	303 52 16.701	2783.9638
		1484		234 20	34.500	.170	3.881	234 20 30.514	1.341	350 21 43.292	3196.3811
		1481	HIW 2	277 31	42.500	.170	-2.737	277 31 31.896	-.946	33 32 44.675	6368.8370
1465	BC 20	1420	WH1 3	291 17	20.800	.170	-.061	291 17 12.872	-.021	47 18 25.650	2181.7579
		1464	HIW 3	294 19	26.600	.170	2.430	294 19 21.163	.840	50 20 33.942	8817.0556
		1485	TR1 18	295 21	25.500	.170	-5.392	295 21 12.242	-1.863	51 22 25.020	5219.2256
		1483		307 13	.300	.170	-3.316	307 12 49.117	-1.146	63 14 1.895	6468.1575
1466	BC 20	1487	PR1 4	307 23	44.000	.170	-5.210	307 23 30.923	-1.800	63 24 43.701	5921.2339
		1486	PR1 6	313 6	29.500	.170	-.351	313 6 21.282	-.121	69 7 34.060	5144.0013
		1417	WH1 1-71	332 43	19.800	.170	-2.687	332 43 9.246	-.928	88 44 22.025	4858.7170
		1481	HIW 2		0.000	.170	.895	0 0 0.000	.309	264 32 36.982	3284.1252
1466	BC 20	1482	HIW 1	22 19	4.300	.170	2.022	22 19 5.427	.699	286 51 42.409	9128.5526
		1447		35 18	36.700	.170	1.099	35 18 36.904	.380	299 51 13.885	7308.1426
		1494	HIW 4	213 50	18.300	.170	-.255	213 50 17.150	-.088	118 22 54.132	3759.3881
		1489	HIW 5	235 20	15.200	.170	.814	235 20 15.119	.281	139 52 52.101	5981.5888
1465	BC 20	1450	HIW 6	250 13	32.200	.170	-4.884	250 13 26.421	-1.688	154 46 3.403	9225.8451
		1463	RC 2	325 54	57.200	.170	-.961	325 54 55.344	-.332	230 27 32.326	8817.0556
		1470	RC 11	341 26	47.000	.170	1.269	341 26 47.374	.439	245 59 24.356	9970.4842
		1437	BC 21		0.000	.170	2.338	0 0 0.000	.808	18 53 12.681	3976.0592
1466	BC 20	1432	BC 17	166 49	20.800	.170	-2.338	166 49 16.124	-.808	185 42 28.805	3939.8547
		1432	BC 17		0.000	.170	1.976	0 0 0.000	-.683	135 32 11.688	4105.3077

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FUR. AZ.	DISTANCE
		1438	143 5 11.700	.170	-1.976	143 5 7.748	-.683	278 37 19.436	2941.6184
1467	BC 16	1432	0.000	.170	-.653	0 0 0.000	-.226	91 48 22.629	7168.7346
		1439	120 18 33.500	.170	.653	120 18 34.806	.226	212 6 57.435	6785.5331
1458	BC 7	1437	0.000	.170	-1.595	0 0 0.000	-.551	48 39 59.939	14620.4167
		1439	153 27 51.300	.170	1.595	153 27 54.489	.551	202 7 54.428	3842.4539
1469	HIW 7	1450	0.000	.170	-2.606	0 0 0.000	-.901	50 56 14.918	3573.5466
		1409	55 14 33.600	.170	4.594	55 14 40.801	1.588	106 10 55.718	2177.6425
		1461	82 16 52.300	.170	1.728	82 16 56.634	.597	133 13 11.552	4944.1140
		1475	259 27 40.900	.170	-3.716	259 27 39.790	-1.284	310 23 54.707	3941.7042
1470	RC 11	678567	0.000	.210	-.490	0 0 0.000	-.188	190 47 57.509	4976.4909
		1482	172 13 4.300	.210	.059	172 13 4.848	.022	3 1 2.357	6715.0916
		1447	188 50 20.500	.170	.217	188 50 21.207	.075	19 38 18.715	8178.0546
		1484	217 9 32.000	.170	-7.799	217 9 24.691	-2.695	47 57 22.200	2390.4850
		1481	226 22 12.500	.170	-.492	226 22 12.498	-.170	57 10 10.007	6936.2123
		1483	249 36 17.800	.170	.576	249 36 18.866	.199	80 24 16.374	8200.3979
		1421	258 51 53.000	.170	1.892	258 51 55.382	.654	89 39 52.890	3823.4140
		1420	260 13 .800	.170	2.522	260 13 3.812	.871	91 1 1.320	3915.7569
		1463	293 1 53.500	.210	2.929	293 1 56.919	1.125	123 49 54.428	2783.9638
1471	DP 1	1445	0.000	.170	-2.681	0 0 0.000	-.928	10 43 41.718	4512.1168
		1473	6 42 18.800	.170	-.611	6 42 20.870	-.211	17 26 2.587	690.4593
		1474	83 23 12.800	.170	.960	83 23 16.440	.332	94 6 58.158	716.7425
		1442	87 18 8.500	.170	1.173	87 18 12.353	.405	98 1 54.071	6042.2718
		1439	140 41 17.500	.170	-1.970	140 41 18.210	-.681	151 24 59.928	4292.2379
		1500	311 40 40.500	.170	-.433	311 40 42.747	-.150	322 24 24.465	254.9824
		1401	346 6 31.300	.170	3.563	346 6 37.543	1.231	356 50 19.261	725.5744
1472	IB 751	1445	0.000	.170	.506	0 0 0.000	.175	7 46 19.802	4654.8701
		1474	68 2 41.100	.170	-.348	68 2 40.246	-.120	75 49 .047	520.0274
		1442	88 48 25.800	.170	-1.851	88 48 23.443	-.640	96 34 43.245	5810.4941
		1439	145 3 36.000	.170	1.243	145 3 36.737	.430	152 49 56.539	4035.5498
		1401	336 43 7.600	.170	.693	336 43 7.788	.240	344 29 27.589	937.5207
		1473	351 58 3.500	.170	-.243	351 58 2.751	-.084	359 44 22.553	837.6484
1473	IB 756	1445	0.000	.170	1.263	0 0 0.000	.436	9 31 28.825	3827.2304
		1442	95 3 52.300	.170	-.661	95 3 50.376	-.229	104 35 19.200	5968.4729
		1439	147 50 26.300	.170	-2.547	147 50 22.490	-.880	157 21 51.315	4797.5145
		1472	170 12 52.700	.170	2.058	170 12 53.495	.711	179 44 22.320	837.6484
		1471	187 54 49.200	.170	-1.500	187 54 46.437	-.518	197 28 15.262	690.4593
		1500	208 54 46.000	.170	1.388	208 54 46.125	.480	218 26 14.950	583.0312
1474	DP 2	1439	0.000	.170	-.968	0 0 0.000	-.334	160 12 32.488	3951.3350
		1472	95 36 57.300	.170	.175	95 36 58.442	.060	255 49 30.930	520.0274
		1471	113 55 7.700	.170	-.793	113 55 9.461	.274	274 7 41.949	716.7425
1475	HIW 8	1469	0.000	.170	6.184	0 0 0.000	2.137	130 20 50.231	3941.7042
		1477	133 5 18.700	.170	-1.978	133 5 10.538	-.683	263 26 .769	2035.1196

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ.DIRECTION	ST.CORRN	FUR. AZ.	DISTANCE
		1463 RC 2	165 45 36.000	.170	-2.353	165 45 27.463	-.813	296 6 17.694	5520.1355
1476	PE 1	1417 WHI 1-71	227 24 19.400	.170	-1.853	227 24 11.364	-.640	357 45 1.595	2530.6048
		1478 PE 2	0.000	.170	-.000	0 0 0.000	-.000	168 53 47.283	2741.9500
		1477	172 52 27.200	.170	-.000	172 52 27.200	.000	341 46 14.483	2518.5410
1477		1463 RC 2	0.000	.170	-1.321	0 0 0.000	-.456	312 10 1.449	3962.3542
		1483	74 51 55.000	.170	-3.929	74 51 52.392	-1.358	27 1 53.840	6250.6266
		1475 HIW 8	131 13 48.500	.170	5.250	131 13 55.070	1.814	83 23 56.519	2035.1196
1479	DY 1	1476 PE 1	209 35 23.300	.170	.000	209 35 24.621	.000	161 45 26.069	2518.5410
		1445 HIW 16	0.000	.170	-3.809	0 0 0.000	-1.316	16 37 25.630	4455.7088
		1401 VG 1	18 33 40.000	.170	1.059	18 33 44.868	.366	35 17 10.499	685.9115
		1442	82 17 41.000	.170	-.397	82 17 44.413	-.137	98 55 10.043	6497.0330
1480	BC 13A	1446 U+U 611	220 22 46.500	.170	3.147	220 22 53.457	1.088	237 0 19.087	3567.4599
		678567 67A55	0.000	.170	2.982	0 0 0.000	1.030	271 38 48.766	23789.5072
		678756 MT MYE	38 33 6.300	.170	14.256	38 33 17.574	4.926	310 12 6.339	2548.8864

		1491 HIW 14	128 4 2.500	.170	1.445	128 4 .963	-.499	39 42 49.729	4111.5202
		1437 BC 21	167 19 38.300	.170	-6.537	167 19 28.781	-2.259	78 58 17.547	11209.3929
		6785001 67A24	212 33 31.500	.210	-2.053	212 33 26.465	-.789	124 12 15.230	12218.8618
		678566 67A25	259 35 38.500	.170	-.213	259 35 35.731	-.073	171 14 24.496	110.6047
		1440	274 47 32.600	.170	-.138	274 47 29.756	.048	186 26 18.522	11597.5959
		1401 VG 1	296 27 45.300	.170	2.320	296 27 44.638	.802	208 6 33.404	7454.5323
		1446 U+U 611	305 36 41.800	.170	1.053	305 36 39.871	.364	217 15 28.637	11401.4570
		1445 HIW 16	310 52 5.500	.170	-13.333	310 51 49.185	-4.607	222 30 37.951	3889.8361

1481	HIW 2	1482 HIW 1	0.000	.170	-2.602	0 0 0.000	-.899	298 22 41.952	6216.8218
		1447	23 43 9.700	.170	1.115	23 43 13.417	.385	322 5 55.369	5002.3383
		1493 HIW 12	119 34 36.800	.170	-4.559	119 34 34.842	-1.575	57 57 16.795	9518.8738
		1464 HIW 3	146 6 31.600	.170	-.698	146 6 33.503	-.241	84 29 15.455	3284.1252
		1494 HIW 4	164 12 11.100	.170	1.388	164 12 15.090	.480	102 34 57.042	6740.0673
		1483	198 23 58.000	.170	-2.106	198 23 58.496	-.728	136 46 40.448	3290.0990
		1487 PR1 4	207 56 9.500	.170	-.875	207 56 12.977	.303	146 18 54.929	3196.4541
		1486 PR1 6	221 21 34.400	.170	3.166	221 21 40.168	1.094	159 44 22.120	3705.8455
1482	HIW 1	1463 RC 2	275 13 33.600	.170	3.420	275 13 39.622	1.182	213 36 21.574	6368.8370
		1447	0.000	.170	.687	0 0 0.000	.237	67 24 50.854	2594.1143
		1464 HIW 3	39 17 59.000	.170	-5.818	39 17 52.495	-2.010	106 42 43.348	9128.5526
		678756 MT MYE	49 37 57.200	.170	.663	49 37 57.176	.229	117 2 48.029	23060.8617
		1481 HIW 2	50 52 14.700	.170	-.420	50 52 13.593	-.145	118 17 4.446	6216.8218
		1463 RC 2	99 14 32.000	.170	1.691	99 14 33.004	.584	166 39 23.858	8485.0373
1483		1470 RC 11	115 36 30.800	.170	3.198	115 36 33.310	1.105	183 1 24.164	6715.0916
		1463 RC 2	0.000	.170	.578	0 0 0.000	.200	243 19 57.519	6468.1575
		1485 TR1 18	38 15 21.800	.170	3.692	38 15 24.914	1.276	281 35 22.433	1732.3990
		1481 HIW 2	73 29 5.000	.170	-2.716	73 29 1.706	-.939	316 48 59.225	3290.0990
		1450 HIW 6	255 20 11.000	.170	5.863	255 20 16.285	2.026	138 40 13.804	7500.1912
		1417 WHI 1-71	314 52 24.200	.170	1.648	314 52 25.270	.569	198 12 22.789	2952.2509

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FOR. AZ.	DISTANCE
		1477	323 44 53.500	.170	-1.687	323 44 51.235	-.583	207 4 48.754	6250.6266
		1486	338 39 24.000	.170	-3.887	338 39 19.535	-1.343	221 59 17.054	1450.8498
		1487	358 4 18.600	.170	-3.491	358 4 14.531	-1.206	241 24 12.050	547.2624
1484		1463	RC 2 0.000	.170	.551	0 0 0.000	.190	170 21 10.336	3196.3811
		1470	RC 11 57 38 2.300	.170	-.551	57 38 1.197	-.190	227 59 11.533	2390.4850
1485	TRI 18	1463	RC 2 0.000	.266	-.492	0 0 0.000	-.213	231 26 36.133	5219.2256
		1483	230 7 1.800	.170	-.520	230 7 1.772	-.180	101 33 37.905	1732.3990
		1487	PR1 4 245 9 22.600	.266	-.198	245 9 22.894	-.085	116 35 59.027	1360.9311
		1486	PR1 6 281 32 13.200	.266	1.022	281 32 14.714	.442	152 58 50.847	1600.7819
1486	PR1 6	1463	RC 2 0.000	.266	-1.822	0 0 0.000	-.788	249 12 29.923	5144.0013
		1485	TRI 18 83 47 5.200	.266	-1.328	83 47 5.694	-.574	332 59 35.618	1600.7819
		1481	HIW 2 90 33 10.200	.170	-.813	90 33 11.209	-.281	339 45 41.132	3705.8455
		1487	PR1 4 141 44 56.100	.266	.950	141 44 58.872	.411	30 57 28.795	952.2461
		1483	152 45 41.300	.170	4.256	152 45 47.379	1.471	41 58 17.302	1450.8498
1487	PR1 4	1463	RC 2 0.000	.266	1.913	0 0 0.000	.827	243 30 9.735	5921.2339
		1485	TRI 18 53 7 5.900	.266	.243	53 7 4.229	.105	296 37 13.964	1360.9311
		1481	HIW 2 82 50 38.000	.170	-1.710	82 50 34.377	-.591	326 20 44.112	3196.4541
		1483	177 53 33.700	.170	.939	177 53 32.725	.324	61 23 42.460	547.2624
		1486	PR1 6 327 27 52.800	.266	-1.663	327 27 49.224	-.719	210 57 58.959	952.2461
1488	HIW 11	1401	VG 1 0.000	.170	-1.934	0 0 0.000	-.668	55 54 16.888	1509.7135
		1461	HIW 1KA 249 26 44.800	.170	-1.934	249 26 48.667	.668	305 21 5.555	5179.4504
1489	HIW 5	1464	HIW 3 0.000	.170	.109	0 0 0.000	-.038	319 56 49.354	5981.5888
		1450	HIW 6 218 55 35.200	.170	-.109	218 55 34.981	-.038	178 52 24.335	3772.2124
1490	HIW 7KA	1408	VG 8 0.000	.066	.811	0 0 0.000	.175	306 0 7.848	419.1124
		1407	VG 7 83 29 51.500	.066	-.811	83 29 49.878	-.175	29 29 57.726	660.4633
1491	HIW 14	1495	HIW 15 0.000	.170	1.354	0 0 0.000	.468	25 45 11.038	3423.7929
		1434	HIW 17 88 16 10.500	.170	-2.943	88 16 6.203	-1.017	114 1 17.241	16749.1409
		1480	BC 13A 194 0 20.000	.170	1.508	194 0 20.234	.549	219 45 31.272	4111.5202
1492	HIW 13	1493	HIW 12 0.000	.170	2.517	0 0 0.000	.870	298 54 13.744	9361.6481
		678756	MT MYE 250 0 22.500	.170	-2.517	250 0 17.467	-.870	188 54 31.211	8223.7394
1493	HIW 12	1481	HIW 2 0.000	.170	1.065	0 0 0.000	.368	238 5 35.007	9518.8738
		1492	HIW 13 240 40 14.800	.170	-1.065	240 40 12.670	-.368	118 45 47.677	9361.6481
1494	HIW 4	1481	HIW 2 0.000	.170	1.059	0 0 0.000	.366	282 41 42.334	6740.0673
		1464	HIW 3 15 44 37.700	.170	-1.059	15 44 35.581	-.366	298 26 17.915	3759.3881
1495	HIW 15	678756	MT MYE 0.000	.170	1.797	0 0 0.000	.621	232 51 1.217	7608.8198
		1491	HIW 14 332 55 45.000	.170	-1.797	332 55 41.406	-.621	205 46 42.622	3423.7929
678566	67A25	678567	67A55 0.000	.170	-.475	0 0 0.000	-.164	271 54 32.211	23809.7348
		6785001	67A24 211 54 50.500	.170	-1.691	211 54 49.285	-.584	123 49 21.496	12143.7500
		1401	VG 1 296 42 57.800	.170	2.166	296 43 .442	.749	208 37 32.653	7366.3465
678567	67A55	1480	BC 13A 0.000	.170	2.129	0 0 0.000	.736	91 14 27.766	23789.5072
		1470	RC 11 279 32 36.700	.170	-2.129	279 32 32.442	-.736	10 47 .208	4976.4909
1496		1499	0.000	.170	.160	0 0 0.000	.055	327 58 11.549	370.6694

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OCCUPIED STA.	TO	OBSERVED STA.	DIRECTION	WEIGHT	CORR.	ADJ. DIRECTION	ST. CORR	FOR. AZ.	DISTANCE
		1498	341 29 33.700	.170	-2.447	341 29 31.094	-.845	309 27 42.642	249.1004
1497		1497	344 43 22.500	.170	2.287	344 43 24.628	.790	312 41 36.176	115.6062
		1439	0.000	.170	-2.360	0 0 0.000	-.815	144 23 59.709	4008.8189
		1446 U+U 611	103 38 18.800	.170	-.309	103 38 20.850	-.107	248 2 20.559	3394.0640
		1498	162 16 7.500	.170	.356	162 16 10.216	.123	306 40 9.925	133.8368
		1499	190 16 19.300	.170	-1.915	190 16 19.745	-.662	334 40 19.454	260.9320
		1445 HIW 16	228 21 26.700	.170	7.125	228 21 36.184	2.462	12 45 35.894	5067.8434
1498		1496	348 17 31.800	.170	-2.896	348 17 31.263	-1.001	132 41 30.972	115.6062
		1499	0.000	.170	-3.324	0 0 0.000	-1.148	358 25 37.522	155.9814
		1497	128 14 22.500	.170	.005	128 14 25.828	.002	126 40 3.350	133.8368
1499		1496	131 1 46.700	.170	3.319	131 1 53.342	1.147	129 27 30.864	249.1004
		1439	0.000	.170	-1.633	0 0 0.000	-.564	145 1 22.797	4265.8224
		1496	2 56 35.200	.170	-.123	2 56 36.711	-.042	147 57 59.508	370.6694
		1497	9 38 48.300	.170	-.114	9 38 49.820	-.039	154 40 12.617	260.9320
		1498	33 24 9.300	.170	3.529	33 24 14.462	1.219	178 25 37.259	155.9814
		1446 U+U 611	98 36 20.500	.170	-1.660	98 36 20.474	-.573	243 37 43.271	3388.7652
1500	DV 2	1471 DP 1	0.000	.170	.595	0 0 0.000	-.206	142 24 14.936	254.9824
		1473 IB 756	256 1 39.000	.170	-.595	256 1 37.810	-.206	38 25 52.746	583.0312
678756	MT MYE	1495 HIW 15	0.000	.170	1.139	0 0 0.000	.394	52 44 48.384	7608.8198
		1491 HIW 14	18 52 2.000	.170	-6.194	18 51 54.667	-2.140	71 38 43.050	4819.0169
		1480 BC 13A	77 25 31.200	.170	-11.755	77 25 18.306	-4.062	130 10 6.690	2548.8864
		1482 HIW 1	244 38 51.800	.170	11.947	244 39 2.608	4.128	297 23 50.991	23060.8617
		1492 HIW 13	316 8 20.800	.170	4.863	316 8 24.524	1.680	8 53 12.908	8223.7394
1464	HIW 3	1493 HIW 12	0.000	.170	1.472	0 0 0.000	.509	45 26 34.414	6742.1879
		107 GRAVITY 107	54 41 7.200	.170	-1.472	54 41 4.256	-.509	100 7 38.671	9656.8704

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OCCUPIED STA.	TO	OBSERVED STA.	DISTANCE	HEIGHT	CORR.	PPM	ADJ. DISTANCE	ST. CORR	FOR. AZIMUTH	BACK AZIM
1401	VG 1	1402	VG 2	1560.2280	.176	-.0043	2.7	1560.2323	.198	312 38 30.448 132 37 20.
1402	VG 2	1403	VG 3	752.7450	.128	-.0002	.3	752.7448	-.019	278 35 42.029 98 34 56.
1403	VG 3	1404	VG 4	2157.5780	.568	.0413	19.2	2157.6193	2.496	318 53 24.581 138 51 57.
1404	VG 4	1405	VG 5	1214.1270	.161	-.0042	3.5	1214.1228	-.241	292 19 49.273 112 18 40.
1405	VG 5	1406	VG 6	768.9520	.129	-.0243	31.6	768.9277	-1.960	290 42 26.112 110 41 41.
1406	VG 6	1407	VG 7	1054.3630	.152	-.0041	3.9	1054.3671	.262	351 32 44.445 171 32 34.
1407	VG 7	1408	VG 8	741.0500	.127	-.0092	12.4	741.0592	.765	243 41 36.929 63 40 56.
1408	VG 8	1490	HIW 7KA	419.1180	.073	-.0056	13.4	419.1124	-.626	125 59 47.039 306 0 7.
1407	VG 7	1490	HIW 7KA	660.4700	.120	-.0067	10.2	660.4633	-.610	209 30 17.687 29 29 57.
1408	VG 8	1409	VG 9	1220.9510	.161	-.0049	4.0	1220.9461	-.276	304 12 42.940 124 11 40.
1409	VG 9	1410	VG 10	1337.6990	.167	.0112	8.4	1337.7102	.590	328 5 10.070 148 4 26.
1410	VG 10	1411	VG 11	741.3340	.104	-.0051	6.9	741.3391	.385	271 17 19.798 91 16 34.
1411	VG 11	1412	VG 12	1233.2850	.162	.0100	8.1	1233.2950	.564	325 10 13.335 145 9 30.
1412	VG 12	1413	VG 13A	889.8980	.140	-.0064	7.2	889.9044	.465	312 28 41.675 132 28 1.
1413	VG 13A	1414	VG 14	564.2270	.107	.0034	6.0	564.2304	.338	294 57 39.539 114 57 8.
1414	VG 14	1415	VG 15A	2057.3240	.190	-.0217	10.6	2057.3457	.795	335 14 14.363 155 13 21.
1415	VG 15A	1417	WHI 1-71	1298.5520	.165	-.0117	9.0	1298.5637	.630	309 3 40.432 129 2 38.
1417	WHI 1-71	1418	VG 18	1017.1520	.149	-.0034	3.4	1017.1486	-.224	280 55 16.703 100 54 15.
1418	VG 18	1419	VG 19	742.5940	.127	-.0030	4.0	742.5970	.247	336 40 25.977 156 40 7.
1419	VG 19	1421	RC 4	2135.4350	.560	-.0009	.4	2135.4359	.052	286 8 41.334 106 6 35.
1401	VG 1	1406	VG 6	6245.4080	.114	.0336	5.4	6245.4416	.314	304 25 56.189 124 20 40.
1408	VG 8	1419	VG 19	10426.7720	.151	-.2162	20.7	10426.9882	1.393	314 7 4.348 133 59 23.
1401	VG 1	1480	BC 13A	7454.5440	.128	-.0117	1.8	7454.5323	-.097	28 2 58.141 208 6 33.
1480	BC 13A	1491	HIW 14	4111.5470	.084	-.0268	6.5	4111.5202	-.327	39 42 49.729 219 45 31.
1480	BC 13A	678566	67A25	110.6040	.018	-.0007	6.8	110.6047	.152	171 14 24.496 351 14 25.
678567	67A55	1470	RC 11	4976.6790	.097	-.1881	37.8	4976.4909	-2.035	10 47 .208 190 47 57.
1470	RC 11	1482	HIW 1	6715.0300	.119	-.0616	9.2	6715.0916	.547	3 1 2.357 183 1 24.
1482	HIW 1	1481	HIW 2	6216.6910	.114	-.1308	21.0	6216.8218	1.228	118 17 4.446 298 22 41.
1481	HIW 2	1484	HIW 3	3283.9840	.068	-.1412	43.0	3284.1252	1.938	84 29 15.455 264 32 36.
1464	HIW 3	1494	HIW 4	3759.4030	.077	-.0149	4.0	3759.3881	-.190	118 22 54.132 298 26 17.
1464	HIW 3	1489	HIW 5	5981.4970	.111	-.0918	15.3	5981.5888	.884	139 52 52.101 319 56 49.
1489	HIW 5	1450	HIW 6	3772.1560	.076	-.0564	15.0	3772.2124	.713	178 52 24.335 358 52 28.
1450	HIW 6	1469	HIW 7	3573.4630	.074	-.0836	23.4	3573.5466	1.099	230 59 5.420 50 56 14.
1469	HIW 7	1475	HIW 8	3941.7520	.081	-.0478	12.1	3941.7042	-.597	310 23 54.707 130 20 50.
1475	HIW 8	1463	RC 2	5520.0160	.105	-.1195	21.6	5520.1355	1.212	296 6 17.694 116 1 12.
1470	RC 11	1420	WHI 3	3915.7400	.081	-.0169	4.3	3915.7569	.212	91 1 1.320 271 5 2.
1469	HIW 7	1409	VG 9	2177.6920	.193	-.0495	22.7	2177.6425	-1.725	106 10 55.718 286 13 4.
1450	HIW 6	1462	HIW 9	5111.2090	.099	-.4425	86.8	5110.7665	-4.709	136 16 21.463 316 19 58.
1462	HIW 9	1453	HIW 10	3804.6610	.078	-.0417	11.0	3804.6193	-.530	125 11 53.239 305 15 3.
1453	HIW 10	1401	VG 1	1928.2780	.038	-.0426	22.1	1928.3206	.745	190 20 46.374 10 20 25.
1401	VG 1	1488	HIW 11	1509.6960	.028	-.0175	11.8	1509.7135	.336	235 55 33.489 55 54 16.
1488	HIW 11	1461	HIW 1KA	5179.3870	.100	-.0634	12.2	5179.4504	.669	305 21 5.555 125 16 46.

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OCCUPIED STA.	TO	OBSERVED STA.	DISTANCE	WEIGHT	CORR. PPM	ADJ. DISTANCE	ST. CORR	FOR. AZIMUTH	BACK AZIM
1461	HIW 1KA	1469	HIW 7	4944.0630	.097	.0510	10.3	4944.1140	.555 313 16 52.524 133 13 11.
1481	HIW 2	1493	HIW 12	9518.9290	.145	-.0552	5.8	9518.8738	-.381 57 57 16.795 238 5 35.
1493	HIW 12	1492	HIW 13	9361.7730	.143	-.1249	13.3	9361.6481	-.872 118 45 47.677 298 54 13.
1492	HIW 13	678756	MT MYE	8223.7140	.134	.0254	3.1	8223.7394	.196 188 54 31.211 8 53 12.
678756	MT MYE	1495	HIW 15	7608.9940	.129	-.1742	22.9	7608.8198	-1.421 52 44 48.384 232 51 1.
1495	HIW 15	1491	HIW 14	3423.7120	.071	.0809	23.6	3423.7929	1.089 205 46 42.622 25 45 11.
1491	HIW 14	1434	HIW 17	16749.2540	.180	-.1131	6.8	16749.1409	-.495 114 1 17.241 294 16 55.
1434	HIW 17	1445	HIW 16	20574.1890	.190	-.1335	6.5	20574.0555	-.489 272 28 2.329 92 7 1.
1445	HIW 16	1401	VG 1	3811.7760	.079	-.0364	9.6	3811.7396	-.464 193 21 41.674 13 20 47.
1421	RC 4	1420	WHI 3	129.8740	.023	.0004	3.3	129.8744	.086 135 5 33.293 315 5 38.
1401	VG 1	6785001	67A24	13620.8500	.168	.0240	1.8	13620.8740	.125 91 10 29.630 271 24 23.
6785001	67A24	1480	BC 13A	12218.9610	.161	-.0992	8.1	12218.8618	-.563 304 22 34.525 124 12 15.
678566	67A25	6785001	67A24	12143.7580	.161	-.0080	.7	12143.7500	-.046 123 49 21.496 303 59 39.
1432	BC 17	6785001	67A24	1528.1940	.175	-.0064	4.2	1528.1876	-.305 150 20 48.701 330 21 35.
1415	VG 15A	1416	VG 16	234.5730	.048	-.0000	.0	234.5730	-.000 234 11 40.851 54 11 29.
1480	BC 13A	678567	67A55	23789.5490	.197	-.0418	1.8	23789.5072	-.135 271 38 48.766 91 14 27.
1461	HIW 1KA	1452	HIW 2KA	2285.9270	.047	-.0390	17.0	2285.8880	-.639 107 14 50.011 287 17 3.
1452	HIW 2KA	1457	HIW 3KA	1025.6980	.150	.0095	9.2	1025.7075	.618 86 19 36.025 266 20 38.
1404	VG 4	1422	HIW 4KA	1475.0340	.173	-.0029	2.0	1475.0311	-.141 287 8 7.922 107 6 41.
1422	HIW 4KA	1423	HIW 5KA	674.8830	.120	.0023	3.4	674.8853	.202 202 8 43.097 22 8 27.
1423	HIW 5KA	1461	HIW 1KA	675.7460	.120	.0055	8.2	675.7515	.491 227 36 30.398 47 35 59.
1461	HIW 1KA	1405	VG 5	1519.2210	.174	.0153	10.1	1519.2363	.725 43 11 13.361 223 12 17.
1422	HIW 4KA	1424	HIW 6KA	353.8420	.073	.0046	13.0	353.8466	.606 282 18 37.465 102 18 16.
1424	HIW 6KA	1423	HIW 5KA	706.4660	.123	.0019	2.6	706.4679	.161 172 34 5.157 352 34 10.
1422	HIW 4KA	1404	VG 4	1475.0340	.173	-.0029	2.0	1475.0311	-.141 107 6 41.451 287 8 7.
6785001	67A24	1425		13889.6200	.169	-.0383	2.8	13889.5817	-.196 175 29 55.310 355 31 1.
6785001	67A24	1426	SL 13	24214.1020	.198	-.1167	4.8	24213.9853	-.371 141 59 54.357 322 15 1.
6785001	67A24	1427		11973.6680	.160	-.0579	4.8	11973.6101	-.334 76 28 43.474 256 40 37.
6785001	67A24	1431		9582.8800	.145	-.1512	15.8	9583.0312	1.039 121 4 21.944 301 12 43.
6785001	67A24	1439		12270.8150	.161	-.0643	5.2	12270.7507	-.363 250 8 42.545 69 56 56.
6785001	67A24	1446	U+U 611	17150.4120	.181	.0014	.1	17150.4134	.006 262 46 55.981 82 29 34.
6785000	67A35	1426	SL 13	16238.5250	.178	.1055	6.5	16238.6305	.474 288 40 58.906 108 25 23.
6785000	67A35	1427		32794.8950	.210	-.2004	6.1	32794.6946	-.484 325 45 25.789 145 26 35.
6785000	67A35	6785001	67A24	38772.2310	.250	.0594	1.5	38772.2904	.132 309 1 39.402 128 30 55.
1401	VG 1	1442		6223.7170	.114	.2326	37.4	6223.9496	2.181 104 35 51.852 284 42 .
1401	VG 1	1448		5903.1260	.110	.0667	11.3	5903.1927	.648 121 59 56.835 302 5 3.
1401	VG 1	1471	DP 1	725.5680	.100	.0064	8.8	725.5744	.481 176 50 16.809 356 50 19.
1401	VG 1	1472	ID 751	937.5170	.156	.0037	3.9	937.5207	.266 164 29 12.230 344 29 27.
1401	VG 1	1479	DY 1	685.9170	.091	-.0055	8.0	685.9185	-.417 215 11 34.716 35 11 10.
1406	VG 6	1424	HIW 6KA	239.5890	.013	.0139	58.0	239.6029	1.144 158 40 37.052 338 40 42.
1417	WHI 1-71	1463	RC 2	4858.6550	1.518	.0620	12.8	4858.7170	2.717 268 49 20.861 88 44 22.
1417	WHI 1-71	1483		2952.2620	.861	-.0031	1.1	2952.2589	-.170 18 11 26.036 198 12 22.

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OCCUPIED STA.	TO	OBSERVED STA.	DISTANCE	WEIGHT	CORR.	PPM	ADJ. DISTANCE	ST. CORR	FOR.	AZIMUTH	BACK AZIM
1426	SL 13	1427	22122.4610	.194	-.0255	1.2	22122.4355	-.088	351	45 40.780	171 42 26.
1428		6785001	11249.9340	.156	-.1471	13.1	11250.0811	.893	20	10 6.624	200 14 4.
1428		1425	5970.0450	1.851	-.0041	.7	5970.0409	-.162	123	23 11.513	303 28 15.
1428		1430	4280.5930	.086	-.0398	9.3	4280.5532	-.471	28	5 40.350	208 7 43.
1429		1425	6436.8870	1.980	-.0038	.6	6436.8832	-.145	220	28 36.336	40 24 21.
1429		1430	7452.0800	.127	-.1127	15.1	7452.1927	.932	286	57 14.171	106 49 58.
1429		1431	4966.7060	1.552	-.0031	.6	4966.7029	-.134	36	29 9.201	216 32 9.
1433		1427	3149.1890	.933	-.0054	1.7	3149.1836	-.285	340	52 50.178	160 51 46.
1433		1431	6544.4640	.118	-.0434	6.6	6544.4206	-.394	223	22 24.370	43 17 49.
1434	HIW 17	1427	3827.8140	1.175	-.0012	.3	3827.8128	-.056	96	9 57.108	276 13 50.
1435		1437	2684.9210	.763	-.0014	.5	2684.9196	-.076	316	41 15.985	136 39 22.
1436		1427	7450.6590	.127	-.0065	.9	7450.6525	-.054	54	36 3.144	234 42 15.
1437	BC 21	1427	12387.4420	.162	-.1439	11.6	12387.2981	-.808	120	6 27.330	300 17 24.
1437	BC 21	1432	7863.5070	.131	-.1152	14.6	7863.6222	.916	192	20 58.824	12 19 15.
1437	BC 21	1439	18139.3900	.184	.1317	7.3	18139.5217	.538	223	25 25.950	43 12 42.
1437	BC 21	1443	17152.5190	.181	.0317	1.8	17152.5507	.136	231	17 42.479	51 4 2.
1437	BC 21	1468	14620.3500	.172	-.0667	4.6	14620.4167	.327	228	51 14.562	48 39 59.
1438		1432	6694.5970	.119	-.0188	2.8	6694.5782	-.167	120	11 4.119	300 16 58.
1438		1437	8612.8750	.138	.1839	21.3	8613.0589	1.371	59	54 2.816	240 1 40.
1438		1439	10187.2010	.149	-.1937	19.0	10187.3947	1.269	209	18 57.060	29 13 51.
1439		14401	77.8870	.001	-.0001	1.4	77.8869	-.008	205	51 56.660	25 51 54.
1439		1442	4898.3320	.096	.1774	36.2	4898.5094	1.940	53	22 21.897	233 26 22.
1439		1443	2614.7840	.737	-.0138	5.3	2614.7702	-.782	339	16 7.976	159 15 11.
1439		1449	2846.4010	.822	.0155	5.5	2846.4165	.854	312	36 19.565	132 34 11.
1440		6785001	12319.4100	.048	-.1599	13.0	12319.5699	.492	67	46 25.314	247 58 3.
1440		1428	9586.3870	.145	-.1221	12.7	9586.5091	.838	128	3 5.324	308 10 46.
1440		14401	414.1940	.037	-.0025	6.1	414.1915	-.204	337	44 1.978	157 43 52.
1440		1441	3980.1550	1.228	-.0017	.4	3980.1567	.080	114	21 35.241	294 25 16.
1441		6785001	10010.5810	.148	-.1680	16.8	10010.7490	1.116	51	2 54.521	231 10 51.
1442		1439	4898.5170	1.530	-.0076	1.6	4898.5094	-.332	233	26 22.600	53 22 21.
1442		1444	2514.3470	.700	-.0000	.0	2514.3470	-.000	168	48 27.381	348 48 57.
1442		1448	1861.7090	.460	-.0047	2.5	1861.7043	-.295	213	12 24.076	33 11 21.
1443	BC 5	1449	1279.3010	.259	-.0002	.1	1279.3008	-.011	246	4 10.221	66 2 58.
1445	HIW 16	1401	3811.7640	1.169	-.0244	6.4	3811.7396	-1.198	193	21 41.674	13 20 47.
1446	U+U 611	1401	4211.9970	1.306	-.0404	9.6	4211.9566	-1.893	53	29 3.679	233 32 31.
1446	U+U 611	1404	5299.6290	1.655	-.0398	7.5	5299.5892	-1.672	0	47 6.557	180 47 11.
1446	U+U 611	1439	5831.5760	1.811	-.0125	2.1	5831.5635	-.497	109	54 7.900	289 59 43.
1446	U+U 611	1440	6114.2050	1.891	-.0243	4.0	6114.2293	.943	113	30 10.905	293 35 53.
1446	U+U 611	1461	5101.4530	1.594	-.0235	4.6	5101.4765	1.007	335	48 14.303	155 46 6.
1447		1470	8178.0710	2.407	-.0164	2.0	8178.0546	-.538	199	41 8.342	19 38 18.
1447		1481	5002.3350	1.563	-.0033	.7	5002.3383	-.142	142	2 45.691	322 5 55.
1447		1482	2594.1120	.729	-.0023	.9	2594.1143	-.132	247	27 18.713	67 24 50.

