

X-Section

118+000

1984

001559

DDH 84F-06

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	BT	✓
DOWN HOLE SURVEYS " R "	BT	✓
DOWN HOLE LITHOLOGY " L "	BT	✓
DOWN HOLE STRUCTURE " S "	CSB VTK	BT	✓
DOWN HOLE FAULTS " F "	BT	✓
SAMPLERS DATA " P "	BT	✓
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	BT	BT	✓
ENTER ASSAYS "CAMC"
ENTER ASSAYS "CHEMEX"
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE
SPLINE CALCULATIONS
STRUCTURAL SOLUTIONS
CALCULATE OFFSETS FROM COLLAR
PRINT OUT GENERAL DDH DATA REPORTS

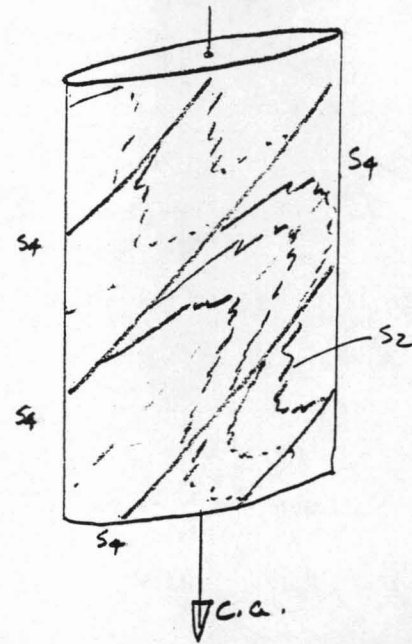
DIAMOND DRILL CORE LOG

Date: April 27 / 84

Hole Number: FA84F-06

Reference Fabric Orientation Diagram:

Project: Faro Zone 1 Fill-In



Location: ANVIL DISTRICT

Claim: FARO 44

MINE ENCL. Ferr. Plane Co-ords.: 9295.86 N

14499.30 E

Grid Co-ords: 118+00 E, 23+00

COLLAR Elevation: 3690.36 feet

All symmetry determinations looking

Total Depth: 301.0 feet

NW with S_4/S_2 dipping 235°
SW with dip azimuth $S_2/235^\circ/S_4, 235^\circ$

Inclination: -90°

Purpose: To test continuity of ore as predicted by 280' spaced holes.

Reason hole Terminated: Through ore zone

Logged by: RST

Date(s) Logged: April 6, 22, 23 1984

Drilling Contractor: ECARON DIAMOND DRILLING LTD

Size	CORE From	To	Collar Cased and Capped: <u>No</u>
<u>NQ</u>	<u>4'</u>	<u>301'</u>	

Hole Cemented: No

Seal down hole: No

Started: April 3 / 84 Completed: April 5 / 84

Code	From				To				Recov.	No.	Unit	Description
	10	14	18	20	22	24	26	28				
L		14		20						1	1C08	8 musc > biot (000) chlorite particularly developed peripheral to 000 veins thru out 15' of unit. Gradational lower unit.
L		20		28						2	1C48	9 pyrite thru out along S2 10%
L		28		36						3	1C0	musc > biot
L		36		58						4	2L01	(000) Qtz veins at 38.7 (2.8'), 48-48 (narrow stringers) 50.0 (1.5') and at end of unit (.4')
L		58		72						5	1C01	Musc > biot (000) Narrow Qtz veinlets thru out @ 62.0 (1.0') and end of unit (.7')
L		72		90						6	1C01	
L		90		99						7	2L01	1 (1E149) [2B0?] 1st 2.6' quite silicious almost 2B0 1E @ start (0.4') at end 2'. relic graphite thru out, poss. 2L from 2A with alteration? No grade.
L		99		121						8	2L01	(2L08*) minor @ 104.0' (1')
L		121		130						9	2D43	9 pyrite over 1st 1.5' minor @ veinlets @ 123.4
L		130		134						10	2E49	8? possible barite present - pinhole porous/poor rec
L		134		138						11	2E08	89 (000?) minor bands of magnet. last 0.6' banded thin contact unknown mineral - cream colour, soft does not react powdered to 20% HCl, light weight.
L		138		148						12	2E42	9 1st .5' > 4% PbZn.
L		148		155						13	2E48	89/ magnetite at 1/10" phenocryst compositionally banded. thru out 10%. Minor Qtz clots thru out.
L		155		161						14	2F4	(2E2) interbanded 60:40 (RT 1952, JK 202, AC 142 1cider)
L		161		175						15	2E08	89 (2F4) minor magnet clots in occasional bands thru out 2F4 @ 163.6 (0.5'), 165.2 (0.4'), 170.0 (0.2')
L		175		177						16	2F4	(RT 362, JK 252, AC 199 2cider)
L		177		179						17	2E87	9 (2F0) 2F0 last 0.9' m. magnet clots pos as replacement veinlets.
L		179		180						18	2K8	ankeritic with compositional banded magnet poss on S2 poss pre D2 vein?
L		180		184						19	2E89	E7 as of 17
L		184		187						20	2J88	1 (2E4) Qtz compositional banded clotted to 1/2" white. 2E4 at 286.1 (0.6') pin hole porous.
L		187		195						21	2J88	(2E089, 2H49) pyrrhotite 10% as replacement veins especially last 1' where → 2H49, 2E089 with cop veinlets at 191.3 (0.4'), 192.5 (1.0')

Code	From				To				Recov.	No.	Unit	Description
	10	14	16	20	22	24	26	28				
L	19	57		21	18				22	2J88	(2E0&3)	bx To 205' open circle bx then headed bx to end - 2E0&3 last 1'S looks like duct flow bx with marcasite clots to 5"
L	21	18		21	87				23	2D48	59(2A14)	1st 1.2' 2A14 also 215-218.6
L	21	87		22	18				24	2A11		→ 2C5 looks like bleached altered 2A.
L	22	18		23	06				25	2L0		
L	23	00		23	57				26	1E19		→ 2A0 marginal unit but 1E19 by finely laminated gte graphite bands low py & K17 base metals
L	23	57		24	58				27	2L2		minor carbonaceous wisps py & sz - looks like previous unit but bleached almost no C. garnets developed in bands thru' out.
L	24	58		25	22				28	1E19		→ 2A0 (2L1) of 26 but interbands of 2L1 appearing to alter 1E19.
L	25	22		25	51				29	2Q0	(2A14)	first 1' 2A14 pre-D2 gte vein ign, py, sp.
L	25	51		26	39				30	2C179	(2H0)	post D2 po veinlets thru' out and minor marcasite some po Sz banded. minor cp in veinlets. at 250 po 0.5' → 2H0 Poss [2Q0] is this a feeder zone?
L	26	39		26	78				31	2L2&9		minor cp and aspy. in veinlets. as at end of unit
L	26	78		27	56				32	1D29		minor py thru' out.
L	27	56		27	98				33	0Q9		py, marc and po developed in gte vein with @ veinlets.
L	27	98		28	50				34	2L14		minor sph & gn < 22 highly siliceous.
L	28	50		29	46				35	0Q9	(2L0)	white gte vein with galena thru' out 15% of vein 2L0 @ 291.2 (1')
L	29	46		30	10				36	2L2		m pyrite thru' out.

Structural Log

Date: Apr 22/84 Logged By: PST

Code	From		To		Feature	S ₁ /S ₂	S ₀		S ₁ /S ₂		S ₂ /S ₄		Description	
	10	14	16	20			Dip	Direct.	Dip	Direct.	Dip	Direct.		Dip
	10	14	16	20	22	24	26	28	32	34	38	40	44	S4
S				111	5	C, S4Z					50	22	10	From here to 72' veining poly metamorphism and fold interference makes it hard to define definitively S ₂ After 72 a steeper crenulation foliation (S ₃ ?) appears to dominate.
S				300		C, S4Z			60	0	110	45		see diag.
S				440		C, S4Z						45		From 42' to approx 69' S ₂ steep indicative of post D ₂ short limbs. From 69 to 121.8 Post D ₂ long limbs.
S				500		C, S4E						40		See diag.
S				740		C, S4Z			55	0	110	50		S ₃ = 35° S ₁ = S ₂
S				888		C, S4Z			65	0	00	30		S ₂ azimuth approx same dir. at 86.4 steep crenulation foliation about 10-15° to c.a.
S				970		C, S4Z			75		30	220		S ₂ approx same azimuth as S ₄ see diag. S ₁ well developed.
S				990		C, S ₂ Z					65	210		S ₂ sample taken.
S				11050		C, S ₂ Z					55	210		↓
S				1140		C, S4Z			65	180	25	220		S4
S				1240		P, S ₂ P					65	210		S ₂ Compositional banding
S				1570		P, S ₂ P					55			↓ " "
S				1700		P, S ₂ P					45			↓ " "
S				1865		P, S ₂ P					60			↓ " "
S				21130		P, S ₂ P					30	210		steep S ₂ 211.8 below bx zone at base of ore to 218 where terminated by another bx zone. 218' on S ₂ sub ⊥ to c.a.
S				2255		C, S4Z			75	0	10	40	220	S4 S ₁ = S ₂
S				2350		C, S4Z			80	0	90	45		↓
S				2434										S ₁ , S ₂ , S ₃ well developed sample taken.
S				2497		C, S4Z			75	190	25	220		S4 S ₁ = S ₂

DISCONTINUITY
Structural Log

Date: Apr 22/84

Logged By: FST

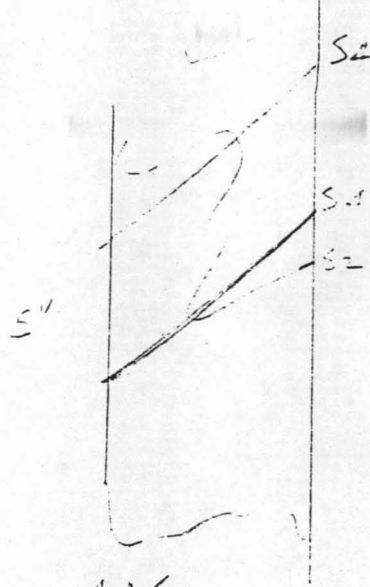
(AT)

For UPPER INTERNAL LOWER

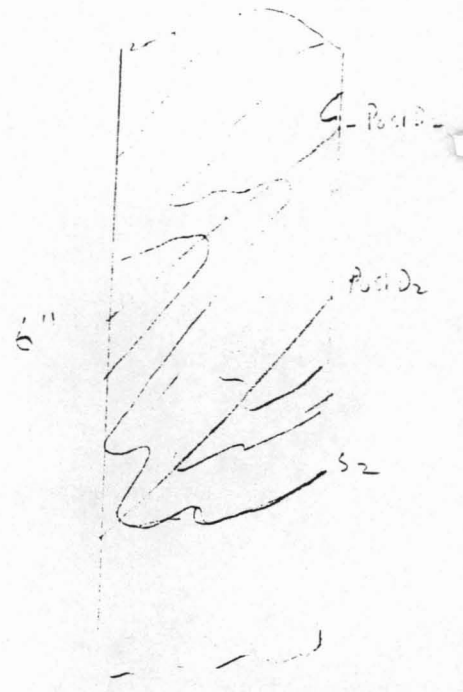
Code	From			To			Feature	S ₁		S ₂		Description	
	10	14	16	20	22	24		26	28	32	34		38
F		A0		100			2BR						
F				20			2BR						6"
F		386		420			V						hyper 30° to ca. poss // S ₄ ? lower cut sub ⊥ to ca.
F				498			1S	25	180				wrt S ₄ narrow shear.
F		580		590			1S	100	000				narrow py filled shear .25" wrt S ₄
F				620			1S	115	000				over 6" core, wrt S ₄
		500		620									narrow qtz veining thin cut sub // S ₂
F				722			1V						.7" quartz vein 80° to ca. 140° wrt S ₂ Invercut.
F				1035			1G						+3' // S ₂
F		1160		1170			1S						lower cut 35° to c.a. sub // S ₂
F		1176		1200			1V S						35° to c.a. sub // S ₂ a2/mr.
F		1256		1270			1JB						fractures in core 35° to ca influence drilling causing broken core.
F		1320		1355			3PR4						lost 1' solid.
F		1390		1430			3PR2						drillers forced worn bit
F		1430		1780			2BJ						as at 1256 fractures sub // to c.a. cause broken core.
F		1957		2070			XJB						fractured, open bx in places broken core. Upper cut 20° to ca. Lower cut // 20° to ca.
F		2103		2118			XJ						fracture and pyrite cemented bx. lower fracture sub // ca.
F		2125		2145			2J						fractured sub // to ca.
F		2165		2180			2JB						as above ground core over lost 4" pass driller gov.
F		2756		2790			2JV	30	000				fractured, veined. wrt S ₄
F		2850		2946			3V						lower cut // S ₂ upper ind.



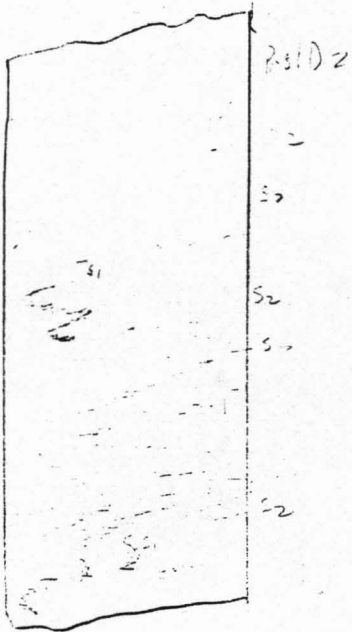
30'



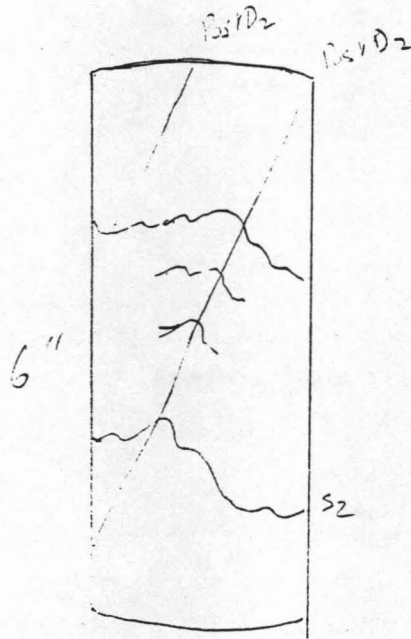
14'



6''



97'



6''

CODE	FROM			TO			SAMPLE			INTR.			REC (m)			UNIT		DESCRIPTION
	10	14	16	20	22	26	28	30	32	34	36	40	42					
P	121	8		126	2		33743	44	44			2D	43	9				
P	126	2		130	7		33744	45	42			2D	03	9				
P	130	7		134	0		33745	33	13			2E	49	8				
P	134	0		138	6		33746	46	40			2E	08	89	(OQ?)			
P	138	6		143	6		33747	50	44			2E	42	9		drillers forced old bit.		
P	143	6		148	4		33748	48	37			2E	A2	9				
P	148	4		152	0		33749	36	36			2E	48	9				
P	152	0		155	6		33750	36	36			2E	48	1.9				
P	155	6		158	7		33751	37	31			2F	A1		(2E2)			
P	158	7		161	8		33752	31	28			2F	A1		(2E2)			
P	161	8		165	3		33753	35	34			2E	08	89	(2F4)			
P	165	3		170	3		33754	50	50			2E	08	89	(2F4)			
P	170	3		175	3		33755	50	50			2E	08	89	(2F4)			
P	175	3		177	9		33756	26	26			2F	A1					
P	177	9		179	8		33757	19	19			2E	87	9	(2F4)			
P	179	8		180	9		33758	10	10			2K	8		high po assay due to sol. Fe in ankente			
P	180	9		184	0		33759	31	30			2E	89	87				
P	184	0		187	9		33760	39	39			2J	88	1	(2E4)			
P	187	9		191	8		33761	39	39			2J	88		(2E089)			
P	191	8		195	7		33762	39	39			2J	88		(2H49)			
P	195	7		201	1		33763	54	54			2J	88					
P	201	1		206	5		33764	54	52			2J	88					
P	206	5		211	8		33765	53	52			2J	88		(2E083)			
P	211	8		215	3		33766	35	35			2D	49	85	(2A14)			
P	215	3		218	7		33767	34	34			2D	49	85	(2A14)			
P	218	7		221	8		33768	31	31			2A	11		→ 2C5			
P	252	2		255	1		33769	28	28			2Q	01		(2A14)			
P	255	1		259	5		33770	44	44			2C	79		(2H0)			
P	259	5		263	9		33771	44	44			2C	79		(2H0)			
P	285	0		289	8		33632	48	46			OQ	9			Not to be composited		
P	289	8		294	6		33633	48	48			OQ	9		(2L0)	" " "		

DDH 75-06

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

ENTER " T " DATA

DOWN HOLE SURVEYS " R "

DOWN HOLE LITHOLOGY " L "

DOWN HOLE STRUCTURE " S "

DOWN HOLE FAULTS " F "

SAMPLERS DATA " P "

CHECK ENTRIES FROM GENERAL
DDH DATA REPORT

ENTER ASSAYS "CAMC"

ENTER ASSAYS "CHEMEX"

LIST DDH ASSAY VALUES
CHECK AGAINST ASSAY
CERTIFICATE

SPLINE CALCULATIONS

STRUCTURAL SOLUTIONS

CALCULATE OFFSETS FROM
COLLAR

PRINT OUT GENERAL DDH
DATA REPORTS

Checked by [initials] 5/17/85 PBT

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..... Nov 25, 85

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CS3 ✓ PBT
PBT Apr 7/85

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✓
SY L43 318°

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DIAMOND DRILL CORE LOG

Date: Feb 15 / 85

Hole Number: 75-06

Reference Fabric Orientation Diagram:

Project: Faro Zone III Re-log

Location: Anvil District

Claim: _____

MINE ENG
~~Terr. Plane~~
Co-ords.:

9285.3 N

14516.6 E

Grid Co-ords: X Sect 118+000 E, L Sect 23+000 N

MINE COLLAR
Elevation:

4042.6 feet

Total Depth: 701 feet.

Inclination: -69°

Purpose: To test dykes in Faro fault.

Reason hole Terminated: _____

ReLogged by: RST

Date(s) Logged: _____

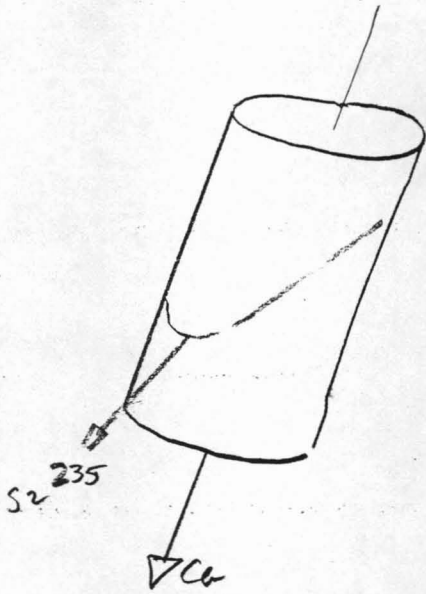
Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped: _____
<u>BQ</u>	<u>0</u>	<u>EOH</u>	

Hole Cemented: _____

Steel down le: _____

Started: May 30 / 75 Completed: June 16 / 75



All symmetry determinations looking

NW with S2 dipping

SW with dip azimuth 235°.

DDH 75-06
2 8

Cyprus Anvil Mining Corp.

Page 3 of 5

Lithologic Log

Date: 11/1/85Logged By: RST

Code	From		To		Recov.		No.		Unit		Description
	10	14	16	20	22	24	26	28	30	34	
L		00		40				1	*		OB
L		40		750				2	1,0,E,0,7		course grained. minor xenoliths
L		750		825				3	1,0,E,2,9		fine grained porphyritic
L		825		920				4	3,D,0,1		dense btd. calc silicate
L		920		1,0,0,7				5	3,B,0,1		poor rec
L		1,007		1,020				6	3,D,6,5		finely laminated biotite
L		1,020		1,1,0,0				7	3,C,0,1		
L		1,1,0,0		1,1,1,1				8	1,D,1,9,5		
L		1,1,1,1		1,2,2,9				9	3,C,0,1		(1D) 100 @ 114.5(6"), 118.0(8") φ 122.0(9")
L		1,229		1,280				10	1,E,0,1		chistolithic
L		1,280		1,480				11	1,0,E,0,1		med. course grained.
L		1,480		1,520				12	3,D,0,1		[1D] poor rec. poss hornfelsed metasomatized ID?
L		1,520		1,530				13	1,D,2,1		
L		1,530		1,947				14	1,D,0,1		
L		1,947		1,957				15	1,H,4,1		
L		1,957		1,972				16	1,D,0,1		
L		1,972		2,000				17	1,H,4,1		
L		2,000		2,370				18	1,D,0,1		
L		2,370		2,470				19	1,D,2,1		
L		2,470		2,484				20	1,D,0,8	4	weakly altered m. py at contact.
L		2,484		2,820				21	1,0,E,9,1		highly altered stromatic kaolinitic sericitic creamy white. Initially might be thought to be IOF with white glassy qtz however minor remnant also altered IOE seen.
L		2,820		6,065				22	1,0,E,0,1		From original logs.
L		6,065		6,105				23	1,C,D,1		
L		6,105		6,150				24	1,0,E,0,1		
L		6,150		6,390				25	1,C,D,1		
L		6,390		6,440				26	1,0,E,0,1		
L		6,440		6,460				27	1,C,D,1		
L		6,460		6,530				28	1,0,E,0,1		
L		6,530		7,010				29	1,C,D,1		

DDH 75-06
2 8

Cyprus Anvil Mining Corp.

Page 5 of 5

(AT)

DISCONTINUITY
Structural Log
Roc. UPPER INTERNAL LOWER

Date: Jan 11/85 Logged By: FST

Code	From				To				Feature	S₀		S₁		S₂		Description
	10	14	16	20	22	24	26	28		32	34	38	40	44		
F				82	S	J										contact 45° to c.a
F		87	0	92	X											cemented bx
F		105	5	106	R											
F		113	0	121	0	3GR	7	35	27	0						
F				162	G											4"
F		168	0	172	0	R		5								
F				200	G											6"
F				223	3	S		40	35	0						2"
F		230	2	235	0	X		99	99	9						Cataclastic texture poss // S ₂
F				248	4	J		35	23	5						contact
F				256	0	J										35° to c.a
																no more measurements take dyke rocks.

DDH 66-46

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	PRT	
DOWN HOLE SURVEYS " R "	PRT	✓ changed 15V to 180
DOWN HOLE LITHOLOGY " L "	✓	PRT		
DOWN HOLE STRUCTURE " S "	✓	cssv PRT Apr 9/85		
DOWN HOLE FAULTS " F "	✓	PRT		
SAMPLERS DATA " P "	✓	PRT		
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	May 28-85	PRT		
ENTER ASSAYS "CAMC"		
ENTER ASSAYS "CHENEX"		
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE		
SPLINE CALCULATIONS		
STRUCTURAL SOLUTIONS		
CALCULATE OFFSETS FROM COLLAR		
PRINT OUT GENERAL DDH DATA REPORTS		
	chged DDHID	Jun 17/85	PRT	

DIAMOND DRILL CORE LOG

Date: Feb 12 / 85

Hole Number: 66-46

Reference Fabric Orientation Diagram:

Project: Fabo Zone III Re-log

Location: Anvil District

Claim: _____

MINE ENG.
~~Fert. Plane~~
Co-ords.:

9398.92 N

14599.93 E

Grid Co-ords: X Sect 118+000E L. Sect 24+000N

Elevation: 4161.05 feet.

All symmetry determinations looking

Total Depth: 800'

NW with 52/54 dipping

Inclination: -90°

SW with dip azimuth 235.

Purpose: _____

Reason hole Terminated: _____

Re Logged by: GL.

Date(s) Logged: _____

Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped:
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Hole Cemented: _____

Steel down le: _____

Started: _____ Completed: _____

DDH E.A.6.6.-4.6
2 8

Cyprus Anvil Mining Corp.

Page 3 of 9

Lithologic Log

Date: Aug 30/84 Logged By: GL

Code	From	To	Recov.	No.	Unit	Description
	10 14 16 20 22 24 26 28 30 34 35					
L	100	120		1	*	TRICONED
L	120	1070		2	10EQ	(1000 & 9)
L	1070	1489		3	3D6	(3B0), ONLY SMALL CHIPS ARE AVAILABLE TO LOOK AT.
L	1489	1830		4	10EQ	
L	1830	1865		5	3A0	(1EQ) MISSING CORE BOX #3, INFO TAKEN FROM 1975 RELOG.
L	1865	2164		6	1D0	
L	2164	2180		7	1H0	[1F0]
L	2180	2222		8	1D0	
L	2222	2230		9	1D4	
L	2230	2240		10	2EQ	1EQ8
L	2240	2311		11	1D4	
L	2311	2805		12	1CD	
L	2805	2940		13	1EQ9	[1CD4], INTENSE RUST STAIN.
L	2940	2985		14	1D0	
L	2985	3013		15	10EQ	
L	3013	3257		16	1CD	
L	3257	4510		17	1CD4	
L	4510	4841		18	10EQ	KAOLINIZED AND SILICIFIED.
L	4841	4859		19	2D47	& 9.
L	4859	4871		20	1D4	
L	4871	4890		21	2D47	
L	4890	4910		22	2G479	
L	4910	4960		23	2J84	MASSIVE MAGNETITE. 4" FRAGMENT OF 10F9 (PINK) AT 491.0'.
L	4960	4972		24	2E*46	PINK CARBONATE ?
L	4972	4985		25	2G4	
L	4985	5031		26	1D4	
L	5031	5060		27	2E89	
L	5060	5068		28	2E24	
L	5068	5088		29	2G24	[2F46]
L	5088	5110		30	2J8*9	
L	5110	5160		31	2J8	(2G0).
L	5160	5208		32	2J8*6	
L	5208	5250		33	2G4	

Lithologic Log

Date: Aug 30/81 Logged By: GL

Code	From		To		Recov.	No.	Unit	Description		
	10	14	16	20					22	24
L	5250		5268			34	2A0	(2B79)		
L	5268		5485			35	2G4	8		
L	5485		5532			36	2E8	4		
L	5532		5662			37	2C3			
L	5662		5818			38	2E4	1		
L	5818		5846			39	2E8	4		
L	5846		5886			40	2E0			
L	5886		5948			41	2E0	8		
								NOT TRUE "BUCKSHOT"		
								TEXTURE.		
L	5948		6053			42	2E4	8		
L	6053		6264			43	2F4			
L	6264		6400			44	2E4	8		
L	6400		6532			45	2E8	9		
L	6532		6637			46	2F4			
L	6637		6658			47	2D7	9		
L	6658		6720			48	2H4	8		
L	6720		6813			49	2C7	8		
L	6813		6943			50	2D4	5		
L	6943		7090			51	2E4	4		
L	7090		7240			52	2F1			
								MISSING CORE BOX 709' TO 724'.		
L	7240		7380			53	2D4	5		
L	7380		7481			54	2A9	7		
L	7481		7606			55	2C7	9		
L	7606		8000			56	1CD	4		
								D breccia noted by DJH.		
								FOH		

Code	From		To		Feature	S/E	S ₀		S ₁ /S ₂		S ₂ /S ₄		Description
	10	14	16	20			22	24	26	28	32	34	
													RFE=S ₂
S				1520	AS ₂							73	23.5
S				2175	AS ₂							60	
S				2338	AS ₂							62	
S				2490	AS ₂							50	
S				2577	AS ₂							60	
S				2679	AS ₂							55	
													RFE=S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				2775	CS _{4Z}			4.2	60.0		15	23.5	
S				2862	CS ₄							18	
S				2967	CS _{4Z}			6.4	90.0		5.0		
													RFE=S ₂ , S ₂ =S ₂
S				3058	AS ₂							35	23.5
S				3115	AS ₄							4.4	23.5
S				3215	CS ₄							5.0	
S				3344	CS _{4Z}			4.3	0.0		2.5		
S				3552	CS ₄							3.5	
													RFE=S ₂ , S ₂ =S ₂
S				3646	AS ₂							4.7	23.5
S				3745	AS ₂							6.0	
S				3867	AS ₂							3.3	
													RFE=S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				3963								4.3	23.5
S				4013	CS _{4Z}			6.2	0.3		5.1		
													RFE=S ₂ , S ₂ =S ₂
S				4208	AS ₂							6.0	23.5
S				4322	AS ₂							4.7	
S				4380	AS _{4Z}			5.5	3.3		3.7	23.5	RFE=S ₄ , S ₂ =S ₄ , S ₀ =S ₂
													RFE=S ₂ , S ₂ =S ₂
S				4975	AS ₂							4.4	23.5
S				5065	AS ₂							4.0	
S				5121	AS ₂							1.2	
S				5267	AS ₂							3.3	
S				5432	AS ₂							5.0	
S				5823	AS ₂							5.6	
S				5961	AS ₂							3.0	

DDH FA66-46
2 8

Cyprus Anvil Mining Corp.

