

66-1  
Collar elev. 4329.00

BENCH 4065  
4329  
BENCH INTER. 4100  
from 229 to 264

002022

1.0	1.76	6.4	9.5	1.76	6.4	9.5
5.0	1.64	4.9	8.1	8.20	24.5	40.5
5.0	2.32	5.7	11.1	11.60	28.5	55.5
4.8	1.88	4.5	6.3	9.02	21.6	30.2
4.9	1.36	4.8	8.6	6.66	23.5	42.1
2.8	—	7.2	17.5	—	20.2	49.0
2.0	1.12	2.2	4.7	2.24	4.4	5.4
5.0	1.58	2.2	5.1	7.90	11.0	25.5
3.7	1.34	2.6	3.7	4.96	9.6	13.7
0.8	2.08	2.2	5.1	<u>1.66</u>	<u>1.8</u>	<u>4.1</u>

35'  
54.0 151.5 275.5  
1.54 4.3 7.9

65-1  
Collar 4309.1  
BENCH INTER. FROM 204 TO 239

5.5	0.42	1.8	0.5	2.31	9.9	2.8
5.3	0.20	0.2	1.8	1.06	1.1	9.5
5.4	0.38	0.4	3.5	2.05	2.2	18.9
2.9	0.66	0.6	4.5	1.91	1.7	13.1
4.1	0.92	2.3	5.1	3.77	9.4	20.9
2.5	2.20	6.1	11.0	5.50	15.3	27.5
3.0	—	3.5	6.5	—	10.5	19.5
2.2	0.58	4.0	6.8	1.28	8.8	15.0
3.1	2.70	7.1	11.5	8.37	22.0	35.7
1.0	0.86	4.5	7.8	.86	4.5	7.8

35.0  
27.11 85.4 170.7  
0.77 2.4 4.9

18.8  
21.69 72.2 139.5  
1.15 3.8 7.4

66-25  
Collar = 4321.2

Bench Inter From  $\frac{4321.2}{4100}$  221.2 TO  $\frac{4321.2}{4065}$  256.2

3.8	3.70	5.5	6.8	14.06	20.9	25.8
5.0	2.70	6.6	9.7	13.50	33.0	48.5
<u>5.0</u>	<u>0.95</u>	<u>2.0</u>	<u>3.4</u>	<u>4.75</u>	<u>10.0</u>	<u>17.0</u>
5.0	0.18	0.1	0.3	0.90	0.5	1.5
5.0	0.13	—	0.2	0.65	—	1.0
5.0	0.21	—	0.1	1.05	—	0.5
5.0	0.16	—	0.20	0.80	—	1.0
1.2	0.51	0.4	0.8	0.61	0.5	1.0

35 36.32 64.9 96.3  
1.04 1.9 2.8

13.8 32.31 63.9 91.3  
2.34 5.0 6.6

66-24  
Collar 4309

BENCH INTER  $\frac{4309}{4100}$  209 TO  $\frac{4309}{4065}$  244

1.0	3.48	3.7	6.3	3.48	3.7	6.3
5.0	2.82	4.1	9.9	14.10	20.5	49.5
5.0	4.90	5.3	6.8	24.50	26.5	34.0
5.0	3.92	4.7	9.4	19.60	23.5	47.0
5.0	2.19	3.5	8.0	10.95	17.5	40.0
5.0	2.34	4.8	8.2	11.70	24.0	41.0
5.0	3.22	3.5	5.0	16.10	17.5	25.0
4.0	1.79	4.2	6.2	<u>7.16</u>	<u>16.8</u>	<u>24.8</u>

35' 107.59 150.0 267.6  
3.07 4.3 7.6

66-44  
Collar 4298.6

BENCH INTER.