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1450	HIW 6	1483	7500.2300	2.250	-.0388	5.2	7500.1912	-1.342	318 45	18.259	138 40 13.
1459	JR 3	1446	3861.5100	.078	.2421	62.7	3861.7521	3.027	186 7	50.196	6 7 24.
1463	RC 2	1484	3196.4100	.950	-.0289	9.0	3196.3811	-1.522	350 21	43.292	170 21 10.
1463	RC 2	1470	2783.9510	.799	.0128	4.6	2783.9638	.709	303 52	16.701	123 49 54.
1464	HIW 3	1447	7308.0540	.126	.0886	12.1	7308.1426	.744	299 51	13.885	119 44 42.
1464	HIW 3	1450	9225.8030	.142	.0421	4.6	9225.8451	.297	154 46	3.403	334 50 5.
1464	HIW 3	1482	9128.5780	.142	-.0254	2.8	9128.5526	-.181	286 51	42.409	106 42 43.
1465	BC 20	1437	3976.0570	1.226	.0022	.6	3976.0592	.107	18 53	12.681	198 54 31.
1465	BC 20	1432	3939.8530	1.214	.0017	.4	3939.8547	.084	185 42	28.805	5 42 4.
1466		1438	2941.6230	.857	-.0046	1.6	2941.6184	-.249	278 37	19.436	98 34 20.
1466		1432	4105.3150	1.270	-.0073	1.8	4105.3077	-.345	135 32	11.688	315 35 7.
1467	BC 16	1432	7168.7270	2.166	.0076	1.1	7168.7346	.269	91 48	22.629	271 55 41.
1467	BC 16	1439	6785.3210	.120	.2121	31.3	6785.5331	1.872	212 6	57.435	32 3 16.
1468	BC 7	1439	3842.4520	1.180	.0019	.5	3842.4539	.091	202 7	54.428	22 6 25.
1469	HIW 7	1461	4944.0900	1.545	.0240	4.8	4944.1140	1.041	133 13	11.552	313 16 52.
1470	RC 11	1484	2390.4300	.049	.0550	23.0	2390.4850	.881	47 57	22.200	227 59 11.
1470	RC 11	1482	6715.0740	.119	.0176	2.6	6715.0916	.156	3 1	2.357	183 1 24.
1471	DP 1	1445	4512.1230	1.406	-.0062	1.4	4512.1168	-.282	10 43	41.718	190 44 33.
1471	DP 1	1439	4292.2450	1.333	-.0071	1.7	4292.2379	-.330	151 24	59.928	331 27 5.
1471	DP 1	1474	716.7450	.098	-.0025	3.5	716.7425	-.190	94 6	58.158	274 7 41.
1471	DP 1	1473	690.4570	.092	.0023	3.4	690.4593	.176	17 26	2.587	197 26 15.
1472	IB 751	1474	520.0220	.055	.0054	10.3	520.0274	.419	75 49	.047	255 49 30.
1472	IB 751	1442	5810.5200	1.805	-.0259	4.5	5810.4941	-1.035	96 34	43.245	276 40 36.
1472	IB 751	1439	4035.5350	1.247	.0148	3.7	4035.5498	.710	152 49	56.539	332 51 49.
1472	IB 751	1445	4654.8790	1.453	-.0089	1.9	4654.8701	-.399	7 46	19.802	187 46 58.
1472	IB 751	1473	837.6450	.129	.0034	4.0	837.6484	.248	359 44	22.553	179 44 22.
1473	IB 756	1439	4797.5000	1.498	.0145	3.0	4797.5145	.641	157 21	51.315	337 23 44.
1473	IB 756	1442	5968.4710	1.850	.0019	.3	5968.4729	.075	104 35	19.200	284 41 12.
1473	IB 756	1445	3827.2030	1.175	.0274	7.2	3827.2304	1.340	9 31	28.825	189 32 7.
1474	DP 2	1439	3951.3160	1.218	.0190	4.8	3951.3350	.917	160 12	32.488	340 13 54.
1475	HIW 8	1417	2530.6170	.706	-.0122	4.8	2530.6048	-.698	357 45	1.595	177 44 55.
1475	HIW 8	1477	2035.1220	.523	-.0024	1.2	2035.1196	-.147	263 26	.769	83 23 56.
1477		1476	2518.5410	.701	.0000	.0	2518.5410	.000	161 45	26.069	341 46 14.
1477		1483	6250.5190	.114	.1076	17.2	6250.6266	1.005	27 1	53.840	207 4 48.
1478	PE 2	1476	2741.9500	.784	-.0000	.0	2741.9500	-.000	348 54	19.675	168 53 47.
1479	DY 1	1446	3567.4700	.074	-.0101	2.8	3567.4599	-.133	237 0	19.087	56 57 15.
1479	DY 1	1445	4455.7080	1.388	.0008	.2	4455.7088	.038	16 37	25.630	196 38 43.
1479	DY 1	1442	6497.0430	1.996	-.0100	1.5	6497.0330	-.376	98 55	10.043	279 1 43.
1480	BC 13A	1445	3889.8490	1.196	-.0129	3.3	3889.8361	-.625	222 30	37.951	42 27 56.
1481	HIW 2	1463	6368.7500	.116	.0870	13.7	6368.8370	.804	213 36	21.574	33 32 44.
1481	HIW 2	1464	3284.1310	.982	-.0058	1.8	3284.1252	-.302	84 29	15.455	264 32 36.
1481	HIW 2	1482	6216.8040	.114	.0178	2.9	6216.8218	.167	298 22	41.952	118 17 4.

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1481	HIW 2	1483		3290.0970	.984	-.0020	.6	3290.0990	.106	136 46	40.448	316 48 59.
1485	TR1 18	1463	RC 2	5219.2440	1.630	-.0184	3.5	5219.2256	-.777	231 26	36.133	51 22 25.
1485	TR1 18	1483		1732.3940	.414	.0050	2.9	1732.3990	.322	101 33	37.905	281 35 22.
1486	PR1 6	1463	RC 2	5144.0160	1.607	-.0147	2.9	5144.0013	-.625	249 12	29.923	69 7 34.
1486	PR1 6	1481	HIW 2	3705.8330	1.132	.0125	3.4	3705.8455	.621	339 45	41.132	159 44 22.
1486	PR1 6	1483		1450.8620	.316	-.0122	8.4	1450.8498	-.820	41 58	17.302	221 59 17.
1487	PR1 4	1463	RC 2	5921.2430	1.837	-.0091	1.5	5921.2339	-.358	243 30	9.735	63 24 43.
1487	PR1 4	1481	HIW 2	3196.4610	.950	-.0069	2.1	3196.4541	-.362	326 20	44.112	146 18 54.
1487	PR1 4	1483		547.2670	.061	-.0046	8.3	547.2624	-.355	61 23	42.460	241 24 12.
1457	HIW 3KA	1403	VG 3	525.0750	.101	-.0134	25.0	525.0616	-1.407	134 11	29.321	314 11 52.
1485	TR1 18	1487	PR1 4	1360.9370	.286	-.0059	4.3	1360.9311	-.402	116 35	59.027	296 37 13.
1486	PR1 6	1487	PR1 4	952.2430	.160	.0031	3.3	952.2461	.225	30 57	28.795	210 57 58.
1485	TR1 18	1486	PR1 6	1600.7820	.367	-.0001	.1	1600.7819	-.009	152 58	50.847	332 59 35.
1485	TR1 18	1487	PR1 4	1360.9370	.286	-.0059	4.3	1360.9311	-.402	116 35	59.027	296 37 13.
1485	TR1 18	1486	PR1 6	1600.7880	.367	-.0061	3.8	1600.7819	-.401	152 58	50.847	332 59 35.
1486	PR1 6	1487	PR1 4	952.2430	.160	.0031	3.3	952.2461	.225	30 57	28.795	210 57 58.
1404	VG 4	1451	JK 2	2108.5820	.550	-.0143	6.8	2108.5677	-.869	168 21	41.873	348 22 7.
1460	IN 4	1454	JK 4	322.4270	.023	.0104	32.3	322.4374	.847	339 33	41.200	159 33 34.
1460	IN 4	1452	HIW 2KA	160.2250	.006	-.0209	130.1	160.2041	-1.743	267 16	45.143	87 16 35.
1459	JK 3	1460	IN 4	214.0770	.011	.0094	43.9	214.0864	.797	311 35	26.401	131 35 16.
1459	JK 3	1404	VG 4	1498.3050	.332	-.0008	.4	1498.3042	-.056	346 55	2.937	166 54 42.
1459	JK 3	1454	JK 4	521.2730	.056	.0020	3.9	521.2750	.158	328 27	25.546	148 27 8.
1459	JK 3	1451	JK 2	611.8880	.074	-.0309	50.4	611.9189	2.371	171 55	10.207	351 55 15.
1458	IN 1	1451	JK 2	708.3230	.123	-.0004	.5	708.3226	-.032	195 45	42.859	15 45 31.
1458	IN 1	1454	JK 4	662.8860	.118	-.0233	35.1	662.8627	-2.086	303 46	4.909	123 45 31.
1458	IN 1	1404	VG 4	1515.1030	.174	.0031	2.0	1515.1061	.145	335 57	8.554	155 56 30.
1458	IN 1	1455	IN 3	582.0910	.109	-.0046	7.9	582.0956	.450	173 55	14.722	353 55 18.
1458	IN 1	1456	IN 2	258.8040	.053	-.0057	22.1	258.7983	-.878	194 28	54.258	14 28 50.
1457	HIW 3KA	1404	VG 4	1634.8760	.178	.0059	3.6	1634.8819	.263	320 23	21.187	140 22 17.
1457	HIW 3KA	1452	HIW 2KA	1025.7330	.150	-.0255	24.9	1025.7075	-1.666	266 20	38.780	86 19 36.
1456	IN 2	1451	JK 2	449.6360	.090	-.0099	22.0	449.6261	-1.141	196 29	51.388	16 29 43.
1455	IN 3	1404	VG 4	2076.6440	.191	-.0542	26.1	2076.5898	-1.972	340 54	51.265	160 54 9.
1455	IN 3	1457	HIW 3KA	791.4520	.131	-.0006	.7	791.4514	-.045	27 20	20.084	207 20 42.
1451	JK 2	1454	JK 4	1109.6520	.155	.0250	22.4	1109.6770	1.535	341 8	28.996	161 8 7.
1451	JK 2	1457	HIW 3KA	1015.3150	.149	-.0106	10.4	1015.3044	-.695	37 27	24.993	217 28 2.
1452	HIW 2KA	1454	JK 4	313.3440	.065	-.0098	31.2	313.3538	1.377	8 42	9.760	188 42 12.
1435	VG 5	1462	HIW 9	1867.8230	.462	-.0310	16.6	1867.7920	-1.952	63 24	11.701	243 25 54.
1457	HIW 3KA	14571	JK1	72.3710	.001	-.0000	.0	72.3710	.000	120 37	21.624	300 37 25.
1475	HIW 8	1463	RC 2	5520.1620	1.721	-.0265	4.8	5520.1355	-1.091	296 6	17.694	116 1 12.
1480	BC 13A	1437	BC 21	11209.6110	.156	-.2181	19.5	11209.3929	-1.329	78 58	17.547	259 9 33.
1480	BC 13A	1440		11597.6020	.158	-.0061	.5	11597.5959	-.036	186 26	18.522	6 24 58.
1482	HIW 1	678756	HT MYE	23061.1300	.196	-.2683	11.6	23060.8617	-.890	117 2	48.029	297 23 50.

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THE STANDARDISED CORRECTIONS HAVE BEEN SCALED BY THE CALCULATED SECOND MOMENT. FACTOR = .8643
 VALUES GREATER THAN THE VALUE OF TAU (4.3001) WILL BE MARKED

OCCUPIED STA.	TO	OBSERVED STA.	DISTANCE	WEIGHT	CORR.	PPH	ADJ. DISTANCE	ST. CORR	FOR. AZIMUTH	BACK AZIM
1496		1498	249.0740	.014	.0264	106.0	249.1004	2.169	309 27 42.642	129 27 30.
1497		1439	4008.8310	1.237	-.0121	3.0	4008.8189	-.582	144 23 59.709	324 26 22.
1497		1445	HIW 16	1.583	-.0056	1.1	5067.8434	-.240	12 45 35.894	192 46 44.
1497		1446	U+U 611	1.022	-.0200	5.9	3394.0640	-1.028	248 2 20.559	67 59 7.
1497		1496		.003	-.0358	309.8	115.6062	-2.934	132 41 30.972	312 41 36.
1497		1498		.004	-.0132	98.5	133.8368	-1.077	306 40 9.925	126 40 3.
1499		1439		1.324	-.0226	5.3	4265.8224	-1.053	145 1 22.797	325 3 52.
1499		1446	U+U 611	1.020	.0472	13.9	3388.7652	2.431	243 37 43.271	63 34 37.
1499		1496		.030	.0104	28.0	370.6694	.840	147 57 59.508	327 58 11.
1499		1497		.015	-.0370	141.7	260.9320	-3.000	154 40 12.617	334 40 19.
1499		1498		.006	-.0244	156.3	155.9814	2.092	178 25 37.259	358 25 37.
1500	DY 2	1473	IB 756	.001	.0882	151.3	583.0312	.827	38 25 52.746	218 26 14.
678756	MT MYE	1480	BC 13A	.712	-.0054	2.1	2548.8864	-.309	130 10 6.690	310 12 6.
1437	BC 21	111	GRAVITY 111	.111	-.0085	1.4	6011.7065	-.081	299 23 33.899	119 18 11.
111	GRAVITY 111	108	GRAVITY 108	.095	.0439	9.1	4817.2569	.486	283 14 2.473	103 9 13.
108	GRAVITY 108	107	GRAVITY 107	.105	.0480	8.7	5514.7960	.488	287 42 37.712	107 37 14.
107	GRAVITY 107	1464	HIW 3	.146	.0414	4.3	9656.8704	-.283	280 17 24.398	100 7 38.
1462	HIW 9	1406	VG 6	.678	.0436	17.8	2455.1356	2.530	256 44 22.623	76 41 56.
1500	DY 2	1471	DP 1	.001	-.0666	261.3	254.9824	-1.429	142 24 14.936	322 24 24.

TOTAL SET OF OBSERVATIONS

PERCENTAGE DIFFERENCE FROM EXPECTED DISTRIBUTION SCALED BY THE 2ND MOMENT
 - SHORT - OVER

ACTUAL NO EXPECTED NO CLASS EDGE 80 70 60 50 40 30 20 10 0 10 20 30 40 50 60 70 80

36	39	-1.604	XXXXX															
26	39	-1.227	XXXXXXXXXXXXXXXXXXXX															
30	39	-.972	XXXXXXXXXXXXXXXXXXXX															
33	39	-.767	XXXXXXXXXX															
35	39	-.591	XXXXXXXXXX															
40	39	-.432								EX								
41	39	-.282								EX								
56	39	-.139								EXX								
60	39	0.000								EXX								
56	39	.139								EXX								
46	39	.282								EXX								
44	39	.432								EXX								
43	39	.591								EXX								
38	39	.767								XXX								
38	39	.972								XXX								
34	39	1.227								XXXXXXX								
24	39	1.604	XXXXXXXXXXXXXXXXXXXX							XXXXXXXXXX								
36	53	*****	XXXXXXXXXXXXXXXXXXXX							XXXXXXXXXXXXXXXXXXXX								

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
1	6785000	67A35	87	1426	SL 13	16.24	108.55	126.49	.136	.112	.82	1.45	20.53		
			107	1427		32.79	145.60	136.74	.071	.054	.76	.34	.070	2.14	5.28
2	6785001	67A24	58	1446	U+U 611	17.15	82.64	136.67	.038	.021	.56	.40	5.40		
			66	1439		12.27	70.05	103.60	.035	.022	.63	.44	.031	2.55	6.91
			67	1440		12.32	67.87	104.21	.036	.025	.69	.49	.032	2.63	7.12
			74	1438		8.05	125.69	33.41	.048	.028	.59	1.22	.028	3.51	14.46
			75	1466		5.60	139.56	49.66	.038	.024	.63	1.39	.024	4.25	16.46
			77	1432	BC 17	1.53	150.35	146.50	.017	.013	.77	1.79	.017	11.19	27.43
			78	1441		10.01	51.11	54.21	.048	.036	.76	.74	.048	4.75	11.65
			79	1428		11.25	20.20	126.31	.074	.055	.75	1.33	.057	5.05	16.04
			81	1425		13.89	175.51	97.35	.079	.055	.70	1.18	.056	4.04	13.91
			82	1429		10.38	149.58	96.47	.064	.059	.93	1.24	.061	5.88	15.04
			83	1431		9.58	121.14	173.87	.063	.056	.89	1.31	.059	6.15	16.11
			85	1433		12.69	90.89	158.59	.069	.061	.88	1.10	.062	4.87	13.32
			87	1426	SL 13	24.21	142.12	126.49	.136	.112	.82	.97	.134	5.55	13.77
			99	1480	BC 13A	12.22	124.29	171.31	.004	.001	.35	.05	.003	.24	.82
104	1401	VG 1	13.62	91.29	131.42	.028	.018	.65	.35	.025	1.82	5.12			
105	1445	HIW 16	13.35	107.51	137.89	.025	.017	.67	.30	.023	1.73	4.58			
106	1437	BC 21	9.06	5.86	105.50	.045	.026	.57	1.01	.026	2.91	12.11			
107	1427		11.97	76.58	136.74	.071	.054	.76	1.15	.058	4.88	14.46			
3	678566	67A25	44	1453	HIW 10	5.57	34.82	170.16	.043	.028	.64	1.35	19.08		
			74	1438		4.10	120.40	33.41	.048	.028	.59	2.39	.028	6.91	28.39
			90	678756	MT MYE	2.63	131.77	38.31	.024	.015	.61	1.91	.015	5.69	22.71
			97	1491	HIW 14	4.19	38.60	52.43	.055	.035	.64	1.80	.054	12.99	32.38
			99	1480	BC 13A	.11	171.24	171.31	.004	.001	.35	2.69	.004	37.10	90.90
			104	1401	VG 1	7.37	28.60	131.42	.028	.018	.65	.79	.019	2.59	9.47
			105	1445	HIW 16	3.82	43.78	137.89	.025	.017	.67	1.34	.017	4.38	15.99
4	678567	67A55	5	1470	RC 11	4.98	10.79	25.48	.071	.034	.48	1.55	34.88		
			7	1463	RC 2	4.66	44.20	23.34	.063	.034	.55	1.74	.060	12.95	33.24
			8	1420	WH1 3	6.84	45.20	33.98	.063	.038	.59	1.17	.063	9.16	22.72
			99	1480	BC 13A	23.79	91.44	171.31	.004	.001	.35	.04	.002	.07	.42
			103	1421	RC 4	6.84	44.11	34.20	.064	.038	.59	1.17	.063	9.23	22.84
5	1470	RC 11	4	678567	67A55	4.98	10.79	25.48	.071	.034	.48	1.55	34.88		
			6	1484		2.39	47.97	75.86	.032	.021	.67	2.07	.030	12.40	32.37
			7	1463	RC 2	2.78	123.85	37.35	.023	.013	.58	1.67	.013	4.71	19.84
			8	1420	WH1 3	3.92	91.05	27.47	.030	.022	.75	1.50	.024	6.13	18.64
			9	1481	HIW 2	6.94	57.22	145.84	.039	.023	.60	1.16	.023	3.36	13.78
			10	1447		8.18	19.66	105.19	.049	.021	.44	1.24	.022	2.65	14.73
			11	1464	HIW 3	9.97	65.91	156.81	.056	.027	.47	1.17	.027	2.67	13.86
			13	1483		8.20	80.47	170.80	.045	.020	.44	1.12	.020	2.41	13.35
			91	1482	HIW 1	6.72	3.02	89.46	.044	.029	.66	1.34	.029	4.33	15.97

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
5	1470	11	103 1421	RC 4	3.82	89.70	28.31	.029	.022	.77	1.51	.024 6.34 18.81
6	1484		5 1470	RC 11	2.39	47.97	75.86	.032	.021	.67	2.07	.030 12.40 32.37
			7 1463	RC 2	3.20	170.36	78.84	.034	.015	.42	2.21	.015 4.56 26.27
			8 1420	WHI 3	2.71	128.02	63.53	.040	.022	.55	2.83	.026 9.68 36.01
			9 1481	HIW 2	4.59	62.02	94.15	.035	.031	.87	1.45	.034 7.44 18.88
			15 1485	TRI 18	4.61	88.70	47.83	.033	.030	.90	1.41	.032 6.93 17.74
			17 1419	VG 19	4.64	117.94	53.46	.041	.027	.65	1.72	.030 6.40 21.61
			18 1418	VG 18	5.24	123.03	52.60	.042	.026	.62	1.58	.028 5.35 19.48
			103 1421	RC 4	2.59	127.67	64.00	.040	.022	.55	2.94	.026 10.21 37.62
7	1463	RC 2	4 678567	67A55	4.66	44.20	23.34	.063	.034	.55	1.74	.060 12.95 33.24
			5 1470	RC 11	2.78	123.85	37.35	.023	.013	.58	1.67	.013 4.71 19.84
			6 1404		3.20	170.36	78.84	.034	.015	.42	2.21	.015 4.56 26.27
			8 1420	WHI 3	2.18	47.32	50.99	.024	.019	.77	1.77	.024 11.12 27.26
			9 1481	HIW 2	6.37	33.58	122.90	.037	.019	.51	1.18	.019 2.93 14.06
			11 1464	HIW 3	8.82	50.40	143.57	.051	.024	.47	1.20	.024 2.77 14.31
			13 1483		6.47	63.28	153.30	.037	.012	.33	1.18	.012 1.87 14.06
			14 1487	PRI 4	5.92	63.46	153.67	.034	.011	.33	1.20	.011 1.92 14.24
			15 1485	TRI 18	5.22	51.41	141.69	.031	.012	.39	1.23	.012 2.35 14.63
			16 1486	PRI 6	5.14	69.17	159.14	.031	.012	.38	1.23	.012 2.28 14.61
			17 1419	VG 19	3.70	74.66	175.51	.027	.019	.71	1.49	.019 5.26 17.88
			18 1418	VG 18	3.87	85.61	179.02	.027	.017	.62	1.44	.017 4.33 17.09
			19 1417	WHI 1-71	4.86	88.78	179.35	.030	.013	.44	1.27	.013 2.72 15.10
			22 1475	HIW 8	5.52	116.06	26.59	.035	.016	.46	1.29	.016 2.89 15.32
			23 1477		3.96	132.14	30.52	.029	.024	.82	1.52	.024 6.13 18.20
			91 1482	HIW 1	8.49	166.67	72.13	.052	.030	.58	1.25	.030 3.53 14.89
			103 1421	RC 4	2.18	43.91	53.35	.024	.019	.77	1.78	.024 11.11 27.36
8	1420	WHI 3	4 678567	67A55	6.84	45.20	33.98	.063	.038	.59	1.17	.063 9.16 22.72
			5 1470	RC 11	3.92	91.05	27.47	.030	.022	.75	1.50	.024 6.13 18.64
			6 1404		2.71	128.02	63.53	.040	.022	.55	2.83	.026 9.68 36.01
			7 1463	RC 2	2.18	47.32	50.99	.024	.019	.77	1.77	.024 11.12 27.26
			9 1481	HIW 2	4.28	26.63	88.85	.034	.024	.71	1.54	.026 6.16 19.31
			13 1483		4.41	71.10	162.46	.029	.025	.85	1.36	.025 5.62 16.21
			14 1487	PRI 4	3.87	72.46	176.30	.027	.025	.91	1.44	.025 6.40 17.21
			15 1485	TRI 18	3.05	54.33	85.51	.026	.024	.89	1.66	.026 8.46 21.30
			16 1486	PRI 6	3.22	83.76	29.98	.027	.023	.85	1.62	.024 7.49 20.21
			17 1419	VG 19	2.02	104.35	23.78	.017	.013	.77	1.77	.013 6.67 21.08
			18 1418	VG 18	2.55	117.69	37.49	.021	.015	.70	1.71	.015 5.96 20.42
			19 1417	WHI 1-71	3.53	112.92	34.50	.027	.017	.61	1.57	.017 4.88 18.92
			20 1416	VG 16	4.69	119.79	36.63	.035	.022	.64	1.54	.023 4.84 18.36
			21 1415	VG 15A	4.79	117.24	32.54	.035	.022	.63	1.51	.022 4.67 18.02
			22 1475	HIW 8	5.15	139.34	51.85	.037	.019	.50	1.49	.019 3.64 17.72
			23 1477		4.35	162.15	69.88	.036	.026	.73	1.70	.026 6.05 20.25
			103 1421	RC 4	.13	135.09	134.95	.004	.002	.36	2.43	.004 32.44 79.48

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
9	1481	HIW 2	5 1470	RC 11	6.94	57.22	145.84	.039	.023	.60	1.16	.023	3.36	13.78
			6 1484		4.59	62.02	94.15	.035	.031	.87	1.45	.034	7.44	18.88
			7 1463	RC 2	6.37	33.58	122.90	.037	.019	.51	1.18	.019	2.93	14.06
			8 1420	WHI 3	4.28	26.63	88.85	.034	.024	.71	1.54	.026	6.16	19.31
			10 1447		5.00	142.07	57.37	.037	.017	.47	1.51	.018	3.54	18.01
			11 1464	HIW 3	3.28	84.52	173.47	.030	.015	.51	1.87	.015	4.62	22.22
			12 1494	HIW 4	6.74	102.64	131.24	.069	.058	.84	1.85	.066	9.85	24.98
			13 1483		3.29	136.80	49.26	.024	.010	.43	1.49	.010	3.14	17.70
			14 1487	PR1 4	3.20	146.33	56.02	.023	.010	.42	1.51	.010	3.05	17.94
			15 1485	TR1 18	2.12	164.84	64.07	.020	.011	.57	1.94	.012	5.57	23.27
			16 1486	PR1 6	3.71	159.75	66.90	.026	.010	.40	1.43	.010	2.81	17.01
			17 1419	VG 19	4.33	179.47	82.25	.034	.021	.64	1.59	.022	5.02	19.00
			24 1493	HIW 12	9.52	58.02	50.05	.085	.075	.88	1.63	.085	8.91	21.88
			91 1482	HIW 1	6.22	118.33	29.78	.043	.024	.56	1.44	.024	3.89	17.10
			103 1421	RC 4	4.24	28.29	88.98	.034	.024	.72	1.53	.027	6.28	19.35
10	1447		5 1470	RC 11	8.18	19.66	105.19	.049	.021	.44	1.24	.022	2.65	14.73
			9 1481	HIW 2	5.00	142.07	57.37	.037	.017	.47	1.51	.018	3.54	18.01
			11 1464	HIW 3	7.31	119.80	31.62	.048	.028	.58	1.34	.028	3.78	15.98
			91 1482	HIW 1	2.59	67.43	158.14	.026	.015	.55	2.10	.015	5.61	24.91
11	1464	HIW 3	5 1470	RC 11	9.97	65.91	156.81	.056	.027	.47	1.17	.027	2.67	13.86
			7 1463	RC 2	8.82	50.40	143.57	.051	.024	.47	1.20	.024	2.77	14.31
			9 1481	HIW 2	3.28	84.52	173.47	.030	.015	.51	1.87	.015	4.62	22.22
			10 1447		7.31	119.80	31.62	.048	.028	.58	1.34	.028	3.78	15.98
			12 1494	HIW 4	3.76	118.41	114.70	.066	.045	.69	2.49	.066	17.50	42.92
			13 1483		2.90	20.57	156.30	.028	.024	.87	1.86	.026	9.05	23.58
			14 1487	PR1 4	3.33	26.74	147.22	.029	.024	.85	1.72	.026	7.67	21.17
			15 1485	TR1 18	3.60	48.94	155.48	.031	.023	.74	1.75	.024	6.59	21.19
			16 1486	PR1 6	4.28	27.68	131.50	.032	.025	.79	1.51	.026	5.97	18.11
			17 1419	VG 19	5.66	34.84	129.47	.041	.031	.75	1.49	.031	5.42	17.72
			24 1493	HIW 12	6.74	45.48	56.17	.085	.073	.87	2.26	.084	12.50	30.75
			28 1489	HIW 5	5.98	139.91	174.05	.058	.045	.78	1.70	.054	9.03	23.66
			29 1450	HIW 6	9.23	154.80	60.80	.053	.033	.63	1.18	.033	3.62	14.09
			91 1482	HIW 1	9.13	106.79	15.41	.058	.029	.50	1.32	.029	3.21	15.68
			108 107	GRAVITY 10	9.66	100.21	82.72	.085	.077	.91	1.66	.084	8.69	21.46
12	1494	HIW 4	9 1481	HIW 2	6.74	102.64	131.24	.069	.058	.84	1.85	.066	9.85	24.98
			11 1464	HIW 3	3.76	118.41	114.70	.066	.045	.69	2.49	.066	17.50	42.92
			13 1483		4.42	77.95	123.42	.070	.052	.74	2.90	.062	13.98	38.96
			14 1487	PR1 4	4.95	76.15	124.61	.071	.053	.74	2.65	.061	12.39	35.09
			20 1416	VG 16	6.45	43.43	121.62	.078	.054	.70	2.47	.056	8.61	29.62
			21 1415	VG 15A	6.22	43.02	121.85	.078	.054	.70	2.55	.055	8.89	30.54
			28 1489	HIW 5	2.84	168.96	132.94	.083	.061	.74	5.04	.076	26.78	71.54

DEPARTMENT OF ENERGY, MINES, AND RESOURCES
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CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM			
13	1483	5	1470	RC 11	8.20	80.47	170.80	.045	.020	.44	1.12	.020	2.41	13.35	
		7	1463	RC 2	6.47	63.28	153.30	.037	.012	.33	1.18	.012	1.87	14.06	
		8	1420	WHI 3	4.41	71.10	162.46	.029	.025	.85	1.36	.025	5.62	16.21	
		9	1481	HIW 2	3.29	136.80	49.26	.024	.010	.43	1.49	.010	3.14	17.70	
		11	1464	HIW 3	2.90	20.57	156.30	.028	.024	.87	1.86	.026	9.05	23.58	
		12	1494	HIW 4	4.42	77.95	123.42	.070	.052	.74	2.90	.062	13.98	38.96	
		14	1487	PRI 4	.55	61.40	60.63	.008	.005	.73	2.06	.008	13.75	33.68	
		15	1485	TRI 18	1.73	101.58	18.54	.013	.008	.58	1.58	.008	4.54	18.85	
		16	1486	PRI 6	1.45	41.98	122.97	.011	.008	.71	1.56	.008	5.50	18.70	
		17	1419	VG 19	2.94	48.92	129.17	.026	.020	.78	1.79	.020	6.86	21.41	
		18	1418	VG 18	3.24	36.32	122.91	.026	.017	.65	1.64	.017	5.22	19.53	
		19	1417	WHI 1-71	2.95	18.20	111.18	.023	.014	.60	1.57	.014	4.62	18.69	
		20	1416	VG 16	3.76	1.59	94.88	.029	.020	.69	1.60	.020	5.37	19.05	
21	1415	VG 15A	3.62	178.64	94.73	.028	.021	.73	1.60	.021	5.69	19.04			
23	1477		6.25	27.06	119.80	.041	.022	.53	1.35	.022	3.48	16.06			
28	1489	HIW 5	5.22	110.94	177.42	.061	.040	.66	2.29	.044	8.40	28.50			
29	1450	HIW 6	7.50	138.71	48.90	.047	.022	.47	1.28	.022	2.92	15.21			
103	1421	RC 4	4.47	72.59	165.72	.029	.025	.85	1.36	.025	5.56	16.11			
14	1487	PRI 4	7	1463	RC 2	5.92	63.46	153.67	.034	.011	.33	1.20	.011	1.92	14.24
			8	1420	WHI 3	3.87	72.46	176.30	.027	.025	.91	1.44	.025	6.40	17.21
			9	1481	HIW 2	3.20	146.33	56.02	.023	.010	.42	1.51	.010	3.05	17.94
			11	1464	HIW 3	3.33	26.74	147.22	.029	.024	.85	1.72	.026	7.67	21.17
			12	1494	HIW 4	4.95	76.15	124.61	.071	.053	.74	2.65	.061	12.39	35.09
			13	1483		.55	61.40	60.63	.008	.005	.73	2.06	.008	13.75	33.68
			15	1485	TRI 18	1.36	116.61	30.03	.011	.006	.57	1.72	.006	4.73	20.42
			16	1486	PRI 6	.95	30.96	113.15	.008	.006	.78	1.76	.006	6.73	21.04
			17	1419	VG 19	2.41	46.10	123.31	.024	.020	.85	2.04	.021	8.53	24.37
			18	1418	VG 18	2.76	31.49	118.21	.024	.017	.73	1.80	.017	6.34	21.38
			19	1417	WHI 1-71	2.58	9.85	103.70	.021	.014	.69	1.68	.015	5.62	19.92
			20	1416	VG 16	3.52	173.86	86.88	.028	.021	.73	1.66	.021	5.85	19.72
			21	1415	VG 15A	3.41	170.43	85.17	.027	.021	.77	1.65	.021	6.17	19.60
103	1421	RC 4	3.93	74.14	179.94	.028	.025	.89	1.43	.025	6.31	17.13			
15	1485	TRI 18	6	1484		4.61	88.70	47.83	.033	.030	.90	1.41	.032	6.93	17.74
			7	1463	RC 2	5.22	51.41	141.69	.031	.012	.39	1.23	.012	2.35	14.63
			8	1420	WHI 3	3.05	54.33	85.51	.026	.024	.89	1.66	.026	8.46	21.30
			9	1481	HIW 2	2.12	164.84	64.07	.020	.011	.57	1.94	.012	5.57	23.27
			11	1464	HIW 3	3.60	48.94	155.48	.031	.023	.74	1.75	.024	6.59	21.19
			13	1483		1.73	101.58	18.54	.013	.008	.58	1.58	.008	4.54	18.85
			14	1487	PRI 4	1.36	116.61	30.03	.011	.006	.57	1.72	.006	4.73	20.42
			16	1486	PRI 6	1.60	152.99	61.63	.013	.007	.52	1.67	.007	4.24	19.78
			17	1419	VG 19	2.34	12.77	92.73	.025	.020	.80	2.20	.020	8.70	26.33
			18	1418	VG 18	2.97	4.30	95.03	.025	.018	.72	1.76	.018	6.12	20.94
			19	1417	WHI 1-71	3.25	166.17	79.85	.024	.016	.66	1.51	.016	4.86	17.96
20	1416	VG 16	4.41	158.79	71.44	.032	.021	.67	1.49	.021	4.85	17.69			
21	1415	VG 15A	4.35	155.80	67.90	.031	.022	.70	1.47	.022	4.98	17.46			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM
15	I485	18	103 1421	RC 4	3.07	56.73	83.15	.026	.024	.91	1.64	.026	8.44 21.07
16	I486	PRI 6	7 1463	RC 2	5.14	69.17	159.14	.031	.012	.38	1.23	.012	2.28 14.61
			8 1420	WHI 3	3.22	83.76	29.98	.027	.023	.85	1.62	.024	7.49 20.21
			9 1481	HIW 2	3.71	159.75	66.90	.026	.010	.40	1.43	.010	2.81 17.01
			11 1464	HIW 3	4.28	27.68	131.50	.032	.025	.79	1.51	.026	5.97 18.11
			13 1483		1.45	41.98	122.97	.011	.008	.71	1.56	.008	5.50 18.70
			14 1487	PRI 4	.95	30.96	113.15	.008	.006	.78	1.76	.006	6.73 21.04
			15 1485	TRI 18	1.60	152.99	61.63	.013	.007	.52	1.67	.007	4.24 19.78
			17 1419	VG 19	1.51	55.60	113.07	.022	.021	.95	2.92	.021	13.86 35.27
			18 1418	VG 18	1.80	31.77	116.39	.021	.018	.83	2.45	.018	9.85 29.11
			19 1417	WHI 1-71	1.73	178.38	99.23	.018	.015	.82	2.18	.015	8.76 26.06
			20 1416	VG 16	2.82	162.09	78.15	.026	.021	.80	1.91	.021	7.46 22.73
			21 1415	VG 15A	2.75	157.44	73.06	.025	.021	.85	1.88	.021	7.77 22.38
			22 1475	HIW 8	4.26	178.01	84.40	.030	.019	.64	1.43	.019	4.42 16.99
			23 1477		4.86	22.65	117.45	.035	.022	.63	1.50	.022	4.60 17.84
			35 1413	VG 13A	5.25	152.41	57.82	.044	.028	.64	1.72	.028	5.34 20.43
			36 1414	VG 14	4.81	156.50	61.03	.041	.028	.67	1.77	.028	5.79 21.07
			103 1421	RC 4	3.30	85.51	29.73	.027	.023	.84	1.60	.024	7.28 19.96
17	1419	VG 19	6 1484		4.64	117.94	53.46	.041	.027	.65	1.72	.030	6.40 21.61
			7 1463	RC 2	3.70	74.66	175.51	.027	.019	.71	1.49	.019	5.26 17.88
			8 1420	WHI 3	2.02	104.35	23.78	.017	.013	.77	1.77	.013	6.67 21.08
			9 1481	HIW 2	4.33	179.47	82.25	.034	.021	.64	1.59	.022	5.02 19.00
			11 1464	HIW 3	5.66	34.84	129.47	.041	.031	.75	1.49	.031	5.42 17.72
			13 1483		2.94	48.92	129.17	.026	.020	.78	1.79	.020	6.86 21.41
			14 1487	PRI 4	2.41	46.10	123.31	.024	.020	.85	2.04	.021	8.53 24.37
			15 1485	TRI 18	2.34	12.77	92.73	.025	.020	.80	2.20	.020	8.70 26.33
			16 1486	PRI 6	1.51	55.60	113.07	.022	.021	.95	2.92	.021	13.86 35.27
			18 1418	VG 18	.74	156.67	137.84	.010	.009	.92	2.60	.010	13.46 33.24
			19 1417	WHI 1-71	1.56	124.08	40.07	.018	.014	.80	2.35	.014	9.20 27.96
			20 1416	VG 16	2.79	130.92	43.84	.027	.021	.78	1.98	.021	7.52 23.55
			21 1415	VG 15A	2.86	126.34	34.74	.027	.021	.78	1.93	.021	7.27 22.93
			22 1475	HIW 8	3.68	157.75	65.13	.030	.019	.63	1.67	.019	5.08 19.85
			23 1477		3.69	9.80	104.34	.032	.025	.78	1.80	.025	6.86 21.43
			34 1412	VG 12	6.17	135.45	47.93	.047	.029	.62	1.56	.029	4.71 18.52
			35 1413	VG 13A	5.29	135.95	48.39	.045	.028	.62	1.76	.028	5.35 20.94
			36 1414	VG 14	4.76	138.38	49.93	.043	.028	.66	1.84	.028	5.89 21.91
			100 1408	VG 8	10.43	134.05	46.70	.053	.031	.59	1.04	.031	2.97 12.38
			103 1421	RC 4	2.14	106.13	25.22	.018	.013	.72	1.73	.013	6.14 20.66

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
18	1418	VG 18	6 1484	5.24	123.03	52.60	.042	.026	.62	1.58	.028	5.35	19.48	
			7 1463	RC 2	3.87	85.61	179.02	.027	.017	.62	1.44	.017	4.33	17.09
			8 1420	WHI 3	2.55	117.69	37.49	.021	.015	.70	1.71	.015	5.96	20.42
			13 1483		3.24	36.32	122.91	.026	.017	.65	1.64	.017	5.22	19.53
			14 1487	PRI 4	2.76	31.49	118.21	.024	.017	.73	1.80	.017	6.34	21.38
			15 1485	TR1 18	2.97	4.30	95.03	.025	.018	.72	1.76	.018	6.12	20.94
			16 1486	PRI 6	1.80	31.77	116.39	.021	.018	.83	2.45	.018	9.85	29.11
			17 1419	VG 19	.74	156.67	137.84	.010	.009	.92	2.60	.010	13.46	33.24
			19 1417	WHI 1-71	1.02	100.91	20.99	.012	.012	.99	2.53	.012	12.08	30.02
			20 1416	VG 16	2.15	122.28	40.58	.023	.020	.87	2.16	.020	9.20	25.78
			21 1415	VG 15A	2.25	116.73	22.98	.023	.019	.85	2.08	.019	8.57	24.73
			22 1475	HIW 8	2.93	158.02	68.85	.026	.017	.66	1.81	.017	5.79	21.48
			23 1477		3.10	17.34	115.37	.030	.023	.76	1.99	.023	7.45	23.77
			33 1411	VG 11	6.70	134.93	48.64	.044	.029	.66	1.36	.029	4.38	16.18
34 1412	VG 12	5.49	132.64	47.21	.044	.028	.65	1.63	.028	5.17	19.45			
35 1413	VG 13A	4.60	132.67	47.85	.042	.027	.65	1.88	.028	5.98	22.41			
36 1414	VG 14	4.06	135.09	49.64	.039	.027	.69	2.00	.027	6.70	23.75			
103 1421	RC 4	2.67	118.53	37.14	.022	.015	.67	1.67	.015	5.57	19.97			
19	1417	WHI 1-71	7 1463	RC 2	4.86	88.78	179.35	.030	.013	.44	1.27	.013	2.72	15.10
			8 1420	WHI 3	3.53	112.92	34.50	.027	.017	.61	1.57	.017	4.88	18.92
			13 1483		2.95	18.20	111.18	.023	.014	.60	1.57	.014	4.62	18.69
			14 1487	PRI 4	2.58	9.85	103.70	.021	.014	.69	1.68	.015	5.62	19.92
			15 1485	TR1 18	3.25	166.17	79.85	.024	.016	.66	1.51	.016	4.86	17.96
			16 1486	PRI 6	1.73	178.38	99.23	.018	.015	.82	2.18	.015	8.76	26.06
			17 1419	VG 19	1.56	124.08	40.07	.018	.014	.80	2.35	.014	9.20	27.96
			18 1418	VG 18	1.02	100.91	20.99	.012	.012	.99	2.53	.012	12.08	30.02
			20 1416	VG 16	1.26	139.42	78.96	.017	.015	.89	2.69	.015	12.30	32.81
			21 1415	VG 15A	1.30	129.05	22.02	.016	.015	.96	2.50	.015	11.78	29.81
			22 1475	HIW 8	2.53	177.75	83.26	.022	.014	.62	1.77	.014	5.37	21.01
			23 1477		3.36	34.83	127.97	.030	.019	.66	1.81	.020	5.80	21.48
			32 1410	VG 10	6.39	135.45	51.88	.041	.027	.67	1.31	.028	4.32	15.56
			33 1411	VG 11	5.88	140.48	54.08	.041	.027	.66	1.43	.027	4.56	16.99
34 1412	VG 12	4.65	139.24	52.39	.040	.026	.65	1.76	.026	5.53	20.97			
35 1413	VG 13A	3.77	140.84	53.30	.038	.025	.65	2.09	.025	6.55	24.83			
36 1414	VG 14	3.27	145.15	56.45	.035	.024	.69	2.23	.024	7.44	26.54			
103 1421	RC 4	3.65	113.69	34.57	.028	.017	.60	1.55	.017	4.67	18.62			
20	1416	VG 16	8 1420	WHI 3	4.69	119.79	36.63	.035	.022	.64	1.54	.023	4.84	18.36
			12 1494	HIW 4	6.45	43.43	121.62	.078	.054	.70	2.47	.056	8.61	29.62
			13 1483		3.76	1.59	94.88	.029	.020	.69	1.60	.020	5.37	19.05
			14 1487	PRI 4	3.52	173.86	86.88	.028	.021	.73	1.66	.021	5.85	19.72
			15 1485	TR1 18	4.41	158.79	71.44	.032	.021	.67	1.49	.021	4.85	17.69
			16 1486	PRI 6	2.82	162.09	78.15	.026	.021	.80	1.91	.021	7.46	22.73
			17 1419	VG 19	2.79	130.92	43.84	.027	.021	.78	1.98	.021	7.52	23.55
			18 1418	VG 18	2.15	122.28	40.58	.023	.020	.87	2.16	.020	9.20	25.78
19 1417	WHI 1-71	1.26	139.42	78.96	.017	.015	.89	2.69	.015	12.30	32.81			