Page 6 of 9

Structural Log

Date: Sept 1/84 Logged By: GL

Code	From		To		Feature	SYE	S ₀		S ₁ /S ₂		S ₂ /S ₄		Description	
	10	14	16	20			22	24	26	28	32	34		38
S				6040	PS ₂							72		
S				6568	PS ₂							58		
S				6688	PS ₂							32		
S				6790	PS ₂							24		
S				6940	PS ₂							64		
S				7295	PS ₂							68		
S				7435	PS ₂							34		
S				7480	PS ₂							30		
S				7615	PS ₂							48		
				6734	PS ₂									
S				6734	CS ₄				58	000	37	235		PFE = S ₄ , S ₂ = S ₄ , S ₀ = S ₂
S				7874	CS ₄							41		

DDH F.A.66-46
2 8

Cyprus Anvil Mining Corp.

Page 7 of 9

DISCONTINUITY
Structural Log
UPPER INTERNAL LOWER

Date: Aug 30/84 Logged By: GL

Code	From		To		Feature	S ₁ E	S ₁ Dip Direct.		S Dip Direct.		S ₂ Dip Direct.		Description
	10	14 16	20	22 24 26 28			32 34	38	40	44			
F	00		920		NMM								TRICONED
F	920		1040		1BR								
F	1040		1570		3BR								
F	1570		1800		3GR								INTENSELY GOUGED IOE
F	1830		2070		NMM								
F	2070		2525		2BJ								
F	2525		2845		1BJ								
F	3458		3493		2BG								
F	3493		3950		1BJ								
F	3950		4390		1SX								ONLY MINOR DISPERSED SHEARING AND BRECCIATION IN ALTERED ROCK.
F	4390		4910		3BJ								INTENSELY FRACTURED DUKE ROCK.
F	5010		5060		2BJ								"PYRITE SAND"
F	5080		5740		2BJ								INTENSELY BROKEN SULFIDES.
F	6130		6195		2BJ								QUARTZITE FRAGMENTS IN SULFIDE MATRIX.
F	6630		6785		2D								
F	6785		7080		2BR								
F	7090		7240		NMM								
F	7540		7597		1D								
F	7597		7596		Q								PYRITE BEARING QTR VEIN.
F	7660		7672		Q								BARREN QTR VEIN.
F	7692		7700		3X1								
F	7800		7819		2BR								

Geochemical Log (Sampler's Copy)

Sampled By: _____

Core Code	From			To			Sample No.			Description		
	10	14	16	20	22	27						
	14410		14445		1331911							
P	14445		14510		1331912							
P	14510		14515		1331913							
P	14515		14610		1331914							
P	14610		14615		1331915							
P	14615		14710		1331916							
P	14710		14715		1331917							
P	14715		14810		1331918							
P	14810		14815		1331919		10 E 9				(2D4789)	
P	14815		14910		134010		2 D 7 7				(2G47, 104)	
P	14910		14915		1315012		* 2 J 8 4				(2G479)	
P	14915		15010		1315013		2 E 4 * 8				(2G4, 2J84)	
P	15010		15095		1315014		2 E 8 9					
P	15015		15110		1315015		2 G 2 4				(2E24, 2J8*9)	
P	15110		15115		1315016		2 J 8 9				(2G0)	
P	15115		15210		1315017		2 J 8 * 6					
P	15210		15215		1315018		2 G 4					
P	15215		15310		1315019		2 G 4 8 8				(2A0, 2B79)	
P	15310		15315		1315110		2 G 4 8 8					
P	15315		15410		1315111		2 G 4 8 8					
P	15410		15415		1315112		2 G 4 8 8					
P	15415		15510		1315113		2 G 4 8 8				(2E841)	
P	15510		15515		1315114		2 E 8 4 1				(2C3)	
P	15515		15610		1315115		2 C 3					
P	15610		15615		1315116		2 C 3					
P	15615		15710		1315117		2 E 4 1					
P	15710		15715		1315118		2 E 4 1					
P	15715		15810		1315119		2 E 4 1					
P	15810		15815		1315210		2 E 8 1					
P	15815		15910		1315211		2 E 0 8					
P	15910		15915		1315212		2 E 0 8					
P	15915		16010		1315213		2 E 4 8 1					
P	16010		16015		1315214		2 E 4 8 1					
P	16015		16110		1315215		2 F 0					
P	16110		16115		1315216		2 F 4					
P	16115		16210		1315217		2 F 4					

NOT ENTERED TO
DDHDB
10A & 10E9

X

Code	From	To	Sample No.	Description				
	14	16	20	22	27			
P	161210	161215	13151218	2	F	4		
P	161215	161310	13151219	2	E	4	89	
P	161310	161315	13151310	2	E	4	89	
P	161315	161410	13151311	2	E	4	89	
P	161410	161415	13151312	2	E	8	19	
P	161415	161510	13151313	2	E	8	19	
P	161510	161515	13151314	2	E	8	19 (2F4)	
P	161515	161610	13151315	2	F	4		
P	161610	161615	13151316	2	F	4	(2D79)	
P	161615	161710	13151317	2	H	4	89E1	
P	161710	161715	13151318	2	H	4	89E1 (2D789)	
P	161715	161810	13151319	2	C	7	89	
P	161810	161815	13151410	2	A	0	[2C5] (2E4)	
P	161815	161910	13151411	2	D	4	E5 (2C0)	
P	161910	161915	13151412	2	D	4	E5 (2C0) <i>no</i>	
P	161915	171010	13151413	2	E	4	4 <i>for</i>	
P	171010	171015	13151414	2	E	4	4	
P	171015	171110	13151415	2	E	4		
P	171110	171115	13151416	2	F	1		
P	171115	171210	13151417	2	F	1		
P	171210	171215	13151418	2	F	1		
P	171215	171310	13151419	2	D	4	85	
P	171310	171315	13151510	2	D	4	85	384
P	171315	171410	13151511	2	D	4	85 (2A97)	315
P	171410	171415	13151512	2	A	9	7	302
P	171415	171510	13151513	2	C	7	9	315
P	171510	171515	13151514	2	C	7	9	320
P	171515	171610	13151515	2	C	7	9	
P	171610	171615	13151516	x				NOT IN DDHDB

*what
min's is 7*

DDH: 66046 UTM-N: 9398.9 UTM-E: 14599.9 UTM-ELEV: 4161.1 TOTAL DEPTH: 800.0 SECTION:
 RFE: RFE DIR: 0 PLUNGE ANGLES: 0 0 DHD CALC: 1 SS CALC: 0

---DEPTHS---		SAMPLE NO.	INT.	REC.	ROCK UNIT	S.G. PULP	-----ASSAYS-----												
FROM	TO						Cu %	Pb %	Zn %	Ag(AA) g/mT	Ag(FA) g/mT	Au(FA) g/mT	Po %	Py %	TOT Fe	BaO %	Hg %	Mn %	As %
480.0	485.0	70804	5.0	.0	2JE	2.96	.13	3.01	2.95	26.50			13	7	20	3.59		.24	
485.0	490.0	70805	5.0	.0	2ED	4.03	.19	4.38	5.65	67.70			13	7	20	9.16		.24	
490.0	495.0	70806	5.0	.0	2EJ	3.94	.10	6.03	6.57	29.90			14	18	33	5.67		.35	
495.0	500.0	70807	5.0	.0	2E3	3.86	.15	2.33	3.04	31.90			14	18	33	2.16		.35	
500.0	505.0	70808	5.0	.0	1CD	3.83	.22	1.82	1.69	28.50			14	18	33	.93		.35	
505.0	510.0	70809	5.0	.0	2F0	4.30	.30	5.32	4.76	56.40			14	18	33	3.59		.35	
510.0	515.0	70810	5.0	.0	2J8	3.85	.47	2.83	3.16	51.60			17	9	26	7.87		.35	
515.0	520.0	70811	5.0	.0	2J8	4.20	.10	3.41	3.16	36.00			17	9	26	6.78		.35	
520.0	525.0	70812	5.0	.0	2JG	4.44	.13	6.85	6.76	90.30			17	9	26	23.70		.35	
525.0	530.0	70813	5.0	.0	2G	4.61	.14	5.76	6.33	75.50			17	9	26	23.07		.35	
530.0	535.0	70814	5.0	.0	2G	4.68	.11	8.10	7.30	103.40			4	21	25	26.06		.29	
535.0	540.0	70815	5.0	.0	2G	4.49	.10	5.68	6.28	77.20			4	21	25	23.15		.29	
540.0	545.0	70816	5.0	.0	2G	4.75	.13	4.38	5.14	59.40			4	21	25	17.72		.29	
545.0	550.0	70817	5.0	.0	2GE	4.48	.13	3.20	4.63	41.90			4	21	25	7.91		.29	
550.0	555.0	70818	5.0	.0	2E8	3.29	.16	2.41	3.25	37.00			2	27	30	.18		.11	
555.0	560.0	70819	5.0	.0	2C0	3.28	.06	1.77	.19	69.10			2	27	30	.04		.11	
560.0	565.0	70820	5.0	.0	2C0	3.51	.02	.18	.14	11.90			2	27	30	.04		.11	
565.0	570.0	70821	5.0	.0	2E0	4.54	.12	2.50	1.83	27.70			2	27	30	.02		.11	
570.0	575.0	70822	5.0	.0	2E0	4.66	.10	2.33	1.91	25.80			4	36	40	.03		.12	
575.0	580.0	70823	5.0	.0	2E8	4.23	.33	1.36	2.61	17.90			4	36	40	.08		.12	
580.0	585.0	70824	5.0	.0	2E0	4.45	.21	2.37	2.95	20.70			4	36	40	.09		.12	
585.0	590.0	70825	5.0	.0	2E0	4.69	.20	.52	.67	2.70			4	36	40	.02		.12	
590.0	595.0	70826	5.0	.0	2E0	4.59	.18	1.16	2.33	4.20			5	31	36	.03		.13	
595.0	600.0	70827	5.0	.0	2F0	4.61	.14	4.06	8.82	13.90			5	31	36	.02		.13	
600.0	605.0	70828	5.0	.0	2E8	4.27	.44	2.11	2.75	20.60			5	31	36	.04		.13	
605.0	610.0	70829	5.0	.0	2F0	5.12	.11	2.65	6.52	5.80			5	31	36	.06		.13	
610.0	615.0	70830	5.0	.0	2F0	5.06	.08	3.45	6.99	9.40			3	35	38	.34		.04	
615.0	620.0	70831	5.0	.0	2F0	5.02	.07	4.88	7.65	18.10			3	35	38	.16		.04	
620.0	625.0	70832	5.0	.0	2F0	4.73	.05	5.35	9.58	16.80			3	35	38	.27		.04	
625.0	630.0	70833	5.0	.0	2E8	4.75	.20	1.13	4.85	2.50			3	35	38	.03		.04	
630.0	635.0	70834	5.0	.0	2E8	4.52	.23	1.82	3.44	4.90			7	32	39	.03		.17	
635.0	640.0	70835	5.0	.0	2E8	4.52	.24	2.44	4.31	7.80			7	32	39	.02		.17	
640.0	645.0	70836	5.0	.0	2E8	4.08	.26	.97	2.30	2.00			7	32	39	.02		.17	
645.0	650.0	70837	5.0	.0	2E8	4.09	.56	.64	2.23	4.10			7	32	39	.02		.17	
650.0	655.0	70838	5.0	.0	2E8	4.56	.43	2.38	4.82	8.20			10	25	36	.02		.07	
655.0	660.0	70839	5.0	.0	2F0	4.85	.07	4.95	9.64	11.10			10	25	36	.02		.07	
660.0	665.0	70840	5.0	.0	2E4	3.92	.08	3.61	6.30	17.80			10	25	36	.08		.07	
665.0	670.0	70841	5.0	.0	2H1	4.05	.28	6.27	14.31	44.50			10	25	36	.06		.07	
670.0	675.0	70842	5.0	.0	2D0	3.11	.23	1.72	5.47	31.20			6	15	21	.14		.02	
675.0	680.0	70843	5.0	.0	2C0	3.02	.15	.56	.26	8.60			6	15	21	.09		.02	
680.0	685.0	70844	5.0	.0	2C0	3.02	.03	.85	1.76	10.30			6	15	21	.10		.02	
685.0	690.0	70845	5.0	.0	2D4	3.79	.04	3.88	12.15	28.50			6	15	21	.05		.02	
690.0	695.0	70846	5.0	.0	2F1	4.01	.05	1.83	5.32	21.00			1	35	37	.04		.02	
695.0	700.0	70847	5.0	.0	2F1	5.08	.02	3.15	4.34	14.40			1	35	37	.01		.02	
700.0	705.0	70848	5.0	.0	2F1	4.50	.05	4.09	8.42	19.30			1	35	37	.02		.02	
705.0	710.0	70849	5.0	.0	2F1	5.20	.02	3.51	3.07	16.40			1	35	37	.01		.02	
710.0	715.0	70850	5.0	.0	2F1	3.44	.02	3.51	4.42	15.80			2	30	33	.01		.02	
715.0	720.0	70851	5.0	.0	2F1	3.65	.03	2.72	5.19	14.80			2	30	33	.02		.02	
720.0	725.0	70852	5.0	.0	2F1	3.59	.10	2.62	6.88	19.80			2	30	33	.11		.02	
725.0	730.0	70853	5.0	.0	2F1	3.65	.09	4.12	10.21	29.00			2	30	33	.06		.02	
730.0	735.0	70854	5.0	.0	2F1	3.42	.17	5.96	10.96	115.50			7	9	16	.05		.03	

23MAR84 !THE IMPERIAL ANVIL!

ASSAY LISTING (DEPTH SEQUENCE) DH015

PAGE: 27

DDH: 66046 UTM-N: 9398.9 UTM-E: 14599.9 UTM-ELEV: 4161.1 TOTAL DEPTH: 800.0 SECTION:
 RFE: RFE DIR: 0 PLUNGE ANGLES: 0 0 DHD CALC: 1 SS CALC: 0

---DEPTHS---		SAMPLE NO.	INT.	REC.	ROCK UNIT	S.G. PULP	---ASSAYS---													S.G. W.R.		
FROM	TO						Cu %	Pb %	Zn %	Ag(AA) g/mT	Ag(FA) g/mT	Au(FA) g/mT	Po %	Py %	TOT Fe %	BaO %	Hg %	Mn %	As %		Ba %	
735.0	740.0	70855	5.0	.0	2F1	2.92	.27	2.87	7.41	40.50				7	9	16	.16		.03			
740.0	745.0	70856	5.0	.0	2C0	3.18	.19	.84	2.52	20.80				7	9	16	.22		.03			
745.0	750.0	70857	5.0	.0	2C0	3.03	.22	.25	1.55	13.80				7	9	16	.33		.03			
750.0	755.0	70858	5.0	.0	****	2.99	.35	.04	.31	21.20				15	1	16	.29		.02			
755.0	760.0	70859	5.0	.0	****	2.97	.27	.60	1.27	23.10				15	1	16	.20		.02			

79-02
DDH

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

ENTER " T " DATA

DOWN HOLE SURVEYS " R "

DOWN HOLE LITHOLOGY " L "

DOWN HOLE STRUCTURE " S "

DOWN HOLE FAULTS " F "

SAMPLERS DATA " P "

CHECK ENTRIES FROM GENERAL
DDH DATA REPORT

ENTER ASSAYS "CAMC"

ENTER ASSAYS "CHEMEX"

LIST DDH ASSAY VALUES
CHECK AGAINST ASSAY
CERTIFICATE

SPLINE CALCULATIONS

STRUCTURAL SOLUTIONS

CALCULATE OFFSETS FROM
COLLAR

PRINT OUT GENERAL DDH
DATA REPORTS

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No Core.

May 24/85

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No Assays

Checked DDH/D Jun 11/85 PCT

CYPRUS ANVIL MINING CORPORATION

DIAMOND DRILL CORE LOG

Core Number: 79-02

Fabric Orientation Diagram:

Project: DIKE DRILLING

Location: _____

Claim: _____

Terr. Plane Co-ords.: _____ N

_____ E

Grid Co-ords.: 9361.09 N

14623.66 E

Elevation: 3889.52

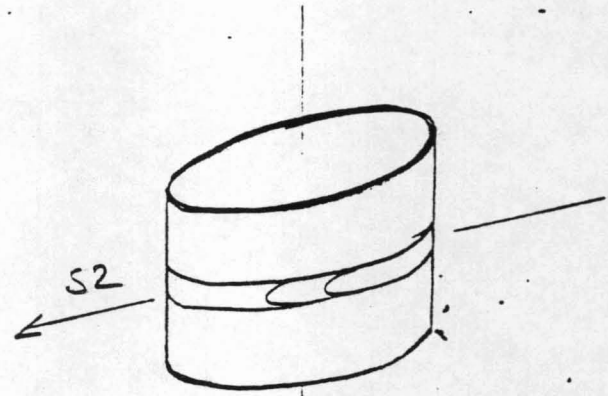
Total Depth: 458'

Purpose: NOT RELOGGED : NO CORE! RFT

Logged by: _____ Date(s) Logged: _____

Drilling Contractor:	Core:	Size	From	To	Collar Cased and Capped:
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____

Started: _____ Completed: _____



All symmetrical terminations looking
NW with S2 dipping
SW with dip azimuth 210° ^{235°}

DDH 74-16

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

ENTER " T " DATA

DOWN HOLE SURVEYS " R "

DOWN HOLE LITHOLOGY " L "

DOWN HOLE STRUCTURE " S "

DOWN HOLE FAULTS " F "

SAMPLERS DATA " P "

CHECK ENTRIES FROM GENERAL
DDH DATA REPORT

ENTER ASSAYS "CAMC"

ENTER ASSAYS "CHENEX"

LIST DDH ASSAY VALUES
CHECK AGAINST ASSAY
CERTIFICATE

SPLINE CALCULATIONS

STRUCTURAL SOLUTIONS

CALCULATE OFFSETS FROM
COLLAR

PRINT OUT GENERAL DDH
DATA REPORTS

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PBT
PAT 4/20/85
PAT 4/24/85
PAT

No Ore

May 20 '85

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Chged DDHID June 17/88 PBT

DIAMOND DRILL CORE LOG

Date: _____

Hole Number: 74-16

Reference Fabric Orientation Diagram:

Project: Favo Zone III Rolog

Location: Anvil District

Claim: _____

MINE ENG

Ferr. Plane Co-ords.: 9515.6 N

14677.1 E

Grid Co-ords: 118+000 E, 25+000 E

Elevation: 4060.7

All symmetry determinations looking

Total Depth: 641.0 feet

NW with S₂⁴ dipping

Inclination: -51° *check.*

SW with dip azimuth 135.

Purpose: _____

Reason hole Terminated: _____

Re Logged by: RST

Date(s) Logged: _____

Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped: _____
_____	_____	_____	
_____	_____	_____	
_____	_____	_____	

Hole Cemented: _____

Steel down le: _____

Started: _____ Completed: _____

79-03

DDH

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

ENTER " T " DATA

DOWN HOLE SURVEYS " R "

DOWN HOLE LITHOLOGY " L "

DOWN HOLE STRUCTURE " S "

DOWN HOLE FAULTS " F "

SAMPLERS DATA " P "

CHECK ENTRIES FROM GENERAL
DDH DATA REPORT

ENTER ASSAYS "CAMC"

ENTER ASSAYS "CHEMEX"

LIST DDH ASSAY VALUES
CHECK AGAINST ASSAY
CERTIFICATE

SPLINE CALCULATIONS

STRUCTURAL SOLUTIONS

CALCULATE OFFSETS FROM
COLLAR

PRINT OUT GENERAL DDH
DATA REPORTS

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No Core.

May 10 80

PRT
PRT April 19/85

PRT

PRT

Checked DDHID (6/17/85) PRT

DIAMOND DRILL CORE LOG

Date: _____

Hole Number: 79-03

Reference Fabric Orientation Diagram:

Project: FARO DIKE DRILLING

Location: ANVIL DISTRICT

Claim: _____

MINE ENG
Terr. Plane
Co-ords.:

9491.46 N

14715.16 E

Grid
Co-ords: X Sect 118 + 000 E L Sect 25 + 000 N

Elevation: 3879.58

All symmetry determinations looking

Total Depth: 516'

NW with S2/54 dipping

Inclination: -90°

SW with dip azimuth 235°.

Purpose: NOTE: In 1984 relogging program 79-03 core not found!

Reason hole Terminated: _____

Logged by: R.L.

Date(s) Logged: _____

Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped:
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Hole Cemented: _____

Steel down Pipe: _____

Started: _____ Completed: _____

DDH 79-03
2 8

Cyprus Anvil Mining Corp.

Page 3 of

Lithologic Log

Date: Corrected
Logged By: DOT

Code	From				To				Recov.	No.	Unit	Description
	10	14	16	20	22	24	26	28				
L	1100		11100						1	1D0	Core not found in 1984 Re-log taken from R.L.'s log and assays	
L	11100		11160						2	1D2		
L	11160		1370						3	1D0		
L	1370		1392						4	1D4		
L	1392		1420						5	2D09		
L	1420		1680						6	2E46		
L	1680		1700						7	2G4 (2E4)		
L	1700		1730						8	2E46		
L	1730		1770						9	2G4		
L	1770		1860						10	2E4		
L	1860		1884						11	2D4		
L	1884		1906						12	2E0 → 2L4		
L	1906		1950						13	1D4		
L	1950		2080						14	1D0		
L	2080		2120						15	2C0		
L	2120		2275						16	1D0		
L	2275		2294						17	2D0		
L	2294		2324						18	2E0		
L	2320		2370						19	2D09		
L	2370		2378						20	2F0		
L	2378		2410						21	2E0		
L	2410		2457						22	2C3		
L	2457		2467						23	2E0		
L	2467		2474						24	2F0		
L	2474		2510						25	2E0		
L	2510		2570						26	2F4		
L	2570		2616						27	2E4		
L	2616		2636						28	2D4		
L	2636		2650						29	2F4		
L	2650		2750						30	2D4		
L	2750		2758						31	2E0		
L	2758		2783						32	2D4		
L	2783		2789						33	2F4		
L	2789		2796						34	2D4		
L	2796		2807						35	2F4		
L	2807		2817						36	2D4		

DDH 7.9-03
2 8

Cyprus Anvil Mining Corp.