4298.6  
4100  
198.6

4298.6  
4065  
233.6

1.4	0.08	0.3	0.1	0.11	0.4	0.1	
<del>5.0</del>	<del>0.30</del>	<del>0.5</del>	<del>0.5</del>	<del>1.50</del>	<del>2.5</del>	<del>2.5</del>	
5.0	2.40	3.1	3.7	12.00	15.5	18.5	
5.0	2.40	3.0	3.0	12.00	15.0	15.0	
5.0	5.50	9.0	0.4	27.50	45.0	2.0	7.1
5.0	1.17	1.6	2.6	5.85	8.0	13.0	3.6
5.0	3.08	5.1	8.5	15.40	25.5	42.5	3.5
3.6	3.40	7.4	5.2	12.24	26.6	18.7	

35  
8660 138.5 112.3  
2.47 4.0 3.2

28.6  
84.99 135.6 109.7  
2.97 4.7 3.8

66-32  
Collar 4293.2

Bench Inter.

4293.2  
4100  
193.2

4293.2  
4065  
228.2

220 to 225	5.0-1.12	2.0	10.2	5.60	10.0	51.0
225 to 228.2	3.2-1.56	4.5	7.4	4.99	14.4	23.7
8.2'				<u>10.59</u>	<u>24.4</u>	<u>74.7</u>
				1.29	3.0	9.1

66-41  
Collar 4280.3

Bench Inter.

4280.3  
4100  
180.3

4280.3  
4065  
215.3

66-28

2.7	0.78	1.0	2.3	2.10	2.7	6.2
5.0	0.76	4.0	11.2	3.80	20.0	56.0
5.0	0.66	3.9	8.1	<u>3.30</u>	<u>19.5</u>	<u>40.5</u>
<del>5.0</del>	<del>0.39</del>	<del>0.4</del>		9.20	42.2	102.7

12.7  
0.72 3.3 8.1

66-38

Collar 4310.6

Ben. Index

4310.6

4100

210.6

4310.6

4065

245.6

Stault area.

# 4065

LOCATION	PLAN. READ.	TONS	GRADE	
1	0.162	100,150	11.1	1,111,665
2	0.240	148,370	5.5	816,035
3	0.233	144,000	11.6	1,670,400
4	0.345	213,270	7.8	1,663,506
5	0.200	123,640	12.1	1,496,044
		729,430	9.26%	6,757,650
		-38,000		-209,000
		691,430	9.5	6,548,650

# 4030

LOCATION	PLAN READ	TONS	GRADE	
1	0.255	157,640	16.6	2,616,824
2	0.223	137,860	12.5	1,723,250
3	0.113	69,860	5.2	363,272

365,360    12.87    4,703,346

~~38,000~~                      ~~209,000~~

~~327,360~~    ~~13.7~~    ~~4,494,346~~

8.9  
20  
1780  
35 - **5.1**

# 3995

LOCATION	PLAN READ	TONS	GR.	
1	0.198	122,400	10.0	1,224,000
2	0.252	155,780	9.9	1,542,222
3	0.310	191,640	12.5	2,395,500
		469,820	10.99	5,161,722
	9995	488,370	11.00	5,372,070
		+50,000		+780,000
		538,370	11A	6,152,070