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (CM)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST PPM	R.A. PPM		
22	1475	8	30 1469	HIW 7	3.94	130.37	85.64	.031	.031	.97	1.62	.031	7.85	19.49
			32 1410	VG 10	4.83	114.79	45.27	.036	.031	.86	1.51	.032	6.53	18.27
			33 1411	VG 11	4.16	118.86	50.24	.037	.030	.83	1.77	.031	7.50	21.50
			34 1412	VG 12	3.10	108.72	49.31	.037	.030	.80	2.33	.032	10.19	29.06
			35 1413	VG 13A	2.32	99.83	52.05	.036	.029	.79	2.95	.032	13.98	38.39
			36 1414	VG 14	1.78	95.08	56.84	.034	.028	.83	3.57	.032	18.07	47.23
			103 1421	RC 4	5.28	139.24	51.67	.038	.019	.49	1.47	.019	3.54	17.51
23	1477	7 1463	RC 2	3.96	132.14	30.52	.029	.024	.82	1.52	.024	6.13	18.20	
		8 1420	WHI 3	4.35	162.15	69.88	.036	.026	.73	1.70	.026	6.05	20.25	
		13 1483		6.25	27.06	119.80	.041	.022	.53	1.35	.022	3.48	16.06	
		16 1486	PR1 6	4.86	22.65	117.45	.035	.022	.63	1.50	.022	4.60	17.84	
		17 1419	VG 19	3.69	9.80	104.34	.032	.025	.78	1.80	.025	6.86	21.43	
		18 1418	VG 18	3.10	17.34	115.37	.030	.023	.76	1.99	.023	7.45	23.77	
		19 1417	WHI 1-71	3.36	34.83	127.97	.030	.019	.66	1.81	.020	5.80	21.48	
		20 1416	VG 16	3.28	56.61	140.20	.033	.024	.73	2.06	.024	7.33	24.54	
		21 1415	VG 15A	3.52	56.44	142.61	.034	.023	.70	1.96	.023	6.66	23.34	
		22 1475	HIW 8	2.04	83.42	167.65	.022	.014	.61	2.23	.014	6.70	26.61	
		26 1476	PE 1	2.52	161.76	71.77	.039	.015	.39	3.19	.015	5.97	37.93	
		34 1412	VG 12	5.02	98.74	15.41	.043	.036	.85	1.74	.036	7.19	20.75	
		35 1413	VG 13A	4.31	92.16	16.90	.041	.036	.87	1.95	.036	8.41	23.36	
		36 1414	VG 14	3.79	88.86	8.08	.039	.035	.91	2.11	.035	9.34	25.12	
103 1421	RC 4	4.46	161.39	69.19	.036	.026	.72	1.68	.026	5.89	19.94			
24	1493	HIW 12	9 1481	HIW 2	9.52	58.02	50.05	.085	.075	.88	1.63	.085	8.91	21.88
			11 1464	HIW 3	6.74	45.48	56.17	.085	.073	.87	2.26	.084	12.50	30.75
			25 1492	HIW 13	9.36	118.83	172.31	.094	.089	.95	2.04	.091	9.74	24.70
			108 107	GRAVITY 10	7.96	143.94	93.47	.101	.090	.89	2.50	.095	11.89	31.03
25	1492	HIW 13	24 1493	HIW 12	9.36	118.83	172.31	.094	.089	.95	2.04	.091	9.74	24.70
			43 1495	HIW 15	5.94	126.39	5.83	.116	.099	.85	3.88	.103	17.41	47.87
			90 678756	MT MYE	8.22	8.90	165.65	.100	.077	.77	2.03	.097	11.78	29.84
			108 107	GRAVITY 10	4.01	61.32	160.01	.116	.102	.88	5.93	.102	25.42	70.68
			109 108	GRAVITY 10	3.99	154.25	.92	.113	.099	.88	5.27	.110	27.60	69.24
26	1476	PE 1	20 1416	VG 16	4.63	24.95	92.79	.052	.032	.62	2.21	.036	7.67	27.44
			21 1415	VG 15A	4.84	26.31	94.12	.052	.032	.62	2.11	.036	7.41	26.29
			22 1475	HIW 8	2.90	25.18	86.38	.042	.025	.60	2.76	.030	10.35	35.47
			23 1477		2.52	161.76	71.77	.039	.015	.39	3.19	.015	5.97	37.93
			27 1478	PE 2	2.74	168.90	78.91	.063	.015	.24	4.77	.015	5.65	56.61
			30 1469	HIW 7	4.24	89.03	95.20	.053	.042	.80	2.05	.052	12.36	30.35
			33 1411	VG 11	4.92	82.80	83.84	.054	.043	.80	1.82	.054	11.06	27.10
			34 1412	VG 12	4.48	68.69	82.64	.055	.043	.78	2.01	.054	12.11	30.01
			35 1413	VG 13A	4.17	57.64	82.87	.055	.042	.75	2.20	.053	12.71	32.44
			36 1414	VG 14	3.89	50.62	85.26	.055	.040	.73	2.40	.050	12.96	34.42

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
27	1478	PE 2	26 1476	PE 1	2.74	168.90	78.91	.063	.015	.24	4.77	.015	5.65	56.61
			30 1469	H1W 7	4.63	53.35	83.12	.100	.045	.45	2.82	.090	19.41	53.05
			33 1411	VG 11	5.47	52.79	81.66	.102	.046	.45	2.39	.092	16.77	45.53
			34 1412	VG 12	5.65	40.19	81.38	.102	.045	.44	2.75	.083	14.59	44.28
			35 1413	VG 13A	5.76	31.31	81.27	.103	.044	.43	2.99	.074	12.89	43.65
28	1489	H1W 5	11 1464	H1W 3	5.98	139.91	174.05	.058	.045	.78	1.70	.054	9.03	23.66
			12 1494	H1W 4	2.84	168.96	132.94	.083	.061	.74	5.04	.076	26.78	71.54
			13 1483		5.22	110.94	177.42	.061	.040	.66	2.29	.044	8.40	28.50
			20 1416	VG 16	5.33	69.16	167.58	.064	.044	.68	2.47	.044	8.28	29.46
			21 1415	VG 15A	5.10	69.84	167.93	.064	.043	.68	2.57	.044	8.55	30.66
			29 1450	H1W 6	3.77	178.87	168.30	.056	.037	.66	2.04	.055	14.57	36.05
			34 1412	VG 12	5.25	31.73	168.50	.065	.052	.80	2.29	.059	11.26	30.27
			35 1413	VG 13A	5.16	41.48	170.58	.065	.052	.79	2.41	.058	11.16	31.05
			36 1414	VG 14	5.35	47.29	168.95	.066	.051	.77	2.39	.055	10.35	30.08
			29	1450	H1W 6	11 1464	H1W 3	9.23	154.80	60.80	.053	.033	.63	1.18
13 1483		7.50				138.71	48.90	.047	.022	.47	1.28	.022	2.92	15.21
21 1415	VG 15A	5.27				112.48	39.01	.043	.030	.69	1.64	.031	5.86	19.97
28 1489	H1W 5	3.77				178.87	168.30	.056	.037	.66	2.04	.055	14.57	36.05
30 1469	H1W 7	3.57				50.96	41.82	.036	.031	.87	1.82	.036	10.09	24.81
31 1409	VG 9	2.94				13.48	61.45	.036	.031	.85	2.39	.034	11.41	30.39
32 1410	VG 10	2.22				38.94	58.88	.039	.032	.83	3.10	.038	17.28	43.10
33 1411	VG 11	2.73				51.35	51.50	.041	.033	.81	2.51	.041	15.01	36.77
34 1412	VG 12	2.92				76.25	47.46	.045	.033	.74	2.57	.043	14.60	37.83
35 1413	VG 13A	3.49				88.47	45.86	.047	.033	.71	2.38	.041	11.84	33.05
36 1414	VG 14	4.01				92.07	44.08	.047	.034	.72	2.13	.040	10.01	28.64
37 1407	VG 7	3.36				162.93	58.74	.038	.032	.85	2.29	.033	9.66	27.44
38 1424	H1W 6KA	4.65				164.65	58.86	.037	.032	.86	1.62	.032	6.89	19.48
40 1405	VG 5	4.90				157.66	59.52	.037	.032	.85	1.57	.032	6.49	18.67
41 1422	H1W 4KA	4.82				160.93	58.08	.037	.032	.85	1.59	.032	6.65	18.98
88 1404	VG 4	5.82				149.13	50.65	.039	.033	.84	1.38	.033	5.68	16.42
89 1462	H1W 9	5.11				136.30	28.44	.037	.035	.95	1.50	.036	6.96	17.87
100 1408	VG 8	3.56	174.78	60.05	.038	.032	.84	2.13	.033	9.20	25.93			
101 1490	H1W 7KA	3.85	170.08	59.36	.038	.032	.83	2.02	.033	8.55	24.48			
102 1406	VG 6	4.41	164.98	59.49	.037	.031	.85	1.71	.032	7.22	20.46			
30	1469	H1W 7	20 1416	VG 16	4.72	151.05	58.68	.036	.029	.81	1.56	.029	6.12	18.50
			21 1415	VG 15A	4.75	153.86	61.04	.035	.029	.82	1.53	.029	6.09	18.18
			22 1475	H1W 8	3.94	130.37	85.64	.031	.031	.97	1.62	.031	7.85	19.49
			26 1476	PE 1	4.24	89.03	95.20	.053	.042	.80	2.05	.052	12.36	30.35
			27 1478	PE 2	4.63	53.35	83.12	.100	.045	.45	2.82	.090	19.41	53.05
			29 1450	H1W 6	3.57	50.96	41.82	.036	.031	.87	1.82	.036	10.09	24.81
			31 1409	VG 9	2.18	106.20	32.91	.022	.019	.84	2.07	.019	8.67	24.84
			32 1410	VG 10	1.48	69.12	115.47	.024	.023	.94	3.29	.024	15.92	40.35
			33 1411	VG 11	.84	49.72	58.93	.026	.025	.93	6.03	.026	31.41	77.08

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM			
30	1469	7	34	1412	VG 12	1.56	177.71	51.93	.033	.027	.81	4.12	.029	18.69	52.16
			35	1413	VG 13A	2.27	161.58	51.29	.037	.028	.75	3.25	.029	12.73	39.67
			36	1414	VG 14	2.69	152.01	50.52	.037	.028	.76	2.81	.029	10.67	33.75
			37	1407	VG 7	3.89	104.38	27.23	.030	.020	.68	1.56	.021	5.34	18.79
			38	1424	HIW 6KA	4.59	119.11	32.94	.031	.018	.57	1.39	.018	3.88	16.51
			39	1423	HIW 5KA	5.04	125.57	35.88	.032	.017	.53	1.31	.017	3.35	15.59
			40	1405	VG 5	5.17	116.17	32.12	.032	.018	.58	1.27	.019	3.60	15.16
			41	1422	HIW 4KA	4.93	117.92	32.38	.032	.018	.57	1.32	.018	3.68	15.73
			42	1461	HIW 1KA	4.94	133.25	40.10	.032	.017	.52	1.32	.017	3.37	15.70
			100	1408	VG 8	3.36	112.65	33.62	.028	.019	.68	1.73	.020	5.84	20.70
			101	1490	HIW 7KA	3.77	114.12	33.90	.030	.020	.66	1.64	.020	5.39	19.64
			102	1406	VG 6	4.41	117.12	32.70	.031	.018	.59	1.43	.018	4.10	16.99
31	1409	VG 9	20	1416	VG 16	6.44	137.27	49.06	.040	.027	.67	1.29	.027	4.21	15.36
			21	1415	VG 15A	6.42	139.35	50.15	.040	.027	.68	1.28	.027	4.26	15.26
			29	1450	HIW 6	2.94	13.48	61.45	.036	.031	.85	2.39	.034	11.41	30.39
			30	1469	HIW 7	2.18	106.20	32.91	.022	.019	.84	2.07	.019	8.67	24.84
			32	1410	VG 10	1.34	148.08	61.47	.019	.016	.84	2.87	.016	11.68	34.09
			33	1411	VG 11	1.85	128.49	38.25	.025	.018	.73	2.76	.018	9.70	32.76
			34	1412	VG 12	3.05	135.15	43.71	.035	.022	.63	2.34	.022	7.10	27.77
			35	1413	VG 13A	3.94	134.55	44.71	.040	.023	.59	2.07	.023	5.93	24.57
			36	1414	VG 14	4.48	132.12	43.95	.040	.024	.60	1.86	.024	5.42	22.12
			37	1407	VG 7	1.71	102.07	177.74	.017	.015	.90	2.04	.015	9.04	24.42
			38	1424	HIW 6KA	2.51	130.28	27.94	.021	.018	.83	1.73	.018	7.05	20.68
			39	1423	HIW 5KA	3.07	139.18	42.17	.023	.018	.78	1.55	.018	5.87	18.42
			40	1405	VG 5	3.05	123.28	33.33	.023	.018	.80	1.53	.018	5.92	18.22
			41	1422	HIW 4KA	2.83	126.92	30.24	.022	.018	.80	1.62	.018	6.34	19.25
			42	1461	HIW 1KA	3.16	151.50	55.03	.024	.019	.79	1.53	.019	5.88	18.22
			47	1457	HIW 3KA	5.81	125.74	35.22	.032	.020	.64	1.14	.020	3.52	13.53
			48	14571	JK1	5.88	125.68	36.19	.032	.023	.72	1.14	.023	3.98	13.50
			49	1454	JK 4	4.89	130.11	39.12	.029	.021	.71	1.23	.021	4.25	14.65
			50	1452	HIW 2KA	5.06	133.14	41.94	.030	.021	.71	1.21	.021	4.18	14.37
			51	1459	JK 3	5.39	131.85	41.21	.031	.021	.68	1.17	.021	3.87	13.90
			52	1460	IN 4	5.17	131.86	41.28	.030	.021	.71	1.19	.021	4.08	14.16
			53	1458	IN 1	5.55	129.35	38.51	.031	.021	.66	1.16	.021	3.71	13.83
			54	1456	IN 2	5.66	131.73	41.24	.032	.021	.65	1.16	.021	3.67	13.81
			55	1455	IN 3	5.98	133.27	44.86	.034	.021	.64	1.16	.021	3.57	13.74
56	1451	JK 2	5.87	135.70	47.73	.033	.021	.65	1.14	.021	3.62	13.60			
88	1404	VG 4	4.25	120.16	29.30	.027	.019	.73	1.29	.019	4.56	15.31			
89	1462	HIW 9	4.30	101.22	.32	.029	.021	.72	1.36	.021	4.91	16.33			
100	1408	VG 8	1.22	124.20	84.81	.014	.013	.94	2.31	.014	11.34	28.45			
101	1490	HIW 7KA	1.64	124.66	52.81	.017	.015	.90	2.08	.015	9.27	24.99			
102	1406	VG 6	2.30	127.44	31.27	.020	.017	.83	1.81	.017	7.32	21.53			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
32	1410	VG 10	19 1417	WHI 1-71	6.39	135.45	51.88	.041	.027	.67	1.31	.028 4.32 15.56
			20 1416	VG 16	5.14	134.47	49.02	.037	.027	.72	1.49	.027 5.20 17.70
			21 1415	VG 15A	5.10	137.07	51.64	.037	.027	.73	1.48	.027 5.29 17.61
			22 1475	HIW 8	4.83	114.79	45.27	.036	.031	.86	1.51	.032 6.53 18.27
			29 1450	HIW 6	2.22	38.94	58.88	.039	.032	.83	3.10	.038 17.28 43.10
			30 1469	HIW 7	1.48	69.12	115.47	.024	.023	.94	3.29	.024 15.92 40.35
			31 1409	VG 9	1.34	148.08	61.47	.019	.016	.84	2.87	.016 11.68 34.09
			33 1411	VG 11	.74	91.28	155.64	.012	.011	.95	3.27	.011 15.30 39.18
			34 1412	VG 12	1.77	125.44	37.11	.025	.017	.71	2.86	.017 9.83 33.94
			35 1413	VG 13A	2.66	127.79	40.86	.031	.020	.64	2.43	.020 7.62 28.92
			36 1414	VG 14	3.21	125.55	39.64	.033	.021	.64	2.14	.021 6.69 25.41
			37 1407	VG 7	2.81	122.09	45.41	.028	.022	.79	2.02	.022 7.95 24.28
			38 1424	HIW 6KA	3.81	136.45	47.37	.030	.023	.77	1.64	.023 6.09 19.44
			39 1423	HIW 5KA	4.40	141.88	50.93	.032	.023	.73	1.49	.023 5.27 17.71
			40 1405	VG 5	4.30	130.78	47.01	.031	.023	.75	1.50	.024 5.47 17.87
			41 1422	HIW 4KA	4.11	133.67	46.70	.031	.023	.76	1.55	.023 5.71 18.48
			42 1461	HIW 1KA	4.50	150.49	57.45	.032	.023	.73	1.47	.023 5.21 17.49
			49 1454	JK 4	6.17	133.94	45.81	.036	.025	.70	1.22	.025 4.13 14.45
			50 1452	HIW 2KA	6.36	136.25	47.38	.037	.026	.70	1.19	.026 4.03 14.19
			51 1459	JK 3	6.68	135.06	46.46	.038	.025	.68	1.16	.025 3.81 13.76
			52 1460	IN 4	6.47	135.18	46.87	.037	.026	.69	1.18	.026 3.97 14.01
53 1458	IN 1	6.83	132.96	44.29	.038	.025	.67	1.15	.025 3.72 13.66			
54 1456	IN 2	6.95	134.83	45.91	.039	.025	.66	1.14	.025 3.65 13.59			
88 1404	VG 4	5.46	126.75	41.57	.034	.025	.73	1.28	.025 4.54 15.26			
89 1462	HIW 9	5.30	111.82	21.13	.034	.028	.82	1.32	.028 5.23 15.71			
100 1408	VG 8	2.50	136.70	55.59	.027	.020	.76	2.19	.020 8.13 26.13			
101 1490	HIW 7KA	2.92	135.17	53.03	.029	.021	.74	2.02	.021 7.30 24.09			
102 1406	VG 6	3.59	135.00	48.00	.030	.023	.76	1.71	.023 6.28 20.31			
33	1411	VG 11	18 1418	VG 18	6.70	134.93	48.64	.044	.029	.66	1.36	.029 4.38 16.18
			19 1417	WHI 1-71	5.88	140.48	54.08	.041	.027	.66	1.43	.027 4.56 16.99
			20 1416	VG 16	4.62	140.77	53.66	.036	.026	.71	1.62	.026 5.58 19.31
			21 1415	VG 15A	4.62	143.68	57.22	.036	.026	.71	1.61	.026 5.58 19.15
			22 1475	HIW 8	4.16	118.86	50.24	.037	.030	.83	1.77	.031 7.50 21.50
			26 1476	PE 1	4.92	82.80	83.84	.054	.043	.80	1.82	.054 11.06 27.10
			27 1478	PE 2	5.47	52.79	81.66	.102	.046	.45	2.39	.092 16.77 45.53
			29 1450	HIW 6	2.73	51.35	51.50	.041	.033	.81	2.51	.041 15.01 36.77
			30 1469	HIW 7	.84	49.72	58.93	.026	.025	.93	6.03	.026 31.41 77.08
			31 1409	VG 9	1.85	128.49	38.25	.025	.018	.73	2.76	.018 9.70 32.76
			32 1410	VG 10	.74	91.28	155.64	.012	.011	.95	3.27	.011 15.30 39.18
			34 1412	VG 12	1.23	145.16	60.52	.019	.015	.79	3.11	.015 11.92 36.96
			35 1413	VG 13A	2.11	139.85	53.53	.027	.018	.67	2.62	.018 8.59 31.10
			36 1414	VG 14	2.63	134.67	49.14	.029	.020	.67	2.29	.020 7.52 27.30
			37 1407	VG 7	3.47	115.81	35.60	.033	.023	.70	1.98	.024 6.83 23.43
			38 1424	HIW 6KA	4.36	129.52	39.32	.035	.024	.70	1.65	.024 5.56 19.55
			39 1423	HIW 5KA	4.90	135.16	42.82	.036	.024	.68	1.52	.024 4.98 18.01
			40 1405	VG 5	4.89	125.25	39.76	.036	.025	.68	1.51	.025 5.02 17.91
			41 1422	HIW 4KA	4.68	133.67	46.70	.035	.024	.69	1.56	.024 5.23 18.57

DEPARTMENT OF ENERGY, MINES, AND RESOURCES
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CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
33	1411	11	42 1461	HIW 1KA	4.92	143.05	47.48	.036	.025	.69	1.51	.025	5.09	17.95
			100 1408	VG 8	3.07	126.79	41.58	.032	.022	.69	2.14	.022	7.20	25.41
			101 1490	HIW 7KA	3.49	126.69	41.30	.034	.023	.68	1.99	.023	6.58	23.65
			102 1406	VG 6	4.15	127.91	39.44	.034	.024	.69	1.71	.024	5.71	20.30
34	1412	VG 12	17 1419	VG 19	6.17	135.45	47.93	.047	.029	.62	1.56	.029	4.71	18.52
			18 1418	VG 18	5.49	132.64	47.21	.044	.028	.65	1.63	.028	5.17	19.45
			19 1417	WHI 1-71	4.65	139.24	52.39	.040	.026	.65	1.76	.026	5.53	20.97
			20 1416	VG 16	3.40	139.18	50.45	.033	.024	.71	2.03	.024	7.01	24.11
			21 1415	VG 15A	3.38	143.14	56.36	.033	.024	.72	2.01	.024	7.05	23.87
			22 1475	HIW 8	3.10	108.72	49.31	.037	.030	.80	2.33	.032	10.19	29.06
			23 1477		5.02	98.74	15.41	.043	.036	.85	1.74	.036	7.19	20.75
			26 1476	PE 1	4.48	68.69	82.64	.055	.043	.78	2.01	.054	12.11	30.01
			27 1478	PE 2	5.65	40.19	81.38	.102	.045	.44	2.75	.083	14.59	44.28
			28 1489	HIW 5	5.25	31.73	168.50	.065	.052	.80	2.29	.059	11.26	30.27
			29 1450	HIW 6	2.92	76.25	47.46	.045	.033	.74	2.57	.043	14.60	37.83
			30 1469	HIW 7	1.56	177.71	51.93	.033	.027	.81	4.12	.029	18.69	52.16
			31 1409	VG 9	3.05	135.15	43.71	.035	.022	.63	2.34	.022	7.10	27.77
			32 1410	VG 10	1.77	125.44	37.11	.025	.017	.71	2.86	.017	9.83	33.94
			33 1411	VG 11	1.23	145.16	60.52	.019	.015	.79	3.11	.015	11.92	36.96
			35 1413	VG 13A	.89	132.47	43.11	.013	.012	.89	3.04	.012	13.04	36.07
			36 1414	VG 14	1.44	125.69	34.04	.018	.014	.78	2.58	.014	9.83	30.69
			37 1407	VG 7	4.58	123.39	40.85	.041	.026	.63	1.86	.026	5.74	22.15
			38 1424	HIW 6KA	5.56	132.95	43.00	.042	.027	.63	1.57	.027	4.77	18.69
			39 1423	HIW 5KA	6.12	137.17	44.81	.043	.027	.61	1.46	.027	4.35	17.38
40 1405	VG 5	6.07	129.22	43.06	.043	.027	.62	1.47	.027	4.42	17.43			
41 1422	HIW 4KA	5.87	131.19	42.91	.043	.027	.62	1.51	.027	4.56	17.92			
42 1461	HIW 1KA	6.15	143.47	47.64	.043	.027	.62	1.45	.027	4.42	17.28			
100 1408	VG 8	4.26	132.03	44.34	.040	.025	.61	1.96	.025	5.82	23.29			
101 1490	HIW 7KA	4.67	131.49	43.98	.042	.025	.61	1.85	.025	5.45	22.05			
102 1406	VG 6	5.34	131.84	42.92	.042	.026	.62	1.63	.026	4.88	19.32			
35	1413	VG 13A	16 1406	PR1 6	5.25	152.41	57.82	.044	.028	.64	1.72	.028	5.34	20.43
			17 1419	VG 19	5.29	135.95	48.39	.045	.028	.62	1.76	.028	5.35	20.94
			18 1418	VG 18	4.60	132.67	47.85	.042	.027	.65	1.88	.028	5.98	22.41
			19 1417	WHI 1-71	3.77	140.84	53.30	.038	.025	.65	2.09	.025	6.55	24.83
			20 1416	VG 16	2.51	141.54	51.58	.031	.022	.72	2.51	.022	8.82	29.81
			21 1415	VG 15A	2.51	146.89	59.55	.030	.022	.73	2.47	.022	8.80	29.39
			22 1475	HIW 8	2.32	99.83	52.05	.036	.029	.79	2.95	.032	13.98	38.39
			23 1477		4.31	92.16	16.90	.041	.036	.87	1.95	.036	8.41	23.36
			26 1476	PE 1	4.17	57.64	82.87	.055	.042	.75	2.20	.053	12.71	32.44
			27 1478	PE 2	5.76	31.31	81.27	.103	.044	.43	2.99	.074	12.89	43.65
			28 1489	HIW 5	5.16	41.48	170.58	.065	.052	.79	2.41	.058	11.16	31.05
			29 1450	HIW 6	3.49	88.47	45.86	.047	.033	.71	2.38	.041	11.84	33.05
			30 1469	HIW 7	2.27	161.58	51.29	.037	.028	.75	3.25	.029	12.73	39.67
31 1409	VG 9	3.94	134.55	44.71	.040	.023	.59	2.07	.023	5.93	24.57			
32 1410	VG 10	2.66	127.79	40.86	.031	.020	.64	2.43	.020	7.62	28.92			
33 1411	VG 11	2.11	139.85	53.53	.027	.018	.67	2.62	.018	8.59	31.10			

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
35	1413	13A	34	1412	VG 12	.89	132.47	43.11	.013	.012	.89	3.04	.012	13.04	36.07
			36	1414	VG 14	.56	114.96	137.65	.009	.008	1.96	3.02	.009	15.12	37.28
			37	1407	VG 7	5.46	124.86	42.02	.046	.027	.60	1.71	.028	5.05	20.45
			38	1424	HIW 6KA	6.45	132.89	43.82	.046	.028	.60	1.48	.028	4.28	17.58
			100	1408	VG 8	5.15	132.11	44.84	.045	.026	.58	1.79	.026	5.07	21.32
			101	1490	HIW 7KA	5.56	131.65	44.49	.046	.027	1.58	1.71	.027	4.81	20.37
			102	1406	VG 6	6.23	131.93	43.70	.046	.027	.59	1.52	.027	4.37	18.10
36	1414	VG 14	16	1486	PRI 6	4.81	156.50	61.03	.041	.028	.67	1.77	.028	5.79	21.07
			17	1419	VG 19	4.76	138.38	49.93	.043	.028	.66	1.84	.028	5.89	21.91
			18	1418	VG 18	4.06	135.09	49.64	.039	.027	.69	2.00	.027	6.70	23.75
			19	1417	WHI 1-71	3.27	145.15	56.45	.035	.024	1.69	2.23	.024	7.44	26.54
			20	1416	VG 16	2.03	148.70	55.93	.027	.022	.79	2.77	.022	10.67	32.96
			21	1415	VG 15A	2.06	155.23	68.11	.027	.021	.79	2.71	.021	10.41	32.16
			22	1475	HIW 8	1.78	95.08	56.84	.034	.028	1.83	3.57	.032	18.07	47.23
			23	1477		3.79	88.86	8.08	.039	.035	.91	2.11	.035	9.34	25.12
			26	1476	PE 1	3.89	50.62	85.26	.055	.040	.73	2.40	.050	12.96	34.42
			28	1489	HIW 5	5.35	47.29	168.95	.066	.051	.77	2.39	.055	10.35	30.08
			29	1450	HIW 6	4.01	92.07	44.08	.047	.034	.72	2.13	.040	10.01	28.64
			30	1469	HIW 7	2.69	152.81	50.52	.037	.028	1.76	2.81	.029	10.67	33.75
			31	1409	VG 9	4.48	132.12	43.95	.040	.024	.60	1.86	.024	5.42	22.12
			32	1410	VG 10	3.21	125.55	39.64	.033	.021	.64	2.14	.021	6.69	25.41
			33	1411	VG 11	2.63	134.67	49.14	.029	.020	.67	2.29	.020	7.52	27.30
34	1412	VG 12	1.44	125.69	34.04	.018	.014	.78	2.58	.014	9.83	30.69			
35	1413	VG 13A	.56	114.96	137.65	.009	.008	.96	3.02	.009	15.12	37.28			
37	1407	VG 7	6.02	123.94	41.38	.046	.028	.60	1.58	.028	4.69	18.84			
			100	1408	VG 8	5.69	130.43	44.19	.045	.027	.59	1.65	.027	4.72	19.59
			101	1490	HIW 7KA	6.11	130.13	43.85	.047	.027	.58	1.58	.028	4.50	18.84
37	1407	VG 7	29	1450	HIW 6	3.36	162.93	58.74	.038	.032	.85	2.29	.033	9.66	27.44
			30	1469	HIW 7	3.89	104.38	27.23	.030	.020	.68	1.56	.021	5.34	18.79
			31	1409	VG 9	1.71	102.07	177.74	.017	.015	.90	2.04	.015	9.04	24.42
			32	1410	VG 10	2.81	122.09	45.41	.028	.022	.79	2.02	.022	7.95	24.28
			33	1411	VG 11	3.47	115.81	35.60	.033	.023	.70	1.96	.024	6.83	23.43
			34	1412	VG 12	4.58	123.39	40.85	.041	.026	.63	1.86	.026	5.74	22.15
			35	1413	VG 13A	5.46	124.86	42.02	.046	.027	.60	1.71	.028	5.05	20.45
			36	1414	VG 14	6.02	123.94	41.38	.046	.028	.60	1.58	.028	4.69	18.84
			38	1424	HIW 6KA	1.29	169.17	162.08	.015	.014	1.92	2.23	.015	11.70	28.70
			39	1423	HIW 5KA	1.99	170.37	65.85	.018	.016	.88	1.81	.016	7.84	21.63
			40	1405	VG 5	1.58	146.38	50.52	.016	.015	.90	2.14	.015	9.35	25.46
			41	1422	HIW 4KA	1.46	156.34	21.80	.016	.015	.94	2.17	.015	10.51	26.49
			42	1461	HIW 1KA	2.43	3.91	83.59	.020	.016	.82	1.65	.016	6.69	19.75
			45	1402	VG 2	5.45	130.18	41.41	.032	.020	.62	1.23	.020	3.67	14.58
			46	1403	VG 3	4.82	134.87	42.15	.030	.018	.61	1.29	.018	3.82	15.32
			47	1457	HIW 3KA	4.30	134.96	40.87	.028	.018	.65	1.33	.018	4.20	15.88
			48	14571	JK1	4.37	134.72	44.10	.028	.021	.75	1.34	.021	4.86	15.86
			49	1454	JK 4	3.47	143.52	49.17	.025	.018	.74	1.47	.018	5.27	17.44
50	1452	HIW 2KA	3.70	144.96	52.08	.025	.019	.73	1.41	.019	5.02	16.81			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (MP)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
37	1407	7	51	1459	JK 3	3.99	144.16	50.47	.026	-.018	.69	1.36	-.018	4.58	16.18
			52	1460	IN 4	3.78	144.87	51.83	.026	-.019	.72	1.39	-.019	4.90	16.58
			53	1458	IN 1	4.10	140.39	45.83	.027	-.018	.67	1.36	-.018	4.43	16.19
			54	1456	IN 2	4.28	143.21	49.02	.028	-.018	.65	1.35	-.018	4.29	16.05
			55	1455	IN 3	4.60	144.39	52.53	.030	-.019	.62	1.34	-.019	4.07	15.93
			56	1451	JK 2	4.54	147.76	56.75	.029	-.018	.63	1.32	-.018	4.04	15.65
			88	1404	VG 4	2.67	131.64	34.41	.021	-.017	.79	1.63	-.017	6.26	19.39
			89	1462	HIW 9	2.59	100.66	173.07	.024	-.017	.69	1.90	-.018	6.82	23.07
			100	1408	VG 8	.74	63.69	136.68	.009	-.007	.81	2.49	-.008	10.13	30.03
			101	1490	HIW 7KA	.66	29.50	110.65	.010	-.007	.68	3.18	-.007	10.69	37.98
			102	1406	VG 6	1.05	171.54	137.92	.013	-.013	.98	2.50	-.013	12.23	30.18
38	1424	HIW 6KA	29	1450	HIW 6	4.65	164.65	58.86	.037	-.032	.86	1.62	-.032	6.89	19.48
			30	1469	HIW 7	4.59	119.11	32.94	.031	-.018	.57	1.39	-.018	3.88	16.51
			31	1409	VG 9	2.51	130.28	27.94	.021	-.018	.83	1.73	-.018	7.05	20.68
			32	1410	VG 10	3.81	136.45	47.37	.030	-.023	.77	1.64	-.023	6.09	19.44
			33	1411	VG 11	4.36	129.52	39.32	.035	-.024	.70	1.65	-.024	5.56	19.55
			34	1412	VG 12	5.56	132.95	43.00	.042	-.027	.63	1.57	-.027	4.77	18.69
			35	1413	VG 13A	6.45	132.89	43.82	.046	-.028	.60	1.48	-.028	4.28	17.58
			37	1407	VG 7	1.29	169.17	162.08	.015	-.014	.92	2.23	-.015	11.70	28.70
			39	1423	HIW 5KA	.71	172.57	64.77	.008	-.006	.80	2.30	-.007	9.30	27.77
			40	1405	VG 5	.63	94.40	152.81	.010	-.007	.75	2.99	-.008	12.76	37.91
			41	1422	HIW 4KA	.35	102.31	106.40	.005	-.004	.84	2.57	-.005	14.87	36.46
			42	1461	HIW 1KA	1.23	19.42	91.97	.012	-.009	.82	1.91	-.010	7.86	23.05
			45	1402	VG 2	4.52	119.84	35.97	.027	-.016	.59	1.21	-.016	3.48	14.42
			46	1403	VG 3	3.83	123.92	36.53	.024	-.013	.55	1.30	-.013	3.48	15.40
			47	1457	HIW 3KA	3.31	122.30	33.69	.021	-.013	.59	1.34	-.013	3.83	15.89
			48	14571	JK 1	3.38	122.27	35.45	.022	-.017	.78	1.33	-.017	5.04	15.86
			49	1454	JK 4	2.38	129.92	42.47	.018	-.013	.74	1.53	-.013	5.53	18.20
			50	1452	HIW 2KA	2.55	135.95	48.97	.018	-.014	.74	1.48	-.014	5.30	17.59
			51	1459	JK 3	2.88	133.23	45.75	.019	-.013	.67	1.40	-.013	4.56	16.59
			52	1460	IN 4	2.66	133.36	47.30	.019	-.014	.73	1.44	-.014	5.09	17.09
			53	1458	IN 1	3.04	128.58	39.76	.020	-.013	.63	1.39	-.013	4.23	16.53
			54	1456	IN 2	3.15	132.88	44.62	.021	-.013	.61	1.40	-.013	4.14	16.59
			55	1455	IN 3	3.47	135.43	50.14	.024	-.014	.58	1.40	-.014	4.00	16.67
			56	1451	JK 2	3.37	139.73	55.68	.022	-.013	.59	1.37	-.013	3.98	16.31
			57	1488	HIW 11	5.64	137.39	60.75	.045	-.022	.48	1.61	-.023	4.16	19.47
			59	1479	DY 1	6.06	129.60	47.07	.031	-.018	.57	1.05	-.018	2.95	12.49
			88	1404	VG 4	1.83	106.19	12.97	.014	-.010	.74	1.57	-.010	5.67	18.70
			89	1462	HIW 9	2.43	71.12	160.34	.021	-.011	.51	1.79	-.011	4.42	21.24
			92	1499		6.38	132.37	51.66	.032	-.020	.63	1.01	-.020	3.16	12.12
			93	1498		6.49	133.36	52.01	.032	-.020	.61	1.00	-.020	3.06	12.00
94	1496		6.74	133.22	51.51	.032	-.020	.62	.98	-.020	3.04	11.73			
95	1500	DY 2	6.26	127.70	44.62	.031	-.019	.63	1.00	-.019	3.08	11.95			
98	1497		6.63	133.23	51.53	.032	-.020	.61	.99	-.020	2.99	11.84			
100	1408	VG 8	1.30	135.96	11.48	.017	-.013	.80	2.50	-.015	11.23	31.60			
101	1490	HIW 7KA	.89	140.62	2.30	.017	-.014	.84	3.51	-.016	17.34	45.61			
102	1406	VG 6	.24	158.68	159.91	.009	-.003	.34	2.53	-.009	35.92	88.02			