Page 4 of

Lithologic Log

Date:

Corrected by
Logged By: RST

Code	From		To		Recov.		No.		Unit	Description
	10	14	16	20	22	24	26	28		
L	281	7	283	0				37	2FA	
L	283	0	286	6				38	2DA	
L	286	6	288	7				39	2EO	<p>N.B. Probably 2CE ie 2EO9 should be 2E19.</p>
L	288	7	300	6				40	2C39	
L	300	6	302	6				41	2EO9	
L	302	6	305	2				42	2C39	
L	305	2	307	4				43	2EO9	
L	307	4	310	0				44	2C39	
L	310	0	311	2				45	2EO9	
L	311	2	312	0				46	2C39	
L	312	0	313	8				47	2EO9	
L	313	8	314	1				48	2C39	
L	314	1	315	7				49	2EO9	
L	315	7	319	0				50	2C39	
L	319	0	342	0				51	2E1	
L	342	0	348	8				52	2FA	
L	348	8	353	0				53	2E4	
L	353	0	360	0				54	2D0	
L	360	0	361	7				55	2EO	
L	361	7	366	0				56	2D05	[2A14?]
L	366	0	387	6				57	2EO	
L	387	6	396	6				58	2C3	
L	396	6	401	0				59	2D0	
L	401	0	407	0				60	1D4	
L	407	0	454	8				61	1D0	(OwO)
L	454	8	467	0				62	2C0	(1D0)
L	467	0	489	0				63	1D0	
L	489	0	492	0				64	2C0	
L	492	0	496	6				65	2D0	
L	496	6	516	0				66	1OEO	

DDH 79-03
 2 (118-25) 8

Cyprus Anvil Mining Corp.
 Lithologic Log

Page 1 of 1
 Logged By: RL/EO

Code	From		To		Unit		Code		Description
	10	14	16	20	22	23	25	27	
L	110	0	113	70	01		1D	0	110 → 116 mildly graphitic
L	113	70	113	92	02		1D	4	
L	113	92	114	20	03		2G	2D	09
L	114	20	116	18	04		2G	4	BARITIC 2E46
L	116	18	117	10	05		2G	E	(BANDED 2G + 2E) 2G4, 2E4
L	117	10	117	30	06		2E	E	2E46
L	117	30	117	70	07		2G	0	2G4
L	117	70	118	16	08		2E	0	2E4
L	118	16	118	18	09		2D	0	2D4
L	118	18	119	10	10		2C	0	approaching 1D0. 244 → 2C0
L	119	10	119	50	11		1D	4	
L	119	50	120	18	12		1D	0	
L	120	18	121	12	13		2C	0	
L	121	20	122	75	14		1D	0	/
L	122	75	122	94	15		2D	0	/
L	122	94	123	20	16		2E	0	
L	123	20	123	37	17		2D	0	9
L	123	37	123	78	18		2F	0	
L	123	78	124	10	19		2E	0	
L	124	10	124	57	20		2D	0	2C3
L	124	57	124	67	21		2E	0	
L	124	67	124	74	22		2F	0	
L	124	74	125	10	23		2E	0	
L	125	10	125	70	24		2F	0	2F4
L	125	70	126	16	25		2E	0	4
L	126	16	126	36	26		2D	0	4
L	126	36	126	50	27		2F	0	4
L	126	50	127	50	28		2D	0	4
L	127	50	127	58	29		2E	0	
L	127	58	127	83	30		2D	0	4
L	127	83	127	89	31		2F	0	4
L	127	89	127	96	32		2D	0	4
L	127	96	128	07	33		2F	0	4
L	128	07	128	17	34		2D	0	4
L	128	17	128	30	35		2F	0	4

Structural Log

Code	From		To		Feature				S ₁ Dip Direct.		S ₂ Dip Direct.		Description
	10	14	18	20	22	24	26	28	32	34	38		
			113							510	2110	235°	
S			1210							518	2110		
S			1311							417	2110		
S			1318							415	2110		
S			147							410	2110		
S			1513							611	2110		
S			162							510	2110		
S			172							515	2110		
S			1812							513	2110		
S			192							42	2110		
S			11012							516	2110		
S			1113							615	2110		
S			122							513	2110		
S			1311							616	2110		
S			2103							817	2110	Qtzites	
			222							510	2110		
			254							411	2110		
S			31015							515	2110		
S			3114							510	2110		
S			3217							610	2110		
S			3915							715	2110	Qtzites.	
S			41012							410	2110		
S			41019							610	2110		
S			41118							417	2110		
S			4218							516	2110		
S			4411							512	2110		
S			447							413	2110		
S			4519							616	2110		
S			4615							610	2110		
S			4714							610	2110		

Geochemical Log (Sampler's Copy)

Logged By: _____

Sampled By: _____

Code	From		To		Sample No.	Description
	10	14	18	22		
						COLLAR ELEVATION 3879.6'
	11392		11400		2D09	0.8' } BENCH 2D0
	11400		11450		2E46	(2D09) } 5.0
	11450		11500		2E46	5.0 } 3730
	11500		11550		2E46	5.0
	11550		11600		2E46	5.0 } 3710
	11600		11650		2E46	5.0
	11650		11700		2E46	5.0 } (2G4)
	11700		11750		2E46	5.0 } (2G4)
	11750		11800		2G4	5.0 } (2E4)
	11800		11850		2E4	5.0 } 3690
	11850		11885		2D4	3.5 }
						188.5' - 227.5' WASTE
	12275		12300		2D0	2.5 } 3650
	12300		12350		2D09	5.0 } (2E0)
	12350		12400		2F0	5.0 } 3630 (2D09)
	12400		12450		2C3	5.0
	12450		12500		2F0	5.0 } (2E0)
	12500		12550		2FA	5.0
	12550		12600		2E4	5.0 } 3610
	12600		12650		2D4	5.0 } (2FA)
	12650		12700		2D4	5.0
	12700		12750		2D4	5.0
	12750		12800		2FA	5.0 } (2D4)
	12800		12850		2FA	5.0 } 3590 (2D4)
	12850		12900		2FA	5.0 } (2D4)

Code	From		To		Sample No.	Description
	10	14	18	20	22	
	29100		29150		2C39	5.0 } <u>BENCH</u>
	29150		30100		2C39	5.0 } 3570
	30100		30150		2C39	5.0 }
	310150		31100		2E09	5.0 } (2C39)
	31100		31150		2E09	5.0 } (2C39)
	31150		32100		2C39	5.0 } (2E09
	32100		32150		2C39	5.0 } 3550 (2E09
	32150		33300		2E1	5.0 }
	33300		33350		2E1	5.0 }
	33350		3400		2E1	5.0 }
	3400		3450		2FA	5.0 } 3530
	3450		3500		2EA	5.0 }
	3500		3550		2FA	5.0 }
	3550		36100		2D0	5.0 } 3510
	36100		36150		2D05	5.0 }
	36150		3700		2E0	5.0 } (2D05)
	3700		37150		2E0	5.0 }
	37150		3800		2E0	5.0 }
	3800		3850		2E0	5.0 } 3490
	3850		3900		2C3	5.0 }
	3900		3950		2C3	5.0 }
	3950		40100		2D0	5.0 } 3470
	40100		40110		2D0	1.0 }

DDH: 79003 UTM-N: 9491.5 UTM-E: 14715.2 UTM-ELEV: 3879.6 TOTAL DEPTH: 516.0 SECTION:
 RFE: RFE DIR: 0 PLUNGE ANGLES: 0 0 DHD CALC: 1 SS CALC: 0

---DEPTHS---		SAMPLE NO.	INT.	REC.	ROCK UNIT	S.G. PULP	---ASSAYS---												
FROM	TO						Cu %	Pb %	Zn %	Ag(AA) g/mT	Ag(FA) g/mT	Au(FA) g/mT	Po %	Py %	TOT Fe	BaO %	Hg %	Mn %	As %
139.2	140.0	74616	.8	.0	2C0	3.40	.30	2.55	1.69	41.80		.44	10	7	17	.80		.30	
140.0	145.0	74617	5.0	.0	2G0	4.57	.24	6.89	6.43	120.00		.31	16	10	27	1.70		.43	
145.0	150.0	74618	5.0	.0	2G0	4.55	.16	6.76	5.96	111.50		.45	5	18	23	2.00		.38	
150.0	155.0	74619	5.0	.0	2G0	4.68	.11	7.49	7.67	100.50		.72	4	16	20	2.60		.28	
155.0	160.0	74620	5.0	.0	2G0	4.72	.17	7.46	6.41	112.20		.84	8	15	24	2.30		.39	
160.0	165.0	74621	5.0	.0	2G0	4.74	.15	6.39	5.56	90.50		.61	7	18	26	2.00		.46	
165.0	170.0	74622	5.0	.0	2G0	4.58	.13	7.15	5.98	104.10		.64	6	14	20	2.50		.44	
170.0	175.0	74623	5.0	.0	2GE	4.60	.09	3.74	3.90	57.60		.53	3	25	29	1.80		.18	
175.0	180.0	74624	5.0	.0	2E	4.67	.08	4.70	5.83	34.30		.78	2	22	25	2.10		.12	
180.0	185.0	74625	5.0	.0	2E	4.78	.02	3.51	5.72	46.70		.23	2	32	34	1.20		.02	
185.0	188.5	74626	3.5	.0	2D	4.01	.09	3.47	10.30	52.50		.36	3	18	22	1.10		.04	
227.5	230.0	74628	2.5	.0	2D0	4.08	.15	3.36	3.63	29.20		.14	2	28	31			.02	
230.0	235.0	74629	5.0	.0	2ED	4.09	.13	.69	.46	8.60		.09	1	33	34			.01	
235.0	240.0	74630	5.0	.0	2EF	4.43	.24	2.15	3.46	20.60		.08	1	35	37			.01	
240.0	245.0	74631	5.0	.0	2D0	4.54	.27	1.19	1.49	11.00		.06	2	38	41			.10	
245.0	250.0	74632	5.0	.0	2EF	4.46	.18	1.42	1.93	4.50		.05	8	34	42			.36	
250.0	255.0	74633	5.0	.0	2F	4.61	.15	6.50	9.71	44.90		.04	7	28	35			.30	
255.0	260.0	74634	5.0	.0	2E	4.70	.16	2.66	4.10	13.00		.03	6	35	42			.19	
260.0	265.0	74635	5.0	.0	2DF	4.36	.17	5.73	8.92	20.60		.18	5	27	32			.10	
265.0	270.0	74636	5.0	.0	2D	3.80	.11	3.87	3.49	78.60		.93	1	24	26			.03	
270.0	275.0	74637	5.0	.0	2D	3.78	.11	4.03	8.02	18.20		.37	3	20	23			.03	
275.0	280.0	74638	5.0	.0	2ED	4.16	.12	4.90	8.41	23.70		.38	5	24	30			.18	
280.0	285.0	74639	5.0	.0	2DF	4.08	.16	4.96	9.70	12.70		.12	7	21	28			.28	
285.0	290.0	74640	5.0	.0	2E	4.03	.19	.36	3.38	2.10		.07	10	22	32			.29	
290.0	295.0	74641	5.0	.0	2C0	3.75	.24	.14	1.20	3.10		.09	7	21	29			.18	
295.0	300.0	74642	5.0	.0	2C0	4.01	.36	.07	1.61	2.10		.07	7	25	33			.18	
300.0	305.0	74643	5.0	.0	2C0	3.77	.62	.06	.97	4.10		.07	7	21	28			.17	
305.0	310.0	74644	5.0	.0	2C0	3.98	.41	.27	1.53	2.10		.05	9	25	35			.25	
310.0	315.0	74645	5.0	.0	2C0	4.11	.25	.13	1.36	2.10		.05	9	26	36			.26	
315.0	320.0	74646	5.0	.0	2C0	4.01	.43	.27	1.68	3.80		.05	6	28	34			.17	
320.0	325.0	74647	5.0	.0	2E0	4.30	.55	.06	.87	3.40		.04	4	34	38			.15	
325.0	330.0	74648	5.0	.0	2E0	4.39	.52	.02	.81	2.40		.05	5	35	40			.15	
330.0	335.0	74649	5.0	.0	2E0	4.27	.18	.02	1.14	1.00		.05	4	34	39			.13	
335.0	340.0	74650	5.0	.0	2E0	4.43	.11	.35	2.41	1.70		.05	4	35	39			.11	
340.0	345.0	74651	5.0	.0	2F0	4.48	.08	4.69	9.12	9.30		.05	3	29	33			.08	
345.0	350.0	74652	5.0	.0	2F0	4.31	.03	7.46	12.10	22.30		.05	2	23	26			.02	
350.0	355.0	74653	5.0	.0	2E4	4.33	.03	5.13	11.00	18.20		.05	3	25	28			.02	
355.0	360.0	74654	5.0	.0	2E4	3.57	.04	1.45	4.64	7.60		.09	3	17	21			.06	
360.0	365.0	74655	5.0	.0	2D0	3.74	.06	.95	3.10	6.90		.07	2	22	25			.02	
365.0	370.0	74656	5.0	.0	****	4.70	.02	2.37	4.96	13.40		.07	1	37	38			.01	
370.0	375.0	74657	5.0	.0	2E0	4.89	.01	.94	.66	6.90		.05	4	40	45			.01	
375.0	380.0	74658	5.0	.0	2E0	4.86	.01	.08	.17	.70		.05	3	42	45			.01	
380.0	385.0	74659	5.0	.0	2E0	4.86	.02	.96	1.82	6.90		.05	3	40	44			.01	
385.0	390.0	74660	5.0	.0	2C0	4.51	.05	.78	2.02	17.20		.06	3	36	40			.02	
390.0	395.0	74661	5.0	.0	2C0	3.38	.11	.48	1.65	8.90		.06	3	17	20			.01	
395.0	400.0	74662	5.0	.0	2D0	3.35	.09	2.70	4.22	50.10		.08	3	12	15			.03	
400.0	401.0	74663	1.0	.0	2D0	3.12	.09	2.95	3.26	78.20		.05	4	5	10			.04	

DDH 66-06

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	PST	✓
DOWN HOLE SURVEYS " R "	PST	OK
DOWN HOLE LITHOLOGY " L "	✓	PST
DOWN HOLE STRUCTURE " S "	✓	PST
DOWN HOLE FAULTS " F "	✓	PST
SAMPLERS DATA " P "	PST
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	May 27/85	PST	OK Done
ENTER ASSAYS "CAMC"
ENTER ASSAYS "CHEMEX"
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE
SPLINE CALCULATIONS
STRUCTURAL SOLUTIONS
CALCULATE OFFSETS FROM COLLAR
PRINT OUT GENERAL DDH DATA REPORTS

PST 524' take core cut
PST 4/23/85 to 4/30/85

To Enter Assays from original log Done

Chyd DDHID June 17/85 PST

DIAMOND DRILL CORE LOG

Date: _____

Hole Number: 66-06

Reference Fabric Orientation Diagram:

Project: Favo Zone III Re-log

Location: Anvil District

Claim: _____

MINE ENG
~~Ferr. Plane~~
Co-ords.:

9599.5 N

14800.0 E

Grid Co-ords: 118+000 / 26+000

MINE COLLAR
Elevation: 4188.3 feet

All symmetry determinations looking

Total Depth: 766'

NW with S2/54 dipping

Inclination: -90°

SW with dip azimuth 235°.

Purpose: _____

Reason hole Terminated: _____

Re Logged by: GL

Date(s) Logged: _____

Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped: _____
_____	_____	_____	
_____	_____	_____	
_____	_____	_____	

Hole Cemented: _____

Steel down Pipe: _____

Started: _____ Completed: _____

DDH FA.66-.06
2 8

Cyprus Anvil Mining Corp.

Page 3 of 8

Lithologic Log

Date: Aug 25/84 Logged By: GL

Code	From	To	Recov.	No.	Unit	Description
	10 14 16 20 22 24 26 28 30 34 35					
						RELOG
L	00	1020		1	*	TRICONED
L	1020	2179		2	1DQ4	4 → 1D4 MOSTLY ALTERED 1D
L	2179	3685		3	1QEQ	(1OE9), CORE MISSING FROM 313' TO 395', GET INFO FROM ORIGINAL LOG.
L	3685	4096		4	1D4	
L	4096	4107		5	2D3	[2E24]
L	4107	4216		6	1D4	
L	4216	4241		7	2GQ	HIGHLY WEATHERED SOFT WHITE BARITE? IN MA. SUL.
L	4211	4262		8	2D34	[2E41]
L	4262	4278		9	2CQ9	WITH VISIBLE CHALCOPYRITE.
L	4278	4375		10	1D4	
L	4375	4410		11	2H1	(OQ9), QZ VNS ARE BROKEN UP + HAVE qz-py BEARING FRACTURES
L	4410	4570		12	1D4	
L	4570	4578		13	2EQ	
L	4578	4646		14	2D4	5, FEW C STREAKS AT 461.3' TO 461.4'
L	4646	4659		15	2E4	
L	4659	4676		16	2D0	
L	4676	4772		17	2E0	
L	4772	4850		18	2D4	(2E1)
L	4850	4873		19	2A4	
L	4873	4940		20	2E1	[2E3], WITH VISIBLE CP
L	4940	5141		21	2EB1	79
L	5141	5222		22	2A4	(2D4)(2E1), MINOR UNITS ARE TOO SHORT TO BREAK-OUT.
L	5222	5306		23	2C3	
L	5306	5371		24	2D0	
L	5371	5477		25	2C3	
L	5477	5493		26	2E4	
L	5493	5570		27	2Q3	
L	5570	5585		28	2D3	
L	5585	5595		29	2A4	
L	5595	5637		30	2D4	8

Structural Log

Code	From		To		Feature	SYM	S ₀ /S ₂		S ₁		S ₂ /S ₄		Description
	10	14	16	20			22	24	26	28	32	34	
													RELOG, RFE=S ₂ , S ₂ =S ₂
S				1028	PS ₂							52	23.5
S				1157	PS ₂							55	
S				1251	PS ₂							56	
S				1392	PS ₂							54	
S				1546	PS ₂							34	
													RFE=S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				1628	CS ₄							39	23.5
S				1805	CS ₄ Z							42	
S				1865	CS ₄ E							74	
													RFE=S ₂ , S ₂ =S ₂
S				1965	PS ₂							40	23.5
S				2113	PS ₂							38	
S				2167	PS ₂							38	
S				3962	PS ₂							17	
S				4044	PS ₂							32	
S				4106	PS ₂							57	
S				4249	PS ₂							61	
S				4299	PS ₂							61	
S				4363	PS ₂							76	
S				4614	PS ₂							33	
S				4862	PS ₂							56	
S				5047	PS ₂							62	
S				5153	PS ₂							57	
S				5211	PS ₂							61	
S				5574	PS ₂							58	
S				5647	PS ₂							63	
S				5742	PS ₂							52	
S				5818	PS ₂							52	
S				5895	PS ₂							66	
S				6008	PS ₂							52	
S				6083	PS ₂							78	
S				6231	PS ₂							27	

DDH F.A.66-06
2 8

Cyprus Anvil Mining Corp.

(M)

DISCONTINUITY
~~Structural Log~~
UPPER INTERNAL LOWER

Date: Aug 25/84 Logged By: GL

Code	From				To				Feature	%	S Dip Direct.		S Dip Direct.		S Dip Direct.		Description
	10	14	16	20	22	24	26	28			32	34	38	40	44		
F	11620			2178	2BJ												INTENSELY BROKEN CORE, MINOR GOUGE DISPERSED THROUGHOUT.
F	2178			3130	2BG												
F	2178			3130	2BG												ABUNDANT GOUGE AND FRACTURES THROUGHOUT. "SANDY" CORE (ALTERAT.)
F	3130			3950	NNN												
F	3970			4230	3GB												POSSIBLE FAULT?
F	4280			4560	3BG												SMALL CHIPS REMAIN
F	4865			5006	1D												OTZITE FRINGS IN SULFIDES.
F	5047			5047	1A												
F	5047			5047	1D												
F	5240			5550	2BJ												
F	6241			6471	1J												
F	6471			6558	2BJ												
F	6558			6725	1BJ												
F	6725			6750	2BJ												
F	6750			7660	1BJ												ABUNDANT HEPPLED FRACTURES.

Code	From		To		Sample No.	Description
	10	14 16	20	22 27		
	1316	165	1317	165	101616	17
P	1317	165	1317	17	101616	18
P	1317	17	1318	12	101616	19
P	1318	12	1318	17	101617	10
P	1318	17	1319	12	101617	11
P	1319	12	1319	17	101617	12
P	1319	17	1401	2	101617	13
P	1401	2	1401	7	101617	14
P	1401	7	1411	1	101617	15
P	1411	1	1411	6	101617	16
P	1411	6	1421	1	101617	17
P	1421	1	1421	35	101617	18
P	1421	35	1421	83	101617	19
P	1421	83	1431	2	101618	10
P	1431	2	1431	7	101618	11
P	1431	7	1441	1	101618	12
P	1441	1	1441	6	101618	13
P	1441	6	1451	1	101618	14
P	1451	1	1451	16	101618	15
P	1451	16	1461	10	101618	16
P	1461	10	1461	15	101618	17
P	1461	15	1471	10	101618	18
P	1471	10	1471	15	101618	19
P	1471	15	1481	10	101619	10
P	1481	10	1481	15	101619	11
P	1481	15	1491	10	101619	12
P	1491	10	1491	15	101619	13
P	1491	15	1501	10	101619	14
P	1501	10	1501	15	101619	15
P	1501	15	1511	10	101619	16
P	1511	10	1511	15	101619	17
P	1511	15	1521	10	101619	18
P	1521	10	1521	14	101619	19
P	1521	14	1521	19	101717	1
P	1521	19	1531	4	101717	2

DO NOT ENTER TO DATABASE !!

ORE STARTS AT 407

Not Entered
See original
logs for
assays!

*2C3

DDH: 66006 UTM-N: 9599.5 UTM-E: 14800.0 UTM-ELEV: 4188.3 TOTAL DEPTH: 766.0 SECTION:
 RFE: RFE DIR: 0 PLUNGE ANGLES: 0 0 DHD CALC: 1 SS CALC: 0

---DEPTHS---		SAMPLE NO.	INT.	REC.	ROCK UNIT	S.G. PULP	ASSAYS													
FROM	TO						Cu %	Pb %	Zn %	Ag(AA) g/mT	Ag(FA) g/mT	Au(FA) g/mT	Po %	Py %	TOT Fe %	BaO %	Hg %	Mn %	As %	Ba %
423.5	428.3	70337	4.8	.0	****	3.96														
437.0	441.0	70339	4.0	.0	****	3.14														
456.0	460.0	70341	4.0	.0	2A0	3.10	.16	.93	3.15	20.40		4	22	26	.18					.07
460.0	465.0	70342	5.0	.0	2A4	3.28	.19	2.89	9.07	40.10		4	22	26	.20					.07
465.0	470.0	70343	5.0	.0	2E	4.60	.28	2.84	4.91	52.60		4	22	26	.06					.07
470.0	475.0	70344	5.0	.0	2E	4.56	.19	.35	1.36	8.70		4	22	26	.07					.07
475.0	480.0	70345	5.0	.0	2D	4.00	.27	3.29	6.91	29.80		4	22	26	.10					.07
480.0	485.0	70346	5.0	.0	2D	3.71	.06	1.35	3.38	15.60		3	26	30	.12					.09
485.0	490.0	70347	5.0	.0	2A0	3.59	.04	1.00	2.80	14.60		3	26	30	.09					.09
490.0	495.0	70348	5.0	.0	2C	4.04	.29	.30	.84	19.10		3	26	30	.04					.09
495.0	500.0	70349	5.0	.0	2C	3.89	.29	.01	.86	7.10		3	26	30	.03					.09
500.0	505.0	70350	5.0	.0	2C	4.06	.31	.69	1.66	9.30		3	26	30	.03					.15
505.0	510.0	70351	5.0	.0	2C	4.10	.22	.51	1.04	6.60		3	26	30	.02					.15
510.0	515.0	70352	5.0	.0	2C	3.93	.23	.93	1.92	13.70		3	26	30	.05					.15
515.0	520.0	70353	5.0	.0	2A4	3.81	.09	3.53	7.29	146.00		3	26	30	.10					.15
520.0	524.0	70354	4.0	.0	2A4	3.22	.14	3.26	4.60	55.20		4	17	21	.17					.11
524.0	529.0	70355	5.0	.0	2D	3.32	.23	1.89	1.64	40.50		4	17	21	.11					.11
529.0	534.0	70356	5.0	.0	2D	3.69	.16	2.90	2.35	46.70		4	17	21	.10					.11
534.0	539.0	70357	5.0	.0	2C	3.74	.14	.56	1.56	14.00		4	17	21	.08					.11
539.0	544.0	70358	5.0	.0	2C	3.88	.12	.55	1.80	11.50		2	27	29	.05					.06
544.0	549.0	70359	5.0	.0	2C	4.57	.07	.10	1.74	3.90		2	27	29	.04					.06
549.0	554.0	70360	5.0	.0	2D	4.17	.10	1.63	4.58	11.30		2	27	29	.05					.06
554.0	559.0	70361	5.0	.0	2D	4.29	.25	2.22	2.84	22.00		2	27	29	.03					.06
559.0	564.0	70362	5.0	.0	2D	3.71	.07	4.43	7.87	16.00		2	21	24	.06					.03
564.0	569.0	70363	5.0	.0	2D	3.94	.08	1.82	5.80	12.10		2	21	24	.06					.03
569.0	574.0	70364	5.0	.0	2A4	3.55	.10	3.10	11.22	12.50		2	21	24	.14					.03
574.0	579.0	70365	5.0	.0	2D	4.07	.05	4.82	9.17	16.10		2	21	24	.05					.03
579.0	584.0	70366	5.0	.0	2D	3.75	.07	4.65	10.19	16.50		3	23	26	.06					.05
584.0	589.0	70367	5.0	.0	2A4	3.62	.04	5.66	11.10	12.70		3	23	26	.09					.05
589.0	594.0	70368	5.0	.0	2D	4.00	.04	2.06	6.18	7.60		3	23	26	.06					.05
594.0	599.0	70369	5.0	.0	2D	4.25	.06	2.14	4.90	8.20		3	23	26	.03					.05
599.0	604.0	70370	5.0	.0	2D	3.70	.05	3.74	9.66	21.70		3	17	21	.10					.04
604.0	609.0	70371	5.0	.0	2D	3.44	.06	2.00	7.14	16.00		3	17	21	.17					.04
609.0	614.0	70372	5.0	.0	2D	4.22	.04	1.76	5.56	20.30		3	17	21	.08					.04
614.0	619.0	70373	5.0	.0	2D	3.13	.18	2.69	5.95	73.70		3	17	21	.27					.04
619.0	622.8	70374	3.8	.0	2D	3.07	.07	1.33	4.01	22.60		3	17	21	.32					.04

DDH 74-01

COMPLETE

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

ENTER " T " DATA

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DOWN HOLE SURVEYS " R "

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DOWN HOLE LITHOLOGY " L "

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DOWN HOLE STRUCTURE " S "

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DOWN HOLE FAULTS " F "

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SAMPLERS DATA " P "

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CHECK ENTRIES FROM GENERAL
DDH DATA REPORT

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ENTER ASSAYS "CAMC"

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ENTER ASSAYS "CHENEX"

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LIST DDH ASSAY VALUES
CHECK AGAINST ASSAY
CERTIFICATE

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SPLINE CALCULATIONS

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STRUCTURAL SOLUTIONS

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CALCULATE OFFSETS FROM
COLLAR

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PRINT OUT GENERAL DDH
DATA REPORTS

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Copied DDH 11/10 Jue 17/85 PBT

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DIAMOND DRILL CORE LOG

Date: _____

Hole Number: 74-01

Reference Fabric Orientation Diagram:

Project: Favo Zone III Re-log

Location: Anvil District

Claim: _____

MINE ENG
Terr. Plane
Co-ords.:

9701.5 N

14,908.2 E

Grid
Co-ords: X Sect 118+000E, L Sect 27+000N

MINE COLLAR
Elevation:

4112.8 feet

All symmetry determinations looking

Total Depth: 523 feet

NW with S2 dipping

Inclination: -90°

SW with dip azimuth 235.

Purpose: _____

Reason hole Terminated: _____

ReLogged by: G.L.