# 3960

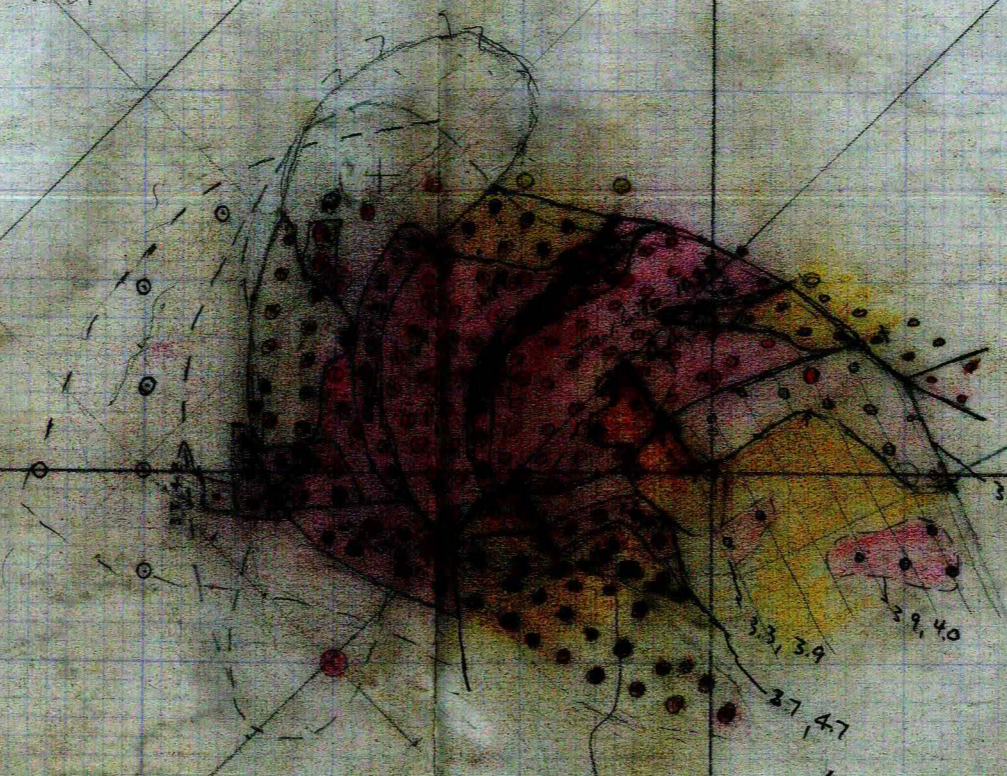
LOCATION	PLAN READ	TONS	GR.	
1	0.140	86,550	11.4	986,670
2	0.260	160,730	17.2	2,764,556
3	0.174	107,570	11.4	1,226,298
4	0.148	91,490	15.6	1,427,244
	722	446,340	14.35	6,404,768
		25,000	17.2	
	715	466,730	14.35	
		25,000	17.2	
		<u>491,700</u>	14.5	

966,730

SEC 10  
WB-31

365

B1



Jan 12 - 8:30 am

40,500 N

0.067

Jan 22

42, 47

Jan 6th 41,416 @ 10.4

Jan 8th 37,000 @ 14.27

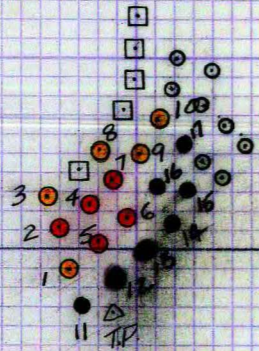
13000 E

4065

4065 (EAST) BENCH - MAR. 23/70

□ = WASTE HOLES

AVER. ELEV.  
= 4103



10,500 N

#1 = 6135

#11 = 6165

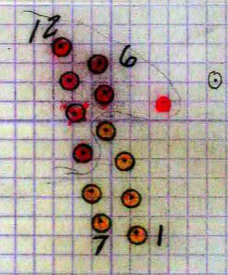
13,000 E

70-23  
D

4065 BENCH (WEST) - MAR. 17/70

10,500 N

AVER. ELEV.  
= 4103



#1 = 6123

#7 = 6129

#12 = 6134

(#12 SAMPLED 18/3/70  
AFTER LOADING) - NOT RELIABLE

13,000 E

7019 Δ

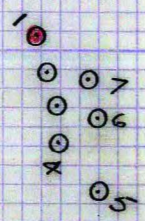
4065 (WEST) BENCH - MAR. 16/70

Δ 5519

13,000 E

10,500 N

AVER. ELEV. = 4102



#1 = 6116

Same as 5857.

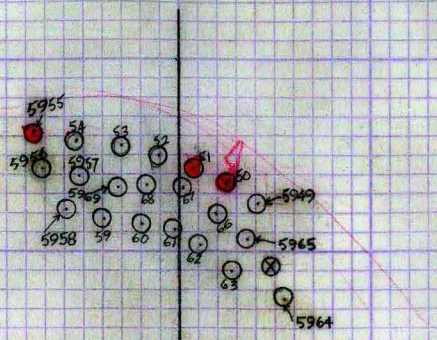
Not used in averages.