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CLARKE 1866

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
39	1423	HIW 5KA	30	1469	HIW 7	5.04	125.57	35.88	.032	-.017	.53	1.31	.017	3.35	15.59
			31	1409	VG 9	3.07	139.18	42.17	.023	-.018	.78	1.55	.018	5.87	18.42
			32	1410	VG 10	4.40	141.88	50.93	.032	-.023	.73	1.49	-.023	5.27	17.71
			33	1411	VG 11	4.90	135.16	42.82	.036	-.024	.68	1.52	-.024	4.98	18.01
			34	1412	VG 12	6.12	137.17	44.81	.043	-.027	.61	1.46	-.027	4.35	17.38
			37	1407	VG 7	1.99	170.37	65.85	.018	-.016	.88	1.81	-.016	7.84	21.63
			38	1424	HIW 6KA	.71	172.57	64.77	-.008	-.006	.80	2.30	-.007	9.30	27.77
			40	1405	VG 5	.85	39.68	137.34	.010	-.009	.89	2.52	-.009	10.94	29.93
			41	1422	HIW 4KA	.67	22.14	102.94	.007	-.007	.87	2.28	-.007	9.68	27.22
			42	1461	HIW 1KA	.68	47.60	38.84	.009	-.007	.82	2.17	-.009	12.67	31.15
			45	1402	VG 2	4.13	112.01	30.92	.025	-.016	.63	1.24	-.016	3.90	14.87
			46	1403	VG 3	3.40	114.95	31.24	.023	-.014	.61	1.36	-.014	4.05	16.21
			47	1457	HIW 3KA	2.91	111.54	26.65	.020	-.013	.65	1.42	-.013	4.49	16.87
			48	14571	JK1	2.98	111.76	22.51	.020	-.017	.84	1.42	-.017	5.79	16.83
			49	1454	JK 4	1.92	115.47	32.32	.016	-.013	.83	1.75	-.014	7.05	20.78
			50	1452	HIW 2KA	2.03	123.96	41.55	.017	-.014	.83	1.69	-.014	6.86	20.18
			51	1459	JK 3	2.37	122.34	39.05	.018	-.013	.76	1.54	-.014	5.72	18.40
			52	1460	IN 4	2.16	121.43	39.68	.017	-.014	.82	1.61	-.014	6.46	19.22
			53	1458	IN 1	2.57	117.59	32.91	.019	-.013	.70	1.51	-.013	5.15	18.03
			54	1456	IN 2	2.65	123.06	39.37	.020	-.013	.68	1.53	-.014	5.11	18.23
			55	1455	IN 3	2.94	127.08	47.12	.022	-.014	.65	1.52	-.015	4.94	18.22
			56	1451	JK 2	2.81	131.89	53.63	.021	-.014	.67	1.49	-.014	5.03	17.96
			57	1488	HIW 11	5.08	132.79	60.24	.043	-.022	.50	1.70	-.024	4.80	20.87
			59	1479	DY 1	5.57	124.63	43.89	.029	-.018	.60	1.07	-.018	3.22	12.84
			88	1404	VG 4	1.68	83.46	173.53	.014	-.011	.78	1.68	-.011	6.37	19.97
			89	1462	HIW 9	2.67	56.07	152.70	.022	-.013	.59	1.66	-.013	4.86	19.86
			92	1499		5.86	127.91	48.58	.030	-.020	.66	1.04	-.020	3.43	12.44
93	1498		5.96	129.06	49.03	.030	-.019	.65	1.03	-.020	3.33	12.31			
94	1496		6.21	129.08	48.38	.030	-.020	.66	1.00	-.020	3.28	12.00			
95	1500	DY 2	5.78	122.75	40.44	.029	-.019	.66	1.02	-.019	3.32	12.22			
98	1497		6.10	129.01	48.50	.030	-.019	.64	1.01	-.020	3.24	12.13			
100	1408	VG 8	1.92	148.65	38.27	.019	-.015	.81	1.98	-.016	8.16	24.01			
101	1490	HIW 7KA	1.54	154.67	38.06	.018	-.016	.86	2.40	-.016	10.64	29.24			
102	1406	VG 6	.94	169.06	22.38	.010	-.009	.94	2.08	-.010	10.31	25.67			
104	1401	VG 1	5.62	117.62	39.55	.028	-.017	.62	1.00	-.018	3.16	12.05			
40	1405	VG 5	29	1450	HIW 6	4.90	157.66	59.52	.037	-.032	.85	1.57	-.032	6.49	18.67
			30	1469	HIW 7	5.17	116.17	32.12	.032	-.018	.58	1.27	-.019	3.60	15.16
			31	1409	VG 9	3.05	123.28	33.33	.023	-.018	.80	1.53	-.018	5.92	18.22
			32	1410	VG 10	4.30	130.78	47.01	.031	-.023	.75	1.50	-.024	5.47	17.87
			33	1411	VG 11	4.89	125.25	39.76	.036	-.025	.68	1.51	-.025	5.02	17.91
			34	1412	VG 12	6.07	129.22	43.06	.043	-.027	.62	1.47	-.027	4.42	17.43
			37	1407	VG 7	1.58	146.38	50.52	.016	-.015	.90	2.14	-.015	9.35	25.46
			38	1424	HIW 6KA	.63	94.40	152.81	.010	-.007	.75	2.99	-.008	12.76	37.91
			39	1423	HIW 5KA	.85	39.68	137.34	.010	-.009	.89	2.52	-.009	10.94	29.93
			41	1422	HIW 4KA	.29	84.65	139.88	.010	-.008	.82	6.55	-.009	29.58	82.40
			42	1461	HIW 1KA	1.52	43.20	124.73	.013	-.010	.83	1.71	-.011	6.91	20.35
			44	1453	HIW 10	4.97	105.87	2.57	-.041	-.025	.61	1.69	-.026	5.30	20.44

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS (M)	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
40	1405	5	45	1402	VG 2	3.95	123.79	42.63	.025	-.016	-.63	1.27	.016	3.99	15.22
			46	1403	VG 3	3.29	129.38	43.76	-.022	-.013	.60	1.38	.013	4.05	16.38
			47	1457	HIW 3KA	2.77	128.46	42.30	-.019	-.013	-.66	1.43	.013	4.60	17.06
			48	14571	JK1	2.84	128.26	54.02	-.020	-.017	-.84	1.43	.017	6.01	17.21
			49	1454	JK 4	1.90	141.13	63.91	-.016	-.013	1.79	1.73	.013	6.79	20.73
			50	1452	HIW 2KA	2.12	147.39	69.10	-.017	-.013	-.76	1.64	.013	6.18	19.64
			51	1459	JK 3	2.41	142.71	61.06	-.018	-.013	-.71	1.52	.013	5.30	18.11
			52	1460	IN 4	2.20	143.78	66.82	-.017	-.013	-.75	1.58	.013	5.97	19.02
			53	1458	IN 1	2.54	136.66	51.28	-.019	-.013	-.68	1.51	.013	5.02	17.92
			54	1456	IN 2	2.68	141.34	55.67	-.020	-.013	-.65	1.51	.013	4.76	17.92
			55	1455	IN 3	3.02	143.36	59.58	-.022	-.013	-.60	1.51	.013	4.43	17.98
			56	1451	JK 2	2.96	148.49	66.44	-.021	-.012	-.59	1.47	.013	4.29	17.56
			57	1488	HIW 11	5.19	142.17	63.46	-.044	-.021	-.48	1.73	.022	4.32	20.83
			59	1479	DY 1	5.56	133.37	53.19	-.029	-.017	-.59	1.08	.018	3.21	12.94
			60	1471	DP 1	5.99	131.65	52.23	-.029	-.018	-.60	.99	.018	3.01	11.92
			61	1472	IB 751	6.27	131.59	52.24	-.030	-.018	-.59	.97	.018	2.90	11.61
			62	1473	IB 756	5.74	125.36	49.25	-.029	-.018	-.63	1.02	.019	3.32	12.37
			88	1404	VG 4	1.21	112.32	12.35	-.011	-.011	-.97	1.87	.011	8.77	22.22
			89	1462	HIW 9	1.87	63.42	156.50	-.018	-.011	-.60	1.94	.011	5.67	23.09
			92	1499		5.90	136.17	58.62	-.030	-.019	-.64	1.04	.020	3.40	12.57
93	1498		6.01	137.16	58.79	-.030	-.019	-.63	1.03	.020	3.29	12.41			
94	1496		6.26	136.86	58.32	-.031	-.020	-.64	1.01	.020	3.26	12.09			
95	1500	DY 2	5.74	131.18	51.49	-.029	-.019	-.66	1.03	.019	3.38	12.32			
98	1497		6.14	136.94	58.16	-.031	-.019	-.63	1.02	.020	3.21	12.22			
100	1408	VG 8	1.83	122.66	28.01	-.018	-.014	-.80	2.05	.014	7.93	24.38			
101	1490	HIW 7KA	1.41	121.67	25.46	-.018	-.015	-.86	2.59	.015	10.77	30.79			
102	1406	VG 6	.77	110.70	145.09	-.009	-.008	-.92	2.17	.008	10.84	27.20			
104	1401	VG 1	5.50	126.28	50.38	-.028	-.017	-.62	1.02	.018	3.24	12.28			
41	1422	HIW 4KA	29	1450	HIW 6	4.82	160.93	58.08	-.037	-.032	-.85	1.59	.032	6.65	18.98
			30	1469	HIW 7	4.93	117.92	32.38	-.032	-.018	-.57	1.32	.018	3.68	15.73
			31	1409	VG 9	2.83	126.92	30.24	-.022	-.018	-.80	1.62	.018	6.34	19.25
			32	1410	VG 10	4.11	133.67	46.70	-.031	-.023	-.76	1.55	.023	5.71	18.48
			33	1411	VG 11	4.68	127.54	39.36	-.035	-.024	-.69	1.56	.024	5.23	18.57
			34	1412	VG 12	5.87	131.19	42.91	-.043	-.027	-.62	1.51	.027	4.56	17.92
			37	1407	VG 7	1.46	156.34	21.80	-.016	-.015	-.94	2.17	.015	10.51	26.49
			38	1424	HIW 6KA	.35	102.31	106.40	-.005	-.004	-.84	2.57	.005	14.87	36.46
			39	1423	HIW 5KA	.67	22.14	102.94	-.007	-.007	-.87	2.28	.007	9.68	27.22
			40	1405	VG 5	-.29	84.65	139.88	-.010	-.008	-.82	6.55	.009	29.58	82.40
			42	1461	HIW 1KA	1.32	34.88	113.57	-.012	-.010	-.82	1.82	.010	7.37	21.76
			45	1402	VG 2	4.18	121.30	38.81	-.025	-.015	-.60	1.24	.015	3.69	14.87
			46	1403	VG 3	3.50	126.06	39.68	-.023	-.013	-.56	1.34	.013	3.68	15.96
			47	1457	HIW 3KA	2.98	124.63	37.35	-.020	-.012	-.61	1.39	.012	4.10	16.55
			48	14571	JK1	3.05	124.53	42.48	-.021	-.017	-.81	1.39	.017	5.48	16.55
			49	1454	JK 4	2.07	134.47	50.63	-.016	-.013	-.76	1.64	.013	6.09	19.54
			50	1452	HIW 2KA	2.27	140.91	57.21	-.017	-.013	-.75	1.57	.013	5.71	18.69
			51	1459	JK 3	2.58	137.27	52.06	-.018	-.012	-.68	1.46	.013	4.87	17.42
			52	1460	IN 4	2.36	137.79	55.27	-.017	-.013	-.74	1.52	.013	5.48	18.11
			53	1458	IN 1	2.72	131.88	44.54	-.019	-.012	-.64	1.46	.012	4.53	17.32

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
41	1422	4KA	54 1456	IN 2	2.85	136.50	49.31	.020	.012	.62	1.46	.012	4.37	17.36
			55 1455	IN 3	3.18	138.92	54.34	.023	.013	.58	1.46	.013	4.16	17.43
			56 1451	JK 2	3.10	143.71	60.53	.022	.013	.58	1.43	.013	4.09	17.03
			57 1488	HIW 11	5.35	139.57	62.08	.044	.021	.48	1.67	.023	4.27	20.26
			59 1479	DY 1	5.75	131.21	49.59	.030	.017	.58	1.07	.018	3.09	12.75
			60 1471	DP 1	6.19	129.70	48.46	.030	.018	.59	.98	.018	2.89	11.78
			61 1472	IB 751	6.47	129.73	48.60	.030	.018	.58	.96	.018	2.79	11.49
			62 1473	IB 756	5.96	123.55	45.48	.030	.018	.61	1.01	.019	3.16	12.19
			88 1404	VG 4	1.48	107.12	17.11	.012	.010	.81	1.71	.010	6.69	20.32
			89 1462	HIW 9	2.14	66.21	157.69	.020	.012	.57	1.95	.012	5.44	23.17
			92 1499		6.08	134.04	54.64	.031	.020	.64	1.03	.020	3.29	12.37
			93 1498		6.19	135.05	54.92	.031	.019	.62	1.02	.020	3.19	12.23
			94 1496		6.44	134.83	54.41	.031	.020	.64	1.00	.020	3.16	11.93
			95 1500	DY 2	5.94	129.16	47.33	.030	.019	.64	1.02	.019	3.24	12.17
			98 1497		6.33	134.87	54.36	.031	.019	.62	1.01	.020	3.11	12.05
			100 1408	VG 8	1.61	128.97	19.71	.018	.014	.79	2.24	.015	9.09	27.19
101 1490	HIW 7KA	1.19	130.02	13.56	.018	.015	.84	2.95	.015	12.89	36.04			
102 1406	VG 6	.53	124.60	164.41	.009	.006	.67	3.03	.008	15.70	43.68			
104 1401	VG 1	5.72	124.37	46.28	.028	.017	.60	1.01	.018	3.09	12.11			
42	1461	HIW IKA	30 1469	HIW 7	4.94	133.25	40.10	.032	.017	.52	1.32	.017	3.37	15.70
			31 1409	VG 9	3.16	151.50	55.03	.024	.019	.79	1.53	.019	5.88	18.22
			32 1410	VG 10	4.50	150.49	57.45	.032	.023	.73	1.47	.023	5.21	17.49
			33 1411	VG 11	4.92	143.05	47.48	.036	.025	.69	1.51	.025	5.09	17.95
			34 1412	VG 12	6.15	143.47	47.64	.043	.027	.62	1.45	.027	4.42	17.28
			37 1407	VG 7	2.43	3.91	83.59	.020	.016	.82	1.65	.016	6.69	19.75
			38 1424	HIW 6KA	1.23	19.42	91.97	.012	.009	.82	1.91	.010	7.86	23.05
			39 1423	HIW 5KA	.68	47.60	38.84	.009	.007	.82	2.17	.009	12.67	31.15
			40 1405	VG 5	1.52	43.20	124.73	.013	.010	.83	1.71	.011	6.91	20.35
			41 1422	HIW 4KA	1.32	34.88	113.57	.012	.010	.82	1.82	.010	7.37	21.76
			45 1402	VG 2	4.46	104.15	23.51	.026	.017	.66	1.18	.017	3.85	14.11
			46 1403	VG 3	3.71	105.28	23.27	.023	.015	.65	1.28	.015	4.09	15.31
			47 1457	HIW 3KA	3.26	100.82	16.86	.021	.014	.68	1.32	.014	4.42	15.76
			48 14571	JK 1	3.33	101.24	5.74	.022	.018	.83	1.34	.018	5.41	15.95
			49 1454	JK 4	2.26	99.39	12.40	.017	.015	.85	1.58	.015	6.50	18.73
			50 1452	HIW 2KA	2.29	107.27	20.99	.017	.015	.87	1.57	.015	6.61	18.70
			51 1459	JK 3	2.63	107.99	24.41	.019	.015	.80	1.45	.015	5.66	17.24
			52 1460	IN 4	2.44	105.98	19.90	.018	.015	.86	1.50	.015	6.23	17.82
			53 1458	IN 1	2.88	104.84	21.51	.020	.015	.74	1.41	.015	5.09	16.83
			54 1456	IN 2	2.89	109.98	29.13	.020	.015	.73	1.44	.015	5.19	17.17
			55 1455	IN 3	3.13	114.84	39.21	.022	.016	.71	1.43	.016	5.18	17.28
			56 1451	JK 2	2.95	118.72	45.33	.021	.015	.74	1.42	.016	5.38	17.16
			57 1488	HIW 11	5.18	125.32	57.96	.043	.022	.52	1.61	.026	5.10	20.25
			58 1446	U+U 61T	5.10	155.79	66.60	.027	.015	.56	1.10	.015	2.97	13.10
88 1404	VG 4	2.26	73.36	160.84	.016	.012	.76	1.45	.012	5.35	17.27			
89 1462	HIW 9	3.34	54.36	147.75	.024	.014	.60	1.46	.014	4.25	17.36			
100 1408	VG 8	2.15	166.59	57.93	.020	.016	.84	1.86	.017	7.81	22.40			
101 1490	HIW 7KA	1.85	175.05	63.52	.019	.017	.88	2.13	.017	9.37	25.72			
102 1406	VG 6	1.62	13.08	94.16	.013	.011	.85	1.85	.011	7.65	22.04			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
42	1461	1KA												
43	1495	HIW 15	25 1492	HIW 13	5.94	126.39	5.83	-.116	.099	.85	3.88	-.103	17.41	47.87
			90 678756	MT MYE	7.61	52.80	43.30	.069	.065	.94	1.77	.069	9.09	22.31
			97 1491	HIW 14	3.42	25.77	18.61	-.056	-.043	.78	2.63	-.056	16.24	39.90
			109 108	GRAVITY 10	3.05	88.63	53.84	-.102	.083	.82	6.08	.096	31.63	82.09
			110 111	GRAVITY 11	2.02	125.55	90.60	-.099	.083	.84	9.08	-.094	46.75	120.61
44	1453	HIW 10	3 678566	67A25	5.57	34.82	170.16	-.043	-.028	.64	1.35	.037	6.56	19.08
			40 1405	VG 5	4.97	105.87	2.57	-.041	.025	.61	1.69	.026	5.30	20.44
			45 1402	VG 2	1.71	60.64	176.61	-.039	-.022	.55	4.40	.026	15.19	56.11
			46 1403	VG 3	2.35	71.98	176.82	-.040	-.022	.56	3.40	-.026	10.06	41.32
			47 1457	HIW 3KA	2.64	82.12	176.47	-.040	-.022	.56	3.10	.022	8.49	36.95
			48 14571	JK 1	2.58	81.12	173.18	-.040	-.024	.60	3.22	-.024	9.34	38.31
			49 1454	JK 4	3.59	88.12	177.37	-.040	-.023	.57	2.32	-.023	6.38	27.61
			50 1452	HIW 2KA	3.66	83.30	176.59	-.041	-.023	.56	2.29	.023	6.21	27.18
			51 1459	JK 3	3.36	80.39	176.22	-.040	-.022	.56	2.46	.023	6.75	29.33
			52 1460	IN 4	3.50	83.12	176.23	-.040	-.023	.56	2.38	.023	6.50	28.27
			53 1458	IN 1	3.08	80.91	176.60	-.040	-.023	.56	2.68	.023	7.39	31.96
			54 1456	IN 2	3.19	76.65	176.67	-.040	-.023	.56	2.58	.023	7.33	30.94
			55 1455	IN 3	3.16	70.32	176.61	-.040	-.024	.59	2.56	.025	8.01	31.23
			56 1451	JK 2	3.44	70.14	175.64	-.040	-.023	.58	2.35	.025	7.23	28.65
			57 1488	HIW 11	3.17	30.20	34.28	-.046	-.035	.77	2.29	.046	14.37	35.24
			58 1446	U+U 611	5.77	40.29	169.08	-.040	-.025	.61	1.26	.032	5.52	17.18
			59 1479	DY 1	2.57	16.79	179.97	-.038	-.021	.56	1.84	.037	14.23	35.92
			60 1471	DP 1	2.64	6.66	178.92	-.037	-.021	.56	1.65	.037	14.03	34.60
			61 1472	IB 751	2.80	1.96	179.17	-.037	-.021	.57	1.56	.037	13.28	32.56
			62 1473	IB 756	1.97	2.90	179.63	-.038	-.020	.54	2.15	.038	19.10	46.85
			63 1474	DP 2	2.70	171.31	.34	-.037	-.022	.59	1.71	.037	13.73	33.92
			64 1443	BC 5	4.03	168.27	12.58	-.041	-.031	.77	1.69	-.039	9.78	24.86
			65 1449	BC 3	4.48	4.47	12.07	-.043	-.030	.71	1.41	-.043	9.58	23.58
			69 1468	BC 7	4.27	131.60	153.12	-.046	-.040	.87	1.95	-.045	10.51	26.18
			88 1404	VG 4	3.76	103.79	179.13	-.040	-.024	.60	2.14	-.025	6.69	26.00
			89 1462	HIW 9	3.80	125.22	176.68	-.038	-.028	.73	1.87	.032	8.47	24.51
			92 1499		2.98	13.55	177.43	-.039	-.025	.64	1.80	.038	12.68	31.81
			93 1498		3.13	12.80	177.44	-.039	-.025	.64	1.71	.038	12.07	30.21
			94 1496		3.25	8.87	176.96	-.039	-.025	.65	1.64	.038	11.78	29.22
			95 1500	DY 2	2.46	10.80	177.58	-.038	-.021	.55	1.85	.037	15.11	37.71
			98 1497		3.19	10.60	177.65	-.039	-.025	.64	1.68	.038	11.92	29.64
			99 1480	BC 13A	5.65	34.04	169.84	-.043	-.028	.65	1.32	-.037	6.48	18.75
			104 1401	VG 1	1.93	10.34	179.48	-.037	-.019	.51	2.11	.036	18.80	46.67
			105 1445	HIW 16	1.89	16.43	175.79	-.037	-.024	.64	2.83	.036	19.02	48.40

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ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM
45	1402	VG 2	37 1407 VG 7	5.45	130.18	41.41	.032	.020	.62	1.23	.020	3.67	14.58
			38 1424 HIW 6KA	4.52	119.04	35.97	.027	.016	.59	1.21	.016	3.48	14.42
			39 1423 HIW 5KA	4.13	112.01	30.92	.025	.016	.63	1.24	.016	3.90	14.87
			40 1405 VG 5	3.95	123.79	42.63	.025	.016	.63	1.27	.016	3.99	15.22
			41 1422 HIW 4KA	4.10	121.30	38.81	.025	.015	.60	1.24	.015	3.69	14.87
			42 1461 HIW 1KA	4.46	104.15	23.51	.026	.017	.66	1.18	.017	3.85	14.11
			44 1453 HIW 10	1.71	60.64	176.61	.039	.022	.55	4.40	.026	15.19	56.11
			46 1403 VG 3	.75	98.59	106.76	.010	.008	.84	2.29	.010	13.21	32.46
			47 1457 HIW 3KA	1.22	113.12	99.76	.012	.011	.95	1.91	.012	9.71	23.85
			48 14571 JK 1	1.15	112.65	119.05	.016	.011	.68	2.01	.016	14.28	35.10
			49 1454 JK 4	2.22	109.01	22.94	.017	.013	.78	1.56	.013	5.92	18.56
			50 1452 HIW 2KA	2.18	100.90	7.10	.017	.013	.77	1.59	.013	5.91	18.87
			51 1459 JK 3	1.85	98.68	179.40	.015	.013	.83	1.71	.013	6.92	20.38
			52 1460 IN 4	2.03	101.96	4.40	.016	.013	.82	1.62	.013	6.48	19.26
			53 1458 IN 1	1.59	102.91	6.22	.014	.013	.89	1.85	.013	8.02	22.04
			54 1456 IN 2	1.61	93.68	179.44	.015	.013	.85	1.89	.013	7.82	22.42
			55 1455 IN 3	1.50	81.40	154.98	.015	.013	.91	1.99	.013	8.93	23.85
			56 1451 JK 2	1.77	79.33	153.11	.015	.013	.83	1.75	.013	7.29	21.04
			57 1488 HIW 11	1.91	3.07	64.93	.039	.021	.53	3.88	.026	13.68	50.29
			58 1446 U+U 611	4.21	32.14	123.44	.022	.016	.71	1.09	.016	3.75	12.93
			59 1479 DY 1	1.78	155.04	71.36	.017	.016	.92	2.02	.016	9.02	23.96
			60 1471 DP 1	2.14	146.30	101.23	.017	.016	.95	1.58	.016	7.64	19.14
			61 1472 IB 751	2.41	144.49	88.79	.017	.016	.94	1.44	.016	6.84	17.47
			62 1473 IB 756	1.79	128.83	164.72	.017	.017	.98	1.93	.017	9.43	23.26
			63 1474 DP 2	2.64	133.93	73.93	.018	.017	.92	1.40	.017	6.52	16.93
			64 1443 BC 5	3.87	143.31	64.03	.030	.021	.71	1.58	.021	5.55	18.91
			65 1449 BC 3	3.80	162.46	49.13	.031	.022	.71	1.61	.024	6.22	19.91
			69 1468 BC 7	5.09	113.03	107.95	.039	.029	.74	1.18	.039	7.71	18.91
			88 1404 VG 4	2.77	128.78	49.64	.019	.012	.65	1.41	.013	4.61	16.96
			89 1462 HIW 9	3.44	151.98	68.40	.025	.020	.82	1.49	.020	5.94	17.69
			92 1499	2.20	158.80	102.53	.021	.018	.88	1.85	.019	8.58	22.80
			93 1498	2.35	160.08	99.88	.021	.018	.88	1.75	.019	7.95	21.40
			94 1496	2.57	157.25	103.41	.021	.018	.88	1.62	.019	7.54	20.02
			95 1500 DY 2	1.89	146.02	139.77	.018	.016	.90	1.78	.018	9.53	23.39
			98 1497	2.46	158.37	98.06	.020	.018	.88	1.67	.019	7.60	20.38
			100 1408 VG 8	5.78	123.43	37.11	.033	.020	.59	1.19	.020	3.43	14.13
			101 1490 HIW 7KA	5.36	123.23	37.30	.033	.020	.62	1.27	.020	3.80	15.06
			102 1406 VG 6	4.71	121.67	36.68	.028	.016	.58	1.20	.016	3.43	14.34
			104 1401 VG 1	1.56	132.63	118.54	.015	.014	.92	1.87	.015	9.80	24.12
			105 1445 HIW 16	3.34	37.40	113.49	.023	.016	.70	1.39	.016	4.92	16.82

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM			
46	1403	VG 3	37	1407	VG 7	4.82	134.87	42.15	.030	.018	.61	1.29	.018	3.82	15.32
			38	1424	H1W 6KA	3.83	123.92	36.53	.024	.013	.55	1.30	.013	3.48	15.40
			39	1423	H1W 5KA	3.40	114.95	31.24	.023	.014	.61	1.36	.014	4.05	16.21
			40	1405	VG 5	3.29	129.38	43.76	.022	.013	.60	1.38	.013	4.05	16.38
			41	1422	H1W 4KA	3.50	126.06	39.68	.023	.013	.56	1.34	.013	3.68	15.96
			42	1461	H1W 1KA	3.71	105.28	23.27	.023	.015	.65	1.28	.015	4.09	15.31
			44	1453	H1W 10	2.35	71.98	176.82	.040	.022	.56	3.40	.024	10.06	41.32
			45	1402	VG 2	.75	98.59	106.76	.010	.008	.84	2.29	.010	13.21	32.46
			47	1457	H1W 3KA	.53	134.19	124.02	.007	.006	.81	2.37	.007	13.96	34.39
			48	14571	JK1	.46	136.33	121.43	.014	.006	.42	2.98	.013	29.09	73.28
			49	1454	JK 4	1.48	114.28	21.39	.013	.009	.71	1.83	.009	6.31	21.79
			50	1452	H1W 2KA	1.43	102.11	4.07	.013	.009	.67	1.91	.009	6.31	22.84
			51	1459	JK 3	1.09	98.74	174.77	.012	.009	.73	2.21	.009	8.14	26.56
			52	1460	IN 4	1.28	103.95	179.72	.012	.009	.74	1.98	.009	7.38	23.79
			53	1458	IN 1	.84	106.79	179.45	.011	.009	.82	2.57	.009	10.55	30.95
			54	1456	IN 2	.87	89.42	176.59	.011	.009	.76	2.67	.009	9.90	31.73
			55	1455	IN 3	.81	65.52	153.07	.011	.010	.86	2.81	.010	11.73	33.37
			56	1451	JK 2	1.09	66.13	149.16	.012	.009	.75	2.22	.009	8.11	26.42
			57	1488	H1W 11	2.12	162.32	64.50	.040	.021	.53	3.83	.021	10.13	45.77
			58	1446	U+U 611	3.97	22.11	110.70	.021	.016	.75	1.11	.016	4.04	13.24
			59	1479	DY 1	2.29	139.12	50.66	.019	.017	.85	1.75	.017	7.23	20.79
			60	1471	DP 1	2.71	134.42	45.84	.019	.017	.90	1.42	.017	6.17	16.89
			61	1472	IB 751	2.98	134.04	48.87	.019	.017	.88	1.32	.017	5.64	15.71
			62	1473	IB 756	2.47	120.00	31.71	.019	.017	.90	1.60	.017	6.93	18.96
			63	1474	DP 2	3.29	126.31	48.17	.020	.017	.86	1.27	.018	5.36	15.12
			64	1443	BC 5	4.44	136.45	58.94	.031	.021	.69	1.43	.022	4.95	17.17
			65	1449	BC 3	4.19	153.17	47.07	.032	.022	.67	1.56	.023	5.43	18.89
			88	1404	VG 4	2.16	138.88	51.51	.016	.009	.56	1.53	.009	4.19	18.18
			89	1462	H1W 9	3.05	163.40	72.00	.023	.019	.85	1.54	.019	6.36	18.26
			92	1499		2.66	144.58	78.88	.021	.019	.91	1.60	.019	7.29	19.22
			93	1498		2.79	146.36	76.88	.021	.019	.90	1.53	.019	6.87	18.41
94	1496		3.03	144.99	79.53	.021	.019	.91	1.43	.020	6.54	17.24			
95	1500	DY 2	2.45	133.59	15.24	.019	.018	.95	1.57	.018	7.40	18.82			
98	1497		2.92	145.48	73.87	.021	.019	.90	1.47	.019	6.56	17.65			
100	1408	VG 8	5.11	126.98	37.41	.031	.018	.58	1.28	.018	3.55	14.93			
101	1490	H1W 7KA	4.69	127.06	37.63	.031	.019	.61	1.35	.019	3.99	16.06			
102	1406	VG 6	4.02	125.87	37.21	.025	.014	.55	1.28	.014	3.45	15.24			
104	1401	VG 1	2.22	121.71	41.18	.017	.016	.94	1.56	.016	7.11	18.55			
105	1445	H1W 16	3.76	47.50	114.48	.023	.018	.77	1.24	.019	5.01	15.23			
47	1457	H1W 3KA	31	1409	VG 9	5.81	125.74	35.22	.032	.020	.64	1.14	.020	3.52	13.53
			37	1407	VG 7	4.30	134.96	40.87	.028	.018	.65	1.33	.018	4.20	15.88
			38	1424	H1W 6KA	3.31	122.30	33.69	.021	.013	.59	1.34	.013	3.83	15.89
			39	1423	H1W 5KA	2.91	111.54	26.65	.020	.013	.65	1.42	.013	4.49	16.87
			40	1405	VG 5	2.77	128.46	42.30	.019	.013	.66	1.43	.013	4.60	17.06
			41	1422	H1W 4KA	2.98	124.63	37.35	.020	.012	.61	1.39	.012	4.10	16.55
			42	1461	H1W 1KA	3.26	100.82	16.86	.021	.014	.68	1.32	.014	4.42	15.76
			44	1453	H1W 10	2.64	82.12	176.47	.040	.022	.56	3.10	.022	8.49	34.95

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
47	1457	3KA	45 1402	VG 2	1.22	113.12	99.76	-012	-011	.95	1.91	.012 9.71 23.85
			46 1403	VG 3	.53	134.19	124.02	-007	-006	.81	2.37	.007 13.96 34.39
			48 14571	JK1	.07	120.62	120.62	-011	-001	.10	3.18	.011 158.11 387.38
			49 1454	JK 4	1.01	104.04	12.16	-010	-007	.70	2.05	.007 6.96 24.39
			50 1452	H1W 2KA	1.03	86.34	172.51	-011	-006	.60	2.14	.006 6.28 25.42
			51 1459	JK 3	.73	74.13	160.01	-010	-006	.65	2.69	.006 8.48 31.96
			52 1460	IN 4	.87	86.16	163.96	-010	-007	.67	2.31	.007 7.86 27.83
			53 1458	IN 1	.44	73.71	167.99	-008	-006	.78	3.74	.006 14.22 44.42
			54 1456	IN 2	.62	52.58	168.78	-009	-007	.78	2.81	.007 11.71 34.75
			55 1455	IN 3	.79	27.34	109.29	-009	-008	.88	2.38	.008 10.25 28.33
			56 1451	JK 2	1.02	37.46	127.99	-010	-007	.68	2.05	.007 6.75 24.31
			57 1488	H1W 11	2.59	156.83	65.15	-040	-021	.53	3.17	.021 8.15 37.62
			58 1446	U#U 611	4.19	15.44	104.54	-022	-015	.69	1.10	.015 3.67 13.02
			59 1479	DY 1	2.81	138.20	54.31	-020	-017	.83	1.50	.017 6.04 17.83
			60 1471	DP 1	3.23	134.38	51.85	-020	-017	.86	1.26	.017 5.31 15.01
			61 1472	IB 751	3.51	134.06	53.06	-020	-017	.85	1.19	.017 4.92 14.18
			62 1473	IB 756	2.98	122.47	40.23	-020	-018	.88	1.38	.018 5.93 16.47
			63 1474	DP 2	3.81	127.39	51.05	-021	-018	.83	1.15	.018 4.75 13.79
			64 1443	BC 5	4.96	136.21	58.96	-032	-022	.67	1.31	.022 4.48 15.81
			65 1449	BC 3	4.69	151.08	48.46	-033	-022	.66	1.44	.023 4.83 17.31
			88 1404	VG 4	1.63	140.38	51.52	-013	-008	.62	1.61	.008 4.87 19.10
			89 1462	H1W 9	2.60	169.05	88.94	-021	-019	.91	1.63	.019 7.28 19.45
			92 1499		3.18	142.87	75.99	-022	-019	.88	1.39	.020 6.17 16.76
			93 1498		3.31	144.44	74.63	-022	-019	.87	1.34	.019 5.86 16.21
			94 1496		3.55	143.40	75.57	-022	-020	.88	1.27	.020 5.64 15.36
			95 1500	DY 2	2.98	133.70	40.46	-020	-019	.94	1.36	.019 6.23 16.19
			98 1497		3.43	143.76	72.18	-022	-019	.87	1.30	.019 5.63 15.65
			100 1408	VG 8	4.59	126.15	35.45	-029	-018	.61	1.30	.018 3.86 15.45
			101 1490	H1W 7KA	4.17	126.17	35.54	-029	-018	.64	1.41	.018 4.38 16.76
			102 1406	VG 6	3.51	126.63	34.57	-022	-013	.59	1.32	.013 3.79 15.71
104 1401	VG 1	2.74	124.08	49.74	-018	-016	.90	1.35	.016 5.99 16.10			
105 1445	H1W 16	3.83	55.37	114.47	-024	-019	.78	1.21	.020 5.23 15.14			
48	14571	JK1	31 1409	VG 9	5.88	125.68	36.19	-032	-023	.72	1.14	.023 3.98 13.50
			37 1407	VG 7	4.37	134.72	44.10	-028	-021	.75	1.34	.021 4.86 15.86
			38 1424	H1W 6KA	3.38	122.27	35.45	.022	-017	.78	1.33	.017 5.04 15.86
			39 1423	H1W 5KA	2.98	111.76	22.51	-020	-017	.84	1.42	.017 5.79 16.83
			40 1405	VG 5	2.84	128.26	54.02	-020	-017	.84	1.43	.017 6.01 17.21
			41 1422	H1W 4KA	3.05	124.53	42.48	-021	-017	.81	1.39	.017 5.48 16.55
			42 1461	H1W 1KA	3.33	101.24	5.74	.022	-018	.83	1.34	.018 5.41 15.95
			44 1453	H1W 10	2.58	81.12	173.18	-040	-024	.60	3.22	.024 9.34 38.31
			45 1402	VG 2	1.15	112.65	119.05	-016	-011	.68	2.01	.016 14.28 35.10
			46 1403	VG 3	.46	136.33	121.43	-014	-006	.42	2.98	.013 29.09 73.28
			47 1457	H1W 3KA	.07	120.62	120.62	-011	-001	.10	3.18	.011 158.11 387.38
			49 1454	JK 4	1.08	105.14	132.61	-014	-010	.74	2.11	.013 12.13 31.29
			50 1452	H1W 2KA	1.09	88.49	138.86	-015	-009	.63	2.40	.012 10.72 32.86
			51 1459	JK 3	.78	77.97	132.29	-014	-008	.54	3.30	.011 13.41 44.98
			52 1460	IN 4	.93	88.70	133.20	-014	-008	.58	2.63	.012 12.84 38.27
53 1458	IN 1	.50	79.84	127.27	-014	-007	.55	4.66	.011 21.61 67.05			

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CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM	
48	14571	54	1456	IN 2	.65	58.53	128.87	.014	.008	.58	4.26	.009 13.76 52.63	
		55	1455	IN 3	.79	32.59	120.90	.015	.008	.56	3.02	.008 10.40 45.33	
		56	1451	JK 2	1.03	41.48	124.37	.015	.007	.47	3.04	.007 7.13 36.38	
		57	1488	HIW 11	2.53	157.80	68.26	.040	.023	.57	3.28	.023 9.13 38.99	
		58	1446	U+U 611	4.17	16.40	110.72	.025	.016	.63	1.23	.016 3.79 14.60	
		59	1479	DY 1	2.74	138.66	88.42	.022	.019	.89	1.55	.020 7.37 19.32	
		60	1471	DP 1	3.16	134.69	97.93	.021	.019	.90	1.30	.020 6.47 16.43	
		61	1472	IB 751	3.44	134.34	92.52	.022	.019	.90	1.22	.021 5.99 15.36	
		62	1473	IB 756	2.91	122.52	107.06	.021	.020	.94	1.41	.021 7.24 17.82	
		63	1474	DP 2	3.73	127.52	84.84	.022	.020	.90	1.17	.021 5.72 14.64	
		64	1443	BC 5	4.89	136.44	65.37	.032	.024	.73	1.34	.025 5.07 16.26	
		65	1449	BC 3	4.63	151.53	52.51	.033	.025	.74	1.47	.025 5.36 17.61	
		88	1404	VG 4	1.70	139.56	92.20	.015	.012	.80	1.66	.013 7.91 21.59	
		89	1462	HIW 9	2.65	167.88	108.38	.023	.020	.84	1.75	.021 7.77 21.59	
		92	1499		3.11	143.38	102.65	.024	.020	.84	1.44	.022 7.17 18.76	
		93	1498		3.24	144.96	100.43	.024	.020	.84	1.40	.022 6.80 18.04	
		94	1496		3.48	143.86	101.88	.024	.021	.85	1.32	.023 6.51 17.07	
		95	1500	DY 2	2.91	134.02	118.00	.022	.020	.90	1.40	.022 7.45 18.40	
		98	1497		3.37	144.25	99.11	.024	.020	.85	1.35	.022 6.55 17.33	
		100	1408	VG 8	4.66	126.07	36.78	.029	.021	.72	1.30	.021 4.52 15.40	
		101	1490	HIW 7KA	4.24	126.07	37.06	.029	.022	.75	1.41	.022 5.08 16.69	
102	1406	VG 6	3.58	124.54	36.60	.023	.018	.76	1.32	.018 4.89 15.68			
104	1401	VG 1	2.67	124.18	110.73	.020	.018	.88	1.38	.020 7.50 18.49			
105	1445	HIW 16	3.80	54.38	116.94	.026	.019	.71	1.35	.020 5.38 16.94			
49	1454	JK 4	31	1409	VG 9	4.89	130.11	39.12	.029	.021	.71	1.23	.021 4.25 14.65
			32	1410	VG 10	6.17	133.94	45.81	.036	.025	.70	1.22	.025 4.13 14.45
			37	1407	VG 7	3.47	143.52	49.17	.025	.018	.74	1.47	.018 5.27 17.44
			38	1424	HIW 6KA	2.38	129.92	42.47	.018	.013	.74	1.53	.013 5.53 18.20
			39	1423	HIW 5KA	1.92	115.47	32.32	.016	.013	.83	1.75	.014 7.05 20.78
			40	1405	VG 5	1.90	141.13	63.91	.016	.013	.79	1.73	.013 6.79 20.73
			41	1422	HIW 4KA	2.07	134.47	50.63	.016	.013	.76	1.64	.013 6.09 19.54
			42	1461	HIW 1KA	2.26	99.39	12.40	.017	.015	.85	1.58	.015 6.50 18.73
			44	1453	HIW 10	3.59	88.12	177.37	.040	.023	.57	2.32	.023 6.38 27.61
			45	1402	VG 2	2.22	109.01	22.94	.017	.013	.78	1.56	.013 5.92 18.56
			46	1403	VG 3	1.48	114.28	21.39	.013	.009	.71	1.83	.009 6.31 21.79
			47	1457	HIW 3KA	1.01	104.04	12.16	.010	.007	.70	2.05	.007 6.96 24.39
			48	14571	JK 1	1.08	105.14	132.61	.014	.010	.74	2.11	.013 12.13 31.29
			50	1452	HIW 2KA	.31	8.70	92.45	.005	.004	.91	3.23	.004 14.26 38.41
			51	1459	JK 3	.52	148.45	144.07	.006	.006	.92	2.26	.006 11.96 29.31
			52	1460	IN 4	.32	159.56	139.63	.005	.004	.85	2.67	.005 14.61 36.37
			53	1458	IN 1	.66	123.76	20.57	.008	.006	.75	2.50	.006 9.34 29.98
			54	1456	IN 2	.79	141.84	37.95	.009	.006	.69	2.37	.007 8.33 28.56
			55	1455	IN 3	1.13	147.10	54.24	.012	.008	.64	2.26	.008 7.07 26.81
			56	1451	JK 2	1.11	161.14	71.77	.011	.006	.60	1.97	.006 5.69 23.38
			57	1488	HIW 11	3.30	142.76	64.15	.041	.021	.52	2.50	.022 6.74 30.15
58	1446	U+U 611	4.29	1.86	88.80	.023	.015	.66	1.11	.015 3.58 13.24			
59	1479	DY 1	3.69	129.39	46.79	.023	.017	.75	1.29	.017 4.69 15.32			
60	1471	DP 1	4.13	127.31	63.95	.023	.017	.77	1.13	.017 6.21 12.63			