Date(s) Logged: _____

Drilling Contractor: _____

Size	CORE From	To	Collar Cased and Capped: _____
<u>BQ</u>	<u>0</u>	<u>EOH</u>	
_____	_____	_____	
_____	_____	_____	

Hole Cemented: _____

Steel down the: _____

Started: _____ Completed: _____

DDH 74-01
2 8

Diamond Drill Core Log

Date: _____ Logged By: _____

Code	Drillhole	Elevation				Northing				Easting				Units (feet/metres)	R.F.E.
		2	8	10	16	17	24	25	32	34	39	41	42		
T	74-01	4112.8				9701.5				14908.2			feet	52 /54	

Code	Drillhole	Depth				Zenith Angle	True Azimuth	Comments Entered to DDH DB	
		2	8	10	14				22
R	74-01			00		180.0	0.0	AT COLLAR	
R	74-01			1000		178.3	34.0		
R	74-01			2000		177.1	34.0	1985 ESTIMATE	
R	74-01			3000		176.0	34.0	28	
R	74-01			4000		174.9	34.0		
R	74-01			5000		173.7	34.0		
R									
R									
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Code	Drillhole	Comments, Errant Remarks, Snivellings and /or Lewd Suggestions													
		2	8	10	14	16	17	22	26	28	32	34	39	41	42

From	To	Unit	Code	Description
10 14 16 20 22 23 25 27				
100	1100	01	#1	O.B. or rubble in pit - collected in 'bedrock'
100	1750	02	1CD	[1CD#4] SLIGHT ALTERATION INCREASE TOWARDS 10E to 1CD6 musc > biot.
1750	2270	03	0E8	to OE89 upper contact & indeterminate apparent lower contact Se 50/210 suggests OE8 -> sill
2270	2318	04	1D4	to 1CD4
2318	2980	05	0E8	to OE89 upper contact appears Se 60/210 lower contact grossly Se 50/210, suggests OE8 sill
2980	3130	06	1D4	to 1CD4
3130	3140	07	0E6	contact & ^{was 315.5} indeterminate
3114	3178	08	2C4	[2B4] VISUALLY IT RESEMBLES 2B4 (MOSTLY PYRITE-FREE sphalerite - QTZITE). brecciated MINOR MARLITE
3178	3220	09	1D4	to 1CD4 REMOBI LIZED GALENA + PYRITE IN ALTERED SECTION.
3220	3235	10	2C0	brecciated
3235	3250	11	2D4	py ≈ 5% Pb+Zn < 5%
3250	3280	12	2C0	(2D4)
3280	3570	13	1D4	to 1CD4
3570	3665	14	2C7	#9 Breccia, PITTED (DISSOLVED SULFIDES).
3665	3690	15	2A0	[2A4] Pb+Zn < 5% DISPERSED THIN BLACK CARBONACEOUS RIBBONS.
3690	3770	16	2E0	2C34 -> 2C0, 2C0 FROM 374.5 TO 377.0.
3770	3910	17	1D4	to 1CD4 1D42 FROM 377.8' TO 379.3' MINOR REMOBI LIZED GALENA IN QTZ VN.
3910	3928	18	2E0	2C3#2
3928	4015	19	2A0	Pb+Zn ≈ 5%
4015	4045	20	2D10	#5 not carbonaceous enough for ribbon banded
4045	4750	21	2A0	432.5 -> 441.0 is 2A3, 441.0 TO 446.1 is 2A34, 446.1 TO 475.0 is 30-40% py over interval Pb+Zn < 5% 2A3 -> 2C345
4750	4830	22	2FE	[2E0] interbanded 2F and 2E 6"-12" scale
4830	4875	23	2D10	probably Pb+Zn < 5% over interval (2F4) 2F4 INTERBANDS ARE MINOR. Pb+Zn > 5% py ≈ 20%
4875	4910	24	1D4	to 1CD4 hole too fractured, short
4910	5230		1D4	[1CD4]

DDH FA74-01
2 8

Cyprus Anvil Mining Corp.

Page _____ of _____

Structural Log

Date: Aug 16/84 Logged By: GL

Code	From			To			Feature	SYM	S ₀		S ₁ /S ₂		S ₂ /S ₄		Description	
	10	14	16	20	22	24			26	28	Dip	Direct.	Dip	Direct.		Dip
																RELOG, RFE=S ₂ , S ₂ =S ₂
S				226			P.S.2						41	23.5		
																RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				400			CS.4Z				42	35.0	22	23.5		
																RFE = S ₂ , S ₂ =S ₂
S				491			P.S.2						40	23.5		
																RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				687			CS.4Z			51	30.8	40	23.5			
																RFE = S ₂ , S ₂ =S ₂
S				2277			P.S.2						42	23.5		
S				3013			P.S.2						53			
S				31100			P.S.2						66			
S				3316			P.S.2						61			
S				3364			P.S.2						56			
S				3520			P.S.2						66			
S				3570			P.S.2						72			
S				3664			P.S.2						78			
																RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				3795			CS.43						78	23.5		
																RFE = S ₂ , S ₂ =S ₂
S				3892			P.S.2						57	23.5		
S				3969			P.S.2						60			
S				4073			P.S.2						71			
S				4176									72			
																RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				4259			CS.4D						63	23.5		
																RFE = S ₂ , S ₂ =S ₂
S				4365			P.S.2						75	23.5		
S				4472			P.S.2						61			
																RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				4565			CS.4D						70	23.5		
S				4682			P.S.2						60	23.5		RFE = S ₂ , S ₂ =S ₂
S				4804			P.S.2						77			
S				4952			CS.4Z			38	010.0	47	23.5			RFE = S ₄ , S ₂ =S ₄ , S ₀ =S ₂
S				5064			CS.4S			18	34.0	74				
S				5163			CS.4						73			

See D&T log on following page

Structural Log

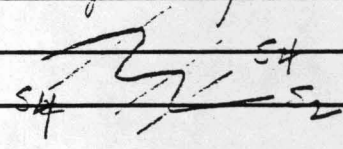
Logged By: Y.R. [unclear]

Code	From		To		Feature	S ₁ Dip Direct.	S ₂ Dip Direct.	Description
	10	14 16	20	22 24 26 28				
	29	80	31	30	RS12			Some relict S ₁ ; geometrically. S ₁ = 50/20
			31	10				
	31	50	31	80	B			Basal to unmarked post D ₂ bed
	31	80	31	90	45			No attitude possible Gauge zone in white mica envelope
	31	80	31	28	081			Post-D ₁ variation
	31	28	31	40	RS12			Geometrically ≡ S ₄
S			31	40	F4 S			D ₄ (F ₄) hinge, similar, asymmetric
	31	40	31	75	RS12			S ₁ = 60/20
S			31	75	F4 Z			D ₄ (F ₄) hinge, similar, asymmetric
	31	75	31	40	RS12			S ₁ = 45/20
S			31	40	F4 Z			F ₄ hinge, similar, asymmetric
	31	40	31	40	RS12			
S			31	60	F4 Z			F ₄ , similar, asymmetric S ₁ = 50/20
	31	60	31	70	RS12			
S			31	70	F4 Z			F ₄ similar, asymmetric S ₁ = 55/20
	31	70	31	80	45			Gauge zone in 104, no attitude possible
	31	80	31	20	RS12			
S			31	20	F4 Z			F ₄ similar, asym., rootless S ₁ = 65/20
S			31	65	F4 3			" " " " = 65/20
	31	20	31	90	RS12			
	31	90	31	50	B			Post D ₁ variation
	31	50	31	80	RS12			Ch 2A0
	31	80	31	70	B			Post D ₁ incipient variation
	31	70	31	90	RS12			
S			31	90	F4 Z		75 2110	S ₄ steeper than S ₂ S ₁ ; S ₄ = 50/20 same Δ
	31	90	31	20	RS12			
S			31	20	F4 3			S ₄ flattening downward S ₄ = 80/20
	31	20	31	65	RS12			
S			31	65	F2		70 2110	No symmetry possible, single hinge S ₄ = 70/20 F ₂ trend 235, 30° SW assuming ⊥ c.a.
	31	65	31	20	RS12			Approx. S ₂ S ₄ no convincing
	31	12	31	60	RS12			No reliable S ₂ & 4 as core. Patches split
			31	60	F2 3			Single hinge showing 3 symmetry
S			31	90	RS12		70 2110	
			31	90	F2			Single hinge, no symmetry, no orient., core split
	31	90	41	105	RS12			
S			41	105	F4 S			F ₄ similar, asymmetric, chn, S ₁ = 70/20

Structural Log

Logged By: 

Code	From				To				Feature	Sym	S ₁		S ₂		Description
	10	14	16	20	22	24	26	28			Dip	Direct.	Dip	Direct.	
	14105		14111	0	RS2										S ₁ = 70/210
			14111	0	F2						70	210			F ₂ axis trend = 180° 25° S; note all measurements assume S ₂ S ₄ which looks OK; no symmetry possible on F ₂ as core bodies fault broken; S ₂ similar, isoclinal, due to west
	14111	0	14126	0	RS2										S ₁ = 70/210
			14126	0	F4										Single, similar isoclinal hinge w/ trend = 230° plunge 18° SW; no sym
	14126	0	14126	5	RS2										S ₁ = 60/210
			14126	5	F2	Z					60	210			Z symmetry, similar, asymmetric, isoclinal F ₂ folds in gtz band in character of F ₂ trend 255° plunge 25° SW
	14126	5	14131	5	RS2										
			14131	5	F2	S					70	210			S symmetry, similar, asymmetric, isoclinal F ₂ folds in gtz bands; F ₂ trends = 220° plunge 18° SW
	14131	5	14137	0	RS2										S ₁ = 70/210
			14137	0	F2	Z					70	210			Z symmetry, similar, asymmetric, isoclinal F ₂ folds in gtz bands; accounted that S ₂ S ₄ ; note, maybe F ₂ folds as folial foliations seen in gtz-rich bands
	14137	0	14416	0	RS2										S ₁ = 75/210
			14416	0	F2	3					75	210			3 symmetry F ₂ hinge zone in gtz bands of 240°; S ₂ S ₄ accu- then F ₂ trend 220-230° plunge 10- 15° SW
	14147	0	14154	5	RS2										
			14154	5	F4	S									S ₁ = 86/210
															S symmetry, isoclinal, similar, asymmetric F ₄ single hinge; S symmetry inferred from steep S ₂ shallow S ₄ relations
	14154	5	1475	5	RS1						70	210			S ₁ = 70/210
			1475	5	RS1										Banding (S ₀) on 240 S ₁ S ₂

Code	From				To				Feature	S ₁		S ₂		Description
	10	14	16	20	22	24	26	28		Dip	Direct.	Dip	Direct.	
	48	13	0	49	11			RSZ						
				49	11			IF4Z						Z, approx. similar close w/ gross Z symmetry S₄ = 60/210
														
	49	10		49	40			CSA#						Z region 491.0-494.0
S				49	20			IF4Z						S ₄ = 50/210
	49	40		49	70			CSA#						S region 494.0-497.0
S				49	60			IF4S						S ₄ = 60/210
	49	70		49	90			CSA#						M region 497.0-499.0
	49	90		50	10			RSZ						
	50	10		50	80			CSA#						S region 501.0-508.0
S				50	60			IF4S						S ₄ = 70/210
	50	80		51	05			CSA#						Z region 508-510.5
S				50	85			IF4Z						S ₄ = 60/210
	51	05		51	45			CSA#						S region
S				51	25			IF4S						S ₄ = 80/210
	51	45		51	85			CSA#						S ₂ subvertical, S ₄ subhorizontal
	51	85		52	25			CSA#						Z region 518.5-522.5
S				52	15			IF4Z						S ₄ = 70/210
														See attached graphic log of 491-523'

DDH FA74-01
2 8

Cyprus Anvil Mining Corp.

Page _____ of _____

DISCONTINUITY
~~Structural Log~~
UPPER INTERNAL LOWER

Date: Aug 16/84 Logged By: GL

Code	From		To		Feature	S ₁ Dip	S ₂ Direct.	S ₃ Dip	S ₄ Direct.	S ₅ Dip	S ₆ Direct.	Description
	10	14	16	20								
												RELOG
F	100		570		1JB							
F	570		1450		2JB							ABUNDANT RUBBLE, MINOR GOUGE.
F	1450		1690		1JB							
F	1690		1800		3GF							INTENSELY FRACTURED + GOUGED, LIKELY FAULT ZONE.
F	1800		1965		1JB							
F	1965		2276		2JB							MINOR GOUGE ALSO.
F	3116		3288		3JB							SOME GOUGE ALSO.
F	3459		3480		3GX							
F	3765		378		12JB							
F			3830		S ₁			15190				THIN PLANAR SHEAR
F	3932		3945		2X ₁							SULFIDE CLASTS IN QUARTZ-VEIN MATRIX.
F	4218		4261		2JB							
F	4819		4830		2JB							
												MOST OF THE SULFIDE SECTION APPEARS TO HAVE HELD TOGETHER QUITE WELL.
F	5072		5093		2JG							POSSIBLE SMALL FAULT.
F	5197		5204		Q							BARREN QTZ VEIN. NOTE: QTZ VEINS NOT VERY ABUNDANT IN THIS HOLE.
												EOH.

DDH: 74001 UTM-N: 9701.5 UTM-E: 14908.2 UTM-ELEV: 4112.8 TOTAL DEPTH: 523.0 SECTION:
 RFE: RFE DIR: 0 PLUNGE ANGLES: 0 0 DHD CALC: 1 SS CALC: 0

---DEPTHS---		SAMPLE NO.	INT.	REC.	ROCK UNIT	S.G. PULP	---ASSAYS---													
FROM	TO						Cu %	Pb %	Zn %	Ag(AA) g/mT	Ag(FA) g/mT	Au(FA) g/mT	Po %	Py %	TOT Fe	BaO %	Hg %	Mn %	As %	Ba %
314.0	319.0	72052	5.0	.0	2D4	3.00	.10	2.97	8.85	53.80					5	11	16	.21		.13
319.0	324.0	72053	5.0	.0	1D4	3.17	.03	.66	.68	16.50					5	11	16	.09		.13
324.0	329.0	72054	5.0	.0	2CD	3.07	.07	6.51	3.18	73.00					4	8	13	.11		.11
358.0	363.0	72056	5.0	.0	2C7	3.32	.37	1.92	.70	23.50					6	16	22	.10		.07
363.0	368.0	72057	5.0	.0	2CA	3.38	.17	1.78	3.00	23.10					6	16	22	.15		.07
368.0	373.0	72058	5.0	.0	2E0	3.82	.11	1.78	2.37	17.20					6	16	22	.08		.07
373.0	378.0	72059	5.0	.0	2E0	3.02	.18	1.12	1.76	18.50					6	16	22	.16		.07
391.0	396.0	72061	5.0	.0	2DA	3.21	.10	2.94	6.32	27.00					3	15	18	.11		.07
396.0	401.0	72062	5.0	.0	2A4	3.40	.05	4.08	10.00	32.20					3	15	18	.22		.07
401.0	406.0	72063	5.0	.0	2D5	3.30	.10	2.00	4.93	29.70					3	15	18	.13		.07
406.0	411.0	72064	5.0	.0	2A4	3.25	.03	2.73	7.23	22.40					1	15	16	.17		.02
411.0	416.0	72065	5.0	.0	2A4	3.18	.05	4.70	7.61	50.10					1	15	16	.16		.02
416.0	421.0	72066	5.0	.0	2A4	3.36	.02	1.94	7.40	19.50					1	15	16	.19		.02
421.0	426.0	72067	5.0	.0	2A4	3.35	.02	2.42	5.70	20.50					1	15	16	.15		.02
426.0	431.0	72068	5.0	.0	2A4	3.45	.03	1.78	5.22	23.30					1	17	19	.14		.02
431.0	436.0	72069	5.0	.0	2A0	3.29	.02	.94	3.26	16.10					1	17	19	.17		.02
436.0	441.0	72070	5.0	.0	2A0	3.23	.03	.58	1.94	13.70					1	17	19	.16		.02
441.0	446.0	72071	5.0	.0	2A4	3.34	.02	1.56	4.36	23.10					1	17	19	.13		.02
446.0	451.0	72072	5.0	.0	2A0	3.08	.03	.52	.72	24.80					1	18	19	.22		.02
451.0	456.0	72073	5.0	.0	2A0	3.23	.04	.34	1.84	9.10					1	18	19	.19		.02
456.0	461.0	72074	5.0	.0	2A0	3.14	.06	.50	1.80	13.50					1	18	19	.18		.02
461.0	466.0	72075	5.0	.0	2A0	3.28	.03	.38	.98	13.50					1	18	19	.14		.02
466.0	471.0	72076	5.0	.0	2A0	3.19	.03	.54	1.82	17.20					2	22	24	.23		.03
471.0	476.0	72077	5.0	.0	2A4	3.63	.02	2.59	6.42	19.50					2	22	24	.16		.03
476.0	481.0	72078	5.0	.0	2FE	4.76	.01	2.28	5.61	16.30					2	22	24	.04		.03
481.0	486.0	72079	5.0	.0	2D4	4.08	.02	5.07	10.47	37.10					2	22	24	.05		.03
486.0	491.0	72080	5.0	.0	2D0	3.34	.06	2.35	5.70	27.70					2	22	24	.13		.03

DDH 76X-10

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	RPT	✓
DOWN HOLE SURVEYS " R "	RPT	OK
DOWN HOLE LITHOLOGY " L "	✓	RPT
DOWN HOLE STRUCTURE " S "	✓	RPT
DOWN HOLE FAULTS " F "	✓ Enter 6126.6, 340	RPT	RPT	✓
SAMPLERS DATA " P "
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	May 27/85	RPT
ENTER ASSAYS "CAMC"
ENTER ASSAYS "CHENEX"
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE
SPLINE CALCULATIONS
STRUCTURAL SOLUTIONS
CALCULATE OFFSETS FROM COLLAR
PRINT OUT GENERAL DDH DATA REPORTS
Chaged DDH ID Jul 17/85 RPT				

WHO DONE IT?
INITIALS PLEASE!!

CHECKED BY??
INITIALS PLEASE!

REMARKS

APR 9/85 RPT APR 30/85

Not Assayed.

CYPRUS ANVIL MINING CORPORATION

DIAMOND DRILL CORE LOG

Hole Number: 76X-10

Fabric Orientation Diagram:

Project: Anvil

Location: Open Pit Sects 28/118

Claim: _____

Terr. Plane Co-ords.: _____ N

_____ E

Grid (Mine) Co-ords.: N 9, 795

E 14, 990

Elevation: 4041.2 feet no check
(Mine-ground) (MSL)

Total Depth: 637'

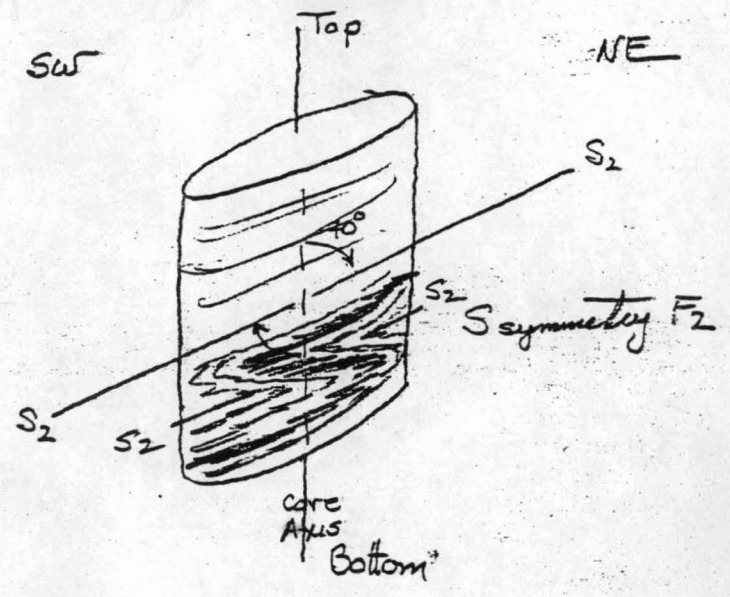
Purpose: Marginal analysis, form of orebody, symmetry NE end Section 118

Logged by: D.S. Jennings

Date(s) Logged: 11 June - June, 1976

Drilling Contractor: Arctic Diamond Drilling

Core:	Size	From	To	Collar Cased and Capped:
<u>BQ</u>	<u>11</u>	<u>637</u>		<u>No</u>
_____	_____	_____		_____
_____	_____	_____		_____



All symmetry determinations looking

NE with S2 dipping 154
SW with dip azimuth 210° 235°

Relogged by G. Lynch
check

Started: 8:00 A.M., 9, June Completed: 11:30 A.M., 13, June

DDH FA 76X 10
2 8

Cyprus Anvil Mining Corp.

Page _____ of _____

Lithologic Log

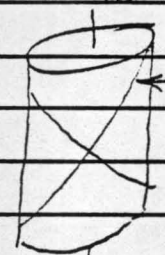
Date: Aug 17/84 Logged By: GL

Code	From		To		Recov.	No.	Unit	Description
	10	14	16	20				
L		00		110		1	*	RELIC, TRICONED
L		110		670		2	1,0E89	WHITE ADVANCED ARGILLIC ALTERATION.
L		670		985		3	1,CD#4	MUSCOVITE >> BIOTITE, GARNET
L		985		1,168		4	1,CD	
L		1,168		1,283		5	1,CD#8	WITH GARNET, LIGHT GREEN COLOUR (CHLORITE)
L		1,283		1,288		6	1,DE9	SMALL CHILLED DYKE
L		1,288		1,323		7	1,CD#8	WITH GARNET, MINOR CHLORITE
L		1,323		2,467		8	1,CD#8	WITH GARNET, MINOR CHLORITE, ABUNDANT PY-MARLASITE LAYERS.
L		2,467		2,926		9	1,DE9	ADVANCED ARGILLIC ALTERATION.
L		2,926		2,956		10	1,DE28	
L		2,956		2,972		11	1,DE9	CHILLED MARGIN.
L		2,972		3,019		12	1,CD4	WITH GARNET.
L		3,019		3,030		13	2,D9	
L		3,030		3,089		14	2,D4	
L		3,089		3,734		15	1,DE9	ADVANCED ARGILLIC ALTERATION.
L		3,734		4,010		16	1,DE28	
L		4,010		4,134		17	1,DE9	" " "
L		4,134		4,404		18	1,DE28	
L		4,404		4,582		19	1,DE9	ADVANCED ARGILLIC ALTERATION, CHILLED MARGIN.
L		4,582		4,710		20	1,CD4	WITH GARNET, IRREGULAR PY-VEINLETS.
L		4,710		4,721		21	1,DE9	(?) CHILLED FELSIC DYKE.
L		4,721		4,847		22	1,CD4	WITH GARNET.
L		4,847		5,538		23	1,CD6	WITH GARNET, POSSIBLY ALTERATION TO MUSCOVITE CAUSES BIOTITE CLOTTING.
L		5,538		5,730		24	1,CD4	WITH GARNET.
L		5,730		5,922		25	1,CD6	" "
L		5,922		5,986		26	1,CD4	
L		5,986		6,370		27	1,CD5	WITH GARNET AND ALSO PYROPHOTITE.
								EOH

Lithologic Log

 Logged By: *DSJ*

Code	From		To		Unit		Code		Description
	10	14	16	20	22	23	25	27	
		100		110	1				O/B, hole cased 0-11'
L		110		1270	2	01010			Rubby core, 3' recovered over 16' = 19% recovery
L		1270		1640	3	01019			Diabase heavily kaolinized, fault gouged w/ moderately altered fragments in kaolinized gouge; poor recovery over interval; approx 20' recovered over 37' = 54%
L		1640		1715	4	11014			Typical WME w/ sulfides (marcasite-pyrite) blebs and blobs; question of whether this "bleaching" due to ore zone or diorite; poor recovery in unit 4' rec. over 7.5' = 53%; diorite above concordant w/ S ₂ @ 640' → diorite = sill; note sulfides dominantly foliaform (S ₂) bands not amoeboid blobs, also minor bio "clots"
L		1715		11300	5	11010			Transition zone; weak Pt. S. O ₂ domed, dls broken & QF banding; unit in position (strat.) of 100
L		11300		11305	16	0158			H ₂ -bio diorite like; upper contact $\approx 150^\circ \Delta 30SW$ lower contact foliaform to S ₂ where S ₂ 55, 210
L		11305		11480	17	11010			As 71.5-130
L		11480		11735	18	11016			Clotted variant of schist unit 100/100 transitional to 104; more visible andalusite than 71.5-148.0; musc. abundance increases towards 104, bio clots decrease; some reaction going on here between normal schists (71.5-148) and 104 which starts @ 173.5
L		11735		12095	19	11014			Typical WME w/ sulfides (marc.) blebs & stungers minor gas & pink, irreg. andalusite porphyroblasts
L		12095		121115	10	21010			H ₂ gray, musc.-bearing, PbS/ZnS minor marc. bearing quartzite; est 1% combined
L		121115		12190	11	11014			WME as 64-71.5; 1735-209.5; 1-15% total sulfides as blebs & stungers w/ py \approx PbS
L		121190		12225	12	21010			As 209-211.5 w/ 104 interbands; est 1-2% comb.
L		12225		12228	13	11014			
L		12228		12240	14	11014			Fault gouge: post D ₂ in age w/ $\Sigma 165 \Delta 80SW$
L		12240		12470	15	11014			Typical WME w/ minor bio metal sulfides & shell gty "sweats"

Code	From	To	Unit	Code	Description
1	10	14 16	20	22 23 25 27	
L	121470	129120	116	OE19	Completely kaolinitized porphyritic (plag-bio) diorite, ash white, showing relict phenocrysts; alteration gradational to "fresh" @ 292
L	129120	129155	117	OE17	Fresh plag-bio diorite ϕ Contact foliiform wrt S ₂ @ 70° to ca. w/ 210° az
L	129155	129175	118	OE19	As 2470-292.0; diorite foliiform wrt S ₂ w/ contact @ 80° to ca. w/ dip azimuth = 210°
L	129175	131010	119	1D14	Gametiferous variant, minor amorphous FeS ₂ and siliceous bands
L	131010	131015	240	OE19	White, aphanitic, diorite w/ 2% marcasite polyxaline "phenos" uniformly diss in rock
L	131015	131020	241	1D14	Fault gouge; no attributes possible as core rubble & ground
L	131020	131085	242	2D14	Contains v. minor 240 and is slightly pyritic but dominantly 204; cut 4-6% to comb.; internal brecciated (post D ₁ or D ₂)
L	131085	131090	243	1D14	Fault gouge @ 90° to ca. top & base of internal
L	131090	131093	244	2C14	Pyritic gylite w/ minor PbS/ZnS
L	131093	131415	246	OE19	As 247.0 - 292.0 w/ definite PbS/ZnS bearing stringers; kaolinitization of diorite probably related to "sublimation" reactions between diorite melt & stopped-in sulfide & enclaves
L	134152	141235	217	OE17	Internal variably kaolinitized but dominantly fresh; rock should be OE7/OE9; many CaCO ₃ filled fractures @ 40° to ca. dipping in opposite directions
					
L	141235	141280	248	1C1D	100% brecciated by 100% fault gouge; sub-angular to rounded schist and v. minor diorite frags. in clayey matrix of schist fault gouge; gouge/breccia zone @ 50° to ca. @ top & bottom of internal
L	141280	141585	249	OE17	As 341.2 - 423.5; actually fresh, partially altered diorite; contact 40° to ca. @ 210° i.e. discordant

Code	From	To	Unit	Code	Description
	10 14 16 20 22 23 25 27				
L	4518.5	4618.0	310	1C10	Clotted variant of schist (possible K alteration zone NE of & below deposit; dk purplish brown "amoeboid" bio clots in musc schist matrix)
L	4618.0	4830.0	311	1D14	"Bleached" WME w/ 1-15% total sulfides dominantly FeS_2 (marcasite?) w/ some suspected base metal sulfides; interval @ 4825-4830 magnetite = 28%; interval may represent F-7 infold of steeply overturned NE limb of ore zone
L	4830.0	4890.0	312	1C16	Clotted variant of QFBMS; prominent bio "clots" & dk. pink pyralite gas porphs. over interval; prominent FeS_2 (marcasite) banding defining S_0 S_1 (?)
L	4890.0	4910.0	313	1C16	Gauge zone in 1C16; zone 60° to c.a. @ 210 \approx $S_2 = S_1$ @ 489'; zone @ 50° c.a. @ 270 dominant to S_1 S_2
L	4910.0	5410.0	314	1C16	Clotted variant of QFBMS as 4830-4890; bio clots appear as "woolies" fold hinges of more competent S_1 banding in musc schist (possible K alteration zone) produced during D_2
L	5410.0	5411.0	316	1C16	Gauge zone in 1C16; zone 35° to c.a. w/ 30° @ 540.0; attitude of contact @ 541.0 uncertain
L	5411.0	5412.5	317	1C16	As 490.0-540.0
L	5412.5	5413.0	318	0E17	Diorite dike @ 60° SW to c.a. @ both contacts; since dike cuts S_1 @ 8° to poorly devel. S_2 , exact orientation difficult
L	5413.0	569.5	319	1C16	As 483.0-489.0, 490.0-540.0
L	569.5	570.5	410	1C16	Gauge zone in 1C16; zone 30° to c.a. w/ 210° @ 569.5, end of interval broken, no reliable attitude
L	570.5	572.0	411	1C16	As 483.0-489.0; 490.0-540.0; 543.0-569.5
L	572.0	574.0	412		Gauge zone in 1C16; gauge @ 60° to c.a., $\approx 210^\circ$ dip azimuth @ top & bottom of interval
L	574.0	598.0	413	1C16	As previous intervals
L	598.0	599.0	414	1C16	Gauge zone in 1C16; best guess is gauge zone 50° to c.a. @ 210 - suspect

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2 8

Cyprus Anvil Mining Corp.