Δ  
70-13



4065 BENCH - FEB. 19/70

AVER. ELEV.  
= 4102



5571

70-13

10,000 N

13,000 E

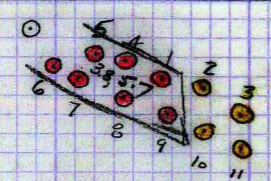
70-16

4065 BENCH - JAN. 30/70

70-15

13,000 E

10,500 N



#1 = 5858

#11 = 5868

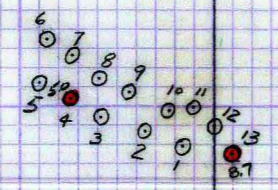
SS-14

4065 BENCH - JAN-27/70

13,000 E

10,500 N

AVER. ELEV. = 4102



① = 5845

⑬ = 5857

△  
70-9

△  
70-11

✓

4065 BENCH - JAN. 24/70

13,000 E

S (5840)

S (5841)

S (5842)

S (5843)

19,500 N

70-5 Δ

S (5844)

Δ  
70-10

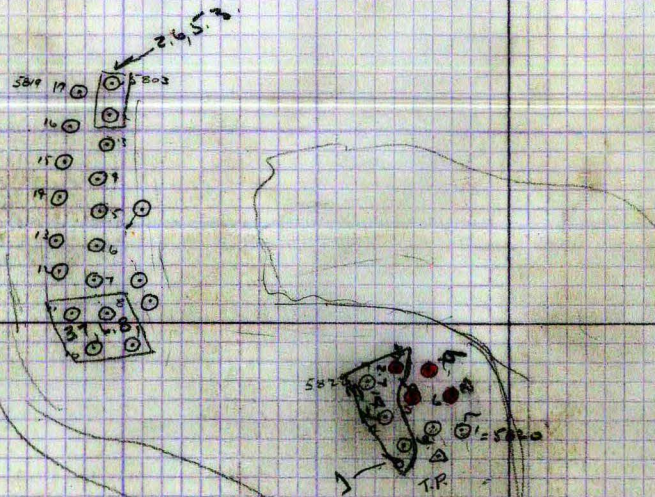
Same as	
S - 5841 -	58 39
42	38
43	37

Not included in averages.