DEPARTMENT OF ENERGY, MINES, AND RESOURCES
 GEODETIC SURVEY OF CANADA PROGRAM GANET

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CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
49	1454	4	61	1472	IB 751	4.41	127.50	44.85	.023	.017	.75	1.08	.018	3.98	12.86
			62	1473	IB 756	3.95	117.85	37.72	.023	.018	.78	1.19	.018	4.56	14.16
			63	1474	DP 2	4.75	122.57	43.63	.024	.018	.75	1.04	.018	3.88	12.50
			64	1443	BC 5	5.84	130.95	54.62	.034	.022	.64	1.18	.023	3.89	14.29
			65	1449	BC 3	5.42	143.27	46.95	.035	.022	.62	1.33	.022	4.06	15.89
			88	1404	VG 4	1.02	176.25	95.38	.010	.008	.76	2.12	.008	7.88	25.26
			89	1462	HIW 9	2.36	11.75	121.31	.021	.017	.81	1.81	.018	7.43	21.92
			92	1499		4.01	133.82	57.39	.024	.020	.82	1.21	.020	4.94	14.55
			93	1498		4.12	135.34	57.69	.024	.019	.81	1.19	.020	4.75	14.26
			94	1496		4.37	135.01	56.85	.024	.020	.82	1.14	.020	4.62	13.67
			95	1500	DY 2	3.89	126.33	38.50	.023	.019	.83	1.20	.019	4.81	14.20
			98	1497		4.26	135.07	56.33	.024	.019	.80	1.16	.020	4.59	13.90
			100	1408	VG 8	3.68	132.06	39.85	.026	.018	.70	1.44	.018	4.94	17.16
			101	1490	HIW 7KA	3.26	132.84	40.58	.025	.019	.74	1.60	.019	5.74	19.03
			102	1406	VG 6	2.59	132.48	42.77	.019	.014	.74	1.49	.014	5.31	17.70
104	1401	VG 1	3.70	118.74	39.73	.021	.017	.79	1.16	.017	4.55	13.91			
105	1445	HIW 16	4.55	64.93	115.71	.024	.021	.87	1.04	.022	4.90	12.95			
50	1452	HIW 2KA	31	1409	VG 9	5.06	133.14	41.94	.030	.021	.71	1.21	.021	4.18	14.37
			32	1410	VG 10	6.36	136.25	47.38	.037	.026	.70	1.19	.026	4.03	14.19
			37	1407	VG 7	3.70	146.96	53.08	.025	.019	.73	1.41	.019	5.02	16.81
			38	1424	HIW 6KA	2.55	135.95	48.97	.018	.014	.74	1.48	.014	5.30	17.59
			39	1423	HIW 5KA	2.03	123.96	41.55	.017	.014	.83	1.69	.014	6.86	20.18
			40	1405	VG 5	2.12	147.39	69.10	.017	.013	.76	1.64	.013	6.18	19.64
			41	1422	HIW 4KA	2.27	140.91	57.21	.017	.013	.75	1.57	.013	5.71	18.69
			42	1461	HIW 1KA	2.29	107.27	20.99	.017	.015	.87	1.57	.015	6.61	18.70
			44	1453	HIW 10	3.66	83.30	176.59	.041	.023	.56	2.29	.023	6.21	27.18
			45	1402	VG 2	2.18	100.90	7.10	.017	.013	.77	1.59	.013	5.91	18.87
			46	1403	VG 3	1.43	102.11	4.07	.013	.009	.67	1.91	.009	6.31	22.84
			47	1457	HIW 3KA	1.03	86.34	172.51	.011	.006	.60	2.14	.006	6.28	25.42
			48	14571	JK1	1.09	88.49	138.86	.015	.009	.63	2.40	.012	10.72	32.86
			49	1454	JK 4	.31	8.70	92.45	.005	.004	.91	3.23	.004	14.26	38.41
			51	1459	JK 3	.35	112.79	151.06	.007	.005	.76	3.36	.006	17.35	46.50
			52	1460	IN 4	.16	87.28	85.68	.005	.003	.62	3.62	.005	28.31	69.38
			53	1458	IN 1	.60	95.60	178.56	.009	.006	.69	3.00	.006	10.21	35.75
			54	1456	IN 2	.62	120.08	16.26	.009	.006	.68	3.04	.006	10.50	36.62
			55	1455	IN 3	.92	134.00	38.56	.011	.008	.72	2.58	.008	8.99	30.67
			56	1451	JK 2	.84	151.25	56.56	.009	.007	.76	2.22	.007	8.25	26.40
			57	1488	HIW 11	3.09	138.58	63.88	.040	.021	.53	2.62	.023	7.52	31.91
			58	1446	U+U 611	3.98	1.32	89.04	.022	.016	.70	1.14	.016	3.91	13.60
			59	1479	DY 1	3.54	125.02	40.81	.022	.017	.77	1.31	.017	4.92	15.56
60	1471	DP 1	3.99	123.36	36.57	.022	.017	.79	1.14	.017	4.36	13.55			
61	1472	IB 751	4.26	123.81	38.07	.023	.018	.78	1.09	.018	4.12	12.95			
62	1473	IB 756	3.86	113.45	29.75	.022	.018	.80	1.20	.018	4.64	14.24			
63	1474	DP 2	4.63	119.02	37.41	.024	.018	.77	1.05	.018	3.98	12.52			
64	1443	BC 5	5.68	128.27	52.78	.033	.022	.66	1.19	.023	4.05	14.42			
65	1449	BC 3	5.21	140.82	44.82	.035	.022	.63	1.37	.022	4.22	16.32			
88	1404	VG 4	1.33	179.17	98.33	.012	.008	.70	1.84	.008	6.35	22.06			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
50	1452	2KA	92	1499	3.84	129.99	51.09	.023	.020	.86	1.23	.020	5.19	14.72	
			93	1498	3.94	131.68	51.95	.023	.020	.84	1.21	.020	5.00	14.43	
			94	1496	4.19	131.55	50.47	.024	.020	.85	1.16	.020	4.84	13.81	
			95	1500	DY 2	3.75	122.09	28.10	.022	.019	.84	1.22	.019	4.96	14.45
			98	1497	4.08	131.52	50.46	.023	.020	.84	1.18	.020	4.82	14.06	
			100	1408	VG 8	3.86	135.95	43.50	.026	.019	.71	1.40	.019	4.82	16.68
			101	1490	HIW 7KA	3.44	137.16	44.68	.026	.019	.74	1.55	.019	5.55	18.38
			102	1406	VG 6	2.78	137.86	48.83	.019	.014	.73	1.44	.014	5.10	17.11
			104	1401	VG 1	3.61	114.05	29.93	.021	.017	.81	1.17	.017	4.65	13.96
			105	1445	HIW 16	4.73	61.77	124.27	.024	.021	.85	1.03	.022	4.55	12.57
51	1459	JK 3	31	1409	5.39	131.85	41.21	.031	.021	.68	1.17	.021	3.87	13.90	
			32	1410	VG 10	6.68	135.06	46.46	.038	.025	.68	1.16	.025	3.81	13.76
			37	1407	VG 7	3.99	144.16	50.47	.026	.018	.69	1.36	.018	4.58	16.18
			38	1424	HIW 6KA	2.88	133.23	45.75	.019	.013	.67	1.40	.013	4.56	16.59
			39	1423	HIW 5KA	2.37	122.34	39.05	.018	.013	.76	1.54	.014	5.72	18.40
			40	1405	VG 5	2.41	142.71	61.06	.018	.013	.71	1.52	.013	5.30	18.11
			41	1422	HIW 4KA	2.58	137.27	52.06	.018	.012	.68	1.48	.013	4.87	17.42
			42	1461	HIW 1KA	2.63	107.99	24.41	.019	.015	.80	1.45	.015	5.66	17.24
			44	1453	HIW 10	3.36	80.39	176.22	.040	.022	.56	2.46	.023	6.75	29.33
			45	1402	VG 2	1.85	98.68	179.40	.015	.013	.83	1.71	.013	6.92	20.38
			46	1403	VG 3	1.09	98.74	174.77	.012	.009	.73	2.21	.009	8.14	26.56
			47	1457	HIW 3KA	.73	74.13	160.01	.010	.006	.65	2.69	.006	8.48	31.96
			48	14571	JK1	.78	77.97	132.29	.014	.008	.54	3.30	.011	13.41	44.98
			49	1454	JK 4	.52	148.45	144.07	.006	.006	.92	2.26	.006	11.96	29.31
			50	1452	HIW 2KA	.35	112.79	151.06	.007	.005	.76	3.36	.006	17.35	46.50
			52	1460	IN 4	.21	131.59	135.95	.006	.003	.41	2.56	.006	29.50	72.45
			53	1458	IN 1	.29	74.76	165.12	.008	.005	.64	5.73	.005	17.91	68.11
			54	1456	IN 2	.28	129.28	179.89	.008	.005	.67	5.38	.007	24.22	72.59
			55	1455	IN 3	.61	145.94	32.72	.010	.008	.86	3.29	.009	14.32	39.88
			56	1451	JK 2	.61	171.92	120.68	.007	.007	.93	2.34	.007	11.15	28.58
			57	1488	HIW 11	2.78	141.70	64.31	.040	.021	.53	2.91	.022	8.08	35.17
			58	1446	U+U 611	3.86	6.13	94.62	.021	.015	.71	1.15	.015	3.95	13.62
			59	1479	DY 1	3.20	126.33	42.65	.021	.017	.80	1.38	.017	5.39	16.41
			60	1471	DP 1	3.65	124.36	37.61	.021	.017	.82	1.18	.017	4.72	14.05
			61	1472	IB 751	3.92	124.78	39.45	.021	.017	.81	1.12	.017	4.43	13.36
			62	1473	IB 756	3.51	113.52	29.40	.021	.018	.83	1.25	.018	5.05	14.88
			63	1474	DP 2	4.28	119.53	38.86	.023	.018	.80	1.08	.018	4.26	12.89
			64	1443	BC 5	5.35	129.27	54.26	.033	.022	.67	1.23	.023	4.26	14.94
			65	1449	BC 3	4.91	142.72	45.27	.034	.022	.64	1.42	.022	4.48	16.91
			88	1404	VG 4	1.50	166.91	83.22	.012	.008	.65	1.66	.008	5.34	19.84
			89	1462	HIW 9	2.76	4.32	109.87	.022	.018	.81	1.61	.018	6.52	19.35
92	1499	3.51	131.67	56.41	.022	.020	.89	1.29	.020	5.63	15.39				
93	1498	3.62	133.47	56.85	.022	.019	.87	1.26	.020	5.40	15.03				
94	1496	3.87	133.21	55.46	.023	.020	.89	1.20	.020	5.21	14.31				
95	1500	DY 2	3.41	123.03	26.04	.021	.018	.88	1.27	.018	5.41	15.12			
98	1497	3.75	133.22	54.71	.022	.019	.87	1.22	.019	5.19	14.60				
100	1408	VG 8	4.18	134.08	42.52	.027	.018	.67	1.35	.018	4.36	15.98			
101	1490	HIW 7KA	3.76	134.98	43.41	.027	.019	.70	1.67	.019	4.98	17.47			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ SEC	AZ	DIST M	R.A. PPM		
51	1459	3	102 1406	VG 6	3.09	135.13	45.94	.021	.014	.67	1.37	.014	4.45	16.25
			104 1401	VG 1	3.26	114.19	29.89	.019	.017	.85	1.22	.017	5.08	14.55
			105 1445	H1W 16	4.52	58.35	121.29	.024	.020	.82	1.06	.021	4.58	13.05
52	1460	IN 4	31 1409	VG 9	5.17	131.86	41.28	.030	.021	.71	1.19	.021	4.08	14.16
			32 1410	VG 10	6.47	135.18	46.87	.037	.026	.69	1.18	.026	3.97	14.01
			37 1407	VG 7	3.78	144.87	51.83	.026	.019	.72	1.39	.019	4.90	16.58
			38 1424	H1W 6KA	2.66	133.36	47.30	.019	.014	.73	1.44	.014	5.09	17.09
			39 1423	H1W 5KA	2.16	121.43	39.68	.017	.014	.82	1.61	.014	6.46	19.22
			40 1405	VG 5	2.20	143.78	66.82	.017	.013	.75	1.58	.013	5.97	19.02
			41 1422	H1W 4KA	2.36	137.79	55.27	.017	.013	.74	1.52	.013	5.48	18.11
			42 1461	H1W 1KA	2.44	105.98	19.90	.018	.015	.86	1.50	.015	6.23	17.82
			44 1453	H1W 10	3.50	83.12	176.23	.040	.023	.56	2.38	.023	6.50	28.27
			45 1402	VG 2	2.03	101.96	4.40	.016	.013	.82	1.62	.013	6.48	19.26
			46 1403	VG 3	1.28	103.95	179.72	.012	.009	.74	1.98	.009	7.38	23.79
			47 1457	H1W 3KA	.87	86.16	163.96	.010	.007	.67	2.31	.007	7.86	27.83
			48 14571	JK 1	.93	88.70	133.20	.014	.008	.58	2.63	.012	12.84	38.27
			49 1454	JK 4	.32	159.56	139.63	.005	.004	.85	2.67	.005	14.61	36.37
			50 1452	H1W 2KA	.16	87.28	85.68	.005	.003	.62	3.62	.005	28.31	69.38
			51 1459	JK 3	.21	131.59	135.95	.006	.003	.41	2.56	.006	29.50	72.45
			53 1458	IN 1	.44	98.59	165.35	.008	.006	.71	3.63	.006	13.91	44.87
			54 1456	IN 2	.49	130.29	4.77	.008	.006	.77	3.25	.007	14.50	41.61
			55 1455	IN 3	.82	142.21	45.87	.011	.009	.81	2.67	.009	10.59	31.82
			56 1451	JK 2	.79	161.78	87.41	.008	.007	.82	2.18	.007	8.94	26.16
			57 1488	H1W 11	2.99	140.98	64.50	.040	.021	.53	2.71	.023	7.62	32.87
			58 1446	U+U 611	3.99	3.62	92.86	.022	.015	.69	1.14	.015	3.83	13.59
			59 1479	DY 1	3.41	126.66	43.95	.022	.017	.79	1.32	.018	5.14	15.78
			60 1471	DP 1	3.86	124.76	39.51	.022	.018	.82	1.15	.018	4.55	13.64
			61 1472	IB 751	4.14	125.13	41.05	.022	.018	.80	1.09	.018	4.28	13.03
			62 1473	IB 756	3.71	114.54	31.53	.022	.018	.82	1.21	.018	4.87	14.41
			63 1474	DP 2	4.49	120.10	40.10	.023	.018	.80	1.06	.019	4.13	12.60
64 1443	BC 5	5.56	129.36	54.34	.033	.022	.67	1.21	.023	4.14	14.59			
65 1449	BC 3	5.12	142.26	45.75	.034	.022	.64	1.38	.022	4.33	16.44			
88 1404	VG 4	1.33	172.26	95.28	.012	.008	.67	1.82	.008	6.19	21.88			
89 1462	H1W 9	2.64	8.02	115.60	.022	.017	.79	1.68	.018	6.72	20.35			
92 1499		3.72	131.66	57.40	.023	.020	.87	1.24	.020	5.38	14.92			
93 1498		3.83	133.36	57.70	.023	.020	.86	1.22	.020	5.17	14.60			
94 1496		4.08	133.12	56.45	.023	.020	.87	1.17	.020	5.00	13.94			
95 1500	DY 2	3.62	123.53	29.68	.022	.019	.87	1.23	.019	5.19	14.57			
98 1497		3.97	133.14	55.75	.023	.020	.85	1.19	.020	4.98	14.20			
100 1408	VG 8	3.96	134.22	42.70	.026	.019	.70	1.38	.019	4.67	16.38			
101 1490	H1W 7KA	3.55	135.18	43.75	.026	.019	.73	1.52	.019	5.37	18.00			
102 1406	VG 6	2.88	135.40	47.20	.020	.014	.72	1.41	.014	4.92	16.70			
104 1401	VG 1	3.46	115.25	32.55	.020	.017	.85	1.18	.017	4.89	14.09			
105 1445	H1W 16	4.59	60.91	121.38	.024	.020	.83	1.05	.021	4.64	12.98			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
53	I458	IN 1	31	I409	VG 9	5.55	129.35	38.51	.031	.021	.66	1.16	.021	3.71	13.83
			32	I410	VG 10	6.83	132.96	44.29	.038	.025	.67	1.15	.025	3.72	13.66
			37	I407	VG 7	4.10	140.39	45.83	.027	.018	.67	1.36	.018	4.43	16.19
			38	I424	HIW 6KA	3.04	128.58	39.76	.020	.013	.63	1.39	.013	4.23	16.53
			39	I423	HIW 5KA	2.57	117.59	32.91	.019	.013	.70	1.51	.013	5.15	18.03
			40	I405	VG 5	2.54	136.66	51.28	.019	.013	.68	1.51	.013	5.02	17.92
			41	I422	HIW 4KA	2.72	131.88	44.54	.019	.012	.64	1.46	.012	4.53	17.32
			42	I461	HIW 1KA	2.88	104.84	21.51	.020	.015	.74	1.41	.015	5.09	16.83
			44	I453	HIW 10	3.08	80.91	176.60	.040	.023	.56	2.68	.023	7.39	31.96
			45	I402	VG 2	1.59	102.91	6.22	.014	.013	.89	1.85	.013	8.02	22.04
			46	I403	VG 3	.84	106.79	179.45	.011	.009	.82	2.57	.009	10.55	30.95
			47	I457	HIW 3KA	.44	73.71	167.99	.008	.006	.78	3.74	.006	14.22	44.42
			48	I4571	JK 1	.50	79.84	127.27	.014	.007	.55	4.66	.011	21.61	67.05
			49	I454	JK 4	.66	123.76	20.57	.008	.006	.75	2.50	.006	9.34	29.98
			50	I452	HIW 2KA	.60	95.60	178.56	.009	.006	.69	3.00	.006	10.21	35.75
			51	I459	JK 3	.29	74.76	165.12	.008	.005	.64	5.73	.005	17.91	68.11
			52	I460	IN 4	.44	98.59	165.35	.008	.006	.71	3.63	.006	13.91	44.87
			54	I456	IN 2	.26	14.48	12.13	.005	.003	.67	2.65	.005	19.05	46.70
			55	I455	IN 3	.58	173.92	84.59	.008	.007	.86	2.90	.007	12.10	34.42
			56	I451	JK 2	.71	15.76	112.20	.008	.006	.75	2.18	.006	7.94	25.96
			57	I488	HIW 11	2.68	147.39	64.42	.040	.021	.53	3.06	.022	8.07	36.53
			58	I446	U+U 611	3.98	10.00	97.54	.022	.016	.71	1.13	.016	3.92	13.45
			59	I479	DY 1	3.03	130.61	46.35	.021	.017	.81	1.45	.017	5.68	17.23
			60	I471	DP 1	3.47	127.99	42.07	.021	.017	.83	1.23	.017	4.98	14.64
			61	I472	IB 751	3.75	128.16	43.74	.021	.017	.82	1.17	.017	4.65	13.88
			62	I473	IB 756	3.29	116.66	33.40	.021	.018	.84	1.32	.018	5.40	15.70
			63	I474	DP 2	4.08	122.38	42.90	.022	.018	.81	1.12	.018	4.47	13.39
			64	I443	BC 5	5.18	131.87	55.81	.033	.022	.67	1.27	.023	4.36	15.38
			65	I449	BC 3	4.80	145.92	46.33	.034	.022	.65	1.44	.022	4.63	17.20
			88	I404	VG 4	1.52	155.95	66.17	.012	.008	.65	1.68	.008	5.31	19.93
			89	I462	HIW 9	2.68	178.51	102.30	.021	.018	.87	1.62	.019	6.94	19.43
			92	I499		3.36	135.79	62.26	.022	.020	.89	1.34	.020	5.88	16.09
			93	I498		3.48	137.53	62.14	.022	.019	.87	1.31	.020	5.62	15.66
			94	I496		3.72	137.00	61.55	.023	.020	.88	1.24	.020	5.41	14.86
			95	I500	DY 2	3.22	126.86	30.70	.021	.019	.89	1.33	.019	5.76	15.79
			98	I497		3.61	137.13	59.92	.022	.019	.87	1.27	.019	5.40	15.17
			100	I408	VG 8	4.33	130.80	39.25	.028	.018	.64	1.34	.018	4.14	15.89
			101	I490	HIW 7KA	3.91	131.31	39.71	.028	.018	.67	1.46	.018	4.72	17.33
			102	I406	VG 6	3.25	130.70	40.33	.022	.013	.63	1.37	.013	4.15	16.24
			104	I401	VG 1	3.04	117.64	36.05	.019	.017	.87	1.29	.017	5.45	15.38
			105	I445	HIW 16	4.25	57.25	117.58	.024	.020	.82	1.11	.021	4.88	13.81

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54	1456	IN 2	31 1409 VG 9	5.66	131.73	41.24	.032	.021	.65	1.16	.021	3.67	13.81
			32 1410 VG 10	6.95	134.83	45.91	.039	.025	.66	1.14	.025	3.65	13.59
			37 1407 VG 7	4.26	143.21	49.02	.028	.018	.65	1.35	.018	4.29	16.05
			38 1424 HIW 6KA	3.15	132.88	44.62	.021	.013	.61	1.40	.013	4.14	16.59
			39 1423 HIW 5KA	2.65	123.06	39.37	.020	.013	.68	1.53	.014	5.11	18.23
			40 1405 VG 5	2.68	141.34	55.67	.020	.013	.65	1.51	.013	4.76	17.92
			41 1422 HIW 4KA	2.85	136.50	49.31	.020	.012	.62	1.46	.012	4.37	17.36
			42 1461 HIW 1KA	2.89	109.98	29.13	.020	.015	.73	1.44	.015	5.19	17.17
			44 1453 HIW 10	3.19	76.65	176.67	.040	.023	.56	2.58	.023	7.33	30.94
			45 1402 VG 2	1.61	93.68	179.44	.015	.013	.85	1.89	.013	7.82	22.42
			46 1403 VG 3	.87	89.42	176.59	.011	.009	.76	2.67	.009	9.90	31.73
			47 1457 HIW 3KA	.62	52.58	168.78	.009	.007	.78	2.81	.007	11.71	34.75
			48 14571 JK 1	.65	58.53	128.87	.014	.008	.58	4.26	.009	13.76	52.63
			49 1454 JK 4	.79	141.84	37.95	.009	.006	.69	2.37	.007	8.33	28.56
			50 1452 HIW 2KA	.62	120.08	16.26	.009	.006	.68	3.04	.006	10.50	36.62
			51 1459 JK 3	.28	129.28	179.89	.008	.005	.67	5.38	.007	24.22	72.59
			52 1460 IN 4	.49	130.29	4.77	.008	.006	.77	3.25	.007	14.50	41.61
			53 1458 IN 1	.26	14.48	12.13	.005	.003	.67	2.65	.005	19.05	46.70
			55 1455 IN 3	.35	158.94	24.95	.008	.007	.82	4.56	.008	21.96	59.07
			56 1451 JK 2	.45	16.50	6.58	.006	.005	.92	2.45	.006	12.81	31.46
			57 1488 HIW 11	2.51	143.05	63.88	.040	.021	.53	3.24	.022	8.83	38.98
			58 1446 U+U 61I	3.72	9.69	94.88	.021	.016	.75	1.17	.016	4.27	13.93
			59 1479 DY 1	2.92	126.06	41.95	.021	.017	.80	1.50	.017	5.86	17.87
			60 1471 DP 1	3.37	123.96	36.77	.021	.017	.82	1.27	.017	5.07	15.10
			61 1472 IB 751	3.65	124.44	38.69	.021	.017	.81	1.20	.017	4.74	14.26
			62 1473 IB 756	3.25	112.19	29.07	.021	.018	.83	1.35	.018	5.43	16.02
			63 1474 DP 2	4.01	118.86	38.45	.022	.018	.81	1.14	.018	4.52	13.65
			64 1443 BC 5	5.07	129.27	54.16	.032	.022	.68	1.29	.023	4.48	15.64
			65 1449 BC 3	4.64	143.52	44.78	.034	.022	.64	1.49	.022	4.75	17.78
			88 1404 VG 4	1.73	161.31	69.82	.014	.008	.60	1.65	.008	4.84	19.60
			89 1462 HIW 9	2.93	179.90	97.28	.022	.019	.84	1.57	.019	6.39	18.65
			92 1499	3.23	131.87	54.45	.022	.020	.89	1.39	.020	6.09	16.61
			93 1498	3.34	133.81	55.12	.022	.019	.88	1.36	.019	5.82	16.17
			94 1496	3.59	133.51	53.72	.022	.020	.89	1.28	.020	5.59	15.30
			95 1500 DY 2	3.13	122.48	24.96	.021	.018	.87	1.38	.018	5.85	16.37
			98 1497	3.48	133.54	53.09	.022	.019	.87	1.31	.019	5.59	15.65
			100 1408 VG 8	4.45	133.78	42.51	.029	.018	.63	1.33	.018	4.07	15.83
			101 1490 HIW 7KA	4.04	134.59	43.23	.028	.019	.66	1.45	.019	4.63	17.21
			102 1406 VG 6	3.37	134.66	44.94	.022	.014	.61	1.37	.014	4.06	16.26
			104 1401 VG 1	2.99	112.81	29.83	.019	.016	.85	1.32	.016	5.50	15.75
			105 1445 HIW 16	4.44	54.99	119.34	.024	.020	.82	1.08	.021	4.65	13.28

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55	1455	IN 3	31 1409 VG 9	5.98	133.27	44.86	.034	.021	.64	1.16	.021	3.57	13.74
			37 1407 VG 7	4.60	144.39	52.53	.030	.019	.62	1.34	.019	4.07	15.93
			38 1424 HIW 6KA	3.47	135.43	50.14	.024	.014	.58	1.40	.014	4.00	16.67
			39 1423 HIW 5KA	2.94	127.08	47.12	.022	.014	.65	1.52	.015	4.94	18.22
			40 1405 VG 5	3.02	143.36	59.58	.022	.013	.60	1.51	.013	4.43	17.98
			41 1422 HIW 4KA	3.18	138.92	54.34	.023	.013	.58	1.46	.013	4.16	17.43
			42 1461 HIW 1KA	3.13	114.84	39.21	.022	.016	.71	1.43	.016	5.18	17.28
			44 1453 HIW 10	3.16	70.32	176.61	.040	.024	.59	2.56	.025	8.01	31.23
			45 1402 VG 2	1.50	81.40	154.98	.015	.013	.91	1.99	.013	8.93	23.85
			46 1403 VG 3	.81	65.52	153.07	.011	.010	.86	2.81	.010	11.73	33.37
			47 1457 HIW 3KA	.79	27.34	109.29	.009	.008	.88	2.38	.008	10.25	28.33
			48 14571 JK 1	.79	32.59	120.90	.015	.008	.56	3.82	.008	10.40	45.33
			49 1454 JK 4	1.13	147.10	54.24	.012	.008	.64	2.26	.008	7.07	26.81
			50 1452 HIW 2KA	.92	134.00	38.56	.011	.008	.72	2.58	.008	8.99	30.67
			51 1459 JK 3	.61	145.94	32.72	.010	.008	.86	3.29	.009	14.32	39.88
			52 1460 IN 4	.82	142.21	45.87	.011	.009	.81	2.67	.009	10.59	31.82
			53 1458 IN 1	.58	173.92	84.59	.008	.007	.86	2.90	.007	12.10	34.42
			54 1456 IN 2	.35	158.94	24.95	.008	.007	.82	4.56	.008	21.96	59.07
			56 1451 JK 2	.27	67.96	19.32	.008	.007	.89	6.02	.008	28.74	75.15
			57 1488 HIW 11	2.17	140.51	64.20	.040	.021	.53	3.74	.023	10.53	45.35
			58 1446 U+U 611	3.42	12.71	93.57	.021	.016	.77	1.27	.016	4.80	15.21
			59 1479 DY 1	2.64	121.90	45.27	.021	.018	.82	1.66	.018	6.74	19.86
			60 1471 DP 1	3.09	120.22	39.89	.021	.018	.85	1.38	.018	5.73	16.44
			61 1472 IB 751	3.37	121.04	41.59	.021	.018	.84	1.29	.018	5.31	15.42
			62 1473 IB 756	3.02	107.32	31.59	.021	.018	.86	1.44	.018	6.09	17.20
			63 1474 DP 2	3.75	115.39	41.14	.022	.019	.83	1.21	.019	5.02	14.54
			64 1443 BC 5	4.77	127.17	55.08	.032	.022	.69	1.36	.023	4.89	16.59
			65 1449 BC 3	4.30	142.27	45.08	.034	.022	.65	1.60	.022	5.16	19.12
			88 1404 VG 4	2.08	160.91	71.74	.017	.009	.53	1.69	.009	4.31	20.02
			89 1462 HIW 9	3.26	177.69	88.90	.024	.019	.78	1.55	.019	5.86	18.40
			92 1499	2.92	128.73	59.84	.022	.020	.90	1.54	.020	6.89	18.50
			93 1498	3.03	130.98	59.66	.022	.020	.88	1.50	.020	6.58	17.96
			94 1496	3.28	130.87	58.71	.023	.020	.90	1.40	.020	6.25	16.83
			95 1500 DY 2	2.86	118.29	26.71	.021	.019	.90	1.51	.019	6.59	17.90
			98 1497	3.16	130.80	57.33	.022	.020	.88	1.44	.020	6.28	17.28
			100 1408 VG 8	4.77	135.58	46.62	.031	.019	.61	1.32	.019	3.94	15.70
			101 1490 HIW 7KA	4.36	136.49	47.54	.030	.019	.64	1.43	.019	4.43	16.98
			102 1406 VG 6	3.69	136.90	50.14	.025	.014	.59	1.37	.014	3.91	16.32
			104 1401 VG 1	2.76	107.54	34.40	.019	.017	.89	1.42	.017	6.25	17.02
			105 1445 HIW 16	4.54	50.68	115.60	.025	.020	.80	1.09	.021	4.58	13.37

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56	1451	JK 2	31 1409 VG 9	5.87	135.70	47.73	.033	.021	.65	1.14	.021	3.62 13.60
			37 1407 VG 7	4.54	147.76	56.75	.029	.018	.63	1.32	.018	4.04 15.65
			38 1424 HIW 6KA	3.37	139.73	55.68	.022	.013	.59	1.37	.013	3.98 16.31
			39 1423 HIW 5KA	2.81	131.89	53.63	.021	.014	.67	1.49	.014	5.03 17.96
			40 1405 VG 5	2.96	148.49	66.44	.021	.012	.59	1.47	.013	4.29 17.56
			41 1422 HIW 4KA	3.10	143.71	60.53	.022	.013	.58	1.43	.013	4.09 17.03
			42 1461 HIW 1KA	2.95	118.72	45.33	.021	.015	.74	1.42	.016	5.38 17.16
			44 1453 HIW 10	3.44	70.14	175.64	.040	.023	.58	2.35	.025	7.23 28.65
			45 1402 VG 2	1.77	79.33	153.11	.015	.013	.83	1.75	.013	7.29 21.04
			46 1403 VG 3	1.09	66.13	149.16	.012	.009	.75	2.22	.009	8.11 26.42
			47 1457 HIW 3KA	1.02	37.46	127.99	.010	.007	.68	2.05	.007	6.75 24.31
			48 14571 JKI	1.03	41.48	124.37	.015	.007	.47	3.04	.007	7.13 36.38
			49 1454 JK 4	1.11	161.14	71.77	.011	.006	.60	1.97	.006	5.69 23.38
			50 1452 HIW 2KA	.84	151.25	56.56	.009	.007	.76	2.22	.007	8.25 26.40
			51 1459 JK 3	.61	171.92	120.68	.007	.007	.93	2.34	.007	11.15 28.58
			52 1460 IN 4	.79	161.78	87.41	.008	.007	.82	2.18	.007	8.94 26.16
			53 1458 IN 1	.71	15.76	112.20	.008	.006	.75	2.18	.006	7.94 25.96
			54 1456 IN 2	.45	16.50	6.58	.006	.005	.92	2.45	.006	12.81 31.46
			55 1455 IN 3	.27	67.96	19.32	.008	.007	.89	6.02	.008	28.74 75.15
			57 1488 HIW 11	2.27	133.90	64.48	.040	.021	.53	3.46	.024	10.68 43.00
			58 1446 U*U 611	3.27	8.76	93.30	.020	.015	.74	1.29	.015	4.67 15.34
			59 1479 DY 1	2.81	117.37	42.35	.021	.017	.83	1.51	.018	6.28 18.17
			60 1471 DP 1	3.27	116.41	35.05	.020	.017	.86	1.27	.017	5.35 15.18
			61 1472 IB 751	3.54	117.49	37.20	.021	.018	.85	1.20	.018	4.99 14.33
			62 1473 IB 756	3.23	104.24	25.75	.021	.018	.86	1.32	.018	5.58 15.72
			63 1474 DP 2	3.94	112.46	36.88	.022	.018	.84	1.13	.019	4.72 13.55
			64 1443 BC 5	4.91	124.42	54.11	.032	.022	.69	1.30	.023	4.75 15.90
			65 1449 BC 3	4.38	138.81	44.20	.033	.022	.65	1.56	.022	4.96 18.59
			88 1404 VG 4	2.11	168.37	81.25	.016	.008	.47	1.59	.008	3.62 18.92
			89 1462 HIW 9	3.36	2.09	96.61	.024	.018	.74	1.50	.018	5.39 17.83
			92 1499	3.07	124.26	57.66	.021	.020	.92	1.42	.020	6.49 17.10
			93 1498	3.16	126.55	57.54	.022	.019	.90	1.39	.020	6.23 16.68
			94 1496	3.41	126.76	55.50	.022	.020	.92	1.31	.020	5.94 15.71
			95 1500 DY 2	3.04	114.31	18.70	.020	.018	.90	1.39	.018	6.08 16.51
			98 1497	3.30	126.56	54.60	.022	.019	.90	1.34	.020	5.95 16.09
			100 1408 VG 8	4.68	138.68	50.06	.030	.019	.63	1.30	.019	3.98 15.50
			101 1490 HIW 7KA	4.27	139.92	51.33	.029	.019	.65	1.41	.019	4.48 16.77
			102 1406 VG 6	3.60	140.97	55.38	.023	.014	.59	1.34	.014	3.90 15.97
			104 1401 VG 1	2.98	104.18	24.91	.019	.017	.90	1.29	.017	5.68 15.38
			105 1445 HIW 16	4.80	51.65	119.23	.025	.019	.78	1.03	.020	4.20 12.65

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
57	1488	HIW 11	38 1424	HIW 6KA	5.64	137.39	60.75	.045	.022	.48	1.61	.023 4.16 19.47
			39 1423	HIW 5KA	5.08	132.79	60.24	.043	.022	.50	1.70	.024 4.80 20.87
			40 1405	VG 5	5.19	142.17	63.46	.044	.021	.48	1.73	.022 4.32 20.83
			41 1422	HIW 4KA	5.35	139.57	62.08	.044	.021	.48	1.67	.023 4.27 20.26
			42 1461	HIW 1KA	5.18	125.32	57.96	.043	.022	.52	1.61	.026 5.10 20.25
			44 1453	HIW 10	3.17	30.20	34.28	.046	.035	.77	2.29	.046 14.37 35.24
			45 1402	VG 2	1.91	3.07	64.93	.039	.021	.53	3.88	.026 13.68 50.29
			46 1403	VG 3	2.12	162.32	64.50	.040	.021	.53	3.83	.021 10.13 45.77
			47 1457	HIW 3KA	2.59	156.83	65.15	.040	.021	.53	3.17	.021 8.15 37.62
			48 14571	JK 1	2.53	157.80	68.26	.040	.023	.57	3.28	.023 9.13 38.99
			49 1454	JK 4	3.30	142.76	64.15	.041	.021	.52	2.50	.022 6.74 30.15
			50 1452	HIW 2KA	3.09	138.58	63.88	.040	.021	.53	2.62	.023 7.52 31.91
			51 1459	JK 3	2.78	141.70	64.31	.040	.021	.53	2.91	.022 8.08 35.17
			52 1460	IN 4	2.99	140.98	64.50	.040	.021	.53	2.71	.023 7.62 32.87
			53 1458	IN 1	2.68	147.39	64.42	.040	.021	.53	3.06	.022 8.07 36.53
			54 1456	IN 2	2.51	143.05	63.88	.040	.021	.53	3.24	.022 8.83 38.98
			55 1455	IN 3	2.17	140.51	64.20	.040	.021	.53	3.74	.023 10.53 45.35
			56 1451	JK 2	2.27	133.90	64.48	.040	.021	.53	3.46	.024 10.68 43.00
			58 1446	U+U 611	2.70	52.17	63.72	.039	.021	.55	1.68	.038 14.04 34.89
			59 1479	DY 1	.90	71.54	60.67	.038	.016	.42	4.00	.038 41.82 104.00
			60 1471	DP 1	1.30	84.62	60.97	.038	.017	.44	3.43	.035 27.11 71.18
			61 1472	IB 751	1.50	92.19	61.06	.038	.017	.45	3.34	.034 22.30 61.63
			62 1473	IB 756	1.69	62.47	60.76	.038	.018	.47	2.16	.038 22.46 55.04
			63 1474	DP 2	2.01	88.00	61.17	.038	.018	.46	2.41	.035 17.50 46.80
			64 1443	BC 5	2.70	116.46	61.42	.045	.022	.49	2.98	.031 11.61 40.63
			65 1449	BC 3	2.13	144.06	56.58	.045	.023	.50	4.40	.023 10.71 52.26
			66 1439		4.95	137.49	59.73	.042	.018	.43	1.72	.020 3.98 20.84
			67 1440		5.37	139.79	57.63	.043	.021	.48	1.68	.022 4.02 19.82
			68 14401	1440 ECC	4.98	138.33	57.97	.043	.019	.44	1.76	.020 4.02 21.10
			69 1468	BC 7	4.79	91.06	79.01	.049	.034	.70	1.51	.048 10.11 25.04
			88 1404	VG 4	4.18	150.48	65.77	.042	.020	.49	2.06	.021 4.95 24.54
			89 1462	HIW 9	5.16	162.96	70.27	.045	.025	.55	1.80	.025 4.80 21.36
			92 1499		.91	99.59	62.92	.039	.020	.51	6.45	.034 37.06 105.82
			93 1498		.95	108.81	62.91	.039	.020	.51	6.81	.031 32.38 101.08
			94 1496		1.19	113.04	63.08	.039	.020	.52	5.71	.030 25.05 81.16
			95 1500	DY 2	1.18	74.08	61.05	.038	.018	.49	3.47	.037 31.32 78.27
			98 1497		1.08	110.99	62.79	.039	.020	.50	6.13	.030 27.83 89.10
			101 1490	HIW 7KA	6.53	137.83	58.81	.049	.026	.52	1.53	.027 4.09 18.40
			102 1406	VG 6	5.86	138.24	60.57	.046	.022	.48	1.57	.024 4.02 19.03
			104 1401	VG 1	1.51	55.92	61.95	.037	.015	.41	2.16	.037 24.53 60.38
			105 1445	HIW 16	5.03	25.06	70.41	.040	.022	.53	1.33	.032 6.40 19.63