Page _____ of _____

Structural Log

Date: Aug 17/84 Logged By: GL

Core Code	From		To		Feature	S ₀ Dip Direct.	S ₁ /S ₂ Dip Direct.		S ₂ /S ₄ Dip Direct.		Description
	10	14 16	20 22 24	26 28			32 34	38 40	44		
											RELOG.
S			722		PS, 2				52	23.5	RFE = S ₂ , S ₂ = S ₂
S			837		PS, 2				50		
S			993		PS, 2				61		
											RFE = S ₄ , S ₂ = S ₄ , S ₀ = S ₂
S			1153		CS, 4 Z		58	00	3.4	23.5	
											RFE = S ₂ , S ₂ = S ₂
S			1305		PS, 2				61	23.5	
S			1392		PS, 2				55		
S			1522		PS, 2				48		
S			1636		PS, 2				60		
S			1778		PS, 2				42		
S			1966		PS, 2				69		
											RFE = S ₄ , S ₂ = S ₄ , S ₀ = S ₂
S			2158		CS, 4 Z		65	040	51	23.5	
											RFE = S ₂ , S ₂ = S ₂
S			2294		PS, 2				64	23.5	
S			2976		PS, 2				80		
											RFE = S ₄ , S ₂ = S ₄ , S ₀ = S ₂
S			4641		CS, 4 Z				43	23.5	
S			4728		CS, 4 E				55		
S			4870		CS, 4 3				67		
S			4957		CS, 4 3				78		
S			5038		CS, 4				64		
S			5102		CS, 4 Z				43		
S			5231		CS, 4 3				71		
S			5319		CS, 4 3				77		
S			5420		PS, 2				83	23.5	RFE = S ₂ + S ₂ = S ₂
S			5510		CS, 4 3				85	23.5	RFE = S ₄ , S ₂ = S ₄ , S ₀ = S ₂
S			5746		CS, 4 E				54		
S			5844		CS, 4				70		
S			6015		CS, 4 E				61		
S			6153		CS, 4				55		
S			6206		CS, 4				84		
S			6270		CS, 4 E				80		

Structural Log

 Logged By: [Signature]

	To				Feature	SYN	S ₁		S ₂		Description
	14	16	20	22			24	26	28	32	
							Dip	Direct.	Dip	Direct.	
5		130			RS2						
		130			F2	Σ					Σ symmetry, asymmetric, similar, isoclinal
0		2160			RS2						F ₂ fold in gtz vein in 1D4
		2160			CS4Z				70	2110	S ₄ = 60/210
0		2228			W1						Attitude: Σ 165 Δ 80°SW
8		2250			RS2						
		2250			CS4Z				75	2110	F ₄ , similar, asymmetric, close to tight
5		23170			RS2						S ₄ = 70/210
		23170			CS4Z						" " " close S ₄ = 50/210
		2465			RS2						Dike 246.5 - 247.0
0		30110			RS2						Dike 301.0 - 301.5
5		3020			W1						Attitude - not possible, bubbly core
0		3050			CS4						Poorly banded 2D4
		3050			F43						Close, similar, F ₄ hinge w/ M(3)
		3085			CS4						symmetry S ₄ = 85/210
5		090			W1						Attitude: 90° to c.a. @ top & bottom
0		30930			CS4						
3		4585									Thrust Dike
		4640			RS2						S ₄ = 50/210
		4640			CS4	Σ					Z symmetry, asymmetric, similar, tight F ₄
2		48105			RS2						S ₄ = 65/210
		48105			CS4	Σ					" " " " " "
		4845			RS2						S ₄ = 40/210
		4845			CS4	Σ					" " " " " "
		4885			CS43						S ₄ = 80/210
		4885			CS4	Σ					S ₂ subsect. three intervals S ₄ 75°-90° to c.a.
		4885			CS4	Σ					S ₄ = 40/210
		4890			RS2						
		4900			W1						

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2 8

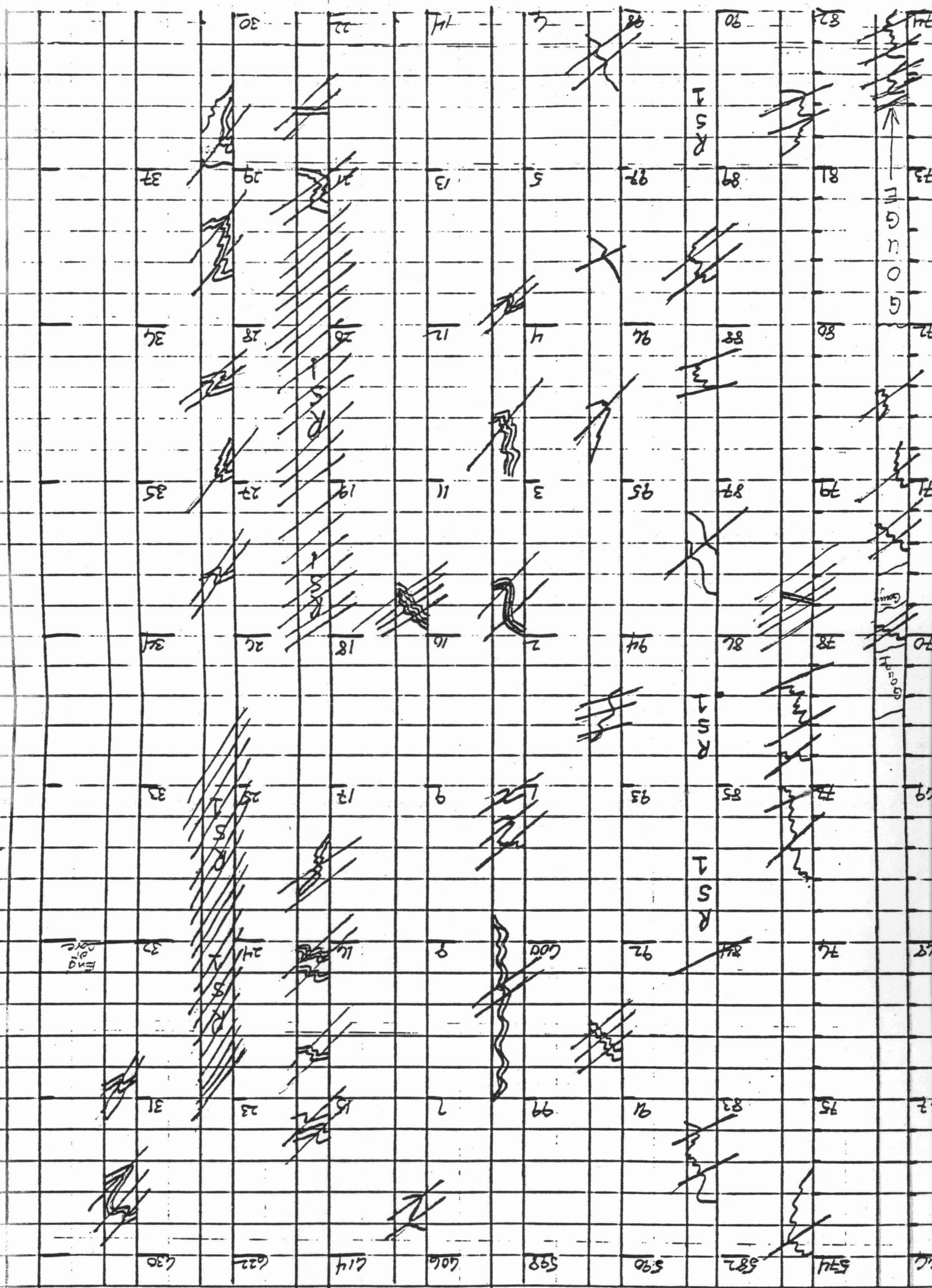
Cyprus Anvil Mining Corp.

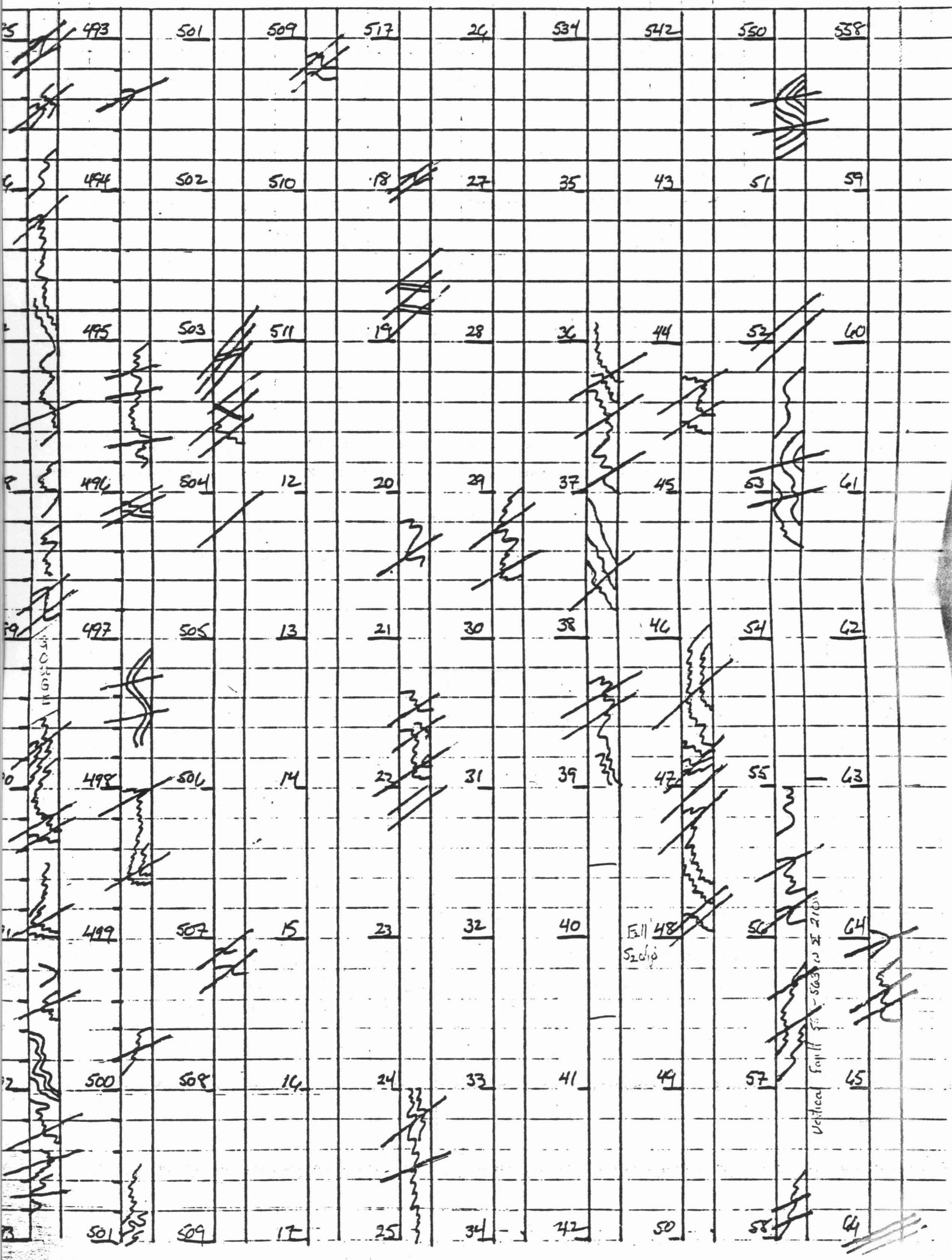
Page _____ of _____

DISCONTINUITY
~~Structural~~ Log
UPPER INTERNAL LOWER

Date: Aug 17/84 Logged By: GL

Code	From	To	Feature	S		S		S		Description
				Dip	Direct.	Dip	Direct.	Dip	Direct.	
I	10	14 16	20 22 24 26 28	32 34	38 40	44				RELOG
F	110	680	3GX							INTENSELY FRACTURED BROKEN AND GOUGED, LIKELY FAULT.
F	680	11137	2BJ							MINOR GOUGE PATCHES ALSO.
F	1214	1223	Q						6200D	BARREN VN
F	1266	1291	2BJ							
F	1428	1437	Q							BARREN VN
F	1490	1782	1JB							MINOR GOUGE PATCHES.
F	1782	1882	2BJ							
F	1915	2190	1BJ							
F	2190	2470	2BJ							MINOR DISPERSED GOUGE
F	2470	3753	1GJ							7 DISCONTINUOUS BUT ABUNDANT FRACTURES AND GOUGE THROUGHOUT INTRUSIVE UNIT, NOT A MAJOR FAULT THOUGH(?)
F	3753	4406	2GJ							
F	4889	4897	3GX							
F	5402	5412	3GX							
F	5447	5450	3GX							
F	5596	5646	S							ONE LONG THIN CONTINUOUS SHEAR DOWN CENTER OF CORE AXIS. (NOT A MAJOR FAULT THOUGH)
F	5680	6194	2JG							DISPERSED GOUGE PATCHES AND BROKEN CORE.
F	6052	6108	1BJ							
F	6110	6134	2XG							
F	6156	6178	2BJ							
F	6228	6233	3GB							
										EOM





Full 48
S200

Vertical Fault 50-503 to 210

DDH 76X-14

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	PJT	✓
DOWN HOLE SURVEYS " R "	PJT	OK
DOWN HOLE LITHOLOGY " L "	✓	PJT
DOWN HOLE STRUCTURE " S "
DOWN HOLE FAULTS " F "	✓	PJT
SAMPLERS DATA " F "
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	May 27/85	PJT	No Ore
ENTER ASSAYS "CAMC"
ENTER ASSAYS "CHENEX"
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE
SPLINE CALCULATIONS
STRUCTURAL SOLUTIONS
CALCULATE OFFSETS FROM COLLAR
PRINT OUT GENERAL DDH DATA REPORTS

nb In DDHDB as 76X-14 already

CYPRUS ANVIL MINING CORPORATION

DIAMOND DRILL CORE LOG

Hole Number: 76 X-14

Fabric Orientation Diagram:

Project: Anvil

Location: Pit, Section 118

Claim: _____

Terr. Plane Co-ords.: _____ N

_____ E

Grid Co-ords.: 9,870.26 N

(Mine) 15,107.46 E

Elevation: 4,076.04 ^{check.} ~~3111.6~~ (MSL)

Total Depth: 829'

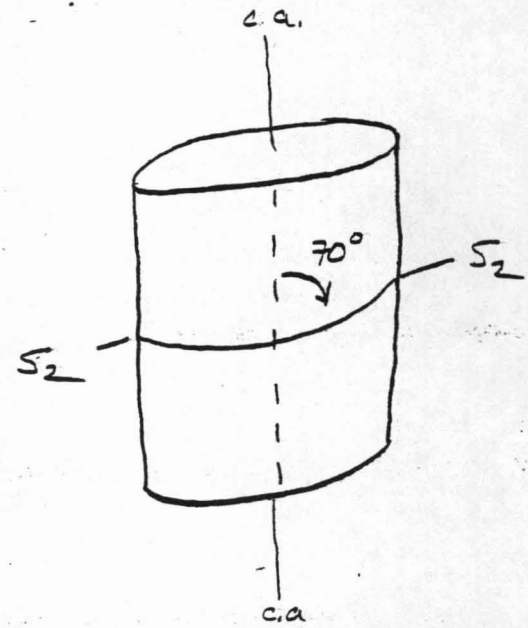
Purpose: Test NE extension of outbody on 118

Logged by: [Signature] Date(s) Logged: _____

Drilling Contractor: ADD Core: Size From To Collar Cased and Capped: _____

BD 0 ECH

Started: _____ Completed: _____



All symmetry determinations looking NW with S2 dipping SW with dip azimuth 210°.

Code	From		To		Unit		Code	Description
	10	14	16	20	22	23		
		00		80	1		#	Overburden
L		80		101.5	2	1C10	#8	thinly bedded, moderately to weakly and. bearing #8 (chloritic) thin clay to transition zone; non-carbonaceous
L		101.5		122.0	3	1D14	[1C10/48] CHLORITIC	thin clay to white mica envelope lith. w/ minor (~5%) bro-and. clots & characteristic more stringers/bands
L		122.0		128.0	4	1C10		→ 1D4; musc.-rich non-carb. bro-musc.-and. schist transitional to 1D4
L		128.0		145.5	5	1D14	[1C10/47] LESS CHLORITIC	as 109.5-122.0 w/ minor (<2%) bro-and. "clots" & typical more stringers/bands/blocks
L		145.5		150.2	6	1C10	1D4 [1C10/47]	→ 1D4 as 122.0-128.0
L		150.2		152.0	7	1C10	1D4	→ 1D4 bedded & gougled; interval = fault zone; top of fault zone 115 ₂ = 50°, 210°, base 115 ₂ = 45°, 210°
L		152.0		184.5	8	1D4		as 101.5-112.0, 128.0-145.5
L		184.5		199.2	9	1C6	488 WHITE MICA DOMINATES, GREENISH (chloritic)	bro-and. clotted musc. >> bro, non-carb., weakly andalusite bearing schist, clots = bro + pink and?
L		199.2		200.0	10	1C6	488	gouge & breccia; 20°, 210° @ top & bottom of gouge zone
L		200.0		253.9	11	1C10	#148	→ 1C10; interbedded clotted = banded trans. zone
L		253.9		254.6	12	1C10		reddish brown "quartz veins" diorite w/ plagioclase only 60°, 210° top; 50°, 210° bottom, 10E IS FOLDED!
L		254.6		265.5	13	1C10		good "clotted" schist; no coherent banding
L		265.5		299.8	14	1C10	#8	1C10; as 200.0-253.9; interbedded clotted w/af banded transition zone lith
L		299.8		300.1	15	1C10		→ 1C10 gouge, 45°, 210° top and bottom of gouge zone
L		300.1		300.7	16	1C10		→ 1C10
L		300.7		301.6	17	1C10		→ 1C10 gouge zone; 75°, 210° @ top of zone; base undetermined
L		301.6		302.5	18	1C10		→ 1C10
L		302.5		302.6	19	1C10		→ 1C10 gouge zone; 35°, 210° (approx)
L		302.6		310.2	20	1C10		→ 1C6; ⇒ 1C (ortho-feld. schist)
L		310.2		320.0	21	1C10		gouge & breccia; 50°, 210° @ top & base of gouge zone; un- usual occurrence of dior. gouge w/ sub-rounded diorite frags. bounded by schists
L		320.0		322.3	22	1C10		typical thinly bedded ortho-feld. schist
L		322.3		323.3	23	1D14		w/ 1-3% py + cp. Hbls & stringers
L		323.3		325.4	24	1C10		→ 1C5
L		325.4		326.5	25	1C10	6 (1C10/48) QUARTZ CHLORITE	→ 1C6 unrecognizable; 320.0 → 325.4 looks like 1C

Lithologic Log

Logged By: *[Signature]*

Code	From	To	Unit	Code	Description
	10 14 16 20 22 23 25 27				
	31650	31660	216	PCD 49 +C16	w/ 2-1" bands sub-mass (70%) py 11 S, 11 S ₂
	31660	31885	217	ICD 49 +C16	→ 1C5 interbanded "clotted" & banded ABUNDANT GARNET ABUNDANT DISCORDANT PLANAR PYRITE
L	31885	31895	218	ICD 4 OE8	4 WHITE MICA GOUGE (SCHIST FRAGMENTS) gouge & breccia; on 319.0-320.0; gouge must synchronously w/ cooling i.e. detrition → intrusion → faulting
L	31895	31990	219	ICD 4 L16	4 19 MILD STOCKWORK OF PLANAR PYRITE VEINLETS (DISCORDANT)
L	31990	40127	30	1C15	→ 1C0; banded or normal 1C
L	4027	41190	31	1C16	→ 1C5 interbanded
L	41190	4425	312	OE8	9 w/ fine killee kb. kw. diorite sill?; upper contact 70° dip direction relative to S ₂ uncertain; best guess " 11 S ₂ = 70°-210°
L	4425	4450	313	OE8	9 gouge & breccia; 30° to ca. top & bottom
L	4450	4700	314	OE8	9 lower contact wobbly, good attitude → S ₂ impossible, gouge @ base of diorite grossly 11 S ₂ ; best bet is diorite = sill w/ top & bottom 70°, 210° silica-chlorite AIT. (propyl.)
L	4700	49105	315	1C16	4
L	49105	4917	316	1C16	4 on 470.0-490.5 w/ 5% banded stringers & amorphous mass > po > cp
L	4917	4970	317	1C16	24
L	4970	5000	318	1C14	minor bio-and. clots + amorphous pyrite/marcasite
L	5000	50115	319	1C14	gouge & breccia; top 30°, 210°; base 50° ≈ 210°
L	50115	50143	40	1C16	clotted OFBMS
L	5043	51280	41	1C15	banded " with MINOR DISCORDANT PYRITE VEINLETS which HAVE SMALL SEMI-LITIC HALOS.
L	51280	51305	412	1C16	clotted "
L	51305	51397	413	1C15	banded "
L	51397	51564	414	1C16	clotted "
L	51564	51595	415	1C15	banded "
L	51595	51610	416	1C15	" " ; breccia & gouge; top 70°, 210° base indet.
L	51610	51613	417	1C15	9 " " PYRITE-MARCASITE VEINLETS
L	51613	51647	418	1C15	" " ; " " " " ; top 10° uncertain dip base of gouge indeterminate attitude
L	51647	51730	419	1C15	9 → 1C0; N.B. all banded OFBMS (1C5) = normal OFBMS
L	51730	51737	510	1C15	breccia & gouge; 60°, 210° top & base of gouge
L	51737	51784	511	1C15	9 banded PY-MARC VEINLETS & BANDS.
L	51784	51792	512	1C16	clotted; sample showing "bondage" of D
L	51792	51858	513	1C15	to produce "clots"
L	51858	51875	514	1C16	clotted
L	51875	6015	515	1C15	conical; Note: "clotted" texture in schist

Code	From	To	Unit	Code	Description
	10	14 16	20	22 23 25 27	most probably due to thickness of D, compositional banding (and competency / ductility contrast between $S_0 \parallel S_1 \equiv RSI$ banding) controlling λ of D_2 folds. Where D_1 laminations thin, get small λ tight to isoclinal F folds w/ no "failure" (brittle failure or boudinage) in $S_1 \parallel S_0$. Where D_1 laminations / bands thick (0.3 - 1.0"), get buckle folding + boudinage of D_1 banding giving rise to "clots". Therefore, clotted texture is a function of org. (S_0) banding thickness & ductility contrast during D_2 and in no way represents K/Si or "zone" or facies
L	16011 5	16013 5	5B	1C16	clotted
L	16013 5	16114 5	5B	1C15	VISIBLE ANDALUSITE, ABUNDANT 2"-4" QTZ VEINS.
L	16114 5	16812 7	5B	1C16	EXCELLENT ANDALUSITE, MINOR GARNET.
L	16812 7	16817 0	5B	1C14	bleached w/ minor mass & bio clots
L	16817 0	16818 0	6D	1C10	pegmatite, hypersthene, musc, white; top contact undulating; base 80°, 210°
L	16818 0	17012 3	6A	1C16	clotted
L	17012 3	17040 6	6B	1C14	9 ABUNDANT PYRITE MARCASITE VEINLETS.
L	17040 6	17073 5	6B	0E9	SILICIFIED GRAPHIC ALASKITE → OF9 in thin zone on gorge / K/Si zone; intrusive, contact exposed; top 40° = 210°, base 50°, 210° foliation "Sill" w/ S_2
L	17073 5	17137 6	6B	1C49	siliceous, amoeboid mass, siliceous, white
L	17137 6	17246 6	6B	1C5	banded, 1C51 siliceous w/ 2% py stringers & amoeboid clots
L	17246 6	17817 6	6B	1C5 & 1C1F	interbanded 1C5 and 1F8 (Gothic, chlor clumped) in 1"-3' bands; white, musc peg. sills @ 760-761 and 780.3-781.7
L	17817 6	17886 6	6B	1C5	minor 1C5
L	17886 6	18028 8	6B	1C5	724.6-781.7
L	18028 8	18110 0	6A	0H9	GRAPHIC TEXTURE 1 folds - gas-schistite peg. showing irreg. post D_1 contacts; top 30° = 210° base 50°, 210° → discordant post- D_2 like
L	18110 0	18240 2	6A	1C5	→ 1C51 (1F8) + ... 822 → 823.4

Structural Log

Core	From				To				Feature	E Dip	S ₀		S ₁		S ₂		Description
	10	14	16	20	22	24	26	28			Dip	Direct.	Dip	Direct.	Dip	Direct.	
S				113	0	C1S13	Z			610	01010	515	21315	RFE = S3			
S				116	5	C1S13	Z					510					
S				121	5	C1S13						410					
S				131	8	C1S13	Z			615	11810	415					
S				144	3	C1S13	Z			710	01010	410					
S				152	8	C1S13	Z					410					
S				158	4	C1S13	M					410					
S				160	0	C1S13	Z					610					
S				167	0	C1S13	S			310	01010	710					
S				175	9	C1S13	Z			810	01010	610					
S				181	5	C1S13	Z			910	01010	710					
S				183	5	C1S13	Z					410					
S				189	5	C1S13	S					610					
S				196	5	C1S13	Z					510					
S				11212	3	C1S13	Z			610	01010	510					
S	11314	3		1183	0	C1S13	Z					510					
S				11816	5	C1S13	Z					715					
S				11915	0	C1S13	Z					610					
S				12014	8	C1S13	Z					510					
S				12113	4	C1S13	Z			715	01010	615					
S				12218	0	C1S13	Z					610					
S				12318	3	C1S13	Z			715	11810	615					
S				12414	5	C1S13	Z					610					
S				12511	0	C1S13	Z					710					
S				12518	4	C1S13	S					610					
S				12519	4	C1S13	Z					710					
S				12519	7	C1S13	Z					510					
S				12610	5	C1S13	Z					610					
S				12611	3	C1S13	S			515	01010	710					
S				12612	8	C1S13	S					710					
S				12614	3	C1S13	S			610	01010	710					
S				12615	0	C1S13	Z	810	01010	810	01010	610					
S				12616	3	C1S13	Z					710					
S				12617	5	C1S13	Z					710					
S				12713	5	C1S13	Z					710					
S				12811	0	C1S13	Z					710					