4065 BENCH - JAN. 22/70

E 13,000

AVER. ELEU.  
= 4103



AVER. ELEU.  
= 4101

N 10,500

S820	1	0.4	1.9
	2	0.4	2.0
	3	2.5	4.7
	4	2.6	5.2
	5	0.2	3.7
	6	0.3	2.1
	7	0.3	1.9
	8	2.1	3.1
	9	3.6	5.7

7.2

7.8

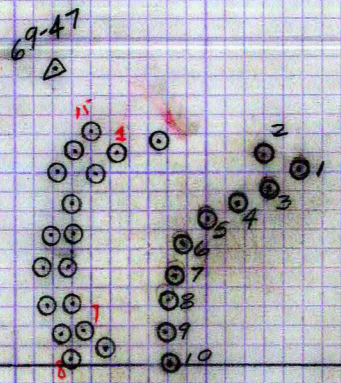
5.2

9.3

27.47

108 187  
4 4  
= 2.7 4.7

4065 BENCH - JAN. 16/70



① = 577B

⑩ = 5787

⑪ 5788

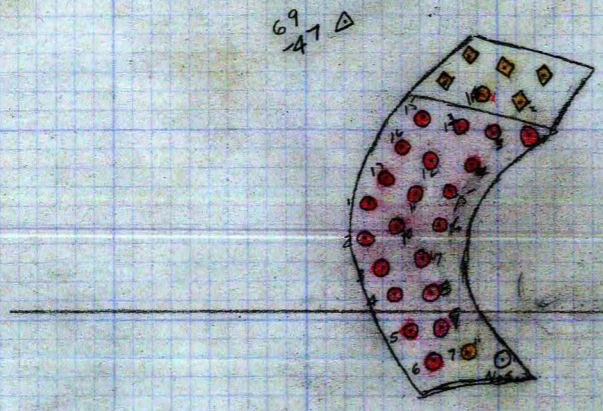
⑬ 5802

△  
69-44

4065 BENCH - JAN. 8/70

AVER. ELEV.  
= 4102

#1 = 5748  
#7 = 5754



69  
47 Δ

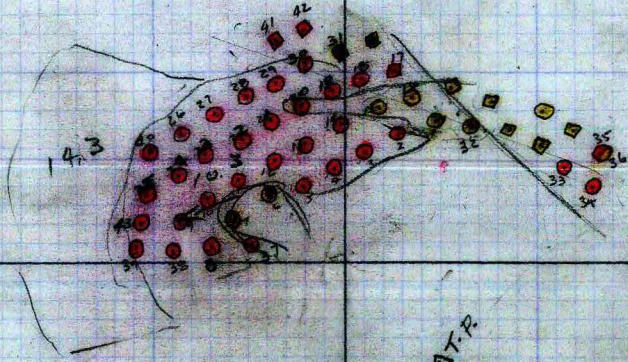
69  
44 Δ

10,000 N

13,000 E

4065 BENCH - JAN. 6/70

69  
47



AVER. ELEU.  
= 4100

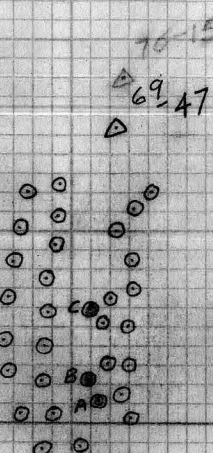
10,500 N

69  
44

10,000 N

13000 E

4065 BENCH - JAN. 23/70



70-15  
69-47  
△

△  
70-5

N 10,500

A = 5837  
B = 5838  
C = 5839

△  
69-44

△  
55-14

E 13,000

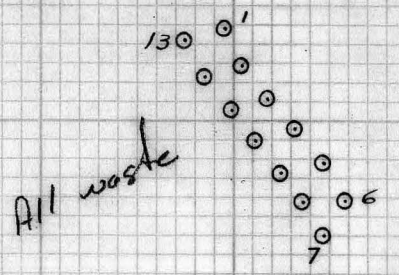
4065 (WEST) BENCH - MAR. 10/70

13,000 E

10,500 N

AVER. ELEV.  
= 4101

- #1 = 6079
- #6 = 6084
- #7 = 6085
- #13 = 6091



70  
-13

BLAST JAN. 8-70

		Conc.	Pb	Zn	Pb	Zn	Conc.
5-7	18	6.0	2.0	4.0	6.0		
					4.0	2.0	6.0
7-10	10	8.1	3.4	4.7			
	11	9.4	3.8	5.6			
		<sup>2</sup> 17.5	<sup>2</sup> 7.2	<sup>2</sup> 10.3			
		8.8	3.0	5.2	3.6	5.2	8.8
10 +	1	11.9	5.3	6.6			
	3	16.7	8.0	8.7			
	4	20.6	10.2	10.4			
	5	18.0	6.7	11.3			
	6	12.3	5.4	6.9			
	7	11.4	5.2	6.2			
	8	14.3	7.0	7.3			
	9	15.9	7.3	8.6			
	12	18.0	8.9	9.1			
	13	15.8	7.4	8.4			
	15	16.7	7.9	8.8			
	16	18.0	8.6	9.4			
	17	12.9	5.5	7.4			
	19	14.2	5.7	8.5			
	20	14.2	5.9	8.3			
	21	14.2	5.6	8.6			
	22	14.0	5.6	8.4			
	23	13.5	5.2	8.3			
		<sup>18</sup> 27.26	<sup>18</sup> 12.14	<sup>18</sup> 15.12	6.8	8.4	15.2