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
58	1446	U+U 611	2 6785001	67A24	17.15	82.64	136.67	.038	.021	.56	.40	.028	1.63	5.40
			42 1461	HIW 1KA	5.10	155.79	66.60	.027	.015	.56	1.10	.015	2.97	13.10
			44 1453	HIW 10	5.77	40.29	169.08	.040	.025	.61	1.26	.032	5.52	17.18
			45 1402	VG 2	4.21	32.14	123.44	.022	.016	.71	1.09	.016	3.75	12.93
			46 1403	VG 3	3.97	22.11	110.70	.021	.016	.75	1.11	.016	4.04	13.24
			47 1457	HIW 3KA	4.19	15.44	104.54	.022	.015	.69	1.10	.015	3.67	13.02
			48 14571	JKI	4.17	16.40	110.72	.025	.016	.63	1.23	.016	3.79	14.60
			49 1454	JK 4	4.29	1.86	88.80	.023	.015	.66	1.11	.015	3.58	13.24
			50 1452	HIW 2KA	3.98	1.32	89.04	.022	.016	.70	1.14	.016	3.91	13.60
			51 1459	JK 3	3.86	6.13	94.62	.021	.015	.71	1.15	.015	3.95	13.62
			52 1460	IN 4	3.99	3.62	92.86	.022	.015	.69	1.14	.015	3.83	13.59
			53 1458	IN 1	3.98	10.00	97.54	.022	.016	.71	1.13	.016	3.92	13.45
			54 1456	IN 2	3.72	9.69	94.88	.021	.016	.75	1.17	.016	4.27	13.93
			55 1455	IN 3	3.42	12.71	93.57	.021	.016	.77	1.27	.016	4.80	15.21
			56 1451	JK 2	3.27	8.76	93.30	.020	.015	.74	1.29	.015	4.67	15.34
			57 1488	HIW 11	2.70	52.17	63.72	.039	.021	.55	1.68	.038	14.04	34.89
			59 1479	DY 1	3.57	56.98	158.83	.018	.015	.80	1.05	.015	4.19	12.62
			60 1471	DP 1	3.86	62.55	157.60	.019	.013	.70	1.00	.013	3.42	11.90
			61 1472	IB 751	3.97	66.24	159.41	.019	.013	.70	.98	.013	3.34	11.69
			62 1473	IB 756	4.38	56.13	153.35	.020	.014	.71	.94	.014	3.26	11.22
			63 1474	DP 2	4.49	67.35	157.98	.020	.015	.72	.93	.015	3.24	11.07
			64 1443	BC 5	4.58	84.29	35.33	.026	.021	.80	1.10	.024	5.16	14.16
			65 1449	BC 3	3.39	91.07	28.42	.029	.018	.63	1.66	.021	6.23	21.07
			66 1439		5.83	109.95	20.27	.024	.012	.51	.84	.012	2.08	9.97
			67 1440		6.11	113.55	20.62	.027	.013	.50	.90	.013	2.18	10.71
			88 1404	VG 4	5.30	.79	88.67	.027	.014	.51	1.03	.014	2.59	12.29
			92 1499		3.39	63.60	153.90	.019	.011	.57	1.14	.011	3.17	13.55
			93 1498		3.33	66.04	155.82	.018	.011	.58	1.14	.011	3.22	13.58
			94 1496		3.45	69.75	156.74	.019	.011	.56	1.15	.011	3.17	13.72
			95 1500	DY 2	3.82	58.79	154.67	.020	.014	.68	1.08	.014	3.55	12.81
			98 1497		3.39	68.01	157.54	.019	.011	.57	1.13	.011	3.12	13.41
			99 1480	BC 13A	11.40	37.20	135.90	.038	.021	.55	.68	.021	1.88	8.12
			104 1401	VG 1	4.21	53.51	146.81	.019	.012	.65	.93	.012	2.95	11.07
			105 1445	HIW 16	7.54	34.47	122.76	.028	.015	.53	.77	.015	1.98	9.18
59	1479	DY 1	38 1424	HIW 6KA	6.06	129.60	47.07	.031	.018	.57	1.05	.018	2.95	12.49
			39 1423	HIW 5KA	5.57	124.63	43.89	.029	.018	.60	1.07	.018	3.22	12.84
			40 1405	VG 5	5.56	133.37	53.19	.029	.017	.59	1.08	.018	3.21	12.94
			41 1422	HIW 4KA	5.75	131.21	49.59	.030	.017	.58	1.07	.018	3.09	12.75
			44 1453	HIW 10	2.57	16.79	179.97	.038	.021	.56	1.84	.037	14.23	35.92
			45 1402	VG 2	1.78	155.04	71.36	.017	.016	.92	2.02	.016	9.02	23.96
			46 1403	VG 3	2.29	139.12	50.66	.019	.017	.85	1.75	.017	7.23	20.79
			47 1457	HIW 3KA	2.81	138.20	54.31	.020	.017	.83	1.50	.017	6.04	17.83
			48 14571	JKI	2.74	138.66	88.42	.022	.019	.89	1.55	.020	7.37	19.32
			49 1454	JK 4	3.69	129.39	46.79	.023	.017	.75	1.29	.017	4.69	15.32
			50 1452	HIW 2KA	3.54	125.02	40.81	.022	.017	.77	1.31	.017	4.92	15.56
			51 1459	JK 3	3.20	126.33	42.65	.021	.017	.80	1.38	.017	5.39	16.41
			52 1460	IN 4	3.41	126.66	43.95	.022	.017	.79	1.32	.018	5.14	15.78

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM		
59	1479	1	53	1458	IN 1	3.03	130.61	46.35	.021	.017	.81	1.45	.017	5.68	17.23
			54	1456	IN 2	2.92	126.06	41.95	.021	.017	.80	1.50	.017	5.86	17.87
			55	1455	IN 3	2.64	121.90	45.27	.021	.018	1.82	1.66	.018	6.74	19.86
			56	1451	JK 2	2.81	117.37	42.35	.021	.017	.83	1.51	.018	6.28	18.17
			57	1488	HIW 11	.90	71.54	60.67	.038	.016	.42	4.00	.038	41.82	104.00
			58	1446	U+U 611	3.57	56.98	158.83	.018	.015	.80	1.05	.015	4.19	12.62
			60	1471	DP 1	.47	110.63	24.61	.012	.009	.75	5.13	.009	18.66	60.94
			61	1472	IB 751	.73	117.95	28.42	.012	.009	.78	3.30	.009	12.44	39.17
			62	1473	IB 756	.81	52.38	21.89	.013	.010	.75	2.66	.012	14.74	38.31
			63	1474	DP 2	1.17	100.61	39.88	.013	.011	.81	2.20	.011	9.54	27.29
			64	1443	BC 5*	2.16	133.62	60.62	.026	.017	.65	2.45	.018	8.38	29.88
			65	1449	BC 3	2.05	168.93	43.47	.028	.018	.63	2.51	.022	10.56	33.47
			66	1439		4.65	147.69	55.24	.021	.012	.55	.94	.012	2.50	11.13
			67	1440		5.11	149.24	45.85	.024	.015	.64	.95	.016	3.14	11.52
			68	14401	1440 ECC	4.70	148.49	48.08	.023	.013	.56	1.00	.013	2.81	11.98
			69	1468	BC 7	3.95	95.43	110.00	.037	.026	.69	1.38	.036	9.23	22.99
			70	1442		6.50	98.97	5.95	.032	.013	.41	1.02	.013	2.04	12.15
			88	1404	VG 4	4.45	139.00	58.99	.025	.016	.65	1.18	.017	3.78	13.95
			89	1462	HIW 9	5.22	153.02	74.52	.030	.021	.69	1.17	.021	4.07	14.10
			92	1499		.44	174.26	66.82	.017	.015	.90	7.72	.015	34.33	92.50
			93	1498		.60	175.35	67.61	.017	.015	.89	5.67	.015	25.02	68.02
			94	1496		.79	162.25	77.62	.017	.015	.92	4.36	.015	19.47	51.81
			95	1500	DY 2	.28	82.24	.20	.013	.010	.77	9.46	.010	35.87	112.80
			98	1497		.69	166.99	66.65	.016	.015	.89	4.90	.015	21.26	58.41
			102	1406	VG 6	6.27	130.66	47.39	.032	.018	.57	1.04	.018	2.91	12.44
104	1401	VG 1	.69	35.19	36.73	.010	.007	.67	1.96	.010	14.22	34.85			
105	1445	HIW 16	4.46	16.63	103.73	.021	.011	.54	.95	.011	2.53	11.35			
60	1471	DP 1	40	1405	VG 5	5.99	131.65	52.23	.029	.018	.60	.99	.018	3.01	11.92
			41	1422	HIW 4KA	6.19	129.70	48.46	.030	.018	.59	.98	.018	2.89	11.78
			44	1453	HIW 10	2.64	6.66	178.92	.037	.021	.56	1.65	.037	14.03	34.60
			45	1402	VG 2	2.14	146.30	101.23	.017	.016	.95	1.58	.016	7.64	19.14
			46	1403	VG 3	2.71	134.42	45.84	.019	.017	.90	1.42	.017	6.17	16.89
			47	1457	HIW 3KA	3.23	134.38	51.85	.020	.017	.86	1.26	.017	5.31	15.01
			48	14571	JK1	3.16	134.69	97.93	.021	.019	.90	1.30	.020	6.47	16.43
			49	1454	JK 4	4.13	127.31	43.95	.023	.017	.77	1.13	.017	4.21	13.42
			50	1452	HIW 2KA	3.99	123.36	36.57	.022	.017	.79	1.14	.017	4.36	13.55
			51	1459	JK 3	3.65	124.36	37.61	.021	.017	.82	1.18	.017	4.72	14.05
			52	1460	IN 4	3.86	124.76	39.51	.022	.018	.82	1.15	.018	4.55	13.64
			53	1458	IN 1	3.47	127.99	42.07	.021	.017	.83	1.23	.017	4.98	14.64
			54	1456	IN 2	3.37	123.96	36.77	.021	.017	.82	1.27	.017	5.07	15.10
			55	1455	IN 3	3.09	120.22	39.89	.021	.018	.85	1.38	.018	5.73	16.44
			56	1451	JK 2	3.27	116.41	35.05	.020	.017	.86	1.27	.017	5.35	15.18
			57	1488	HIW 11	1.30	84.62	60.97	.038	.017	.44	3.43	.035	27.11	71.18
			58	1446	U+U 611	3.86	62.55	157.60	.019	.013	.70	1.00	.013	3.42	11.90
			59	1479	DY 1	.47	110.63	24.61	.012	.009	.75	5.13	.009	18.66	60.94
			61	1472	IB 751	.28	130.33	95.39	.007	.006	.96	4.86	.007	23.91	59.38
			62	1473	IB 756	.69	17.44	20.32	.008	.006	.81	1.91	.008	11.35	27.82

DEPARTMENT OF ENERGY, MINES AND RESOURCES
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CYPRUS ANVIL MINE CONTROL--HORIZ. ADJUSTMENT--SEPT, 1979.

CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
60	1471	1												
		64	1443	BC 5	1.74	139.62	64.87	.025	.015	.62	2.88	.016	9.33	34.96
		65	1449	BC 3	1.84	1.33	45.21	.026	.016	.62	2.43	.022	11.98	34.93
		66	1439		4.29	151.43	61.13	.019	.009	.49	.90	.009	2.15	10.74
		67	1440		4.75	152.75	48.91	.022	.014	.66	.93	.015	3.13	11.26
		68	14401	1440 ECC	4.34	152.27	51.60	.021	.011	.53	.97	.012	2.65	11.72
		69	1468	BC 7	3.50	93.44	110.31	.037	.023	.64	1.46	.036	10.18	25.59
		70	1442		6.04	98.08	3.88	.030	.012	.41	1.04	.013	2.09	12.34
		71	1448		5.52	115.87	22.25	.030	.022	.75	1.13	.023	4.08	13.39
		88	1404	VG 4	4.86	136.40	58.30	.025	.017	.67	1.05	.017	3.51	12.57
		89	1462	HIW 9	5.57	149.80	74.70	.030	.021	.69	1.08	.021	3.84	13.10
		92	1499		.48	55.05	79.79	.015	.013	.88	5.96	.015	31.32	78.25
		93	1498		.58	42.03	80.50	.015	.013	.87	5.00	.014	24.98	64.22
		94	1496		.62	18.34	93.78	.015	.014	.88	5.12	.014	22.29	61.25
		95	1500	DY 2	.25	142.41	148.27	.009	.003	.34	2.48	.009	33.71	82.97
		98	1497		.58	28.78	80.27	.015	.013	.87	5.09	.014	23.93	63.51
		104	1401	VG 1	.73	176.84	171.32	.008	.006	.79	1.76	.008	10.79	26.47
		105	1445	HIW 16	4.51	10.74	101.94	.020	.009	.44	.93	.009	2.00	11.00
61	1472	1B 751												
		40	1405	VG 5	6.27	131.59	52.24	.030	.018	.59	.97	.018	2.90	11.61
		41	1422	HIW 4KA	6.47	129.73	48.60	.030	.018	.58	.96	.018	2.79	11.49
		44	1453	HIW 10	2.80	1.96	179.17	.037	.021	.57	1.56	.037	13.28	32.56
		45	1402	VG 2	2.41	144.49	88.79	.017	.016	.94	1.44	.016	6.84	17.47
		46	1403	VG 3	2.98	134.04	48.87	.019	.017	.88	1.32	.017	5.64	15.71
		47	1457	HIW 3KA	3.51	134.06	53.06	.020	.017	.85	1.19	.017	4.92	14.18
		48	14571	JK1	3.44	134.34	92.52	.022	.019	.90	1.22	.021	5.99	15.36
		49	1454	JK 4	4.41	127.50	44.85	.023	.017	.75	1.08	.018	3.98	12.86
		50	1452	HIW 2KA	4.26	123.81	38.07	.023	.018	.78	1.09	.018	4.12	12.95
		51	1459	JK 3	3.92	124.78	39.45	.021	.017	.81	1.12	.017	4.43	13.36
		52	1460	IN 4	4.14	125.13	41.05	.022	.018	.80	1.09	.018	4.28	13.03
		53	1458	IN 1	3.75	128.16	43.74	.021	.017	.82	1.17	.017	4.65	13.88
		54	1456	IN 2	3.65	124.44	38.69	.021	.017	.81	1.20	.017	4.74	14.26
		55	1455	IN 3	3.37	121.04	41.59	.021	.018	.84	1.29	.018	5.31	15.42
		56	1451	JK 2	3.54	117.49	37.20	.021	.018	.85	1.20	.018	4.99	14.33
		57	1488	HIW 11	1.50	92.19	61.06	.038	.017	.45	3.34	.034	22.30	61.63
		58	1446	U+U 611	3.97	66.24	159.41	.019	.013	.70	.98	.013	3.34	11.69
		59	1479	DY 1	.73	117.95	28.42	.012	.009	.78	3.30	.009	12.44	39.17
		60	1471	DP 1	.28	130.33	95.39	.007	.006	.96	4.86	.007	23.91	59.38
		62	1473	1B 756	.84	179.74	22.94	.008	.007	.92	1.79	.008	9.20	22.80
		63	1474	DP 2	.52	75.82	79.06	.008	.005	.64	2.13	.008	16.13	39.55
		64	1443	BC 5	1.47	141.37	65.93	.025	.015	.62	3.39	.016	10.91	41.05
		65	1449	BC 3	1.68	8.66	45.21	.026	.016	.63	2.49	.023	13.71	37.88
		66	1439		4.04	152.85	63.01	.018	.009	.50	.93	.009	2.24	11.02
		67	1440		4.50	154.09	49.40	.021	.014	.68	.96	.015	3.31	11.56
		68	14401	1440 ECC	4.08	153.72	52.26	.020	.011	.55	1.00	.012	2.82	12.08
		69	1468	BC 7	3.29	90.54	110.42	.037	.023	.63	1.56	.035	10.74	27.30
		70	1442		5.81	96.63	2.90	.030	.012	.41	1.06	.012	2.11	12.56
		71	1448		5.25	115.12	21.21	.029	.022	.76	1.16	.022	4.26	13.75
		88	1404	VG 4	5.13	136.07	58.16	.025	.017	.66	1.01	.017	3.35	12.16
		89	1462	HIW 9	5.07	148.80	73.80	.030	.021	.69	1.08	.021	3.84	13.10

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM			
61	1472	751	92	1499	.61	81.07	80.47	.015	.013	.87	4.54	.015	25.19	61.71		
			93	1498	.65	67.26	81.35	.015	.013	.87	4.24	.015	23.33	57.58		
			94	1496	.58	44.77	94.43	.016	.014	.87	5.29	.014	25.07	66.14		
	95	1500	DY 2	.53	136.12	158.05	.010	.007	.75	2.94	.009	17.47	44.17			
	98	1497		.59	56.03	81.54	.015	.013	.86	4.69	.015	24.97	62.68			
	104	1401	VG 1	.94	164.49	164.05	.008	.007	.93	1.59	.008	8.32	20.38			
	105	1445	HIW 16	4.65	7.78	99.89	.021	.009	.43	.92	.009	1.93	10.89			
	62	1473	IB 756	40	1405	5.74	125.36	49.25	.029	.018	.63	1.02	.019	3.32	12.37	
				41	1422	HIW 4KA	5.96	123.55	45.48	.030	.018	.61	1.01	.019	3.16	12.19
				44	1453	HIW 10	1.97	2.90	179.63	.038	.020	.54	2.15	.038	19.10	46.85
45				1402	VG 2	1.79	128.83	164.72	.017	.017	.98	1.93	.017	9.43	23.26	
46				1403	VG 3	2.47	120.00	31.71	.019	.017	.90	1.60	.017	6.93	18.96	
47				1457	HIW 3KA	2.98	122.47	40.23	.020	.018	.88	1.38	.018	5.93	16.47	
48				14571	JKI	2.91	122.52	107.06	.021	.020	.94	1.41	.021	7.24	17.82	
49				1454	JK 4	3.95	117.85	37.72	.023	.018	.78	1.19	.018	4.56	14.16	
50				1452	HIW 2KA	3.86	113.45	29.75	.022	.018	.80	1.20	.018	4.64	14.24	
51				1459	JK 3	3.51	113.52	29.40	.021	.018	.83	1.25	.018	5.05	14.88	
52				1460	IN 4	3.71	114.54	31.53	.022	.018	.82	1.21	.018	4.87	14.41	
53				1458	IN 1	3.29	116.66	33.40	.021	.018	.84	1.32	.018	5.40	15.70	
54				1456	IN 2	3.25	112.19	29.07	.021	.018	.83	1.35	.018	5.43	16.02	
55				1455	IN 3	3.02	107.32	31.59	.021	.018	.86	1.44	.018	6.09	17.20	
56				1451	JK 2	3.23	104.24	25.75	.021	.018	.86	1.32	.018	5.58	15.72	
57				1488	HIW 11	1.69	62.47	60.76	.038	.018	.47	2.16	.038	22.46	55.04	
58				1446	U+U 611	4.38	56.13	153.35	.020	.014	.71	.94	.014	3.26	11.22	
59				1479	DY 1	.81	52.38	21.89	.013	.010	.75	2.66	.012	14.74	38.31	
60				1471	DP 1	.69	17.44	20.32	.008	.006	.81	1.91	.008	11.35	27.82	
61				1472	IB 751	.84	179.74	22.94	.008	.007	.92	1.79	.008	9.20	22.80	
63				1474	DP 2	.87	144.43	60.31	.010	.008	.79	2.39	.008	9.22	28.50	
64				1443	BC 5	2.19	155.13	65.06	.026	.016	.61	2.43	.016	7.14	28.88	
65				1449	BC 3	2.51	5.70	47.80	.027	.017	.64	1.82	.023	9.19	26.30	
66				1439		4.80	157.38	65.17	.021	.010	.47	.89	.010	2.03	10.54	
67				1440		5.26	158.04	55.20	.023	.015	.65	.90	.016	2.96	10.80	
68				14401	1440 ECC	4.85	158.07	56.60	.022	.012	.54	.93	.012	2.57	11.20	
69				1468	BC 7	3.40	104.79	107.98	.037	.024	.65	1.45	.037	10.81	26.50	
70				1442		5.97	104.64	9.04	.030	.013	.41	1.05	.013	2.15	12.47	
71				1448		5.66	122.80	29.73	.031	.022	.73	1.12	.022	3.97	13.34	
88				1404	VG 4	4.57	128.80	54.52	.025	.017	.70	1.10	.018	3.95	13.30	
89	1462	HIW 9	5.13	144.10	72.83	.029	.021	.73	1.15	.022	4.35	14.02				
92	1499		1.11	32.69	76.83	.016	.014	.88	2.80	.015	13.65	35.43				
93	1498		1.24	28.63	78.42	.016	.014	.87	2.52	.015	11.94	31.59				
94	1496		1.31	17.86	89.08	.016	.014	.88	2.54	.015	11.10	30.54				
95	1500	DY 2	.58	38.43	9.82	.009	.006	.76	2.48	.008	13.92	35.90				
98	1497		1.27	22.62	78.07	.016	.014	.86	2.49	.014	11.45	30.86				
104	1401	VG 1	.26	104.91	5.01	.010	.007	.73	7.65	.007	27.70	91.44				
105	1445	HIW 16	3.83	9.53	100.83	.019	.010	.53	1.01	.010	2.57	11.95				

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
63	1474	DP 2	44 1453	HIW 10	2.70	171.31	.34	.037	-.022	.59	1.71	-.037 13.73 33.92
			45 1402	VG 2	2.64	133.93	73.93	.018	.017	.92	1.40	-.017 6.52 16.93
			46 1403	VG 3	3.29	126.31	48.17	.020	-.017	.86	1.27	-.018 5.36 15.12
			47 1457	HIW 3KA	3.81	127.39	51.05	.021	-.018	.83	1.15	-.018 4.75 13.79
			48 14571	JK 1	3.73	127.52	84.84	.022	.020	.90	1.17	-.021 5.72 14.64
			49 1454	JK 4	4.75	122.57	43.63	.024	-.018	.75	1.04	-.018 3.88 12.50
			50 1452	HIW 2KA	4.63	119.02	37.41	.024	-.018	.77	1.05	-.018 3.98 12.52
			51 1459	JK 3	4.28	119.53	38.86	.023	-.018	.80	1.08	-.018 4.26 12.89
			52 1460	IN 4	4.49	120.10	40.10	.023	-.018	.80	1.06	-.019 4.13 12.60
			53 1458	IN 1	4.08	122.38	42.90	.022	-.018	.81	1.12	-.018 4.47 13.39
			54 1456	IN 2	4.01	118.86	38.45	.022	-.018	.81	1.14	-.018 4.52 13.65
			55 1455	IN 3	3.75	115.39	41.14	.022	-.019	.83	1.21	-.019 5.02 14.54
			56 1451	JK 2	3.94	112.46	36.88	.022	-.018	.84	1.13	-.019 4.72 13.55
			57 1488	HIW 11	2.01	88.00	61.17	.038	-.018	.46	2.41	-.035 17.50 46.80
			58 1446	U+U 611	4.49	67.35	157.98	.020	-.015	.72	.93	-.015 3.24 11.07
			59 1479	DY 1	1.17	100.61	39.88	.013	-.011	.81	2.20	-.011 9.54 27.29
			60 1471	DP 1	.72	94.12	95.04	.008	-.007	.82	1.96	-.008 11.60 28.41
			61 1472	IB 751	.52	75.82	79.06	.008	-.005	.64	2.13	-.008 16.13 39.55
			62 1473	IB 756	.87	144.43	60.31	.010	-.008	.79	2.39	-.008 9.22 28.50
			64 1443	BC 5	1.34	162.09	69.28	.025	-.015	.61	3.87	-.015 11.50 46.02
			65 1449	BC 3	1.95	22.92	48.14	.026	-.017	.66	2.04	-.025 12.78 33.05
			66 1439		3.95	160.22	70.98	.019	-.009	.49	.98	-.009 2.34 11.67
			67 1440		4.42	160.71	58.12	.021	-.015	.71	.99	-.015 3.51 11.87
			68 14401	1440 ECC	4.01	161.02	59.42	.020	-.012	.58	1.04	-.012 3.08 12.47
			69 1468	BC 7	2.79	93.28	108.93	.037	-.022	.61	1.76	-.036 12.97 32.55
			71 1448		4.86	119.00	28.15	.029	-.023	.81	1.22	-.023 4.77 14.48
			73 1467	BC 16	5.34	67.65	11.04	.055	-.036	.66	1.93	-.043 8.03 25.20
			88 1404	VG 4	5.41	131.29	56.28	.026	-.017	.66	.99	-.018 3.37 11.97
			89 1462	HIW 9	6.01	144.15	71.52	.031	-.021	.69	1.04	-.022 3.74 12.64
			92 1499		1.13	78.65	81.32	.017	-.014	.84	2.55	-.017 14.65 35.90
			93 1498		1.17	71.07	82.60	.016	-.014	.84	2.45	-.016 14.02 34.55
			94 1496		1.06	59.48	92.38	.017	-.014	.84	2.91	-.016 15.14 38.80
			95 1500	DY 2	.91	106.24	144.88	.010	-.009	.82	2.12	-.010 10.73 28.13
			98 1497		1.10	65.29	83.10	.016	-.014	.83	2.61	-.016 14.70 36.55
			104 1401	VG 1	1.08	135.79	63.75	.010	-.009	.89	1.83	-.009 8.06 21.97
			105 1445	HIW 16	4.49	1.61	94.86	.021	-.010	.46	.97	-.010 2.18 11.57
64	1443	BC 5	44 1453	HIW 10	4.03	168.27	12.58	.041	-.031	.77	1.69	-.039 9.78 24.86
			45 1402	VG 2	3.87	143.31	64.03	.030	-.021	.71	1.58	-.021 5.55 18.91
			46 1403	VG 3	4.44	136.45	58.94	.031	-.021	.69	1.43	-.022 4.95 17.17
			47 1457	HIW 3KA	4.96	136.21	58.96	.032	-.022	.67	1.31	-.022 4.48 15.81
			48 14571	JK 1	4.89	136.44	65.37	.032	-.024	.73	1.34	-.025 5.07 16.26
			49 1454	JK 4	5.84	130.95	54.62	.034	-.022	.64	1.18	-.023 3.89 14.29
			50 1452	HIW 2KA	5.68	128.27	52.78	.033	-.022	.66	1.19	-.023 4.05 14.42
			51 1459	JK 3	5.35	129.27	54.26	.033	-.022	.67	1.23	-.023 4.26 14.94
			52 1460	IN 4	5.56	129.36	54.34	.033	-.022	.67	1.21	-.023 4.14 14.59
			53 1458	IN 1	5.18	131.87	55.81	.033	-.022	.67	1.27	-.023 4.36 15.38
			54 1456	IN 2	5.07	129.27	54.16	.032	-.022	.68	1.29	-.023 4.48 15.64

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
64	1443	5										
		55	1455	IN 3	4.77	127.17	55.08	.032	.022	.69	1.36	.023 4.89 16.59
		56	1451	JK 2	4.91	124.42	54.11	.032	.022	.69	1.30	.023 4.75 15.90
		57	1488	HIW 11	2.70	116.46	61.42	.045	.022	.49	2.96	.031 11.61 40.63
		58	1446	U+U 611	4.58	84.29	35.33	.026	.021	.80	1.10	.024 5.16 14.16
		59	1479	DY 1	2.16	133.62	60.62	.026	.017	.65	2.45	.018 8.38 29.88
		60	1471	DP 1	1.74	139.62	64.87	.025	.015	.62	2.88	.016 9.33 34.96
		61	1472	IB 751	1.47	141.37	65.93	.025	.015	.62	3.39	.016 10.91 41.05
		62	1473	IB 756	2.19	155.13	65.86	.026	.016	.61	2.43	.016 7.14 28.88
		63	1474	DP 2	1.34	162.09	69.28	.025	.015	.61	3.87	.015 11.50 46.02
		65	1449	BC 3	1.28	66.06	164.94	.015	.012	.79	2.38	.012 9.27 28.44
		66	1439		2.61	159.26	67.85	.023	.012	.54	1.78	.012 4.70 21.17
		67	1440		3.08	160.11	57.15	.025	.017	.69	1.66	.018 5.76 19.98
		68	14401	1440 ECC	2.67	160.48	58.38	.024	.014	.59	1.85	.015 5.57 22.35
		69	1468	BC 7	2.62	64.83	105.54	.039	.025	.64	2.50	.034 12.89 36.51
		70	1442		4.88	84.42	1.54	.031	.024	.79	1.29	.024 4.99 15.33
		71	1448		3.99	105.76	45.85	.032	.028	.90	1.60	.029 7.34 19.49
		73	1467	BC 16	5.61	53.89	17.19	.057	.041	.72	1.74	.052 9.26 24.95
		78	1441		6.52	134.19	34.55	.046	.026	.56	1.44	.026 4.06 17.25
		88	1404	VG 4	6.60	137.25	59.47	.036	.021	.58	1.11	.022 3.34 13.44
		92	1499		1.85	124.70	63.21	.026	.017	.65	2.72	.019 10.55 34.69
		93	1498		1.76	120.60	63.17	.026	.017	.65	2.78	.020 11.35 36.12
		94	1496		1.51	119.14	64.99	.026	.017	.68	3.17	.021 13.67 41.62
		95	1500	DY 2	1.99	139.98	64.46	.025	.017	.67	2.57	.018 8.81 31.04
		98	1497		1.63	120.10	63.50	.026	.017	.65	2.97	.020 12.28 38.80
		104	1401	VG 1	2.36	150.35	65.22	.025	.016	.63	2.22	.016 6.82 26.41
		106	1437	BC 21	17.15	51.18	108.79	.059	.036	.60	.64	.044 2.55 8.44
65	1449	BC 3										
		44	1453	HIW 10	4.48	4.47	12.07	.043	.030	.71	1.41	.043 9.58 23.58
		45	1402	VG 2	3.80	162.46	49.13	.031	.022	.71	1.61	.024 6.22 19.91
		46	1403	VG 3	4.19	153.17	47.07	.032	.022	.67	1.56	.023 5.43 18.89
		47	1457	HIW 3KA	4.69	151.08	48.46	.033	.022	.66	1.44	.023 4.83 17.31
		48	14571	JK1	4.63	151.53	52.51	.033	.025	.74	1.47	.025 5.36 17.61
		49	1454	JK 4	5.42	143.27	46.95	.035	.022	.62	1.33	.022 4.06 15.89
		50	1452	HIW 2KA	5.21	140.82	44.82	.035	.022	.63	1.37	.022 4.22 16.32
		51	1459	JK 3	4.91	142.72	45.27	.034	.022	.64	1.42	.022 4.48 16.91
		52	1460	IN 4	5.12	142.26	45.75	.034	.022	.64	1.38	.022 4.33 16.44
		53	1458	IN 1	4.80	145.92	46.33	.034	.022	.65	1.44	.022 4.63 17.20
		54	1456	IN 2	4.64	143.52	44.78	.034	.022	.64	1.49	.022 4.75 17.78
		55	1455	IN 3	4.30	142.27	45.08	.034	.022	.65	1.60	.022 5.16 19.12
		56	1451	JK 2	4.38	138.81	44.20	.033	.022	.65	1.56	.022 4.96 18.59
		57	1488	HIW 11	2.13	144.06	56.58	.045	.023	.50	4.40	.023 10.71 52.26
		58	1446	U+U 611	3.39	91.07	28.42	.029	.018	.63	1.66	.021 6.23 21.07
		59	1479	DY 1	2.05	168.93	43.47	.028	.018	.63	2.51	.022 10.56 33.47
		60	1471	DP 1	1.84	1.33	45.21	.026	.016	.82	2.43	.022 11.98 34.93
		61	1472	IB 751	1.68	8.66	45.21	.026	.016	.63	2.49	.023 13.71 37.88
		62	1473	IB 756	2.51	5.70	47.80	.027	.017	.64	1.82	.023 9.19 26.30
		63	1474	DP 2	1.95	22.92	48.14	.026	.017	.66	2.04	.025 12.78 33.05
		64	1443	BC 5	1.28	66.06	164.94	.015	.012	.79	2.38	.012 9.27 28.44
		66	1439		2.85	132.59	61.07	.025	.013	.61	1.80	.013 6.62 21.35

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
65	1449 3	67	1440		3.25	137.00	35.12	.028	.016	.56	1.76	.016	5.07	21.17
		68	14401	1440 ECC	2.87	134.08	37.91	.027	.013	.48	1.94	.013	4.60	23.15
		69	1468	BC 7	3.90	65.24	109.84	.038	.030	.77	1.81	.034	8.79	24.07
		92	1499		1.61	167.47	44.98	.028	.017	.63	3.22	.021	12.99	42.10
		93	1498		1.46	166.31	44.58	.027	.017	.63	3.55	.021	14.14	46.23
		94	1496		1.26	173.09	44.14	.027	.018	.66	3.91	.022	17.45	52.71
		95	1500	DY 2	2.05	176.84	43.99	.027	.018	.66	2.32	.022	10.91	32.00
		98	1497		1.36	169.92	44.38	.027	.017	.63	3.71	.021	15.61	49.35
		104	1401	VG 1	2.57	.06	46.28	.027	.017	.65	1.82	.022	8.69	25.51
		66	1439	2	6785001	67A24	12.27	70.05	103.60	.035	.022	.63	.44	.031
57	1488			HIW 11	4.95	137.49	59.73	.042	.018	.43	1.72	.020	3.98	20.84
58	1446			U+U 61 I	5.83	109.95	20.27	.024	.012	.51	.84	.012	2.08	9.97
59	1479			DY 1	4.65	147.69	55.24	.021	.012	.55	.94	.012	2.50	11.13
60	1471			DP 1	4.29	151.43	61.13	.019	.009	.49	.90	.009	2.15	10.74
61	1472			IB 751	4.04	152.85	63.01	.018	.009	.50	.93	.009	2.24	11.02
62	1473			IB 756	4.80	157.38	65.17	.021	.010	.47	.89	.010	2.03	10.54
63	1474			DP 2	3.95	160.22	70.98	.019	.009	.49	.98	.009	2.34	11.67
64	1443			BC 5	2.61	159.26	67.85	.023	.012	.54	1.78	.012	4.70	21.17
65	1449			BC 3	2.85	132.59	41.07	.025	.013	.51	1.80	.013	4.43	21.35
67	1440				.47	164.83	10.80	.014	.008	.54	4.08	.013	28.13	74.14
68	14401			1440 ECC	.08	25.87	25.77	.012	.001	.07	2.30	.012	152.53	373.71
69	1468			BC 7	3.84	22.12	111.34	.037	.018	.48	1.98	.018	4.58	23.53
70	1442				4.90	53.41	157.58	.027	.015	.55	1.11	.016	3.21	13.46
71	1448				3.22	64.94	151.97	.026	.022	.85	1.68	.022	6.94	19.96
72	1444			SL 7	4.45	84.14	56.75	.038	.029	.77	1.45	.036	8.12	20.80
73	1467			BC 16	6.79	32.09	18.41	.055	.041	.74	1.27	.055	8.05	19.97
74	1438				10.19	29.27	58.69	.054	.039	.72	.87	.051	5.00	13.04
78	1441				4.29	119.23	26.03	.041	.019	.48	1.95	.020	4.55	23.19
92	1499				4.27	145.04	56.09	.020	.011	.56	.99	.011	2.69	11.75
93	1498		4.14	143.85	55.33	.020	.011	.56	1.00	.011	2.72	11.87		
94	1496		3.90	144.77	57.10	.019	.012	.63	1.03	.012	3.14	12.20		
95	1500	DY 2	4.54	150.93	60.19	.020	.012	.59	.90	.012	2.55	10.64		
98	1497		4.01	144.42	55.68	.020	.011	.57	1.01	.011	2.79	12.00		
104	1401	VG 1	4.96	155.04	63.54	.020	.010	.51	.84	.010	2.07	10.02		
105	1445	HIW 16	8.29	171.61	82.99	.030	.012	.41	.74	.012	1.46	8.80		
106	1437	BC 21	18.14	43.32	107.27	.061	.032	.52	.64	.039	2.15	8.26		
67	1440	2	6785001	67A24	12.32	67.87	104.21	.036	.025	.69	.49	.032	2.63	7.12
		57	1488	HIW 11	5.37	139.79	57.63	.043	.021	.48	1.66	.022	4.02	19.82
		58	1446	U+U 61 I	6.11	113.55	20.62	.027	.013	.50	.90	.013	2.18	10.71
		59	1479	DY 1	5.11	149.24	45.85	.024	.015	.64	.95	.016	3.14	11.52
		60	1471	DP 1	4.75	152.75	48.91	.022	.014	.66	.93	.015	3.13	11.26
		61	1472	IB 751	4.50	154.09	49.40	.021	.014	.68	.98	.015	3.31	11.56
		62	1473	IB 756	5.26	158.04	55.20	.023	.015	.65	.90	.016	2.96	10.80
		63	1474	DP 2	4.42	160.71	58.12	.021	.015	.71	.99	.015	3.51	11.87
64	1443	BC 5	3.08	160.11	57.15	.025	.017	.69	1.66	.018	5.76	19.98		