Structural Log

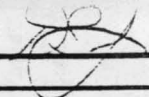
Code	From		To		Feature	E S ₁	S ₀		S ₁		S ₂		Description													
	10	14	16	20			Dip	Direct.	Dip	Direct.	Dip	Direct.		Dip	Direct.											
1	28	32	34	38	40	44																				
S	1	1	1	12	9	11	0	C1S13	Z	8	10	1	18	10	8	10	1	18	10	7	10	2	13	15		
S	1	1	1	13	10	16	5	C1S13	Z																	
S	1	1	1	13	10	18	8	C1S13	Z																	
S	1	1	1	13	11	18	0	C1S13	Z																	
S	1	1	1	13	12	11	0	C1S13	Z																	
S	1	1	1	13	13	10	5	C1S13	Z	8	10	0	10	10	8	10	0	10	10	7	15					
S	1	1	1	13	14	14	5	C1S13	Z																	
S	1	1	1	13	15	13	7	C1S13	Z																	
S	1	1	1	13	16	14	5	C1S13	Z																	
S	1	1	1	13	17	11	0	C1S13	Z																	
S	1	1	1	13	18	7	4	C1S13	Z																	
S	1	1	1	13	19	12	5	C1S13	Z																	
S	1	1	1	13	19	15	0	C1S13	Z																	
S	1	1	1	14	10	15	0	C1S13	Z	8	10	1	18	10	8	10	1	18	10	7	10					
S	1	1	1	14	11	15	8	C1S13	Z																	
S	1	1	1	14	14	15	0	01E18																		
S	1	1	1	14	17	15	0	C1S13	Z																	
S	1	1	1	14	18	10	5	C1S13	Z																	
S	1	1	1	15	10	11	5	C1S13	Z																	
S	1	1	1	15	10	15	7	C1S13	Z	9	10	0	10	10	9	10	0	10	10	7	10					
S	1	1	1	15	11	15	0	C1S13	Z																	
S	1	1	1	15	11	19	0	C1S13	Z																	
S	1	1	1	15	12	11	0	C1S13	Z																	
S	1	1	1	15	13	13	3	C1S13	Z																	
S	1	1	1	15	13	15	3	C1S13	Z	6	10	1	18	10	6	10	1	18	10	6	10					
S	1	1	1	15	14	15	5	C1S13	Z																	
S	1	1	1	15	16	11	5	C1S13	Z																	
S	1	1	1	15	16	19	5	C1S13	Z																	
S	1	1	1	15	17	13	5	C1S13	Z																	
S	1	1	1	15	17	16	2	C1S13	Z																	
S	1	1	1	15	17	19	5	C1S13	Z	6	10	1	18	10	6	10	1	18	10	8	10					
S	1	1	1	15	18	11	2	C1S13	Z																	
S	1	1	1	15	18	14	5	C1S13	Z																	
S	1	1	1	15	18	19	3	C1S13	Z																	
S	1	1	1	15	19	14	5	C1S13	Z																	
S	1	1	1	15	19	17	5	C1S13	Z																	

Structural Log

Logged By: *[Signature]*

Code	From	To	Feature	Sym	S ₁		S ₂		Description
					Dip	Direct.	Dip	Direct.	
	10	14 16	20 22	24 26	28	32	34	38	
S		130	F4	Z		60	2110		S ₄ = 55/210
S		165	F4	Z					= 50/210
S		215	S4						= 40/210
S		318	F4	Z		65	01310		= 45/210
S		385	F4	Z		70	2110		= 110/210
S		443	F4	Z		70	2110		= 110/210
S		528	F4	Z					= 40/210
		584		M					Fractures from S ₄ dip, plunge 210°, 50° S ₄ (410° to c.a.)
S		610	F4	Z					S ₄ = 60/210
S		670	F4	S		310	3110		S ₄ = 70/210
S		759	F4	Z		80	2110		= 60/210
S		815	F4	Z		910	0010	S ₂ being	= 70/210
S		835	F4	Z					= 40/210
S		895	F4	S					= 60/210
S		965	F4	Z					= 50/210
S		1122	F4	Z		60	2110		= 50/210
S		1134	F4	Z					= 50/210
S		1140	F4	Z					largely RSD from 134.3 - 157.8
S		1157	F4	Z					RSD 157.8 - 183.0
S		1183	F4	Z					= 50/210
S		1186	F4	Z					= 75/210
S		1191	F4	Z					= 60/210
S		1204	F4	Z					= 50/210
S		1213	F4	Z		715	2110		= 65/210
S		1228	F4	Z					= 60/210
S		1238	F4	Z		715	01310		= 65/210
S		1244	F4	Z					Top of Z short limb = 60/210
S		1251	F4	Z					Base of Z short limb; S ₁ region 2445-25 = 70/210
S		1258	F4	S		610	2110		S ₄ = 65/210
S		1259	F4	Z					= 70/210
S		1259	F4	Z					= 50/210
S		1260	F4	Z					Top of Z short limb = 60/210
S		1261	F4	S		515	2110		S ₁ region " " " = 70/210
S		1261	F4	S					" " " " " = 70/210
S		1264	F4	S		60	2110		" " " " " = 70/210

Structural Log

Logged By: 

Code	From			To			Feature	SYM	S ₁		S ₂		Description
	10	14	16	20	22	24			26	28	32	34	
S				21	21	50	F4 Z		810	210	80	210	Base Z short limb S ₁ = 60/210
S				21	26	163	F4 Z						= 70/210
S				21	26	175	F4 Z						F ₄ trend 120, 25°NW = 70/210
S				21	27	135	F4 Z						= 70/210
S				21	28	110	F4 Z						= 70/210
S				21	29	110	F4 Z	810	030	80	030		= 70/210
S				21	30	165	F4 Z						Top of Z short limb = 80/210
S				21	30	89	F4 Z						Base of Z " " ; S region 300.5-305 = 70/210
S				21	31	180	F4 Z						top of Z short limb ; RSZ 309-319 = 80/210
S				21	32	110	F4 Z						Base of Z " " ; S region 318-321 = 60/210
S				21	33	105	F4 Z	810	210	810	210		= 75/210
S				21	34	145	F4 Z						= 65/210
S				21	35	137	F4 Z						= 40/210
S				21	36	145	F4 Z						= 65/210
S				21	37	110	F4 Z						= 65/210
S				21	38	74	F4 Z						= 50/210
S				21	39	125	F4 Z						Start Z short limb = 70/210
S				21	39	50	F4 Z						End " " " ; S region 39.3-395 = 70/210
S				21	40	50	F4 Z	80	030	80	030		= 70/210
S				21	41	58	F4 Z						= 65/210
S	94	50		41	70	0	QES						Direct sill
S				41	71	50	F4 Z						Start short Z limb, ends 477.0 = 60/210
S				41	81	5	F4 Z						= 65/210
S				41	50	15	F4 Z						= 60/210
S				41	59	57	F4 Z	90		90	000		S. horiz. = 70/210
S				41	51	150	F4 Z						Start Z short limb = 70/210
S				41	52	190	F4 Z						End Z short " ; S region 515-519 = 60/210
S				41	52	110	F4 Z						Start Z short limb = 60/210
S				41	53	133	F4 Z						End " " " ; S region 522.5/533 = 50/210
S				41	53	153	F4 Z	60	030	60	030		= 60/210
S				41	54	155	F4 Z						= 70/210
S				41	56	115	F4 Z						Start Z short limb = 60/210
S				41	56	95	F4 Z						End " " " ; S region 562-569 = 60/210
S				41	57	135	F4 Z						Start " " " = 60/210
S				41	57	162	F4 Z						End " " " ; S region 574-576 = 80/210
S				41	57	115	F4 Z	60	030	60	030		Start " " " = 80/210

Structural Log

Logged By: 

Code	From			To			Feature	# of S ₁	S ₁		S ₂		Description
	10	14	16	20	22	24			26	28	Dip	Direct.	
S				1581	2		F4	Z					End Z short limb S ₄ = 70/210
S				1581	45		F4	Z					Start " " " = 70/210
S				1581	93		F4	Z					End " " " ; S ₂ region 584-589 = 70/210
S				1591	45		F4	Z			50	030	middle of Z region = 70/210
S				1591	75		F4	Z					Start Z short limb = 70/210
S				1601	10		F4	Z					= 70/210
S				1611	30		F4	Z					= 60/210
S				1631	80		F4	Z					= 70/210
S				1651	10		F4	Z					= 70/210
S				1661	10		F4	Z					= 70/210
S				1671	20		F4	Z					= 65/210
S				1691	35		F4	Z					= 65/210
S				1721	15		F4	Z					= 60/210
S				1721	60		F4	S					See graphic log = 60/210
S				1741	60		F4	S					= 60/210
S				1751	65		F4	S					= 60/210
S				1761	65		F4	Z					= 70/210
S				1781	40		F4	Z					= 80/210
S				1791	40		F4	Z					= 65/210
S				1801	08		F4	Z					= 80/210
S				1811	60		F4	Z					= 65/210
S				1821	40		F4	Z					= 60/210

Structural Log

Logged By:

Code	From		To		Feature	Sym	S ₁		S ₂ 54		Description	
	10	14	16	20			22	24	26	28		32
				216150		Z	810	0110	60	2110	End Z short limb	
				21665		Z			70	2110	}	
				21675		Z			70	2110		E trend 120, 25°NW
				21715		Z			70	2110		
				21810		Z			70	2110		
				21910		Z	810	0130	75	2110		
				31015		Z			80	2110	Top of Z short limb	
				31085		Z			70	2110	End of Z " " ; S. region 306.5-30	
				31180		Z			80	2110	top of Z short limb ; RSI 309-319	
				31210		Z			60	2110	base of Z " " ; S. region 318-321	
				31305		Z	510	2110	75	2110		
				31445		Z			65	2110		
				31537		Z			40	2110		
				316145		Z			65	2110	✓✓	
				31710		Z			65	2110		
				31874		Z			50	2110		
				31925		Z			70	2110	Start Z short limb	
				31950		Z			70	2110	End " " " ; S. region 393-395	
				41050		Z	80	0130	70	2110		
				4158		Z			65	2110		
	9450			4700	QES						Droute 'sill	
				4751		Z			60	2110	Start short Z limb, ends 477.0	
				4865		Z			65	2110		
				51015		Z			60	2110		
				5157		Z	90		70	2110	S. hori.	
				51150		Z			70	2110	Start Z short limb	
				51190		Z			60	2110	End Z short " ; 515-519 ES	
				5210		Z			60	2110	Start Z short limb	
				5313		Z			50	2110	End " " " ; S. region 522.5-533	
				53153		Z	60	0130	60	2110		
				54155		Z			70	2110		
				54915		Z			60	2110	Start Z short limb	
				5495		Z			60	2110	End " " " ; S. region 562-569	
				57135		Z			60	2110	Start " " "	
				5762		Z			60	2110	End " " " ; S. region 574-576	
				5775		Z	60	0130	60	2110	Start " " "	

Structural Log

Logged By:

Code	From		To		Feature	SYM	S ₁		S ₂		Description
	10	14	16	20			22	24	26	28	
				581	2				70	210	End Z short limb
				581	4.5				70	210	Start " " "
				581	3				70	210	End " " " ; S. region 584-589
				591	4.5		S ₁₀	920	70	210	middle of Z region
				591	7.5				70	210	Start Z short limb
				601	0				70	210	
				611	3.6				60	210	
				63	8.0				70	210	
				65	1.0				70	210	
				66	1.0				70	210	
				67	2.0				65	210	581-672.0 2 70
				69	1.35				65	210	693.5 - 721.5 2 65
				72	1.5				60	210	
				72	2.0				60	210	See grapher log ✓
				74	0.0				60	210	✓
				75	6.5				60	210	✓
				76	1.5				70	210	✓
				78	1.40				80	210	✓
				79	1.0				65	210	✓
				80	10.8				80	210	✓
				81	6.0				65	210	✓
				82	4.0				60	210	✓

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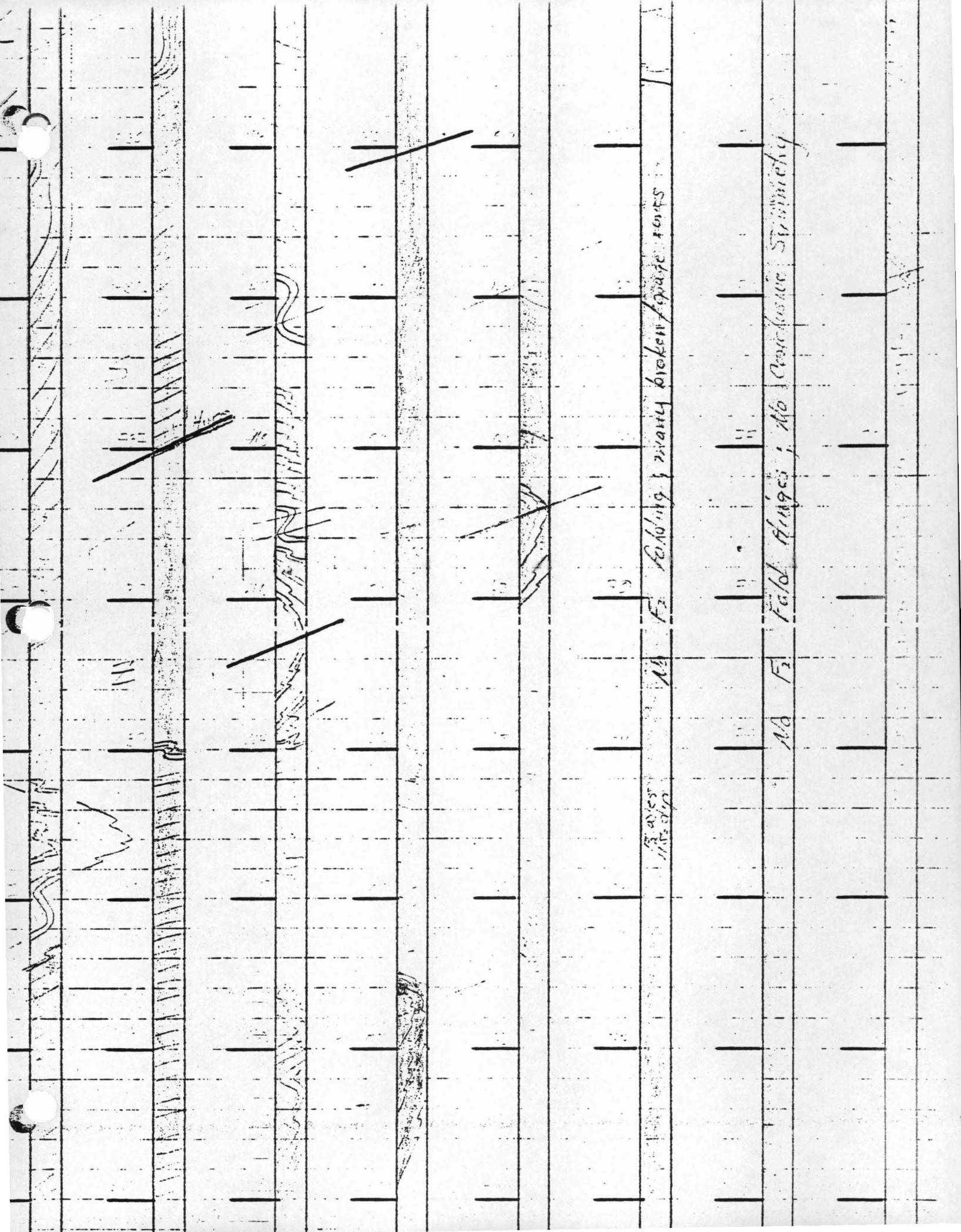
Cyprus Anvil Mining Corp.

Page _____ of _____

DISCONTINUITY
~~Structural Log~~
UPPER MIDDLE LOWER

Date: Aug 14/84 Logged By: GL

Code	From		To		Feature	SYM	S₀		S₁		S₂		Description
	10	14	16	20			Dip	Direct.	Dip	Direct.	Dip	Direct.	
1	10	14	16	20	22	24	26	28	32	34	38	40	44
F	1905		1501		1BJ								
F	1501		1527		3GB								
F	1527		2431		1JG								SMALL DISPERSED PATCHES OF GOUGE.
F	2540		2558		2JB								
F	2672		2678		3G								
F	3000		3028		2GB								
F	3061		3066		Q		603	40			58	090	QTZ-AND-PO VEIN.
F	3189		3201		3GB								
F	3420		3897		2JG								ABUNDANT SMALL PATCHES OF GOUGE + FRACTURED ROCK. HOWEVER DOES NOT APPEAR TO BE A MAJOR FAULT. MILD STOLKWORK OF PY VNS.
F	3897		3996		1B								
F	3996		4370		1B.G								
F	4370		4425		2JG								
F	4425		4454		3G								INTENSE GOUGE.
F	4552		4708		2GJ								
F	5002		5046		2GJ								MINOR X
F	5046		5495		1J								MINOR GOUGE.
F	5495		5643		2JG								
F	5643		6240		1J								
F	6240		6376		2JG								
F	6828		7250		2JG								SMALL SECTION OF BRITTLE BRECCIA FROM 703.1 TO 703.9'
F	7608		7621		2GJ								
F	7802		7828		2GJ								
F	7843		7945		2JS								
F	8026		8038		2JG								



M1

M2

M3

M4

M5

Folds

M6 F5 Faulting & mainly broken quartz veins

M7 F2 Fold Hinges; No Conchoidal Fracture

M8

M9

M10

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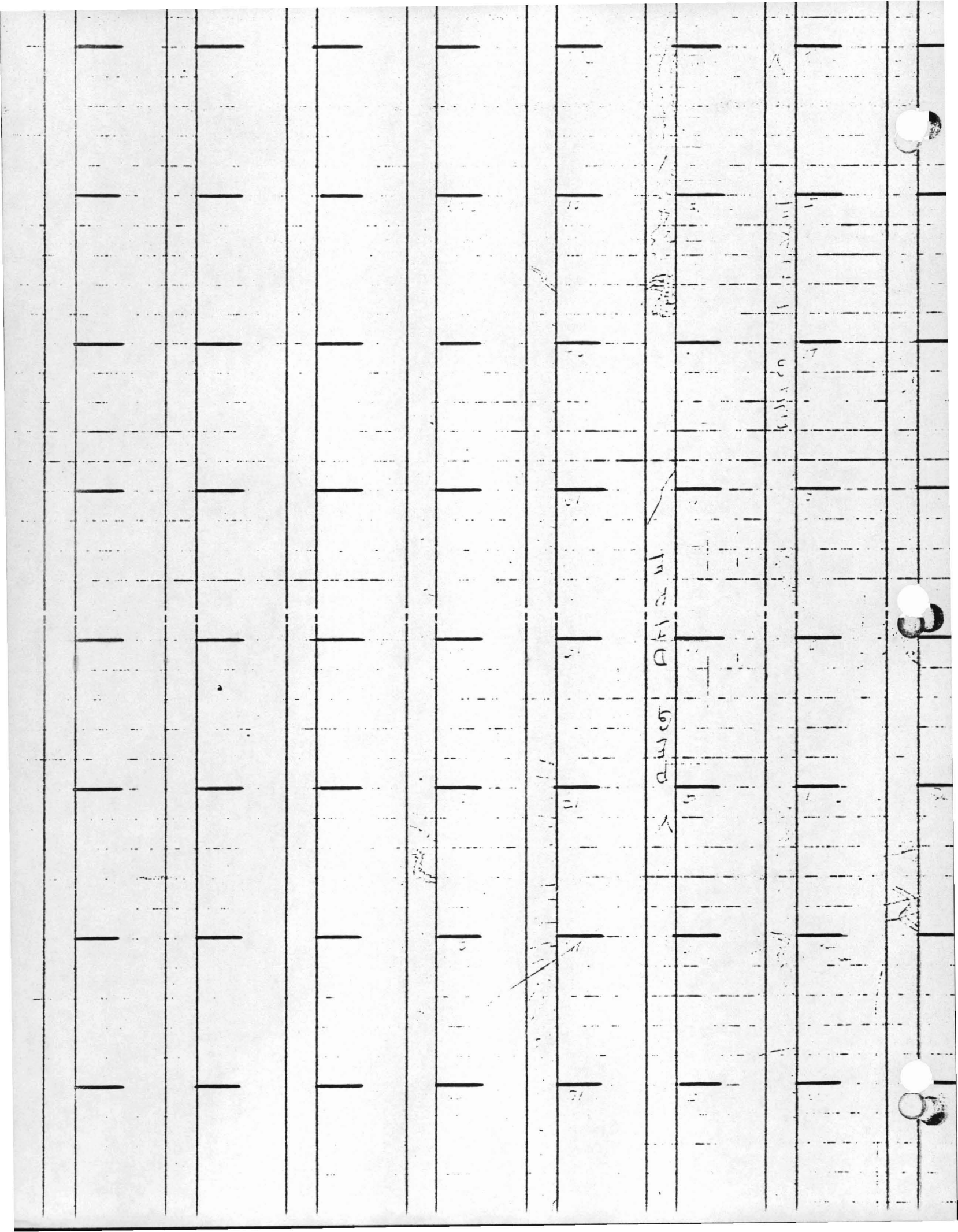
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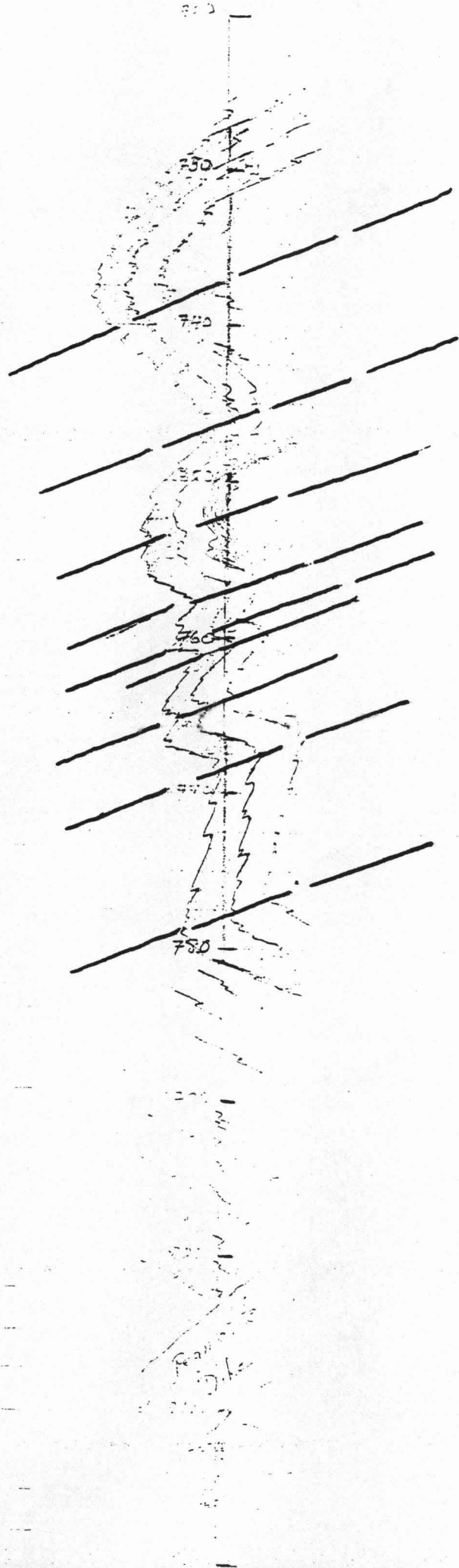
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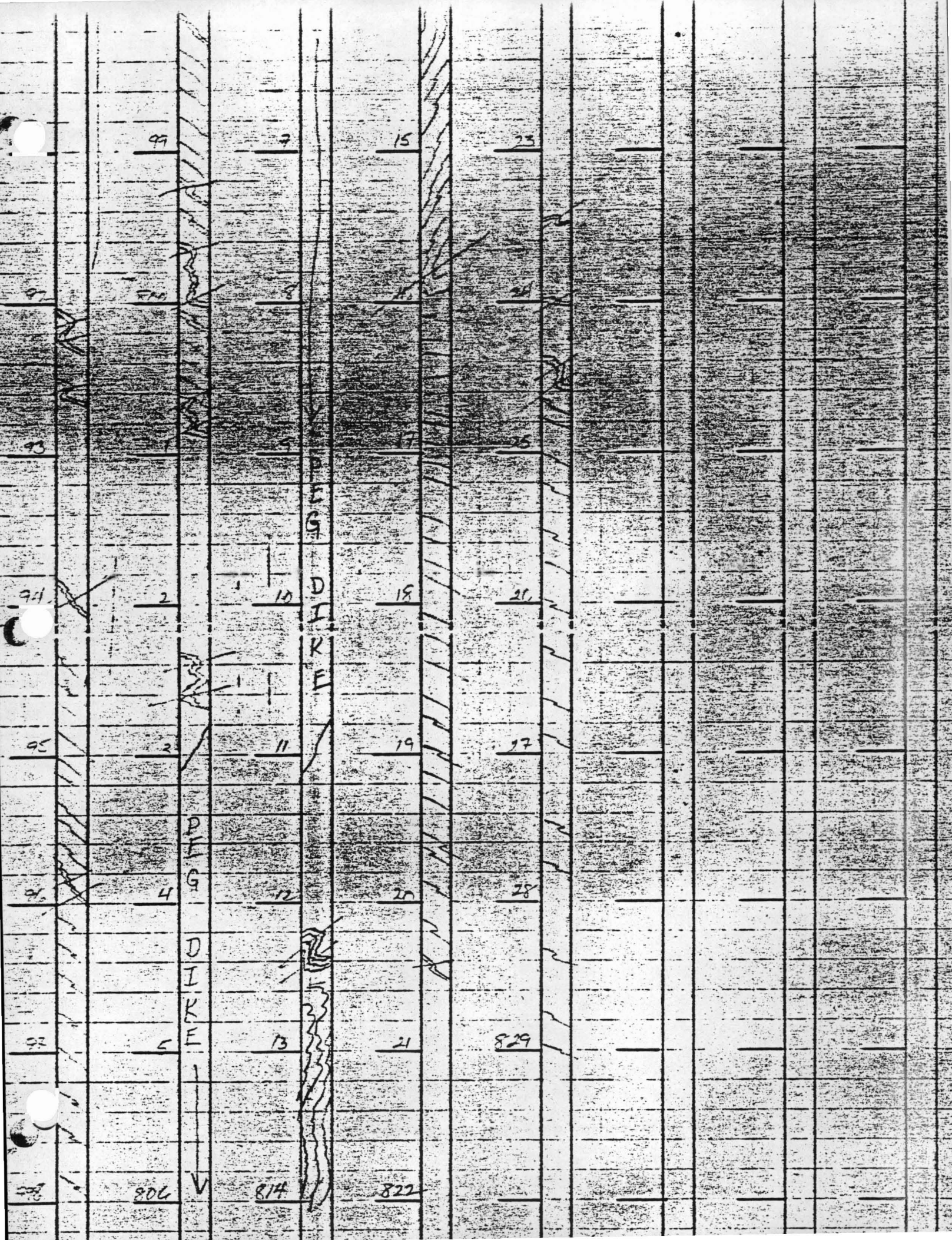
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DDH 76X-14
Graphic Log
Summary