21      21      21  
2961      1306      1655

14.1      6.2      7.9

1	31	16	3.8	17	5.7		
2	5.4	15	4.5	18	7.1	31	4.1
3	9.8	14	6.2	19	9.4	30	7.9
4	11.9	13	9.6	20	3.4	29	7.7
5	13.1	12	12.3	21	7.0	28	11.6
6	3.6	11	18.1	22	13.7	27	13.1
7	3.9	10	6.9	23	11.8	26	13.6
37	12.1			24	12.8	40	16.8
8	6.9	9	10.5	25	15.7		
		38	8.6	43	12.6		
		39	13.5				

5.4	9.8	11.9	6.2	8.6	12.3	5.7	7.1	13.7	7.9	11.6
6.9		13.1	6.9	9.6	10.5		7.0	11.8	7.7	13.1
	12.1		8.1	13.5		9.4	12.8			13.6
							15.7			16.8

2	1	3	2	3	3	1	3	4	2	4
6.1	9.8	12.7	6.5	8.8	12.1	5.7	7.8	13.5	7.8	13.8

	6.0		12.6
	5.4	9.8	10.8
	6.9	8.6	13.6
	6.2	9.6	11.9
S-7	6.9	8.1	13.1
7-10	5.7	12.3	12.1
10+	31	7.1	10.5
		7.0	13.5
		9.4	13.7
	6.2	7.9	11.8
		7.7	12.8
		7.52	15.7
		9	11.6
	8.4		13.1
			16.8
			12.9

$$\frac{2 \times 6}{18 \times 18} \times 35 \times 3.18 = 27$$

$$12 \times 35 \times 3.18 = 1336$$

6	8016	53211
5	6680	4146
9	12024 @ 8.4	101002
16	21376	275750
14	18704 @ 12.9	243152
28	37408	439593
31	41416	355370

area = 0.067 = 41420  
 37412 tons

# BLAST - JAN. 6-70

			Pb	Zn			
5-76	2	5.4	2.5	2.9			
	8	6.9	2.7	4.2			
	14	6.2	2.8	3.4			
	10	6.9	2.7	4.2			
	17	5.7	2.6	3.1			
	41	6.0	2.7	3.3			
		<sup>6</sup> 371	<sup>6</sup> 160	<sup>6</sup> 211	2.7	3.5	6.2
7-10	3	9.8	8.2	1.6			
	13	9.6	4.1	5.5			
	11	8.1	2.8	5.3			
	38	8.6	3.9	4.7			
	18	7.1	3.4	3.7			
	19	9.4	4.0	5.4			
	21	7.0	2.7	4.3			
	30	7.9	3.5	4.4			
	29	7.7	2.4	5.3			
			<sup>9</sup> 752	<sup>9</sup> 350	<sup>9</sup> 402	3.9	4.5
104	4	11.9	4.9	7.0			
	5	13.1	6.4	6.7			
	37	12.1	5.1	7.0			
	12	10.3	4.4	5.9			
	9	10.5	4.3	6.2			
	39	13.5	5.5	8.0			
	22	13.7	5.2	8.5			
	23	11.8	4.2	7.6			
	24	12.8	5.0	7.8			
	25	15.7	6.6	9.1			
	43	12.6	5.2	7.4			
	28	11.6	4.8	6.8			
	27	14.1	5.7	8.4			
	26	13.6	5.8	7.8			
	40	16.8	7.8	9.0			
	42	10.8	5.0	5.8			
			<sup>16</sup> <del>209</del> 859	<sup>16</sup> 1190	5.4	7.5	12.9
	8016	2.7	3.5	21643	28056		
	12024	3.9	4.5	46894	54108		
	21376	5.4	7.5	115430	160320		
	41416	4.44	5.85	183967	242484		

0.168	103,856	11.1 - 35'
0.233	144,039	5.5 - 35'
0.233	144,039	11.6 - 12'
0.333	205,858	7.8 - 35'
0.270	166,912	12.1 - 35'
0.243	150,221	10.2 - 9'