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
67	1440	66	1439		.47	164.83	10.80	.014	.008	.54	4.08	.013 28.13 74.14
		68	14401	1440 ECC	.41	157.73	158.54	.010	.005	.47	2.35	.010 24.49 60.00
		69	1468	BC 7	4.23	18.26	112.87	.038	.022	.59	1.85	.023 5.35 22.02
		70	1442		5.09	48.48	163.40	.030	.018	.59	1.14	.020 4.01 14.47
		71	1448		3.33	56.96	167.30	.029	.024	.83	1.78	.025 7.49 21.53
		72	1444	SL 7	4.39	78.09	49.20	.039	.031	.79	1.57	.038 8.59 22.02
		78	1441		3.98	114.39	26.22	.038	.018	.66	1.99	.018 4.46 23.59
		79	1428		9.59	128.12	127.34	.074	.056	.75	1.20	.074 7.74 18.96
		88	1404	VG 4	9.51	144.47	54.87	.037	.020	.53	.80	.020 2.06 9.44
		92	1499		4.71	146.98	44.95	.023	.015	.86	1.01	.016 3.37 12.15
		93	1498		4.58	145.96	43.78	.023	.015	.66	1.02	.016 3.41 12.32
		94	1496		4.34	146.89	42.84	.022	.016	.71	1.05	.016 3.78 12.69
		95	1500	DY 2	5.00	152.22	47.60	.023	.016	.70	.92	.016 3.28 11.11
		98	1497		4.45	146.53	43.42	.023	.015	.67	1.04	.016 3.51 12.49
99	1480	BC 13A	11.60	6.43	103.67	.036	.025	.69	.64	.025 2.15 7.60		
104	1401	VG 1	5.42	155.88	53.31	.023	.015	.66	.86	.016 2.88 10.37		
68	14401	57	1488	HIW 11	4.98	138.33	57.97	.043	.019	.44	1.76	.020 4.02 21.10
		59	1479	DY 1	4.70	148.49	48.08	.023	.013	.56	1.00	.013 2.81 11.98
		60	1471	DP 1	4.34	152.27	51.60	.021	.011	.53	.97	.012 2.65 11.72
		61	1472	IB 751	4.08	153.72	52.26	.020	.011	.55	1.00	.012 2.82 12.08
		62	1473	IB 756	4.85	158.07	56.60	.022	.012	.54	.93	.012 2.57 11.20
		63	1474	DP 2	4.01	161.02	59.42	.020	.012	.58	1.04	.012 3.08 12.47
		64	1443	BC 5	2.67	160.48	58.38	.024	.014	.59	1.85	.015 5.57 22.35
		65	1449	BC 3	2.87	134.08	37.91	.027	.013	.48	1.94	.013 4.60 23.15
		66	1439		.08	25.87	25.77	.012	.001	.07	2.30	.012 152.53 373.71
		67	1440		.41	157.73	158.54	.010	.005	.47	2.35	.010 24.49 60.00
		69	1468	BC 7	3.92	22.19	111.18	.037	.021	.57	1.95	.021 5.41 23.14
		70	1442		4.97	52.99	165.39	.029	.017	.58	1.13	.019 3.80 14.13
		71	1448		3.28	64.09	172.36	.028	.024	.85	1.73	.024 7.35 20.83
		72	1444	SL 7	4.49	83.30	50.16	.039	.030	.76	1.52	.037 8.19 21.45
78	1441		4.29	118.19	25.64	.039	.019	.49	1.89	.019 4.53 22.44		
92	1499		4.30	145.95	48.12	.022	.013	.57	1.06	.013 2.99 12.67		
93	1498		4.17	144.80	47.20	.022	.012	.56	1.08	.013 3.02 12.87		
94	1496		3.93	145.76	47.08	.021	.013	.82	1.11	.014 3.45 13.30		
95	1500	DY 2	4.59	151.72	50.41	.022	.013	.60	.98	.013 2.93 11.52		
98	1497		4.05	145.39	47.07	.022	.012	.57	1.09	.013 3.11 13.06		
104	1401	VG 1	5.01	155.73	54.83	.022	.012	.56	.89	.013 2.52 10.71		
69	1468	44	1453	HIW 10	4.27	131.60	153.12	.046	.040	.87	1.95	.045 10.51 26.18
		45	1402	VG 2	5.09	113.03	107.95	.039	.029	.74	1.18	.039 7.71 18.91
		57	1488	HIW 11	4.79	91.06	79.01	.049	.034	.70	1.51	.048 10.11 25.04
		59	1479	DY 1	3.95	95.43	110.00	.037	.026	.69	1.38	.036 9.23 22.99
		60	1471	DP 1	3.50	93.44	110.31	.037	.023	.64	1.46	.036 10.18 25.59
		61	1472	IB 751	3.29	90.54	110.42	.037	.023	.63	1.56	.035 10.74 27.30
		62	1473	IB 756	3.40	104.79	107.98	.037	.024	.65	1.45	.037 10.81 26.50
		63	1474	DP 2	2.79	93.26	108.93	.037	.022	.61	1.76	.036 12.97 32.55
		64	1473	IB 756	3.40	104.79	107.98	.037	.024	.65	1.45	.037 10.81 26.50
		65	1474	DP 2	2.79	93.26	108.93	.037	.022	.61	1.76	.036 12.97 32.55

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST		R.A. PPM		
											M	PPM			
69	1468	7	65	1449	BC 3	3.90	65.24	109.84	.038	.030	.77	1.81	.034	8.79	24.07
			66	1439		3.84	22.12	111.34	.037	.018	.48	1.98	.018	4.58	23.53
			67	1440		4.23	18.26	112.87	.038	.022	.59	1.85	.023	5.35	22.02
	68	14401	1440	ECC	3.92	22.19	111.18	.037	.021	.57	1.95	.021	5.41	23.14	
	70	1442			2.57	104.43	123.75	.039	.027	.70	2.33	.038	14.87	37.50	
	71	1448			2.64	146.29	112.61	.042	.030	.71	2.66	.039	14.68	39.11	
	72	1444	SL	7	4.30	136.25	86.54	.049	.037	.75	2.13	.042	9.87	28.05	
	73	1467	BC	16	3.07	44.57	9.54	.058	.048	.83	3.48	.055	17.98	46.49	
	92	1499			3.89	89.07	110.83	.037	.025	.67	1.44	.036	9.27	23.61	
	93	1498			3.89	86.77	111.21	.037	.025	.67	1.46	.036	9.15	23.58	
	94	1496			3.71	84.16	112.09	.038	.025	.65	1.56	.035	9.50	24.88	
	95	1500	DY	2	3.68	96.44	111.41	.037	.024	.66	1.43	.036	9.87	24.66	
	98	1497			3.79	85.47	111.34	.037	.025	.66	1.50	.035	9.33	24.19	
	104	1401	VG	1	3.66	104.80	109.32	.037	.024	.66	1.36	.037	10.01	24.57	
	105	1445	HIW	16	5.35	150.24	101.74	.041	.024	.60	1.33	.032	6.08	18.62	
	106	1437	BC	21	14.62	48.76	107.70	.062	.036	.58	.80	.044	3.04	10.43	
70	1442	59	1479	DY	1	6.50	98.97	5.95	.032	.013	1.41	1.02	.013	2.04	12.15
		60	1471	DP	1	6.04	98.08	3.88	.030	.012	.41	1.04	.013	2.09	12.34
		61	1472	IB	751	5.81	96.63	2.90	.030	.012	.41	1.06	.012	2.11	12.56
		62	1473	IB	756	5.97	104.64	9.04	.030	.013	1.41	1.05	.013	2.15	12.47
		64	1443	BC	5	4.88	84.42	1.54	.031	.024	.79	1.29	.024	4.99	15.33
		66	1439			4.90	53.41	157.58	.027	.015	.55	1.11	.016	3.21	13.46
		67	1440			5.09	48.48	163.40	.030	.018	.59	1.14	.020	4.01	14.47
		68	14401	1440	ECC	4.97	52.99	165.39	.029	.017	.58	1.13	.019	3.80	14.13
		69	1468	BC	7	2.57	104.43	123.75	.039	.027	.70	2.33	.038	14.87	37.50
		71	1448			1.86	33.20	119.70	.021	.013	.64	2.31	.013	7.22	27.44
		72	1444	SL	7	2.51	168.81	78.82	.035	.015	.43	2.84	.015	5.98	33.73
		73	1467	BC	16	2.85	173.41	13.90	.061	.037	.60	2.95	.059	20.71	52.85
		104	1401	VG	1	6.22	104.65	7.77	.031	.013	.41	1.01	.013	2.09	12.04
105	1445	HIW	16	7.37	135.80	27.98	.031	.021	.68	.85	.022	3.01	10.37		
71	1448	60	1471	DP	1	5.52	115.87	22.25	.030	.022	.75	1.13	.023	4.08	13.39
		61	1472	IB	751	5.25	115.12	21.21	.029	.022	.76	1.16	.022	4.26	13.75
		62	1473	IB	756	5.66	122.80	29.73	.031	.022	.73	1.12	.022	3.97	13.34
		63	1474	DP	2	4.86	119.00	28.15	.029	.023	.81	1.22	.023	4.77	14.48
		64	1443	BC	5	3.99	105.76	45.05	.032	.028	.90	1.60	.029	7.34	19.49
		66	1439			3.22	64.94	151.97	.026	.022	.85	1.68	.022	6.94	19.96
		67	1440			3.33	56.96	167.30	.029	.024	.83	1.78	.025	7.49	21.53
		68	14401	1440	ECC	3.28	64.09	172.36	.028	.024	.85	1.73	.024	7.35	20.83
		69	1468	BC	7	2.64	146.29	112.61	.042	.030	.71	2.66	.039	14.68	39.11
		70	1442			1.86	33.20	119.70	.021	.013	.64	2.31	.013	7.22	27.44
		72	1444	SL	7	1.76	121.08	79.45	.036	.023	.83	3.43	.031	17.49	49.99
		73	1467	BC	16	4.44	8.97	18.48	.062	.043	.70	2.02	.061	13.77	33.98
		78	1441			3.56	166.48	23.91	.046	.031	.68	2.18	.041	11.63	31.82
104	1401	VG	1	5.90	122.04	28.55	.031	.022	.73	1.07	.022	3.80	12.77		

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
72	1444	SL 7	66 1439		4.45	84.14	56.75	.038	.029	.77	1.45	.036	8.12	20.80
			67 1440		4.39	78.09	49.20	.039	.031	.79	1.57	.038	8.59	22.02
			68 14401	1440 ECC	4.49	83.30	50.16	.039	.030	.76	1.52	.037	8.19	21.45
			69 1468	BC 7	4.30	136.25	86.54	.049	.037	.75	2.13	.042	9.87	28.05
			70 1442		2.51	168.81	78.82	.035	.015	.43	2.84	.015	5.98	33.73
			71 1448		1.76	121.08	79.45	.036	.023	.63	3.43	.031	17.49	49.99
			78 1441		2.64	14.85	37.40	.053	.036	.68	3.07	.051	19.43	49.61
73	1467	BC 16	63 1474	DP 2	5.34	67.65	11.04	.055	.036	.66	1.93	.043	8.03	25.20
			64 1443	BC 5	5.61	53.89	17.19	.057	.041	.72	1.74	.052	9.26	24.95
			66 1439		6.79	32.09	18.41	.055	.041	.74	1.27	.055	8.05	19.97
			69 1468	BC 7	3.07	44.57	9.54	.058	.048	.83	3.48	.055	17.98	46.49
			70 1442		2.85	173.41	13.90	.061	.037	.60	2.95	.059	20.71	52.85
			71 1448		4.44	8.97	18.48	.062	.043	.70	2.02	.061	13.77	33.98
			74 1438		3.43	23.71	13.90	.064	.037	.57	2.27	.063	18.42	45.56
			75 1466		5.07	57.82	11.86	.058	.035	.60	1.97	.048	9.40	28.13
			77 1432	BC 17	7.17	91.87	4.80	.055	.023	.42	1.58	.023	3.27	18.83
			105 1445	HIW 16	5.40	117.03	8.18	.055	.033	.60	2.02	.036	6.64	24.85
74	1438		2 6785001	67A24	8.05	125.69	33.41	.048	.028	.59	1.22	.028	3.51	14.46
			3 678566	67A25	4.10	120.40	33.41	.048	.028	.59	2.39	.028	6.91	28.39
			66 1439		10.19	29.27	58.69	.054	.039	.72	.87	.051	5.00	13.04
			73 1467	BC 16	3.43	23.71	13.90	.064	.037	.57	2.27	.063	18.42	45.56
			75 1466		2.94	98.60	8.63	.030	.015	.52	2.08	.015	5.22	24.66
			77 1432	BC 17	6.69	120.23	30.92	.045	.024	.53	1.40	.024	3.57	16.63
			99 1480	BC 13A	4.17	121.58	33.25	.047	.028	.60	2.35	.028	6.81	27.89
			106 1437	BC 21	8.61	59.96	2.28	.048	.045	.92	1.14	.046	5.31	13.79
75	1466		2 6785001	67A24	5.60	139.56	49.66	.038	.024	.63	1.39	.024	4.25	16.46
			73 1467	BC 16	5.07	57.82	11.86	.058	.035	.60	1.97	.048	9.40	28.13
			74 1438		2.94	98.60	8.63	.030	.015	.52	2.08	.015	5.22	24.66
			76 1465	BC 20	3.41	73.14	66.04	.039	.030	.78	1.84	.039	11.41	28.05
			77 1432	BC 17	4.11	135.56	47.25	.035	.017	.50	1.74	.017	4.23	20.63
			106 1437	BC 21	6.58	43.76	94.07	.044	.037	.84	1.29	.040	6.04	16.32
			76 1465	BC 20	75 1466		3.41	73.14	66.04	.039	.030	.78	1.84	.039
77 1432	BC 17	3.94	5.70	96.26	.032	.017	.52	1.68	.017	4.26	20.01			
86 1435		3.62	59.99	102.84	.036	.029	.81	1.87	.033	9.20	24.56			
106 1437	BC 21	3.98	18.90	110.00	.033	.017	.51	1.73	.017	4.24	20.50			

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77	1432	2	6785001	67A24	1.53	150.35	146.50	.017	.013	.77	1.79	.017	11.19	27.43			
				BC 16	7.17	91.87	4.80	.055	.023	.42	1.58	.023	3.27	18.83			
					74	1438	6.69	120.23	30.92	.045	.024	.53	1.40	.024	3.57	16.63	
					75	1466	4.11	135.56	47.25	.035	.017	.50	1.74	.017	4.23	20.63	
					76	1465	BC 20	3.94	5.70	96.26	.032	.017	.52	1.68	.017	4.26	20.01
					104	1401	VG 1	12.90	85.46	132.03	.033	.022	.67	.45	.028	2.14	6.22
					106	1437	BC 21	7.86	12.34	104.81	.042	.022	.53	1.11	.023	2.86	13.19
78	1441	2	6785001	67A24	10.01	51.11	54.21	.048	.036	.76	.74	.048	4.75	11.65			
				BC 5	6.52	134.19	34.55	.046	.026	.56	1.44	.026	4.06	17.25			
					66	1439	4.29	119.23	26.03	.041	.019	.48	1.95	.020	4.55	23.19	
					67	1440	3.98	114.39	26.22	.038	.018	.46	1.99	.018	4.46	23.59	
					68	14401	1440 ECC	4.29	118.19	25.64	.039	.019	.49	1.89	.019	4.53	22.44
					71	1448	3.56	166.48	23.91	.046	.031	.68	2.18	.041	11.63	31.82	
					72	1444	SL 7	2.64	14.85	37.40	.053	.036	.68	3.07	.051	19.43	49.61
					79	1428	5.80	137.50	129.21	.076	.065	.86	2.33	.076	13.04	32.03	
79	1428	2	6785001	67A24	11.25	20.20	126.31	.074	.055	.75	1.33	.057	5.05	16.04			
					67	1440	9.59	128.12	127.34	.074	.056	.75	1.20	.074	7.74	18.96	
					78	1441	5.80	137.50	129.21	.076	.065	.86	2.33	.076	13.04	32.03	
					80	1430	SL 12	4.28	28.11	48.39	.061	.046	.76	2.33	.059	13.86	34.85
					81	1425	5.97	123.43	34.22	.053	.021	.41	1.82	.021	3.60	21.57	
80	1430	SL 12	79	1428	4.28	28.11	48.39	.061	.046	.76	2.33	.059	13.86	34.85			
					82	1429	7.45	106.89	33.27	.073	.058	.80	1.98	.060	7.99	23.86	
81	1425	2	6785001	67A24	13.89	175.51	97.35	.079	.055	.70	1.16	.056	4.04	13.91			
					79	1428	5.97	123.43	34.22	.053	.021	.41	1.82	.021	3.60	21.57	
					82	1429	6.44	40.44	129.60	.059	.022	.38	1.88	.022	3.46	22.36	
82	1429	2	6785001	67A24	10.38	149.58	96.47	.064	.059	.93	1.24	.061	5.88	15.04			
					80	1430	SL 12	7.45	106.89	33.27	.073	.058	.80	1.98	.060	7.99	23.86
					81	1425	6.44	40.44	129.60	.059	.022	.38	1.88	.022	3.46	22.36	
					83	1431	4.97	36.51	126.47	.048	.020	.41	1.99	.020	3.95	23.68	
83	1431	2	6785001	67A24	9.58	121.14	173.87	.063	.056	.89	1.31	.059	6.15	16.11			
					82	1429	4.97	36.51	126.47	.048	.020	.41	1.99	.020	3.95	23.68	
					84	1436	4.32	142.53	71.43	.119	.084	.71	5.53	.088	20.44	67.48	
					85	1433	6.54	43.34	39.33	.067	.060	.90	1.90	.067	10.21	25.02	

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84	1436	83	1431		4.32	142.53	71.43	.119	.084	.71	5.53	.088	20.44	67.48
		85	1433		7.24	79.37	70.97	.101	.078	.77	2.25	.101	13.95	34.33
		96	1434	HIW 17	5.24	25.66	76.88	.101	.078	.78	3.65	.088	16.77	47.22
		107	1427		7.45	54.65	81.95	.098	.077	.78	2.27	.094	12.66	32.37
85	1433	2	6785001	67A24	12.69	90.89	158.59	.069	.061	.88	1.10	.062	4.87	13.32
		83	1431		6.54	43.34	39.33	.067	.060	.90	1.90	.067	10.21	25.02
		84	1436		7.24	79.37	70.97	.101	.078	.77	2.25	.101	13.95	34.33
		96	1434	HIW 17	5.91	125.00	35.31	.045	.030	.68	1.56	.030	5.13	18.53
		107	1427		3.15	160.87	70.09	.032	.016	.50	2.11	.016	5.09	25.03
86	1435	76	1465	BC 20	3.62	59.99	102.84	.036	.029	.81	1.87	.033	9.20	24.56
		106	1437	BC 21	2.68	136.67	47.86	.026	.015	.58	2.03	.015	5.72	24.09
		107	1427		9.84	115.76	123.46	.076	.055	.72	1.15	.076	7.68	18.89
87	1426	1	6785000	67A35	16.24	108.55	126.49	.136	.112	.82	1.45	.134	8.25	20.53
		2	6785001	67A24	24.21	142.12	126.49	.136	.112	.82	.97	.134	5.55	13.77
		107	1427		22.12	171.73	128.73	.148	.114	.77	1.22	.133	6.02	16.39
88	1404	29	1450	HIW 6	5.82	149.13	50.65	.039	.033	.84	1.38	.033	5.68	16.42
		31	1409	VG 9	4.25	120.16	29.30	.027	.019	.73	1.29	.019	4.56	15.31
		32	1410	VG 10	5.46	126.75	41.57	.034	.025	.73	1.28	.025	4.54	15.26
		37	1407	VG 7	2.67	131.64	34.41	.021	.017	.79	1.63	.017	6.26	19.39
		38	1424	HIW 6KA	1.83	106.19	12.97	.014	.010	.74	1.57	.010	5.67	18.70
		39	1423	HIW 5KA	1.68	83.46	173.53	.014	.011	.78	1.68	.011	6.37	19.97
		40	1405	VG 5	1.21	112.32	12.35	.011	.011	.97	1.87	.011	8.77	22.22
		41	1422	HIW 4KA	1.48	107.12	17.11	.012	.010	.81	1.71	.010	6.69	20.32
		42	1461	HIW 1KA	2.26	73.36	160.84	.016	.012	.76	1.45	.012	5.35	17.27
		44	1453	HIW 10	3.76	103.79	179.13	.040	.024	.60	2.14	.025	6.69	26.00
		45	1402	VG 2	2.77	128.78	49.64	.019	.012	.65	1.41	.013	4.61	16.96
		46	1403	VG 3	2.16	138.88	51.51	.016	.009	.56	1.53	.009	4.19	18.18
		47	1457	HIW 3KA	1.63	140.38	51.52	.013	.008	.62	1.61	.008	4.87	19.10
		48	14571	JK1	1.70	139.56	92.20	.015	.012	.80	1.66	.013	7.91	21.59
		49	1454	JK 4	1.02	176.25	95.38	.010	.008	.76	2.12	.008	7.88	25.26
		50	1452	HIW 2KA	1.33	179.17	98.33	.012	.008	.70	1.84	.008	6.35	22.06
		51	1459	JK 3	1.50	166.91	83.22	.012	.008	.65	1.68	.008	5.34	19.84
		52	1460	IN 4	1.33	172.26	95.28	.012	.008	.67	1.82	.008	6.19	21.88
		53	1458	IN 1	1.52	155.95	66.17	.012	.008	.65	1.68	.008	5.31	19.93
		54	1456	IN 2	1.73	161.31	69.82	.014	.008	.60	1.65	.008	4.84	19.60
55	1455	IN 3	2.08	160.91	71.74	.017	.009	.53	1.69	.009	4.31	20.02		
56	1451	JK 2	2.11	168.37	81.25	.016	.008	.47	1.59	.008	3.62	18.92		
57	1488	HIW 11	4.18	150.48	65.77	.042	.020	.49	2.06	.021	4.95	24.54		
58	1446	U+U 611	5.30	.79	88.67	.027	.014	.51	1.03	.014	2.59	12.29		
59	1479	DY 1	4.45	139.00	58.99	.025	.016	.65	1.16	.017	3.78	13.95		
60	1471	DP 1	4.86	136.40	58.30	.025	.017	.67	1.05	.017	3.51	12.57		

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88	1404	4	61	1472	IB 751	5.13	136.07	58.16	.025	.017	.66	1.01	.017	3.35	12.16
			62	1473	IB 756	4.57	128.80	54.52	.025	.017	.70	1.10	.018	3.95	13.30
			63	1474	DP 2	5.41	131.29	56.28	.026	.017	.66	.99	.018	3.37	11.97
			64	1443	BC 5	6.60	137.25	59.47	.036	.021	.58	1.11	.022	3.34	13.44
			67	1440		9.51	144.47	54.87	.037	.020	.53	.80	.020	2.06	9.44
			89	1462	HIW 9	1.41	22.89	140.84	.018	.014	.77	2.55	.015	10.68	31.80
			92	1499		4.81	142.02	67.61	.026	.019	.70	1.11	.019	4.00	13.46
			93	1498		4.94	143.10	67.46	.027	.018	.69	1.09	.019	3.84	13.22
			94	1496		5.18	142.45	67.13	.027	.019	.70	1.06	.020	3.79	12.80
			95	1500	DY 2	4.61	136.07	58.27	.025	.018	.74	1.09	.019	4.02	13.12
			98	1497		5.07	142.67	66.50	.027	.018	.69	1.07	.019	3.74	12.95
			100	1408	VG 8	3.03	118.54	26.71	.023	.016	.71	1.55	.016	5.34	18.41
			101	1490	HIW 7KA	2.61	117.34	25.33	.022	.017	.75	1.76	.017	6.42	20.91
			102	1406	VG 6	1.98	111.69	16.13	.015	.011	.74	1.56	.011	5.60	18.54
			104	1401	VG 1	4.33	130.16	57.16	.023	.016	.69	1.08	.017	3.85	13.14
105	1445	HIW 16	4.29	77.69	90.43	.025	.021	.84	1.01	.025	5.74	14.17			
89	1462	HIW 9	29	1450	HIW 6	5.11	136.30	28.44	.037	.035	.95	1.50	.036	6.96	17.87
			31	1409	VG 9	4.30	101.22	.32	.029	.021	.72	1.36	.021	4.91	16.33
			32	1410	VG 10	5.30	111.82	21.13	.034	.028	.82	1.32	.028	5.23	15.71
			37	1407	VG 7	2.59	100.66	173.07	.024	.017	.69	1.90	.018	6.82	23.07
			38	1424	HIW 6KA	2.43	71.12	160.34	.021	.011	.51	1.79	.011	4.42	21.24
			39	1423	HIW 5KA	2.67	56.07	152.70	.022	.013	.59	1.66	.013	4.86	19.86
			40	1405	VG 5	1.87	63.42	156.50	.018	.011	.60	1.94	.011	5.67	23.09
			41	1422	HIW 4KA	2.14	66.21	157.69	.020	.012	.57	1.95	.012	5.44	23.17
			42	1461	HIW 1KA	3.34	54.36	147.75	.024	.014	.60	1.46	.014	4.25	17.36
			44	1453	HIW 10	3.80	125.22	176.68	.038	.028	.73	1.87	.032	8.47	24.51
			45	1402	VG 2	3.44	151.98	68.40	.025	.020	.82	1.49	.020	5.94	17.69
			46	1403	VG 3	3.05	163.40	72.00	.023	.019	.85	1.54	.019	6.36	18.26
			47	1457	HIW 3KA	2.60	169.05	88.94	.021	.019	.91	1.63	.019	7.28	19.45
			48	14571	JK 1	2.65	167.88	108.38	.023	.020	.84	1.75	.021	7.77	21.59
			49	1454	JK 4	2.36	11.75	121.31	.021	.017	.81	1.81	.018	7.43	21.92
			50	1452	HIW 2KA	2.67	11.40	117.77	.022	.017	.78	1.68	.018	6.61	20.23
			51	1459	JK 3	2.76	4.32	109.87	.022	.018	.81	1.61	.018	6.52	19.35
			52	1460	IN 4	2.64	8.02	115.60	.022	.017	.79	1.68	.018	6.72	20.35
			53	1458	IN 1	2.68	178.51	102.30	.021	.018	.87	1.62	.019	6.94	19.43
			54	1456	IN 2	2.93	179.90	97.28	.022	.019	.84	1.57	.019	6.39	18.65
			55	1455	IN 3	3.26	177.69	88.90	.024	.019	.78	1.55	.019	5.86	18.40
			56	1451	JK 2	3.36	2.09	96.61	.024	.018	.74	1.50	.018	5.39	17.83
			57	1488	HIW 11	5.16	162.96	70.27	.045	.025	.55	1.80	.025	4.80	21.36
			59	1479	DY 1	5.22	153.02	74.52	.030	.021	.69	1.17	.021	4.07	14.10
			60	1471	DP 1	5.57	149.80	74.70	.030	.021	.69	1.08	.021	3.84	13.10
61	1472	IB 751	5.83	148.89	73.89	.030	.021	.69	1.05	.022	3.69	12.72			
62	1473	IB 756	5.13	144.10	72.83	.029	.021	.73	1.15	.022	4.35	14.02			
63	1474	DP 2	6.01	144.15	71.52	.031	.021	.69	1.04	.022	3.74	12.64			
88	1404	VG 4	1.41	22.89	140.84	.018	.014	.77	2.55	.015	10.68	31.80			
90	678756	MT MYE	5.97	46.27	70.39	.037	.036	.97	1.26	.037	6.23	15.34			
95	1500	DY 2	5.32	150.15	77.17	.030	.022	.74	1.13	.023	4.25	13.64			
100	1408	VG 8	3.03	118.54	26.71	.023	.016	.71	1.55	.016	5.34	18.41			

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ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
89	1462 9	101	1490	HIW 7KA	2.87	88.09	173.70	.026	.017	.67	1.84	.017	5.98	21.95
		102	1406	VG 6	2.46	76.72	163.38	.021	.011	.51	1.76	.011	4.41	20.97
		104	1401	VG 1	4.94	145.97	74.89	.028	.020	.72	1.15	.021	4.29	14.00
		105	1445	HIW 16	3.66	96.00	92.23	.029	.022	.75	1.25	.029	8.04	19.72
90	678756 MT MYE	3	678566	67A25	2.63	131.77	38.31	.024	.015	.61	1.91	.015	5.69	22.71
		25	1492	HIW 13	8.22	8.90	165.65	.100	.077	.77	2.03	.097	11.78	29.84
		43	1495	HIW 15	7.61	52.80	43.30	.069	.065	.94	1.77	.069	9.09	22.31
		89	1462	HIW 9	5.97	46.27	70.39	.037	.036	.97	1.26	.037	6.23	15.34
		91	1482	HIW 1	23.06	117.22	46.89	.089	.046	.52	.76	.053	2.29	9.46
		97	1491	HIW 14	4.82	71.65	47.54	.057	.037	.65	1.76	.055	11.33	29.21
		99	1480	BC 13A	2.55	130.19	39.00	.024	.015	.61	1.95	.015	5.73	23.17
		105	1445	HIW 16	4.56	8.55	80.78	.029	.028	.96	1.32	.028	6.20	15.72
		109	108	GRAVITY 10	5.44	33.62	54.04	.078	.056	.72	2.25	.076	13.98	35.32
		110	111	GRAVITY 11	8.43	66.01	96.20	.076	.056	.73	1.51	.072	8.50	22.15
91	1482 HIW 1	5	1470	RC 11	6.72	3.02	89.46	.044	.029	.66	1.34	.029	4.33	15.97
		7	1463	RC 2	8.49	166.67	72.13	.052	.030	.58	1.25	.030	3.53	14.89
		9	1481	HIW 2	6.22	118.33	29.78	.043	.024	.56	1.44	.024	3.89	17.10
		10	1447		2.59	67.43	158.14	.026	.015	.55	2.10	.015	5.61	24.91
		11	1464	HIW 3	9.13	106.79	15.41	.058	.029	.50	1.32	.029	3.21	15.68
		90	678756	MT MYE	23.06	117.22	46.89	.089	.046	.52	.76	.053	2.29	9.46
92	1499	38	1424	HIW 6KA	6.38	132.37	51.66	.032	.020	.63	1.01	.020	3.16	12.12
		39	1423	HIW 5KA	5.86	127.91	48.58	.030	.020	.66	1.04	.020	3.43	12.44
		40	1405	VG 5	5.90	136.17	58.62	.030	.019	.64	1.04	.020	3.40	12.57
		41	1422	HIW 4KA	6.08	134.04	54.64	.031	.020	.64	1.03	.020	3.29	12.37
		44	1453	HIW 10	2.98	13.55	177.43	.039	.025	.64	1.80	.038	12.68	31.81
		45	1402	VG 2	2.20	158.80	102.53	.021	.018	.88	1.85	.019	8.58	22.80
		46	1403	VG 3	2.66	144.58	78.88	.021	.019	.91	1.60	.019	7.29	19.22
		47	1457	HIW 3KA	3.18	142.87	75.99	.022	.019	.88	1.39	.020	6.17	16.76
		48	14571	JK1	3.11	143.38	102.65	.024	.020	.84	1.44	.022	7.17	18.76
		49	1454	JK 4	4.01	133.82	57.39	.024	.020	.82	1.21	.020	4.94	14.55
		50	1452	HIW 2KA	3.84	129.99	51.09	.023	.020	.86	1.23	.020	5.19	14.72
		51	1459	JK 3	3.51	131.67	56.41	.022	.020	.89	1.29	.020	5.63	15.39
		52	1460	IN 4	3.72	131.66	57.40	.023	.020	.87	1.24	.020	5.38	14.92
		53	1458	IN 1	3.36	135.79	62.26	.022	.020	.89	1.34	.020	5.88	16.09
		54	1456	IN 2	3.23	131.87	54.45	.022	.020	.89	1.39	.020	6.09	16.61
		55	1455	IN 3	2.92	128.73	59.84	.022	.020	.90	1.54	.020	6.89	18.50
		56	1451	JK 2	3.07	124.26	57.66	.021	.020	.92	1.42	.020	6.49	17.10
		57	1488	HIW 11	.91	99.59	62.92	.039	.020	.51	6.45	.034	37.06	105.82
		58	1446	U+U 611	3.39	63.60	153.90	.019	.011	.57	1.14	.011	3.17	13.55
		59	1479	DY 1	.44	174.26	66.82	.017	.015	.90	7.72	.015	34.33	92.50
60	1471	DP 1	.48	55.05	79.79	.015	.013	.88	5.96	.015	31.32	78.25		
61	1472	IB 751	.61	81.07	80.47	.015	.013	.87	4.54	.015	25.19	61.71		
62	1473	IB 756	1.11	32.69	76.83	.016	.014	.88	2.80	.015	13.65	35.43		
63	1474	DP 2	1.13	78.65	81.32	.017	.014	.84	2.55	.017	14.65	35.90		

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/HJ	AZ SEC	DIST M	PPM	R.A. PPM	
92	1499	64	1443	BC 5	1.85	124.70	63.21	.026	.017	.85	2.72	.019	10.55	34.69
		65	1449	BC 3	1.61	167.47	44.98	.028	.017	.63	3.22	.021	12.99	42.10
		66	1439		4.27	145.04	56.09	.020	.011	.56	.99	.011	2.69	11.75
		67	1440		4.71	146.98	44.95	.023	.015	.66	1.01	.016	3.37	12.15
		68	14401	1440 ECC	4.30	145.95	48.12	.022	.013	.57	1.06	.013	2.99	12.67
		69	1468	BC 7	3.89	89.07	110.83	.037	.025	.67	1.44	.036	9.27	23.61
		88	1404	VG 4	4.81	142.02	67.61	.026	.019	.70	1.12	.019	4.00	13.46
		93	1498		.16	178.43	170.91	.004	.002	.39	2.44	.004	28.57	70.50
		94	1496		.37	147.97	145.05	.007	.004	.31	1.97	.007	18.74	45.95
		95	1500	DY 2	.53	26.38	106.59	.016	.015	.94	6.13	.015	28.14	72.97
		98	1497		.28	154.67	150.83	.006	.003	.41	2.08	.006	24.04	59.01
		102	1406	VG 6	6.60	133.29	51.80	.033	.020	.62	1.01	.020	3.10	12.08
		104	1401	VG 1	1.06	19.39	98.60	.015	.014	.89	2.96	.014	12.82	35.26
		105	1445	HIW 16	4.87	14.66	102.30	.024	.013	.57	1.00	.013	2.76	11.87
93	1498	38	1424	HIW 6KA	6.49	133.36	52.01	.032	.020	.61	1.00	.020	3.06	12.00
		39	1423	HIW 5KA	5.96	129.06	49.03	.030	.019	.65	1.03	.020	3.33	12.31
		40	1405	VG 5	6.01	137.16	58.79	.030	.019	.63	1.03	.020	3.29	12.41
		41	1422	HIW 4KA	6.19	135.05	54.92	.031	.019	.62	1.02	.020	3.19	12.23
		44	1453	HIW 10	3.13	12.80	177.44	.039	.025	.64	1.71	.038	12.07	30.21
		45	1402	VG 2	2.35	160.08	99.88	.021	.018	.88	1.75	.019	7.95	21.40
		46	1403	VG 3	2.79	146.36	76.88	.021	.019	.90	1.53	.019	6.87	18.41
		47	1457	HIW 3KA	3.31	144.44	74.63	.022	.019	.87	1.34	.019	5.86	16.21
		48	14571	JKI	3.24	144.96	100.43	.024	.020	.84	1.40	.022	6.80	18.04
		49	1454	JK 4	4.12	135.34	57.69	.024	.019	.81	1.19	.020	4.75	14.26
		50	1452	HIW 2KA	3.94	131.68	51.95	.023	.020	.84	1.21	.020	5.00	14.43
		51	1459	JK 3	3.62	133.47	56.85	.022	.019	.87	1.26	.020	5.40	15.03
		52	1460	IN 4	3.83	133.36	57.70	.023	.020	.86	1.22	.020	5.17	14.60
		53	1458	IN 1	3.48	137.53	62.14	.022	.019	.87	1.31	.020	5.62	15.66
		54	1456	IN 2	3.34	133.81	55.12	.022	.019	.88	1.36	.019	5.82	16.17
		55	1455	IN 3	3.03	130.98	59.66	.022	.020	.88	1.50	.020	6.58	17.96
		56	1451	JK 2	3.16	126.55	57.54	.022	.019	.90	1.39	.020	6.23	16.68
		57	1488	HIW 11	.95	108.81	62.91	.039	.020	.51	6.81	.031	32.38	101.08
		58	1446	U+U 61I	3.33	66.04	155.82	.018	.011	.58	1.14	.011	3.22	13.58
		59	1479	DY 1	.60	175.35	67.61	.017	.015	.89	5.67	.015	25.02	68.02
		60	1471	DP 1	.58	42.03	80.50	.015	.013	.87	5.00	.014	24.98	64.22
		61	1472	IB 751	.65	67.26	81.35	.015	.013	.87	4.24	.015	23.33	57.58
		62	1473	IB 756	1.24	28.63	78.42	.016	.014	.87	2.52	.015	11.94	31.59
		63	1474	DP 2	1.17	71.07	82.60	.016	.014	.84	2.45	.016	14.02	34.55
		64	1443	BC 5	1.76	120.60	63.17	.026	.017	.65	2.78	.020	11.35	36.12
		65	1449	BC 3	1.46	166.31	44.58	.027	.017	.63	3.55	.021	14.14	46.23
		66	1439		4.14	143.85	55.33	.020	.011	.56	1.00	.011	2.72	11.87
		67	1440		4.58	145.96	43.78	.023	.015	.66	1.02	.016	3.41	12.32
		68	14401	1440 ECC	4.17	144.80	47.20	.022	.012	.56	1.08	.013	3.02	12.87
		69	1468	BC 7	3.89	86.77	111.21	.037	.025	.67	1.46	.036	9.15	23.58
		88	1404	VG 4	4.94	143.10	67.46	.027	.018	.69	1.09	.019	3.84	13.22
		92	1499		.16	178.43	170.91	.004	.002	.39	2.44	.004	28.57	70.50
		94	1496		.25	129.46	133.66	.006	.002	.40	2.00	.006	23.68	58.14

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93	1498	98	1497		.13	126.67	132.07	.005	.002	.32	2.41	.005 34.74 85.45
		102	1406	VG 6	6.71	134.24	52.15	.033	.020	.61	1.00	.020 3.02 11.96
		104	1401	VG 1	1.20	16.74	97.30	.015	.013	.87	2.59	.013 11.07 30.91
		105	1445	HIW 16	5.02	14.17	101.90	.024	.013	.55	.98	.013 2.62 11.62
94	1496	38	1424	HIW 6KA	6.74	133.22	51.51	.032	.020	.62	.98	.020 3.04 11.73
		39	1423	HIW 5KA	6.21	129.08	48.38	.030	.020	.66	1.00	.020 3.28 12.00
		40	1405	VG 5	6.26	136.86	58.32	.031	.020	.64	1.01	.020 3.26 12.09
		41	1422	HIW 4KA	6.44	134.83	54.41	.031	.020	.64	1.00	.020 3.16 11.93
		44	1453	HIW 10	3.25	8.87	176.96	.039	.025	.65	1.64	.038 11.78 29.22
		45	1402	VG 2	2.57	157.25	103.41	.021	.018	.88	1.62	.019 7.54 20.02
		46	1403	VG 3	3.03	144.99	79.53	.021	.019	.91	1.43	.020 6.54 17.24
		47	1457	HIW 3KA	3.55	143.40	75.57	.022	.020	.88	1.27	.020 5.64 15.36
		48	14571	JK1	3.48	143.86	101.88	.024	.021	.85	1.32	.023 6.51 17.07
		49	1454	JK 4	4.37	135.01	56.85	.024	.020	.82	1.14	.020 4.62 13.67
		50	1452	HIW 2KA	4.19	131.55	50.47	.024	.020	.85	1.16	.020 4.84 13.81
		51	1459	JK 3	3.87	133.21	55.46	.023	.020	.89	1.20	.020 5.21 14.31
		52	1460	IN 4	4.08	133.12	56.45	.023	.020	.87	1.17	.020 5.00 13.94
		53	1458	IN 1	3.72	137.00	61.55	.023	.020	.88	1.24	.020 5.41 14.86
		54	1456	IN 2	3.59	133.51	53.72	.022	.020	.89	1.28	.020 5.59 15.30
		55	1455	IN 3	3.28	130.87	58.71	.023	.020	.90	1.40	.020 6.25 16.83
		56	1451	JK 2	3.41	126.76	55.50	.022	.020	.92	1.31	.020 5.94 15.71
		57	1488	HIW 11	1.19	113.04	63.08	.039	.020	.52	5.71	.030 25.05 81.16
		58	1446	U+U 611	3.45	69.75	156.74	.019	.011	.56	1.15	.011 3.17 13.72
		59	1479	DY 1	.79	162.25	77.62	.017	.015	.92	4.36	.015 19.47 51.81
		60	1471	DP 1	.62	18.34	93.78	.015	.014	.88	5.12	.014 22.29 61.25
		61	1472	IB 751	.58	44.77	94.43	.016	.014	.87	5.29	.014 25.07 66.14
		62	1473	IB 756	1.31	17.86	89.08	.016	.014	.88	2.54	.015 11.10 30.54
		63	1474	DP 2	1.06	59.48	92.38	.017	.014	.84	2.91	.016 15.14 38.80
		64	1443	BC 5	1.51	119.14	64.99	.026	.017	.68	3.17	.021 13.67 41.62
		65	1449	BC 3	1.26	173.09	44.14	.027	.018	.66	3.91	.022 17.45 52.71
		66	1439		3.90	144.77	57.10	.019	.012	.63	1.03	.012 3.14 12.20
67	1440		4.34	146.89	42.84	.022	.016	.71	1.05	.016 3.78 12.69		
68	14401	1440 ECC	3.93	145.76	47.08	.021	.013	.62	1.11	.014 3.45 13.30		
69	1468	BC 7	3.71	84.16	112.09	.038	.025	.65	1.56	.035 9.50 24.88		
88	1404	VG 4	5.18	142.45	67.13	.027	.019	.70	1.06	.020 3.79 12.80		
92	1499		.37	147.97	145.05	.007	.004	.51	1.97	.007 18.74 45.95		
93	1498		.25	129.46	133.66	.006	.002	.40	2.00	.006 23.68 58.14		
95	1500	DY 2	.79	2.84	116.75	.016	.015	.91	4.20	.015 19.08 50.64		
98	1497		.12	132.69	132.40	.006	.001	.22	2.47	.006 54.29 133.00		
104	1401	VG 1	1.32	6.73	106.09	.016	.014	.86	2.45	.014 10.30 29.25		