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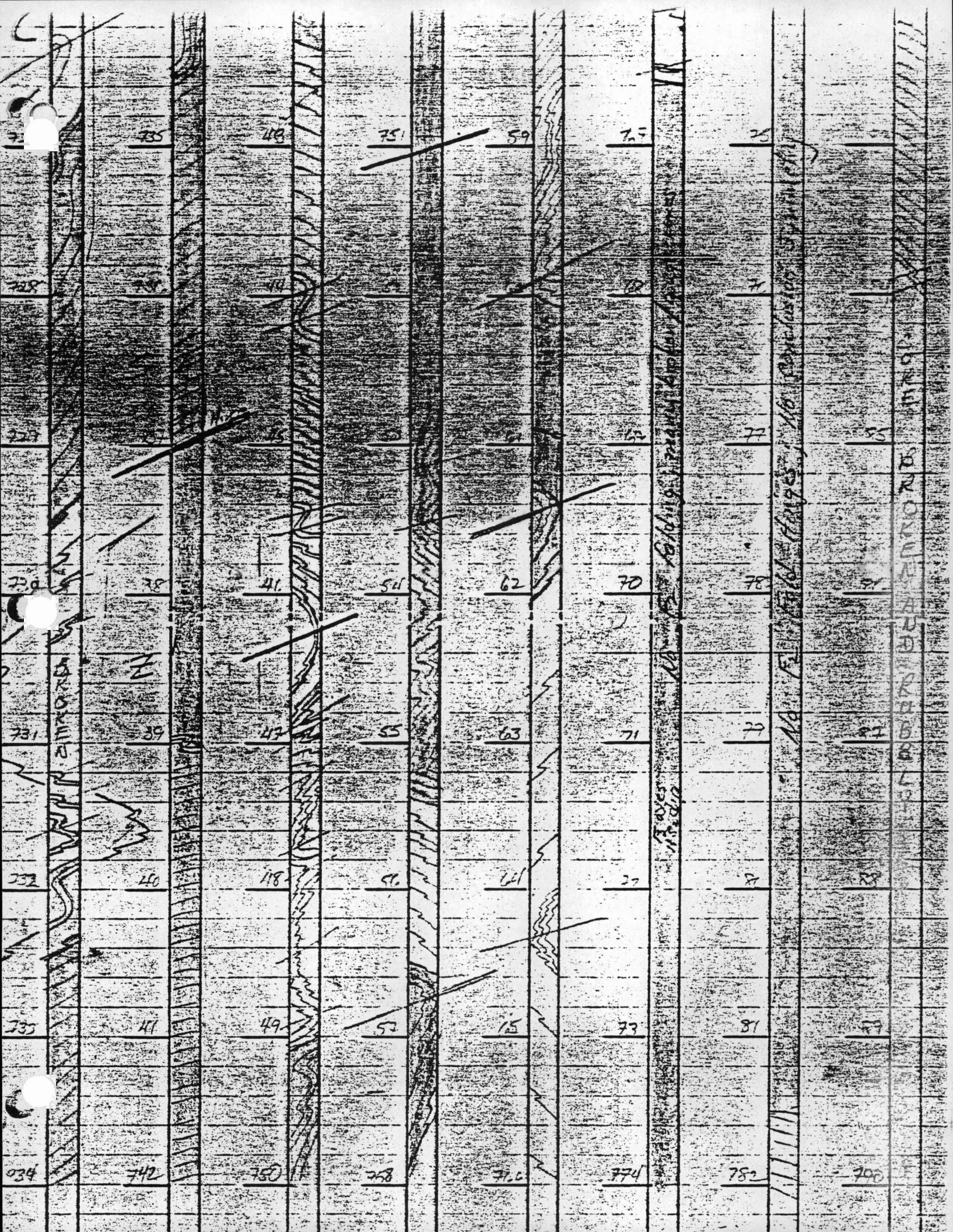
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V



735 48 51 59 75 78
738 47 51 59 70 77
739 45 51 59 70 77
730 41 51 62 70 78
731 43 55 63 71 79
732 40 51 61 77 79
733 41 49 52 75 73 81
734 742 750 758 774 782 790

BRONKHOUGH

Code	From		To		Sample No.	Description
	0	14	16	20		
	1	180	1	180	1013121511	UNIT 2
P	1	180	1	280	1013121512	UNIT 2
P	1	280	1	390	1013121513	UNIT 2
P	1	390	1	500	1013121514	UNIT 2
P	1	500	1	600	1013121515	UNIT 2
P	1	600	1	700	1013121516	UNIT 2
P	1	700	1	800	1013121517	UNIT 2
P	1	800	1	900	1013121518	UNIT 2
P	1	900	1	1015	1013121519	UNIT 2
P	1	1015	1	120	101312160	UNIT 3
P	1	1120	1	220	101312161	UNIT 3
P	1	1220	1	280	101312162	UNIT 4
P	1	1280	1	360	101312163	UNIT 5
P	1	1360	1	455	101312164	UNIT 5
P	1	1455	1	502	101312165	UNIT 6
P	1	1502	1	600	101312166	UNIT 7 AND UNIT 8
P	1	1600	1	700	101312167	UNIT 8
P	1	1700	1	770	101312168	UNIT 8
P	1	1770	1	845	101312169	UNIT 8
P	1	1845	1	920	101312170	UNIT 9
P	1	1920	1	992	101312171	UNIT 9
P	1	1992	2	100	101312172	UNIT 10. AND UNIT 11
P	2	1100	2	200	101312173	UNIT 11
P	2	1200	2	300	101312174	UNIT 11
P	2	1300	2	400	101312175	UNIT 11
P	2	1400	2	470	101312176	UNIT 11
P	2	1470	2	539	101312177	UNIT 11
P	2	1539	2	546	101312178	UNIT 12
P	2	1546	2	655	101312179	UNIT 13
P	2	1655	2	760	101312180	UNIT 14
P	2	1760	2	860	101312181	UNIT 14
P	2	1860	2	930	101312182	UNIT 14
P	2	1930	2	998	101312183	UNIT 14
P	2	1998	3	100	101312184	UNIT 15 to UNIT 20
P	3	1100	3	190	101312185	UNIT 15 to UNIT 20

Geochemical Log (Sampler's Copy)

Logged By: _____
Sampled By: ME

Code	From		To		Sample No.	Description
	10	14	18	20		
	3,2	00	3,2	23	10,3,2,8,17	UNIT 22
P	3,2	23	3,2	33	10,3,2,8,18	UNIT 23
P	3,2	33	3,3	40	10,3,2,8,19	UNIT 24 and UNIT 25
P	3,3	40	3,4	40	10,3,2,9,10	UNIT 25
P	3,4	40	3,5	40	10,3,2,9,11	UNIT 25
P	3,5	40	3,6	55	10,3,2,9,12	UNIT 25
P	3,6	55	3,6	60	10,3,2,9,13	UNIT 26
P	3,6	60	3,7	70	10,3,2,9,14	UNIT 27
P	3,7	70	3,8	85	10,3,2,9,15	UNIT 27
P	3,8	85	3,8	95	10,3,2,9,16	UNIT 28
P	3,8	95	3,9	90	10,3,2,9,17	UNIT 29
P	3,9	90	4,0	90	10,3,2,9,18	UNIT 30 and UNIT 31
P	4,0	90	4,1	90	10,3,2,9,19	UNIT 31
P	4,1	90	4,2	90	10,3,3,0,10	UNIT 32
P	4,2	90	4,3	90	10,3,4,0,1	UNIT 32
P	4,3	90	4,4	90	10,3,4,0,2	UNIT 32 and UNIT 33
P	4,4	90	4,5	90	10,3,4,0,3	UNIT 34
P	4,5	90	4,7	00	10,3,4,0,4	UNIT 34
P	4,7	00	4,8	00	10,3,4,0,5	UNIT 36
P	4,8	00	4,9	05	10,3,4,0,6	UNIT 36
P	4,9	05	4,9	17	10,3,4,0,7	UNIT 37
P	4,9	17	4,9	70	10,3,4,0,8	UNIT 38
P	4,9	70	5,0	15	10,3,4,0,9	UNIT 39 and UNIT 40
P	5,0	15	5,0	43	10,3,4,1,0	UNIT 41
P	5,0	43	5,1	40	10,3,4,1,1	UNIT 42
P	5,1	40	5,2	10	10,3,4,1,2	UNIT 42
P	5,2	10	5,2	80	10,3,4,1,3	UNIT 42
P	5,2	80	5,3	05	10,3,4,1,4	UNIT 43
P	5,3	05	5,3	97	10,3,4,1,5	UNIT 44
P	5,3	97	5,5	00	10,3,4,1,6	UNIT 45
P	5,5	00	5,5	64	10,3,4,1,7	UNIT 45
P	5,5	64	5,6	70	10,3,4,1,8	UNIT 46 to UNIT 50
P	5,6	70	5,7	84	10,3,4,1,9	UNIT 51 and UNIT 52
P	5,7	84	5,7	92	10,3,4,2,0	UNIT 53
P	5,7	92	5,8	58	10,3,4,2,1	UNIT 54
P	5,8	58	5,8	75	10,3,4,2,2	UNIT 55

DDH 76X-09

	COMPLETE	WHO DONE IT? INITIALS PLEASE!!	CHECKED BY?? INITIALS PLEASE!	REMARKS
ENTER " T " DATA	PJT	✓
DOWN HOLE SURVEYS " R "	PJT	OK
DOWN HOLE LITHOLOGY " L " ✓	PJT	PJT
DOWN HOLE STRUCTURE " S " ✓	PJT	ARR30/85
DOWN HOLE FAULTS " F " ✓ Correct 3965	PJT	PJT
SAMPLERS DATA " P "	No	OK	OK
CHECK ENTRIES FROM GENERAL DDH DATA REPORT	OR
ENTER ASSAYS "CAMC"
ENTER ASSAYS "CHEMEX"
LIST DDH ASSAY VALUES CHECK AGAINST ASSAY CERTIFICATE
SPLINE CALCULATIONS
STRUCTURAL SOLUTIONS
CALCULATE OFFSETS FROM COLLAR
PRINT OUT GENERAL DDH DATA REPORTS

Chaged DDH ID June 17/85 PJT

CYPRUS ANVIL MINING CORPORATION

DIAMOND DRILL CORE LOG

Hole Number: 76 X-09

Fabric Orientation Diagram:

Project: Anvil

Location: Open Pit

Claim: _____

Terr. Plane Co-ords.: _____ N

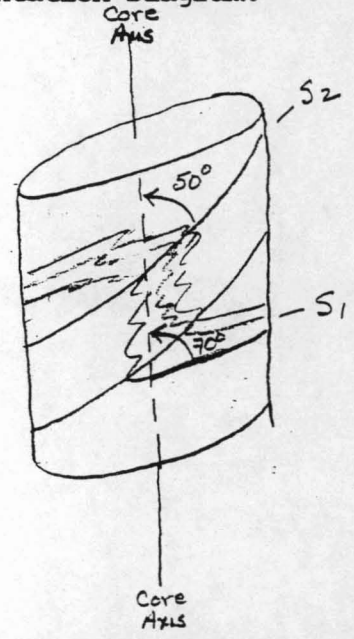
_____ E

~~4173~~ (mine) Co-ords.: N 10, 152.70

E 15, 300.59

Elevation: 4173.23 ~~4063.70~~
(mine) (MSL)

Total Depth: 1237



All symmetry determinations looking

NW with S₂ dipping 54°
SW with dip azimuth 270° 235

NOT RELOGGED RBT

Purpose: Geologic information NE end Section 118

Logged by: D. S. Jennings Date(s) Logged: July 1976

Drilling Contractor: Arctic Diamond Drilling Core: _____ Size _____ From _____ To _____ Collar Cased and Capped: No

Started: _____ Completed: _____

Lithologic Log

Code	From	To	Unit	Code	Description
	10 14 16	20 22 23 25 27			
L	100	170	11	#	Overburden
L	170	1820	12	O1E18	No attitude possible due to broken, ground core
L	1820	1857	13	1C1D	Gouge zone; zone 70°, 210° @ top; base indeterminate
L	1857	19100	14	1C1D	Clotted variant, minor Al ₂ SiO ₅
L	19100	114185	15	1C1D	Normal, non-carbonaceous, weakly andalusitic transition zone schist
L	114185	115100	16	1C1D	Gouge zone; top attitude indeterminate, base 40°, 210
L	115100	116190	17	1C1D	Several pre-D ₁ qtz veins
L	116190	116197	18	1C1D	Gouge zone; 65°, 210 @ top; 70°, 210° @ base
L	116197	11710	19	1C1D	
L	11710	11715	110	1C1D	Gouge zone; 60°, 210 @ 171.0; 70°, 210 @ 171.5
L	11715	121125	111	1C1D	Normal, non-carbonaceous, weakly andalusitic transition zone schist
L	121125	121145	112	1C1D	Breccia and gouge zone adjacent to diorite; zone 70°, 210° @ top; base indeterminate (best guess on base is 60°, 210° for top of diorite i.e. diorite = sill)
L	121145	121405	113	O1E18	Attitude for top of diorite given above; base of diorite ≈ 90° to c.a. showing irreg. intrusive contact ⇒ dike
L	121405	121409	114	1C1D	
L	121409	121415	115	O1E17	Upper contact ≈ 90° to c.a. irreg. contact; lower contact indeterminate as core broken; typical brownish "quartz, quartzite"
L	121415	1217100	116	1C1D	Interval w/ prevalent pre-D ₁ qtz veins, does not show "clotted" appearance
L	1217100	1217120	117	O1E17	Typical brownish "quartz, quartzite" color w/ many irreg. CaCO ₃ fracture fillings; top contact 75°, ≈ 210°, base indeterminate
L	1217120	1217130	118	1C1D	With some irreg. CaCO ₃ filled fracture fillings
L	1217130	1217140	119	O1E17	As 270-272; top contact 45° to c.a. ≈ 210 cross cutting S ₁ & S ₂ ⇒ post D ₁ dike; base 45° to c.a., cannot measure relative to S ₁ /S ₂
L	1217140	1217170	210	1C1D	Pre-D ₁ qtz veins
L	1217170	1218110	211	O1E17	As 270-272, 273-276; no attitude possible on top contact base 30° to c.a. i.e. unit = dike, cannot measure contact attitude to S ₁ /S ₂
L	1218110	1219180	212	1C1D	Little or no andalusite over interval; many pre-D ₁ qtz veins
L	1219180	1219195	213	O1E16	Top & bottom contacts 45° to c.a. subll to S ₁

Code	From	To	Unit	Code	Description
1	10	14 16	20	22 23 25 27	
L	1219.5	1314.30	24	1C1D	"Clotted" variant w/ moderate amt pre-D ₁ gtz veins
L	1314.30	1314.33	25	1C1D	Gouge zone; top & bottom X cut S. / S ₂ w/ 70° 210° attitude
L	1314.33	1315.60	26	1C1D	Strong botite "clot" development, may be part of K/S ₁ alteration zone (pre-D ₁) marking "feeder pipe" for deposit
L	1315.60	1315.70	27	1C1D	Buccla & gouge zone; no attitudes due to broken core
L	1315.70	1315.95	28	1C1D	As 343.3-356.0
L	1315.95	1316.10	29	1C1D	Gouge zone; heavily compacted gouge @ 30° to c.a. 11 S ₂
L	1316.10	1316.80	30	1C1D	As 343.3-356.0; 357.0-359.5
L	1316.80	1317.65	31	1C1D	Non-clotted, weakly andalusitic, non-carbonaceous variant
L	1317.65	1318.10	32	1C1D	"Clotted" variant w/ no gtz veining
L	1318.10	1318.20	33	1C1D	" " gouge and breccia zone; top of interval 50° 210° base 60° 210°
L	1318.20	1319.65	34	1C1D	"Clotted" variant w/ no gtz veining
L	1319.65	1319.85	35	1C1D	" " breccia and gouge zone adjacent to OCC
L	1319.85	1319.95	36	0C1D	Bull gtz & musc. hyper solvus (?) peg. brecciating 1C1D; no contact Xs possible
L	1319.95	1410.20	37	1C1D	Brecciated & gouged "clotted" variant
L	1410.20	1410.35	38	0C1D	Hypersolvus (?) musc. peg; no contact relations possible because of broken core
L	1410.35	1411.25	39	1C1D	"Clotted" variant of transition zone schists
L	1411.25	1416.60	40	1C1D	Normal OFBM schist w/ minor zones of 1C6 (clotted variant) Note: From 281 to 412.5 no andalusite as the gray green pyrophyllite has been present. ∴ 1C6 may start @ 281.0
L	1416.60	1481.20	41	1C1G	Clotted texture in andalusite poor schists
L	1481.20	1513.70	42	1C1D	Normal gtz-felds. member showing minor "clotted" texture and minor gtz veining
L	1513.70	1513.80	43	1C1D	Breccia & gouge; top attitude indeterminate; bottom ≈ 70° 210°
L	1513.80	1517.95	44	1C1D	Very siliceous & muscovite rich, non-clotted light colored variant c.f. "siliceous" zones in 76X-12
L	1517.95	1518.00	45	1C1D	Gouge zone; top 70° to c.a. @ 120°; base 60° to c.a. @ 150°

Lithologic Log

Code	From		To		Unit		Code		Description
	10	14	16	20	22	23	25	27	
L	15810	0	15975	5	46		1610		Siliceous, muscovite-rich variant as 538.0-579.5 with minor thinly banded po-zug up to 5% over 6"
L	15975	5	16100	0	47		11F18		Chloritic metabasite w/ med. red. br. bio interbands metabasite = act-ep-chlor-plag assemblage.
L	16000	0	16125	5	48		1600		As 538.0-579.5, 580.0-597.5; unit from 538.0 to 612.5 c.f. siliceous banded, po-bearing schists in 76X-12
L	16125	5	16460	0	49		1600		<u>Bria and gouge zone</u> ; interval of schists as seen 538.0-612.5 briaated in gouge matrix; no intrusive activity apparent; interval 618.5-622 not briaated with several bands of near massive po 618.5-619.0; <u>bria and gouge zone may represent major fault zone truncating zone 3 SE of this?</u> DDH; may also be related to similar bria & gouge zones seen in 75-10, 456-75-12, 75-11, 71-211 NE i.e. related to smokey gte fields of E/ or Annel batholith; zone 70° to c.a. along 250° @ top; base to 45° to c.a. along ≈ 310°
L	16460	0	16680	0	50		1606		Typical "clotted" variant of schists on other side of major bria/gouge zone
L	16680	0	16750	0	51		1606		<u>Bria & gouge in contact zone of smokey gte fields porphyry</u> ; bria zone 90° to c.a. @ 668.0', 80° to c.a. @ 675.0'
L	16750	0	17320	0	52		01F10		Typical smokey gte fields of w/ Kspar phenos up to 0.5" in length; some flow(?) banding @ 50° to c.a. from 693-732; contorted flow(?) banding 678-683 c.f. schistitic "wavy" flow banding
L	17320	0	17377	7	53		01F9		<u>Gouge and bria zone</u> in smokey gte fields of gouge contains randomly oriented schist & pl frags ⇒ post-intrusion level of gouge; top of zone 45° to c.a., base 60° to c.a.
L	17377	7	18110	3	54		01F10		Smokey gte fields of
L	18110	3	18180	0	55		01F9		<u>Gouge and bria zone</u> in smokey gte fields of; 50° to c.a. @ top & bottom of interval; 1" slime zone 812-813

Structural Log

Code	From		To		Feature	S ₁ /S ₂	S ₀		S ₁ /S ₂		S ₂ /S ₄		Description
	10	14	16	20			Dip	Direct.	Dip	Direct.	Dip	Direct.	
S				2,610	CSAS				20	20	35	23.5	S4
S				2,680	CSAS						45		
S				3,210	CSAS						60		
S				3,290	CSAS						60		See DSJ Log for Details
S				3,330	CSAS				2.0	3.4	7.0		
S				3,370	CSAS				3.0	10.0	5.5		
S				3,530	CSAZ						5.5		
S				3,570	CSAZ						7.0		
S				3,630	CSAZ				3.0	1.6	7.0		
S				3,680	CSAZ				4.0	1.7	6.0		
S				3,750	CSAS				0.5	10.0	7.0		
S				3,790	CSAS						8.0		
S				4,210	CSAZ				4.0	1.9	6.0		
S				4,360	CSAZ				3.0	1.8	8.0		
S	4,360		4,390	4,390	CSAS				5	10.0	7.0		
S				4,540	CSAZ				4.5	1.8	6.0		
S	4,540		4,580	4,580	CSAS								
S	4,580		4,825	4,825	CSAM								
S				4,830	CSAZ						7.5		
S				4,920	CSAZ				2.5	1.9	7.0		
S				5,030	CSAZ						6.0		
S	5,050		5,740	5,740	CSAS				3.0	10.0	7.5		
S	5,740		5,830	5,830	CSAZ				4.0	1.8	7.0		
*				5,800									Fold hinge
S	5,830		6,010	6,010	CSAS				3.0	10.0	7.5		
S				6,040	CSAS						7.5		

Structural Log

Logged By: [Signature]

Code	From		To		Feature	SYE	S ₁		S ₂		Description
	10	14 16	20	22 24 26 28			Dip	Direct.	Dip	Direct.	
			4390			S		05	2110		End Z short limb S₄ = 70/210
	4310	0	4540		C5H						
S			4540			Z		45	0310		Start short limb S₄ = 60/210
	4514	0	4580		C5H						S region
S			4580			Z		510	0310		End short limb S₄ = 60/210
	4580		4825		C5H						
S			4825								F ₁ trend 120° plunge 5° NW relative to S ₄ dip; F ₂ trend 140° plunge 5° NW; measurements approx & relative to S ₄ attitude $\frac{1}{2}$ antiferromal S₄ = 65/210
	4812	5	4830		C5H						
S			4830			Z					Start Z short limb S₄ = 75/210
	4830	0	4920		C5H						S region
S			4920					215	0310		End Z short limb S₄ = 70/225
	4912	0	5103		C5H						
S			5103			Z					Start Z short limb S₄ = 60/210
	5103	0	5105		C5H						S region
S			5105			Z					End Z short limb S₄ = 70/210
	5105	0	5174		C5H						
S			5174			S		310	2110		Start Z short limb S₄ = 75/210
	5174	0	5183		C5H						S region
S			5183			Z		410	0310		End Z short limb S₄ = 70/210
S			5180	6							F ₁ trend 120° plunge 5° NW; F ₂ trend 120° plunge 5° NW approx co-axial $\frac{1}{2}$ antiferromal S₄ = 60/210
	5183	0	6011		C5H						
S			6011			S		310	2110		Start Z short limb S₄ = 75/210
	6011	0	6040		C5H						S region
S			6040			S					End Z short limb S₄ = 75/210