1.480

914,925

348,000

103,8  
 144,0  
 144,  
 205,8  
 -----

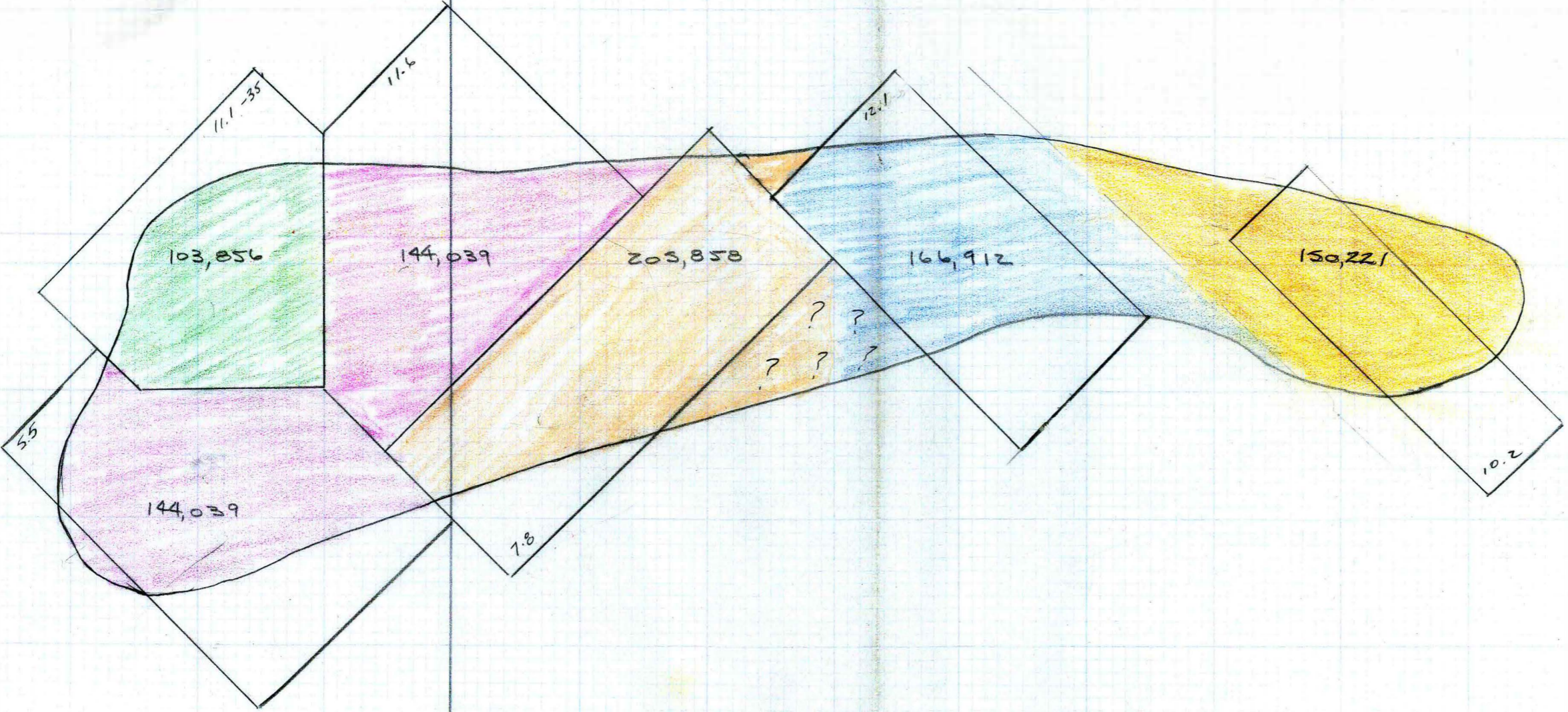
597,700  
 164,000  
 -----  
 433,700

4

4065 Bench.

4 5 6 7 8 9 10 11 12 13 14 15 16

C  
D  
E  
F  
G



E 13000

H 10,000

4065 BENCH.