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95	1500	DY 2	38	1424	HIW 6KA	6.26	127.70	44.62	.031	.019	.63	1.00	.019	3.08	11.95
			39	1423	HIW 5KA	5.78	122.75	40.44	.029	.019	.66	1.02	.019	3.32	12.22
			40	1405	VG 5	5.74	131.18	51.49	.029	.019	.66	1.03	.019	3.38	12.32
			41	1422	HIW 4KA	5.94	129.16	47.33	.030	.019	.64	1.02	.019	3.24	12.17
			44	1453	HIW 10	2.46	10.80	177.58	.038	.021	.55	1.85	.037	15.11	37.71
			45	1402	VG 2	1.89	146.82	139.77	.018	.016	.90	1.78	.018	9.53	23.39
			46	1403	VG 3	2.45	133.59	15.24	.019	.018	.95	1.57	.018	7.40	18.82
			47	1457	HIW 3KA	2.98	133.70	40.46	.020	.019	.94	1.36	.019	6.23	16.19
			48	14571	JK 1	2.91	134.02	118.00	.022	.020	.90	1.40	.022	7.45	18.40
			49	1454	JK 4	3.89	126.33	38.50	.023	.019	.83	1.20	.019	4.81	14.20
			50	1452	HIW 2KA	3.75	122.09	28.10	.022	.019	.84	1.22	.019	4.96	14.45
			51	1459	JK 3	3.41	123.03	26.04	.021	.018	.88	1.27	.018	5.41	15.12
			52	1460	IN 4	3.62	123.53	29.68	.022	.019	.87	1.23	.019	5.19	14.57
			53	1458	IN 1	3.22	126.86	30.70	.021	.019	.89	1.33	.019	5.76	15.79
			54	1456	IN 2	3.13	122.48	24.96	.021	.018	.87	1.38	.018	5.85	16.37
			55	1455	IN 3	2.86	118.29	26.71	.021	.019	.90	1.51	.019	6.59	17.90
			56	1451	JK 2	3.04	114.31	18.70	.020	.018	.90	1.39	.018	6.08	16.51
			57	1488	HIW 11	1.18	74.08	61.05	.038	.018	.49	3.47	.037	31.32	78.27
			58	1446	U+U 611	3.82	58.79	154.67	.020	.014	.68	1.08	.014	3.55	12.81
			59	1479	DY 1	.28	82.24	.20	.013	.010	.77	9.46	.010	35.87	112.80
			60	1471	DP 1	.25	142.41	148.27	.009	.003	.34	2.48	.009	33.71	82.97
			61	1472	IB 751	.53	136.12	158.05	.010	.007	.75	2.94	.009	17.47	44.17
			62	1473	IB 756	.58	38.43	9.82	.009	.006	.76	2.48	.008	13.92	35.90
			63	1474	DP 2	.91	106.24	144.88	.010	.009	.82	2.12	.010	10.73	28.13
			64	1443	BC 5	1.99	139.98	64.46	.025	.017	.67	2.57	.018	8.81	31.04
			65	1449	BC 3	2.05	176.84	43.99	.027	.018	.66	2.32	.022	10.91	32.00
			66	1439		4.54	150.93	60.19	.020	.012	.59	.90	.012	2.55	10.64
67	1440		5.00	152.22	47.60	.023	.016	.70	.92	.016	3.28	11.11			
68	14401	1440 ECC	4.59	151.72	50.41	.022	.013	.60	.96	.013	2.93	11.52			
69	1468	BC 7	3.68	96.44	111.41	.037	.024	.66	1.43	.036	9.87	24.66			
88	1404	VG 4	4.61	136.07	58.27	.025	.018	.74	1.09	.019	4.02	13.12			
89	1462	HIW 9	5.32	150.15	77.17	.030	.022	.74	1.13	.023	4.25	13.64			
92	1499		.53	26.38	106.59	.016	.015	.94	6.13	.015	28.14	72.97			
93	1498		.67	20.14	104.21	.016	.015	.94	4.82	.015	21.89	57.30			
94	1496		.79	2.84	116.75	.016	.015	.91	4.20	.015	19.08	50.64			
98	1497		.72	9.90	102.96	.016	.015	.93	4.47	.015	20.26	53.07			
104	1401	VG 1	.54	12.47	158.41	.011	.006	.59	3.14	.010	18.20	49.94			
105	1445	HIW 16	4.35	13.25	107.79	.020	.011	.51	.97	.011	2.44	11.55			
96	1434	HIW 17	84	1436		5.24	25.66	76.88	.101	.078	1.78	3.65	.088	16.77	47.22
			85	1433		5.91	125.00	35.31	.045	.030	.68	1.56	.030	5.13	18.53
			97	1491	HIW 14	16.75	114.15	92.52	.078	.071	.91	.80	.077	4.59	11.38
			105	1445	HIW 16	20.57	92.29	133.86	.075	.055	.73	.65	.067	3.26	8.96
			106	1437	BC 21	9.03	130.12	118.61	.075	.053	.71	1.24	.075	8.27	20.47
			107	1427		3.83	96.20	4.99	.035	.017	.51	1.87	.018	4.57	22.17

DEPARTMENT OF ENERGY, MINES AND RESOURCES
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CLARKE 1866

ELLIPSES BASED ON THE A PRIORI VARIANCE FACTOR = 1.0000

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 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
97	1491	HIW 14	3 678566	67A25	4.19	38.60	52.43	.055	.035	.64	1.80	.054	12.99	32.38
			43 1495	HIW 15	3.42	25.77	18.61	.056	.043	.78	2.63	.056	16.24	39.90
			90 678756	MT MYE	4.82	71.65	47.54	.057	.037	.65	1.76	.055	11.33	29.21
			96 1434	HIW 17	16.75	114.15	92.52	.078	.071	.91	.88	.077	4.59	11.38
			99 1480	BC 13A	4.11	39.74	52.42	.055	.035	.63	1.81	.054	13.23	32.91
			109 108	GRAVITY 10	3.39	152.58	52.84	.094	.065	.69	5.66	.066	19.42	67.77
			110 111	GRAVITY 11	3.67	58.60	81.13	.088	.068	.77	4.00	.086	23.32	58.94
98	1497	38 1424	HIW 6KA	6.63	133.23	51.53	.032	.020	.61	.99	.020	2.99	11.84	
		39 1423	HIW 5KA	6.10	129.01	48.50	.030	.019	.64	1.01	.020	3.24	12.13	
		40 1405	VG 5	6.14	136.94	58.16	.031	.019	.63	1.02	.020	3.21	12.22	
		41 1422	HIW 4KA	6.33	134.87	54.36	.031	.019	.62	1.01	.020	3.11	12.05	
		44 1453	HIW 10	3.19	10.60	177.65	.039	.025	.64	1.66	.038	11.92	29.64	
		45 1402	VG 2	2.46	158.37	98.06	.020	.018	.88	1.67	.019	7.60	20.38	
		46 1403	VG 3	2.92	145.48	73.87	.021	.019	.90	1.47	.019	6.56	17.65	
		47 1457	HIW 3KA	3.43	143.76	72.18	.022	.019	.87	1.30	.019	5.63	15.65	
		48 14571	JK 1	3.37	144.25	99.11	.024	.020	.85	1.35	.022	6.55	17.33	
		49 1454	JK 4	4.26	135.07	56.33	.024	.019	.80	1.18	.020	4.59	13.90	
		50 1452	HIW 2KA	4.08	131.52	50.46	.023	.020	.84	1.18	.020	4.82	14.06	
		51 1459	JK 3	3.75	133.22	54.71	.022	.019	.87	1.22	.019	5.19	14.60	
		52 1460	IN 4	3.97	133.14	55.75	.023	.020	.85	1.19	.020	4.98	14.20	
		53 1458	IN 1	3.61	137.13	59.92	.022	.019	.87	1.27	.019	5.40	15.17	
		54 1456	IN 2	3.48	133.54	53.09	.022	.019	.87	1.31	.019	5.59	15.65	
		55 1455	IN 3	3.16	130.80	57.33	.022	.020	.88	1.44	.020	6.28	17.28	
		56 1451	JK 2	3.30	126.56	54.60	.022	.019	.90	1.34	.020	5.95	16.09	
		57 1488	HIW 11	1.08	110.99	62.79	.039	.020	.50	6.13	.030	27.83	89.10	
		58 1446	U+U 61I	3.39	68.01	157.54	.019	.011	.57	1.13	.011	3.12	13.41	
		59 1479	DY 1	.69	166.99	66.65	.016	.015	.89	4.90	.015	21.26	58.41	
		60 1471	DP 1	.58	28.78	80.27	.015	.013	.87	5.09	.014	23.93	63.51	
		61 1472	IB 751	.59	56.03	81.54	.015	.013	.86	4.69	.015	24.97	62.68	
		62 1473	IB 756	1.27	22.62	78.07	.016	.014	.86	2.49	.014	11.45	30.86	
		63 1474	DP 2	1.10	65.29	83.10	.016	.014	.83	2.61	.016	14.70	36.55	
		64 1463	BC 5	1.63	120.10	63.50	.026	.017	.65	2.97	.020	12.28	38.80	
		65 1449	BC 3	1.36	169.92	44.38	.027	.017	.63	3.71	.021	15.61	49.35	
		66 1439		4.01	144.42	55.68	.020	.011	.57	1.01	.011	2.79	12.00	
		67 1440		4.45	146.53	43.42	.023	.015	.67	1.04	.016	3.51	12.49	
		68 14401	1440 ECC	4.05	145.39	47.07	.022	.012	.57	1.09	.013	3.11	13.06	
		69 1468	BC 7	3.79	85.47	111.34	.037	.025	.66	1.50	.035	9.33	24.19	
		88 1404	VG 4	5.07	142.67	66.50	.027	.018	.69	1.07	.019	3.74	12.95	
92 1499		.26	154.67	150.83	.006	.003	.41	2.08	.006	24.04	59.01			
93 1498		.13	126.67	132.07	.005	.002	.32	2.41	.005	34.74	85.45			
94 1496		.12	132.69	132.40	.006	.001	.22	2.47	.006	54.29	133.00			
95 1500	DY 2	.72	9.90	102.96	.016	.015	.93	4.47	.015	20.26	53.07			
102 1406	VG 6	6.84	134.09	51.70	.033	.020	.60	.99	.020	2.95	11.80			
104 1401	VG 1	1.26	11.00	95.84	.015	.013	.87	2.48	.013	10.51	29.50			
105 1445	HIW 16	5.07	12.77	100.94	.024	.013	.55	.97	.013	2.56	11.51			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM
99	1480	BC 13A	2 6785001	67A24	12.22	124.29	171.31	.004	.001	.35	.05	.003 .24 .82
			3 678566	67A25	.11	171.24	171.31	.004	.001	.35	2.69	.004 37.10 90.90
			4 678567	67A55	23.79	91.44	171.31	.004	.001	.35	.04	.002 .07 .42
		44	1453	HIW 10	5.65	34.04	169.84	.043	.028	.65	1.32	.037 6.48 18.75
		58	1446	U+U 611	11.40	37.20	135.90	.038	.021	.55	.68	.021 1.88 8.12
		67	1440		11.60	6.43	103.67	.036	.025	.69	.64	.025 2.15 7.60
		74	1438		4.17	121.58	33.25	.047	.028	.60	2.35	.028 6.81 27.89
		90	678756	MT MYE	2.55	130.19	39.00	.024	.015	.61	1.95	.015 5.73 23.17
		97	1491	HIW 14	4.11	39.74	52.42	.055	.035	.63	1.81	.054 13.23 32.91
		104	1401	VG 1	7.45	28.08	130.18	.028	.018	.64	.78	.019 2.53 9.37
		105	1445	HIW 16	3.89	42.49	136.38	.025	.017	.66	1.32	.017 4.26 15.70
		106	1437	BC 21	11.21	79.07	105.86	.045	.026	.58	.56	.042 3.71 9.79
		109	108	GRAVITY 10	6.26	9.79	54.82	.077	.056	.73	2.22	.067 10.74 30.06
100	1408	VG 8	17 1419	VG 19	10.43	134.05	46.70	.053	.031	.59	1.04	.031 2.97 12.38
			29 1450	HIW 6	3.56	174.78	60.05	.038	.032	.84	2.13	.033 9.20 25.93
			30 1469	HIW 7	3.36	112.65	33.62	.028	.019	.68	1.73	.020 5.84 20.70
			31 1409	VG 9	1.22	124.20	84.81	.014	.013	.94	2.31	.014 11.34 28.45
			32 1410	VG 10	2.50	136.70	55.59	.027	.020	.76	2.19	.020 8.13 26.13
			33 1411	VG 11	3.07	126.79	41.58	.032	.022	.69	2.14	.022 7.20 25.41
			34 1412	VG 12	4.26	132.03	44.34	.040	.025	.61	1.96	.025 5.82 23.29
			35 1413	VG 13A	5.15	132.11	44.84	.045	.026	.58	1.79	.026 5.07 21.32
			36 1414	VG 14	5.69	130.43	44.19	.045	.027	.59	1.65	.027 4.72 19.59
			37 1407	VG 7	.74	63.69	136.68	.009	.007	.81	2.49	.008 10.13 30.03
			38 1424	HIW 6KA	1.30	135.96	11.48	.017	.013	.80	2.50	.015 11.23 31.60
			39 1423	HIW 5KA	1.92	148.65	38.27	.019	.015	.81	1.98	.016 8.16 24.01
			40 1405	VG 5	1.83	122.66	28.01	.018	.014	.80	2.05	.014 7.93 24.38
			41 1422	HIW 4KA	1.61	128.97	19.71	.018	.014	.79	2.24	.015 9.09 27.19
			42 1461	HIW 1KA	2.15	166.59	57.93	.020	.016	.84	1.86	.017 7.81 22.40
			45 1402	VG 2	5.78	123.43	37.11	.033	.020	.59	1.19	.020 3.43 14.13
			46 1403	VG 3	5.11	126.98	37.41	.031	.018	.58	1.26	.018 3.55 14.93
			47 1457	HIW 3KA	4.59	126.15	35.45	.029	.018	.61	1.30	.018 3.86 15.45
			48 14571	JK 1	4.66	126.07	36.78	.029	.021	.72	1.30	.021 4.52 15.40
			49 1454	JK 4	3.68	132.06	39.85	.026	.018	.70	1.44	.018 4.94 17.16
			50 1452	HIW 2KA	3.86	135.95	43.50	.026	.019	.71	1.40	.019 4.82 16.68
			51 1459	JK 3	4.18	134.08	42.52	.027	.018	.67	1.35	.018 4.36 15.98
			52 1460	IN 4	3.96	134.22	42.70	.026	.019	.70	1.38	.019 4.67 16.38
53 1458	IN 1	4.33	130.80	39.25	.028	.018	.64	1.34	.018 4.14 15.89			
54 1456	IN 2	4.45	133.78	42.51	.029	.018	.63	1.33	.018 4.07 15.83			
55 1455	IN 3	4.77	135.58	46.62	.031	.019	.61	1.32	.019 3.94 15.70			
56 1451	JK 2	4.68	138.68	50.06	.030	.019	.63	1.30	.019 3.98 15.50			
88 1404	VG 4	3.03	118.54	26.71	.023	.016	.71	1.55	.016 5.34 18.41			
89 1462	HIW 9	3.21	92.68	176.42	.026	.017	.65	1.65	.017 5.29 19.69			
101 1490	HIW 7KA	.42	126.00	109.67	.007	.006	.86	2.88	.007 15.89 39.36			
102 1406	VG 6	1.09	131.08	18.97	.015	.012	.82	2.80	.013 11.73 34.04			

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	R.A. PPM			
101	1490	HIW 7KA	29	1450	HIW 6	3.85	170.08	59.36	.038	.032	.83	2.02	.033	8.55	24.48
			30	1469	HIW 7	3.77	114.12	33.90	.030	.020	.66	1.64	.020	5.39	19.64
			31	1409	VG 9	1.64	124.66	52.81	.017	.015	.90	2.08	.015	9.27	24.99
			32	1410	VG 10	2.92	135.17	53.03	.029	.021	.74	2.02	.021	7.30	24.09
			33	1411	VG 11	3.49	126.69	41.30	.034	.023	.68	1.99	.023	6.58	23.65
			34	1412	VG 12	4.67	131.49	43.98	.042	.025	.61	1.85	.025	5.45	22.05
			35	1413	VG 13A	5.56	131.65	44.49	.046	.027	.58	1.71	.027	4.81	20.37
			36	1414	VG 14	6.11	130.13	43.85	.047	.027	.58	1.58	.028	4.50	18.84
			37	1407	VG 7	.66	29.50	110.65	.010	.007	.68	3.18	.007	10.69	37.98
			38	1424	HIW 6KA	.89	140.62	2.30	.017	.014	.84	3.51	.016	17.34	45.61
			39	1423	HIW 5KA	1.54	154.67	38.06	.018	.016	.86	2.40	.016	10.64	29.24
			40	1405	VG 5	1.41	121.67	25.46	.018	.015	.86	2.59	.015	10.77	30.79
			41	1422	HIW 4KA	1.19	130.02	13.56	.018	.015	.84	2.95	.015	12.89	36.04
			42	1461	HIW 1KA	1.85	175.05	63.52	.019	.017	.88	2.13	.017	9.37	25.72
			45	1402	VG 2	5.36	123.23	37.30	.033	.020	.62	1.27	.020	3.80	15.06
			46	1403	VG 3	4.69	127.06	37.63	.031	.019	.61	1.35	.019	3.99	16.06
			47	1457	HIW 3KA	4.17	126.17	35.54	.029	.018	.64	1.41	.018	4.38	16.76
			48	14571	JK1	4.24	126.07	37.06	.029	.022	.75	1.41	.022	5.08	16.69
			49	1454	JK 4	3.26	132.84	40.58	.025	.019	.74	1.60	.019	5.74	19.03
			50	1452	HIW 2KA	3.44	137.16	44.68	.026	.019	.74	1.55	.019	5.55	18.38
51	1459	JK 3	3.76	134.98	43.41	.027	.019	.70	1.47	.019	4.98	17.47			
52	1460	IN 4	3.55	135.18	43.75	.026	.019	.73	1.52	.019	5.37	18.00			
53	1458	IN 1	3.91	131.31	39.71	.028	.018	.67	1.46	.018	4.72	17.33			
54	1456	IN 2	4.04	134.59	43.23	.028	.019	.66	1.45	.019	4.63	17.21			
55	1455	IN 3	4.36	136.49	47.54	.030	.019	.64	1.43	.019	4.43	16.98			
56	1451	JK 2	4.27	139.92	51.33	.029	.019	.65	1.41	.019	4.48	16.77			
57	1488	HIW 11	6.53	137.83	58.81	.049	.026	.52	1.53	.027	4.09	18.40			
88	1404	VG 4	2.61	117.34	25.33	.022	.017	.75	1.76	.017	6.42	20.91			
89	1462	HIW 9	2.87	88.09	173.70	.026	.017	.67	1.84	.017	5.98	21.95			
100	1408	VG 8	.42	126.00	109.67	.007	.006	.86	2.88	.007	15.89	39.36			
102	1406	VG 6	.67	134.26	9.69	.015	.013	.88	4.37	.014	20.23	53.92			

102	1406	VG 6	29	1450	HIW 6	4.41	164.98	59.49	.037	.031	.85	1.71	.032	7.22	20.46
			30	1469	HIW 7	4.41	117.12	32.70	.031	.018	.59	1.43	.018	4.10	16.99
			31	1409	VG 9	2.30	127.44	31.27	.020	.017	.83	1.81	.017	7.32	21.53
			32	1410	VG 10	3.59	135.00	48.00	.030	.023	.76	1.71	.023	6.28	20.31
			33	1411	VG 11	4.15	127.91	39.44	.034	.024	.69	1.71	.024	5.71	20.30
			34	1412	VG 12	5.34	131.84	42.92	.042	.026	.62	1.63	.026	4.88	19.32
			35	1413	VG 13A	6.23	131.93	43.70	.046	.027	.59	1.52	.027	4.37	18.10
			37	1407	VG 7	1.05	171.54	137.92	.013	.013	.98	2.50	.013	12.23	30.18
			38	1424	HIW 6KA	.24	158.68	159.91	.009	.003	.34	2.53	.009	35.92	88.02
			39	1423	HIW 5KA	.94	169.06	22.38	.010	.009	.94	2.08	.010	10.31	25.67
			40	1405	VG 5	.77	110.70	145.09	.009	.008	.92	2.17	.008	10.84	27.20
			41	1422	HIW 4KA	.53	124.60	164.41	.009	.006	.67	3.03	.008	15.70	43.68
			42	1461	HIW 1KA	1.42	13.08	94.16	.013	.011	.85	1.85	.011	7.65	22.04
			45	1402	VG 2	4.71	121.67	36.68	.028	.016	.58	1.20	.016	3.43	14.34
			46	1403	VG 3	4.02	125.87	37.21	.025	.014	.55	1.28	.014	3.45	15.24

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R.A. = 2.45 X SEMI MAJOR AXIS/DISTANCE EXPRESSED IN PPM
 STANDARD ERROR ELLIPSES

STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM	
102	1406 6	48	14571	JKI	3.58	124.54	36.60	.023	.018	.76	1.32	.018	4.89	15.68
		49	1454	JK 4	2.59	132.48	42.77	.019	.014	.74	1.49	.014	5.31	17.70
		50	1452	H1W 2KA	2.78	137.86	48.83	.019	.014	.73	1.44	.014	5.10	17.11
		51	1459	JK 3	3.09	135.13	45.94	.021	.014	.67	1.37	.014	4.45	16.25
		52	1460	IN 4	2.88	135.40	47.28	.020	.014	.72	1.41	.014	4.92	16.70
		53	1458	IN 1	3.25	130.70	40.33	.022	.013	.63	1.37	.013	4.15	16.24
		54	1456	IN 2	3.37	134.66	44.94	.022	.014	.61	1.37	.014	4.06	16.26
		55	1455	IN 3	3.69	136.90	50.14	.025	.014	.59	1.37	.014	3.91	16.32
		56	1451	JK 2	3.60	140.97	55.38	.023	.014	.59	1.34	.014	3.90	15.97
		57	1488	H1W 11	5.86	138.24	60.57	.046	.022	.48	1.57	.024	4.02	19.03
		59	1479	DY 1	6.27	130.66	47.39	.032	.018	.57	1.04	.018	2.91	12.44
		88	1404	VG 4	1.98	111.69	16.13	.015	.011	.74	1.56	.011	5.60	18.54
		89	1462	H1W 9	2.46	76.72	163.38	.021	.011	.51	1.76	.011	4.41	20.97
		92	1499		6.60	133.29	51.80	.033	.020	.62	1.01	.020	3.10	12.08
93	1498		6.71	134.24	52.15	.033	.020	.61	1.00	.020	3.02	11.96		
98	1497		6.84	134.09	51.70	.033	.020	.60	.99	.020	2.95	11.80		
100	1408	VG 8	1.09	131.08	18.97	.015	.012	.82	2.80	.013	11.73	34.04		
101	1490	H1W 7KA	.67	134.26	9.69	.015	.013	.88	4.37	.014	20.23	53.92		
104	1401	VG 1	6.25	124.39	44.05	.030	.018	.58	.99	.018	2.89	11.89		
103	1421 RC 4	4	678567	67A55	6.84	44.11	34.20	.064	.038	.59	1.17	.063	9.23	22.84
		5	1470	RC 11	3.82	89.70	28.31	.029	.022	.77	1.51	.024	6.34	18.81
		6	1484		2.59	127.67	64.00	.040	.022	.55	2.94	.026	10.21	37.62
		7	1463	RC 2	2.18	43.91	53.35	.024	.019	.77	1.78	.024	11.11	27.36
		8	1420	WHI 3	.13	135.09	134.95	.004	.002	.36	2.43	.004	32.44	79.48
		9	1481	H1W 2	4.24	28.29	88.98	.034	.024	.72	1.53	.027	6.28	19.35
		13	1483		4.47	72.59	165.72	.029	.025	.85	1.36	.025	5.56	16.11
		14	1487	PR1 4	3.93	74.14	179.94	.028	.025	.89	1.43	.025	6.31	17.13
		15	1485	TR1 18	3.07	56.73	83.15	.026	.024	.91	1.64	.026	8.44	21.07
		16	1486	PR1 6	3.30	85.51	29.73	.027	.023	.84	1.60	.024	7.28	19.96
		17	1419	VG 19	2.14	106.13	25.22	.018	.013	.72	1.73	.013	6.14	20.66
		18	1418	VG 18	2.67	118.53	37.14	.022	.015	.67	1.67	.015	5.57	19.97
		19	1417	WHI 1-71	3.65	113.69	34.57	.028	.017	.60	1.55	.017	4.67	18.62
		20	1416	VG 16	4.82	120.20	36.71	.036	.022	.63	1.52	.023	4.69	18.13
21	1415	VG 15A	4.92	117.70	32.78	.036	.022	.62	1.50	.022	4.53	17.81		
22	1475	H1W 8	5.28	139.24	51.67	.038	.019	.49	1.47	.019	3.54	17.51		
23	1477		4.46	161.39	69.19	.036	.026	.72	1.68	.026	5.89	19.94		
104	1401 VG 1	2	6785001	67A24	13.62	91.29	131.42	.028	.018	.65	.35	.025	1.82	5.12
		3	678566	67A25	7.37	28.60	131.42	.028	.018	.65	.79	.019	2.59	9.47
		39	1423	H1W 5KA	5.62	117.62	39.55	.028	.017	.62	1.00	.018	3.16	12.05
		40	1405	VG 5	5.50	126.28	50.38	.028	.017	.62	1.02	.018	3.24	12.28
		41	1422	H1W 4KA	5.72	124.37	46.28	.028	.017	.60	1.01	.018	3.09	12.11
		44	1453	H1W 10	1.93	10.34	179.48	.037	.019	.51	2.11	.036	18.80	46.67
		45	1402	VG 2	1.56	132.63	118.54	.015	.014	.92	1.87	.015	2.80	24.12
		46	1403	VG 3	2.22	121.71	41.18	.017	.016	.94	1.56	.016	7.11	18.55
47	1457	H1W 3KA	2.74	124.08	49.74	.018	.014	.67	1.44	.014	4.41	17.11		

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	PPM	R.A. PPM
104	1401	1											
		49	1454	JK 4	3.70	118.74	39.73	.021	.017	.79	1.16	.017	4.55 13.91
		50	1452	HIW 2KA	3.61	114.05	29.93	.021	.017	.81	1.17	.017	4.65 13.96
		51	1459	JK 3	3.26	114.19	29.89	.019	.017	.85	1.22	.017	5.08 14.55
		52	1460	IN 4	3.46	115.25	32.55	.020	.017	.85	1.18	.017	4.89 14.09
		53	1458	IN 1	3.04	117.64	36.05	.019	.017	.87	1.29	.017	5.45 15.38
		54	1456	IN 2	2.99	112.81	29.83	.019	.016	.85	1.32	.016	5.50 15.75
		55	1455	IN 3	2.76	107.54	34.40	.019	.017	.89	1.42	.017	6.25 17.02
		56	1451	JK 2	2.98	104.18	24.91	.019	.017	.90	1.29	.017	5.68 15.38
		57	1488	HIW 11	1.51	55.92	61.95	.037	.015	.47	2.16	.037	24.53 60.38
		58	1446	U+U 611	4.21	53.51	146.81	.019	.012	.65	.93	.012	2.95 11.07
		59	1479	DY 1	.69	35.19	36.73	.010	.007	.67	1.96	.010	14.22 34.85
		60	1471	DP 1	.73	176.84	171.32	.008	.006	.79	1.76	.008	10.79 26.47
		61	1472	IB 751	.94	164.49	164.05	.008	.007	.93	1.59	.008	8.32 20.38
		62	1473	IB 756	.26	104.91	5.01	.010	.007	.73	7.65	.007	27.70 91.44
		63	1474	DP 2	1.08	135.79	63.75	.010	.009	.89	1.83	.009	8.06 21.97
		64	1443	BC 5	2.36	150.35	65.22	.025	.016	.63	2.22	.016	6.82 26.41
		65	1449	BC 3	2.57	.06	46.28	.027	.017	.65	1.82	.022	8.69 25.51
		66	1439		4.96	155.04	63.54	.020	.010	.51	.84	.010	2.07 10.02
		67	1440		5.42	155.88	53.31	.023	.015	.66	.86	.016	2.88 10.37
		68	14401	1440 ECC	5.01	155.73	54.83	.022	.012	.56	.89	.013	2.52 10.71
		69	1468	BC 7	3.66	104.80	109.32	.037	.024	.66	1.36	.037	10.01 24.57
		70	1442		6.22	104.85	7.77	.031	.013	.41	1.01	.013	2.09 12.04
		71	1448		5.90	122.04	28.55	.031	.022	.73	1.07	.022	3.80 12.77
		77	1432	BC 17	12.90	85.46	132.03	.033	.022	.67	.45	.028	2.14 6.22
		88	1404	VG 4	4.33	130.16	57.16	.023	.016	.69	1.08	.017	3.85 13.14
		89	1462	HIW 9	4.94	145.97	74.89	.028	.020	.72	1.15	.021	4.29 14.00
		92	1499		1.06	19.39	98.60	.015	.014	.89	2.96	.014	12.82 35.26
		93	1498		1.20	16.74	97.30	.015	.013	.87	2.59	.013	11.07 30.91
		94	1496		1.32	6.73	106.09	.016	.014	.86	2.45	.014	10.30 29.25
		95	1500	DY 2	.54	12.47	158.41	.011	.006	.59	3.14	.010	18.20 49.94
		98	1497		1.26	11.00	95.84	.015	.013	.87	2.48	.013	10.51 29.50
		99	1480	BC 13A	7.45	28.08	130.18	.028	.018	.64	.78	.019	2.53 9.37
		102	1406	VG 6	6.25	124.39	44.05	.030	.018	.58	.99	.018	2.89 11.89
		105	1445	HIW 16	3.81	13.35	103.96	.019	.009	.47	1.01	.009	2.31 11.97
		106	1437	BC 21	16.93	59.07	114.80	.056	.031	.56	.60	.040	2.39 8.06
105	1445	HIW 16											
		2	6785001	67A24	13.35	107.51	137.89	.025	.017	.67	.30	.023	1.73 4.58
		3	678566	67A25	3.82	43.78	137.89	.025	.017	.67	1.34	.017	4.38 15.99
		44	1453	HIW 10	1.89	16.43	175.79	.037	.024	.64	2.83	.036	19.02 48.40
		45	1402	VG 2	3.34	37.40	113.49	.023	.016	.70	1.39	.016	4.92 16.82
		46	1403	VG 3	3.76	47.50	114.48	.023	.018	.77	1.24	.019	5.01 15.23
		47	1457	HIW 3KA	3.83	55.37	114.47	.024	.019	.78	1.21	.020	5.23 15.14
		48	14571	JK1	3.80	54.38	116.94	.026	.019	.71	1.35	.020	5.38 16.94
		49	1454	JK 4	4.55	64.93	115.71	.024	.021	.87	1.04	.022	4.90 12.95
		50	1452	HIW 2KA	4.73	61.77	124.27	.024	.021	.85	1.03	.022	4.55 12.57
		51	1459	JK 3	4.52	58.35	121.29	.024	.020	.82	1.06	.021	4.58 13.05
		52	1460	IN 4	4.59	60.91	121.38	.024	.020	.83	1.05	.021	4.64 12.98
		53	1458	IN 1	4.25	57.25	117.58	.024	.020	.82	1.11	.021	4.88 13.88

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105	1445	16													
		55	1455	IN 3	4.54	50.68	115.60	.025	.020	.80	1.09	.021	4.58	13.37	
		56	1451	JK 2	4.80	51.65	119.23	.025	.019	.78	1.03	.020	4.20	12.65	
		57	1488	HIW 11	5.03	25.06	70.41	.040	.022	.53	1.33	.032	6.40	19.63	
		58	1446	U+U 611	7.54	34.47	122.76	.028	.015	.53	.77	.015	1.98	9.18	
		59	1479	DY 1	4.46	16.63	103.73	.021	.011	.54	.95	.011	2.53	11.35	
		60	1471	DP 1	4.51	10.74	101.94	.020	.009	.44	.93	.009	2.00	11.00	
		61	1472	IB 751	4.65	7.78	99.89	.021	.009	.43	.92	.009	1.93	10.89	
		62	1473	IB 756	3.83	9.53	100.83	.019	.010	.53	1.01	.010	2.57	11.95	
		63	1474	DP 2	4.49	1.61	94.86	.021	.010	.46	.97	.010	2.18	11.57	
		66	1439		8.29	171.61	82.99	.030	.012	.41	.74	.012	1.46	8.80	
		69	1468	BC 7	5.35	150.24	101.74	.041	.024	.60	1.33	.032	6.08	18.62	
		70	1442		7.37	135.80	27.98	.031	.021	.68	.85	.022	3.01	10.37	
		73	1467	BC 16	5.40	117.03	8.18	.055	.033	.60	2.02	.036	6.64	24.85	
		88	1404	VG 4	4.29	77.69	90.43	.025	.021	.84	1.01	.025	5.74	14.17	
		89	1462	HIW 9	3.66	96.00	92.23	.029	.022	.75	1.25	.029	8.04	19.72	
		90	678756	MT MYE	4.56	8.55	80.78	.029	.028	.96	1.32	.028	6.20	15.72	
		92	1499		4.87	14.66	102.30	.024	.013	.57	1.00	.013	2.76	11.87	
		93	1498		5.02	14.17	101.90	.024	.013	.55	.98	.013	2.62	11.62	
		95	1500	DY 2	4.35	13.25	107.79	.020	.011	.51	.97	.011	2.44	11.55	
		96	1434	HIW 17	20.57	92.29	133.86	.075	.055	.73	.65	.067	3.26	8.96	
		98	1497		5.07	12.77	100.94	.024	.013	.55	.97	.013	2.56	11.51	
		99	1480	BC 13A	3.89	42.49	136.38	.025	.017	.66	1.32	.017	4.26	15.70	
		104	1401	VG 1	3.81	13.35	103.96	.019	.009	.47	1.01	.009	2.31	11.97	
		106	1437	BC 21	14.52	69.88	114.44	.052	.030	.58	.60	.043	2.95	8.80	
106	1437	BC 21	2	6785001	67A24	9.06	5.86	105.50	.045	.026	.57	1.01	.026	2.91	12.11
		64	1443	BC 5	17.15	51.18	108.79	.059	.036	.60	.64	.044	2.55	8.44	
		66	1439		18.14	43.32	107.27	.061	.032	.52	.64	.039	2.15	8.26	
		69	1468	BC 7	14.62	48.76	107.70	.062	.036	.58	.80	.044	3.04	10.43	
		74	1438		8.61	59.96	2.28	.048	.045	.92	1.14	.046	5.31	13.79	
		75	1466		6.58	43.76	94.07	.044	.037	.84	1.29	.040	6.04	16.32	
		76	1465	BC 20	3.98	18.90	110.00	.033	.017	.51	1.73	.017	4.24	20.50	
		77	1432	BC 17	7.86	12.34	104.81	.042	.022	.53	1.11	.023	2.86	13.19	
		86	1435		2.68	136.67	47.86	.026	.015	.58	2.03	.015	5.72	24.09	
		96	1434	HIW 17	9.03	130.12	118.61	.075	.053	.71	1.24	.075	8.27	20.47	
		99	1480	BC 13A	11.21	79.07	105.86	.045	.026	.58	.56	.042	3.71	9.79	
		104	1401	VG 1	16.93	59.07	114.80	.056	.031	.56	.60	.040	2.39	8.06	
		105	1445	HIW 16	14.52	69.88	114.44	.052	.030	.58	.60	.043	2.95	8.80	
		107	1427		12.39	120.20	121.62	.074	.058	.78	.96	.074	6.00	14.71	
		110	111	GRAVITY II	6.01	119.35	110.14	.071	.050	.71	1.75	.070	11.68	28.80	

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STATION FROM	NAME	STATION TO	NAME	DIST (KM)	MEAN AZ (DEG)	AZ OF MAJ AXIS	SEMI MAJ AXIS (M)	SEMI MIN AXIS (M)	RATIO MN/MJ	AZ SEC	DIST M	DIST PPM	R.A. PPM	
107	1427	1 6785000	67A35	32.79	145.60	136.74	.071	.054	.76	.34	.070	2.14	5.28	
		2 6785001	67A24	11.97	76.58	136.74	.071	.054	.76	1.15	.058	4.88	14.46	
		04 1436		7.45	54.65	81.95	.098	.077	.78	2.27	.094	12.66	32.37	
		85 1433		3.15	160.87	70.09	.032	.016	.50	2.11	.016	5.09	25.03	
		86 1435		9.84	115.76	123.46	.076	.055	.72	1.15	.076	7.68	18.89	
		87 1426	SL 13	22.12	171.73	128.73	.148	.114	.77	1.22	.133	6.02	16.39	
		96 1434	H1W 17	3.83	96.20	4.99	.035	.017	.51	1.87	.018	4.57	22.17	
		106 1437	BC 21	12.39	120.20	121.62	.074	.058	.78	.96	.074	6.00	14.71	
108	107	GRAVITY 10 11	1464	H1W 3	9.66	100.21	82.72	.085	.077	.91	1.66	.084	8.69	21.46
		24	1493	H1W 12	7.96	143.94	93.47	.101	.090	.89	2.50	.095	11.89	31.03
		25	1492	H1W 13	4.01	61.32	160.01	.116	.102	.88	5.93	.102	25.42	70.68
		109	108	GRAVITY 10	5.51	107.67	113.20	.074	.049	.66	1.84	.074	13.42	32.97
109	108	GRAVITY 10 25	1492	H1W 13	3.99	154.25	.92	.113	.099	.88	5.27	.110	27.60	69.24
		43	1495	H1W 15	3.05	88.63	53.84	.102	.083	.82	6.08	.096	31.63	82.09
		90	678756	MT MYE	5.44	33.62	54.04	.078	.056	.72	2.25	.076	13.98	35.32
		97	1491	H1W 14	3.39	152.58	52.84	.094	.065	.69	5.68	.066	19.42	67.77
		99	1480	BC 13A	6.26	9.79	54.82	.077	.056	.73	2.22	.067	10.74	30.06
		108	107	GRAVITY 10	5.51	107.67	113.20	.074	.049	.66	1.84	.074	13.42	32.97
		110	111	GRAVITY 11	4.82	103.19	99.37	.065	.049	.76	2.12	.065	13.53	33.19
110	111	GRAVITY 11 43	1495	H1W 15	2.02	125.55	90.60	.099	.083	.84	9.08	.094	46.75	120.61
		90	678756	MT MYE	8.43	66.01	96.20	.076	.056	.73	1.51	.072	8.50	22.15
		97	1491	H1W 14	3.67	58.60	81.13	.088	.068	.77	4.00	.086	23.32	58.94
		106	1437	BC 21	6.01	119.35	110.14	.071	.050	.71	1.75	.070	11.68	28.80
		109	108	GRAVITY 10	4.82	103.19	99.37	.065	.049	.76	2.12	.065	13.53	33.19

AMNYEDS. 79/11/19. CYBERSHARE LIMITED.

15.18.35.GANET,CM100000,T77770.

15.18.35.ACCOUNT,EDMNX,,P2,GANET.

15.18.35.ATTACH,GANETR.

15.18.36.ATTACH,HIWDATA.

15.18.36.GANETR,HIWDATA,PL=777777.

15.35.39. EXIT

15.35.39. 438.829 CP SECDNDS EXECUTION TIME

15.35.39./E01

15.35.39. ILLEGAL CONTROL CARD.

15.35.40.UFAD, 0.001KUNS.

15.35.40.UEPF, 0.016KUNS.

15.35.40.UEMS, 127.188KUNS.

15.35.40.UECP, 445.700SECS.

15.35.40.AESR, 724.976UNTS.

17.15.07.UCLP, TE6 , 7.617KLNS.