Structural Log

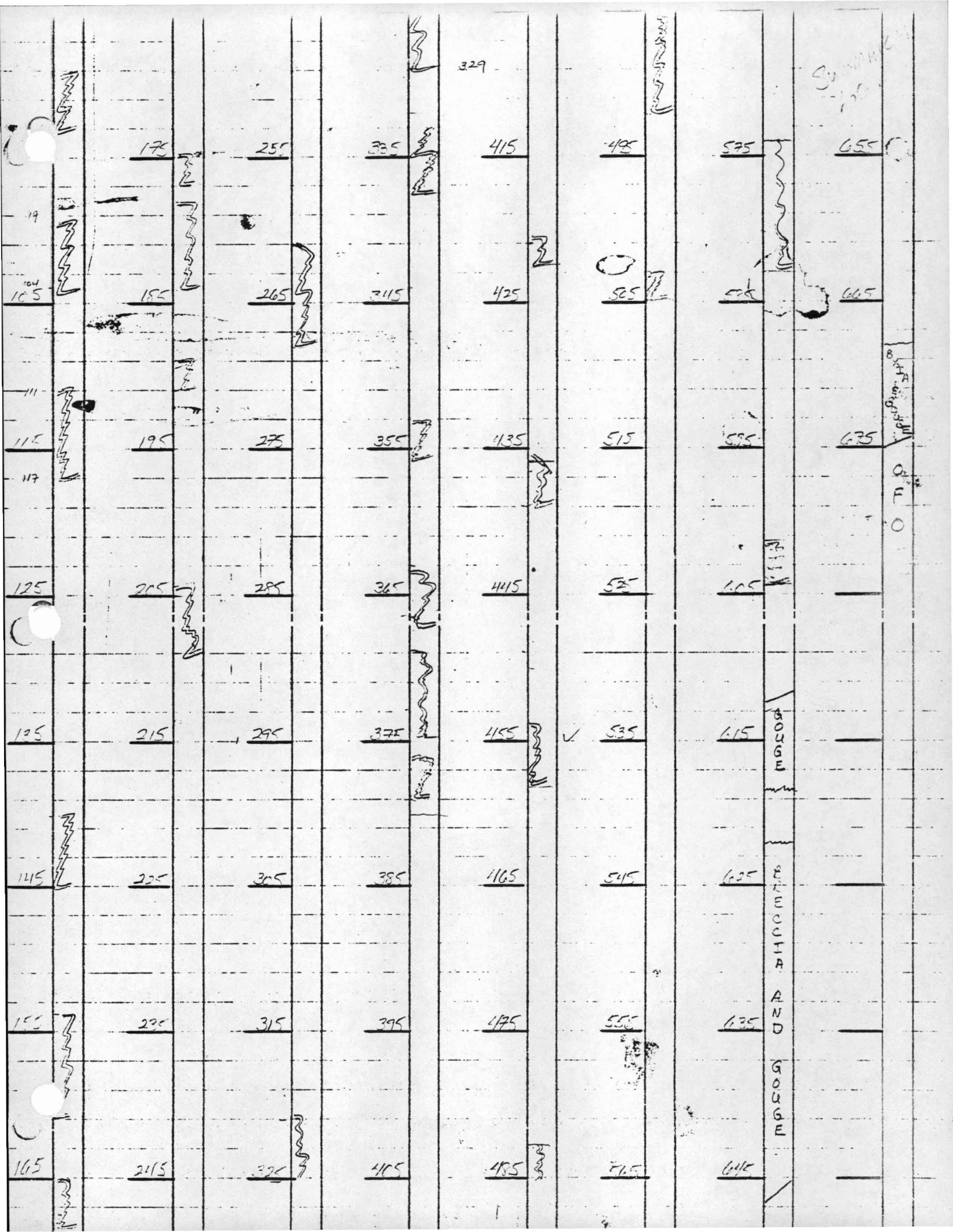
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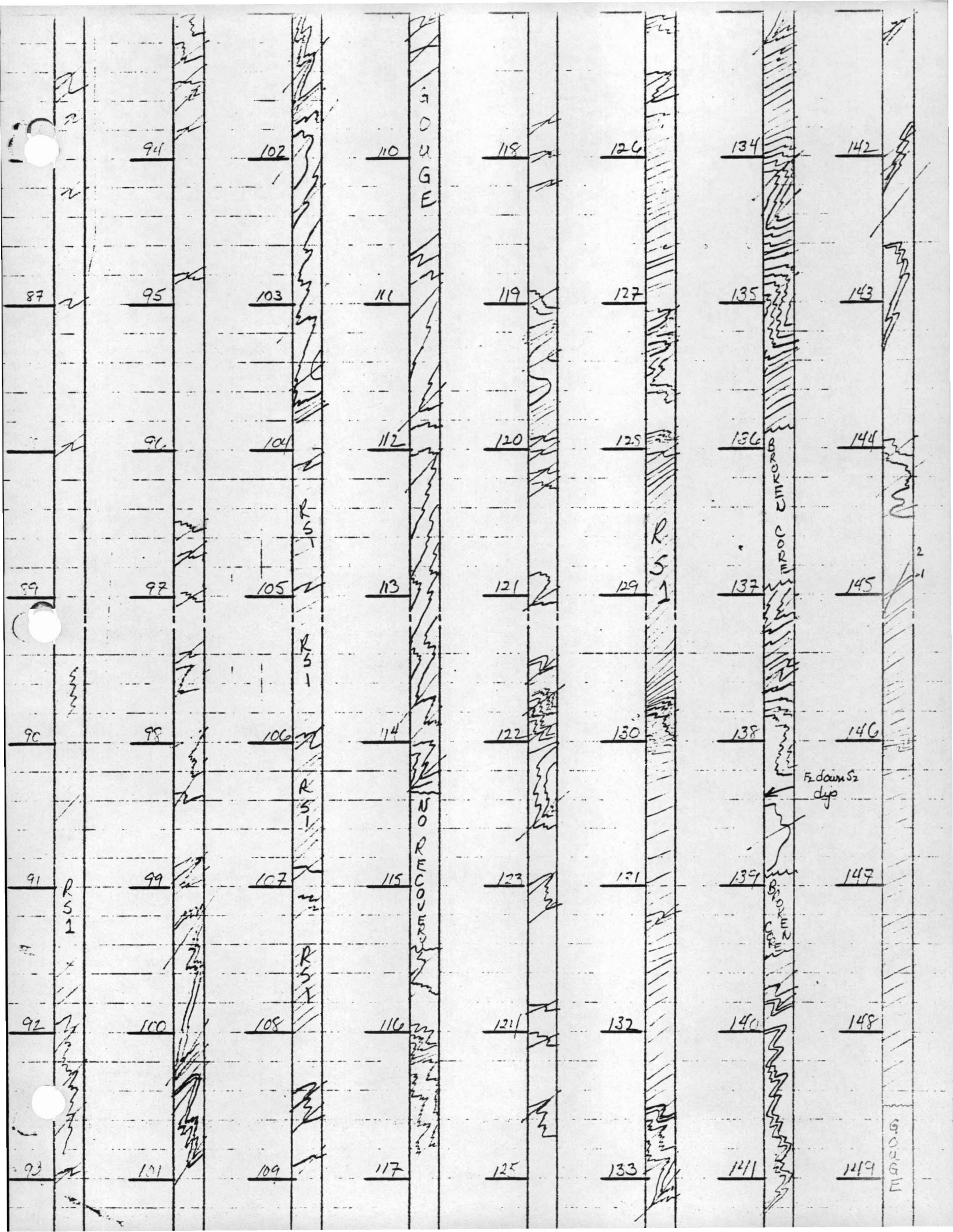
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	10	14	16	20	22	24			26	28	32	34		38	
		8	20		8	9	5	C/S	12						
					8	9	5			S	10	2110	45	2110	Close to light approximated similar F ₂ folds S ₁ =
		8	9	5		9	20	C/S	12						
S					9	20				S	05	2110	50	2110	" " " " " " S ₁ =
		9	20		9	9	0	C/S	12						
S					9	9	0			S	25	2110	50	2110	" " " " " " S ₁ =
		9	9	0		10	40	C/S	12						
S					10	40				S	15	2110	45	2110	" " " " " " S ₁ =
		10	40		11	10		C/S	12						
S					11	10				S	10	2110	35	2110	" " " " " " S ₁ =
		11	10		11	17	0	C/S	12						
S					11	17	0			S	45	2110	60	2110	S ₁ =
		11	17	0		14	0	C/S	12						
S					14	0				S	05	2110	45	2110	S ₁ =
		11	40	0		14	50	C/S	12						
S					14	50		R/S	12			45	2110	terminus of short Z limb S ₁ =	
		11	45	0		15	40	C/S	12						
S					15	40				Z		55	2110	start of short Z limb S ₁ =	
		11	54	0		16	10	C/S	12						
S					16	10				S	30	2110	60	2110	End of short Z limb S ₁ =
		11	61	0		16	50	C/S	12						
S					16	50				S		70	2110	start of short Z limb S ₁ =	
		11	65	0		16	80	C/S	12						
S					16	80				S	10	2130	60	2110	terminus of short Z limb S ₁ =
		11	68	0		17	50	C/S	12						
S					17	50				S	10	2110	50	2110	start of short Z limb S ₁ =
		11	75	0		18	40	C/S	12						
S					18	40				S	10	2100	60	2110	terminus of short Z limb S ₁ =
		11	84	0		18	90	C/S	12						
S					18	90				S	10		65	2110	start of short Z limb S ₁ =
		11	89	0		19	10	C/S	12						
S					19	10				Z		50	2110	terminus of short Z limb S ₁ =	
		11	91	0		20	14	C/S	12						
S					20	14				Z	20	0310	90	2110	start of 2 short limb S ₁ =
		12	014			20	19	0	C/S	12					
S					20	19	0			S	45	2100	70	2110	terminus S ₁ =

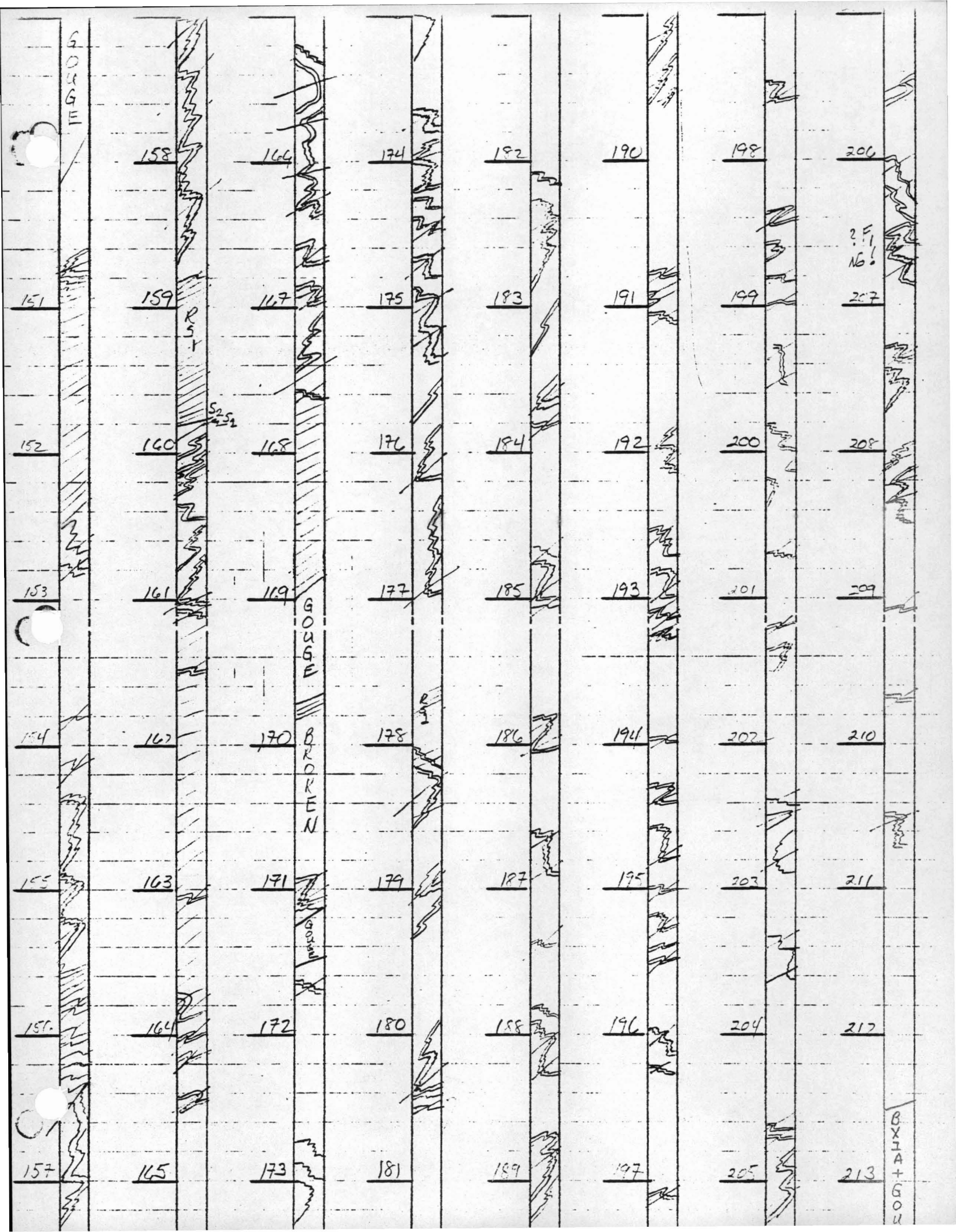
Structural Log

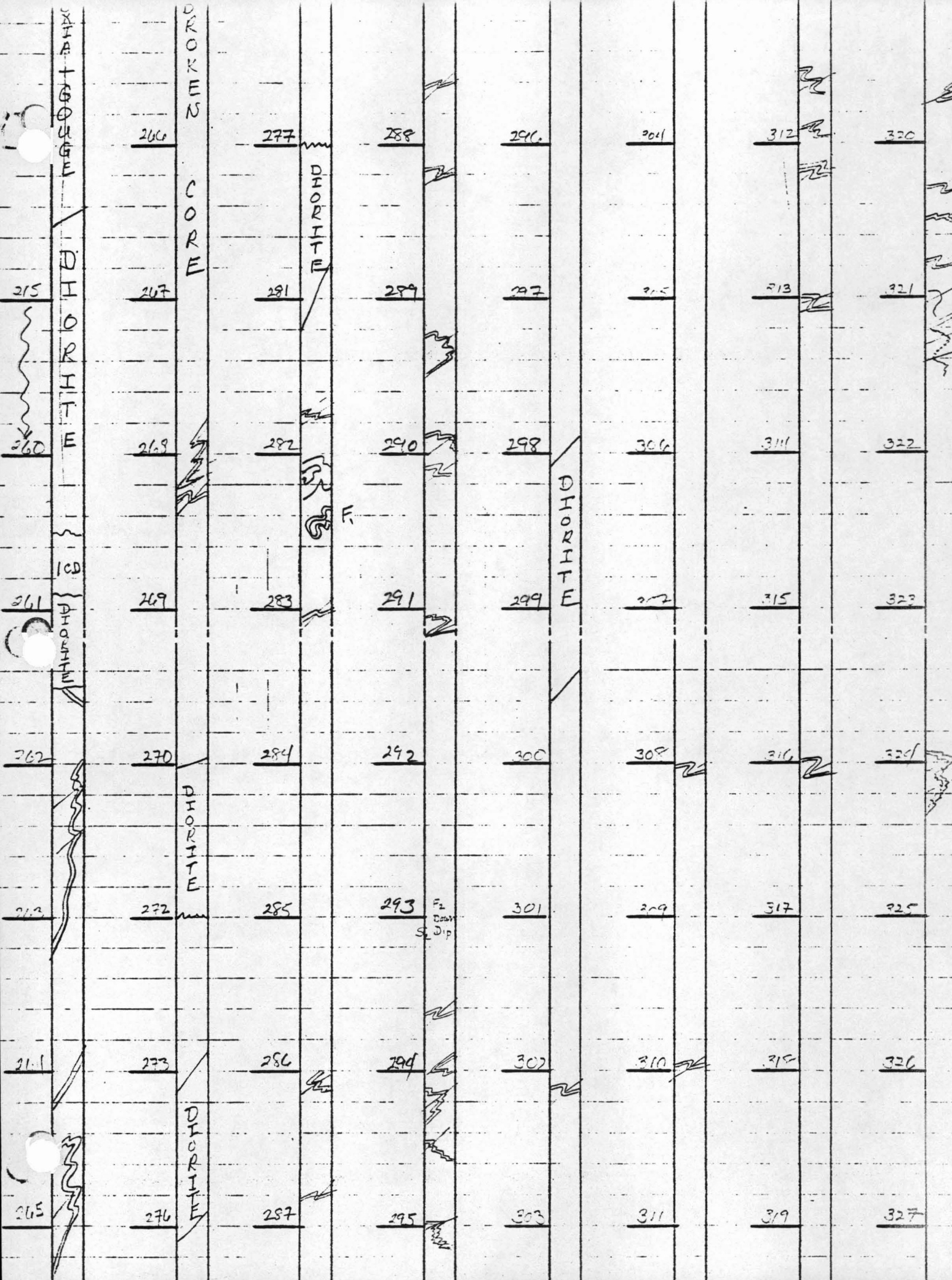
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Code	From		To		Feature	S ₁ Dip Direct.	S ₂ Dip Direct.		Description	
	10	14 16	20	22 24 26 28			32 34	38		
			143190		S	015	2110	710	2110	End Z short limb
	143100		145140		C512					
S			145140		Z	415	0130	610	2110	Start short limb
	145140		145180		C512					S region
S			145180		Z	510	0130	610	2110	End short limb
	145180		14825		C512					
S			14825					615	2110	F ₂ trend 120° plunge 5° NW relative to S ₂ dip; F ₁ trend 140° plunge 5° NW; measurements approx & relative to S ₂ attitude F ₁ antiformal
	14825		14830		C512					
S			14830		Z			715	2110	Start Z short limb
	14830		14920		C512					S region
S			14920			215	0115	710	2110	End Z short limb
	14920		15030		C512					
			15030		Z			610	2110	Start Z short limb
	15030		15050		C512					S region
S			15050		Z			710	2110	End Z short limb
	15050		151740		C512					
S			151740		S	310	2110	715	2110	Start Z short limb
	151740		151830		C512					S region
S			151830		Z	410	0130	710	2110	End Z short limb
S			151806					610	2110	F ₂ trend 120° plunge 5° NW; F ₁ trend 120° plunge 5° NW approx co-axial F ₁ antiformal
	151830		16010		C512					
S			16010		S	310	2110	715	2110	Start Z short limb
	16010		16040		C512					S region
S			16040		S			715	2110	End Z short limb









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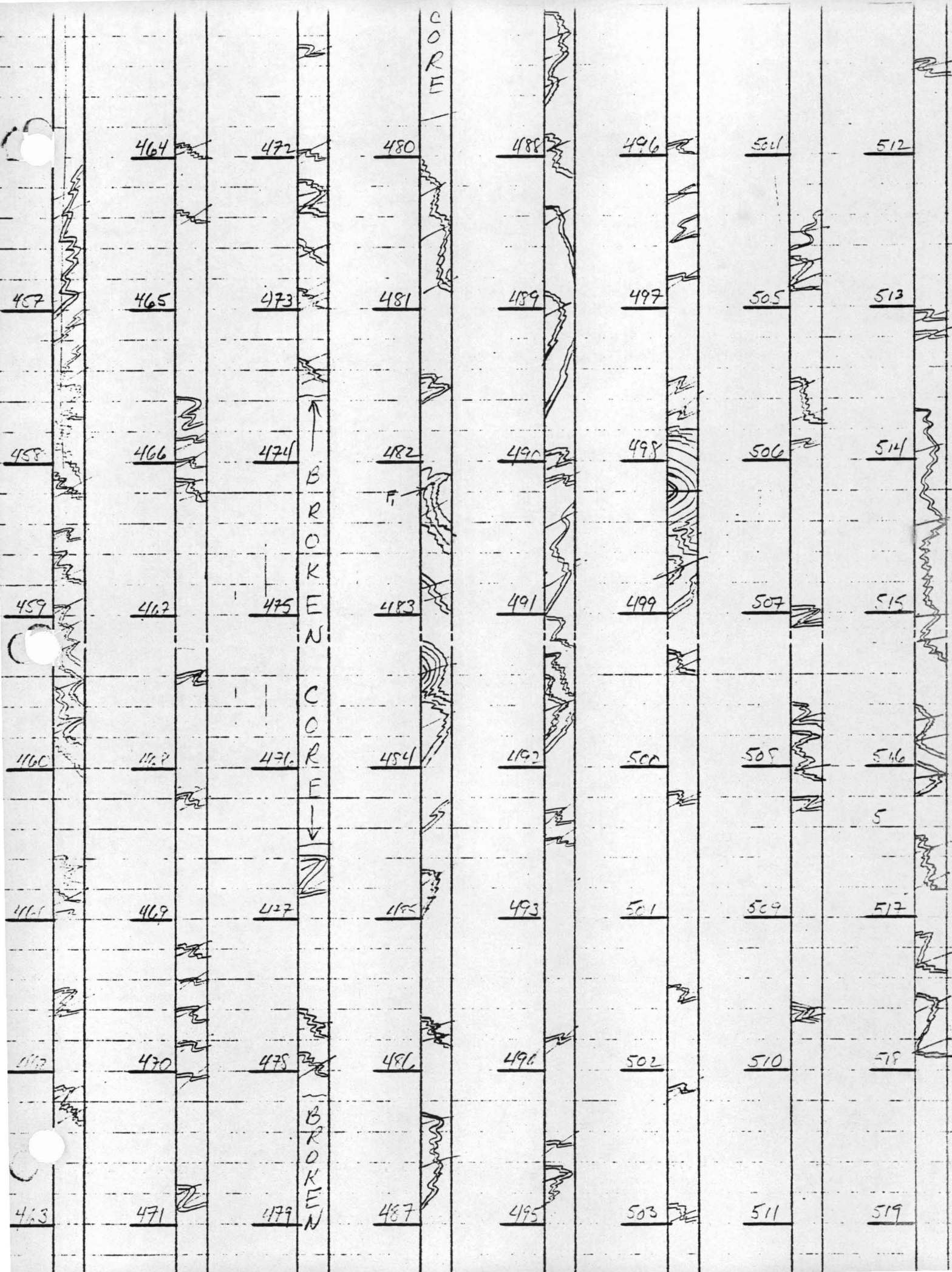
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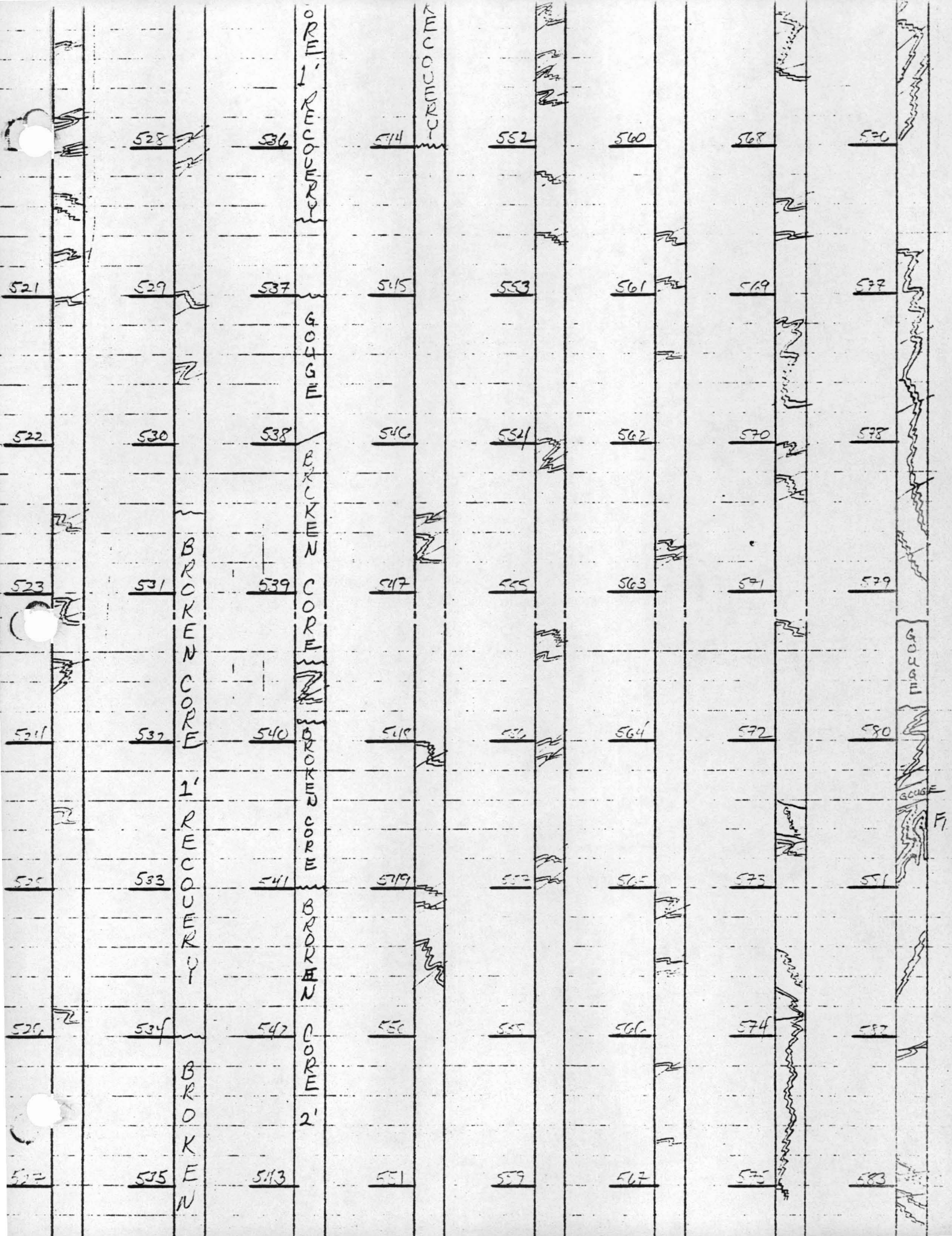
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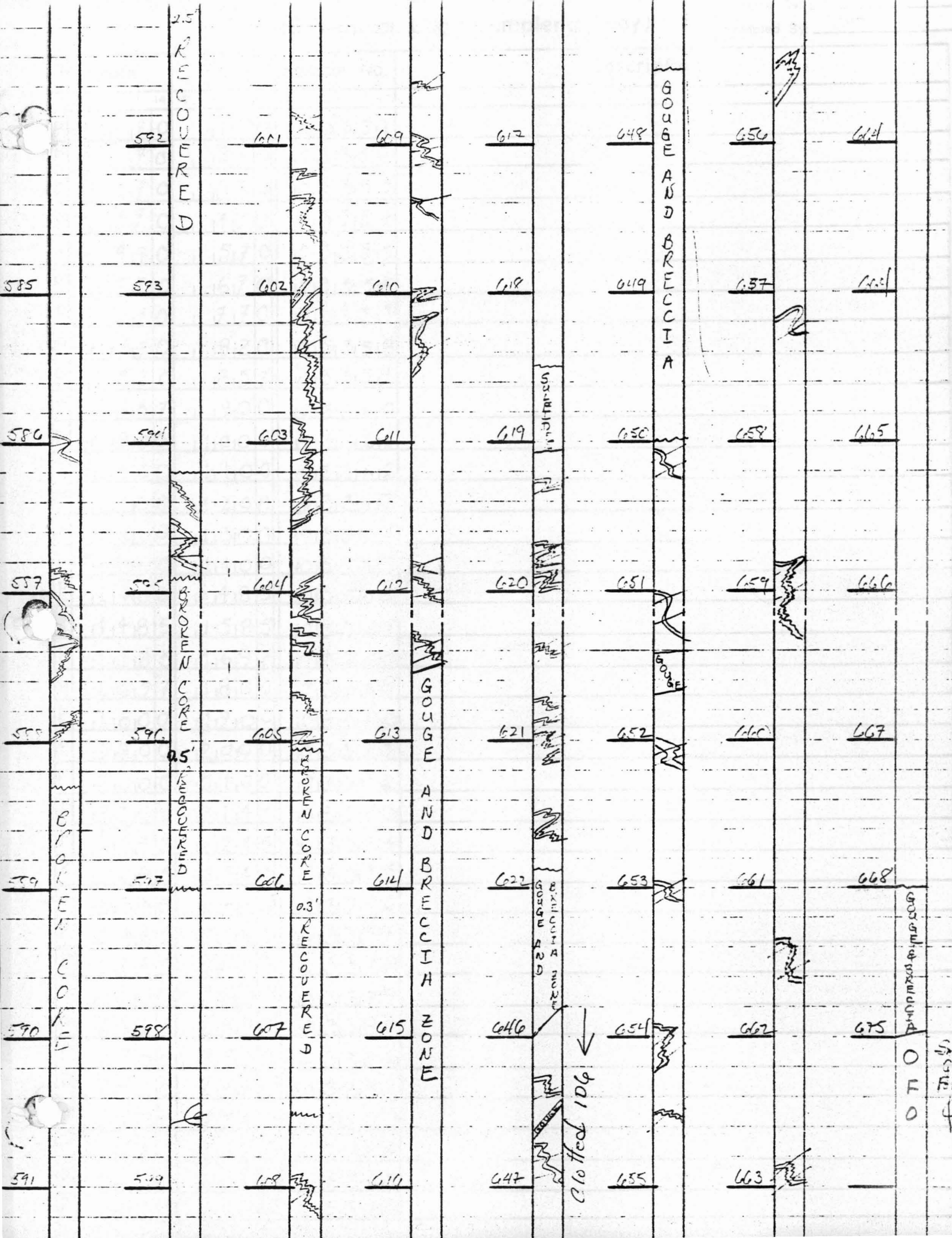
393	400	408	416	424	432	440	448
394	401	409	417	425	433	441	449
395	402	410	418	426	434	442	450
396	403	411	419	427	435	443	451
397	404	412	420	428	436	444	452
398	405	413	421	429	437	445	453
399	406	414	422	430	438	446	454
400	407	415	423	431	439	447	455

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25' RECOVERED

25' RECOVERED

0.3' RECOVERED

GOUGE AND BRECCIA ZONE

0.3' RECOVERED

GOUGE AND BRECCIA

0.3' RECOVERED

Clogged IDG

585	592	601	609	612	618	619	648	650	664
586	593	602	610	618	619	649	649	657	664
587	594	603	611	619	649	650	658	659	665
588	595	604	612	620	651	651	659	659	666
589	596	605	613	621	652	652	660	660	667
590	597	606	614	622	653	653	661	661	668
591	598	607	615	646	654	654	662	662	675
592	599	608	616	647	655	655	663	663	