

Vic ^{V.T.} CONTROL POINTS - TRANSIT

1986 Yr.

007007

	LAT	DEP	EL
T01	350.00	2100.00	1645
D9'	296.00	1997.91	1652.35
T02	386.88	1947.10	1655.96
T03	297.20	1878.10	1656.50
T04	282.49	1740.01	1646.27
T05	314.70	1697.38	1640.70
T06	169.19	1708.29	1641.50
T07	128.05	1826.00	1639.13
T08	138.10	1966.42	1649.14
T09	164.05	2105.64	1661.82
T10	214.20	2134.24	1662.41
T-11	434.06	2076.81	1632.39

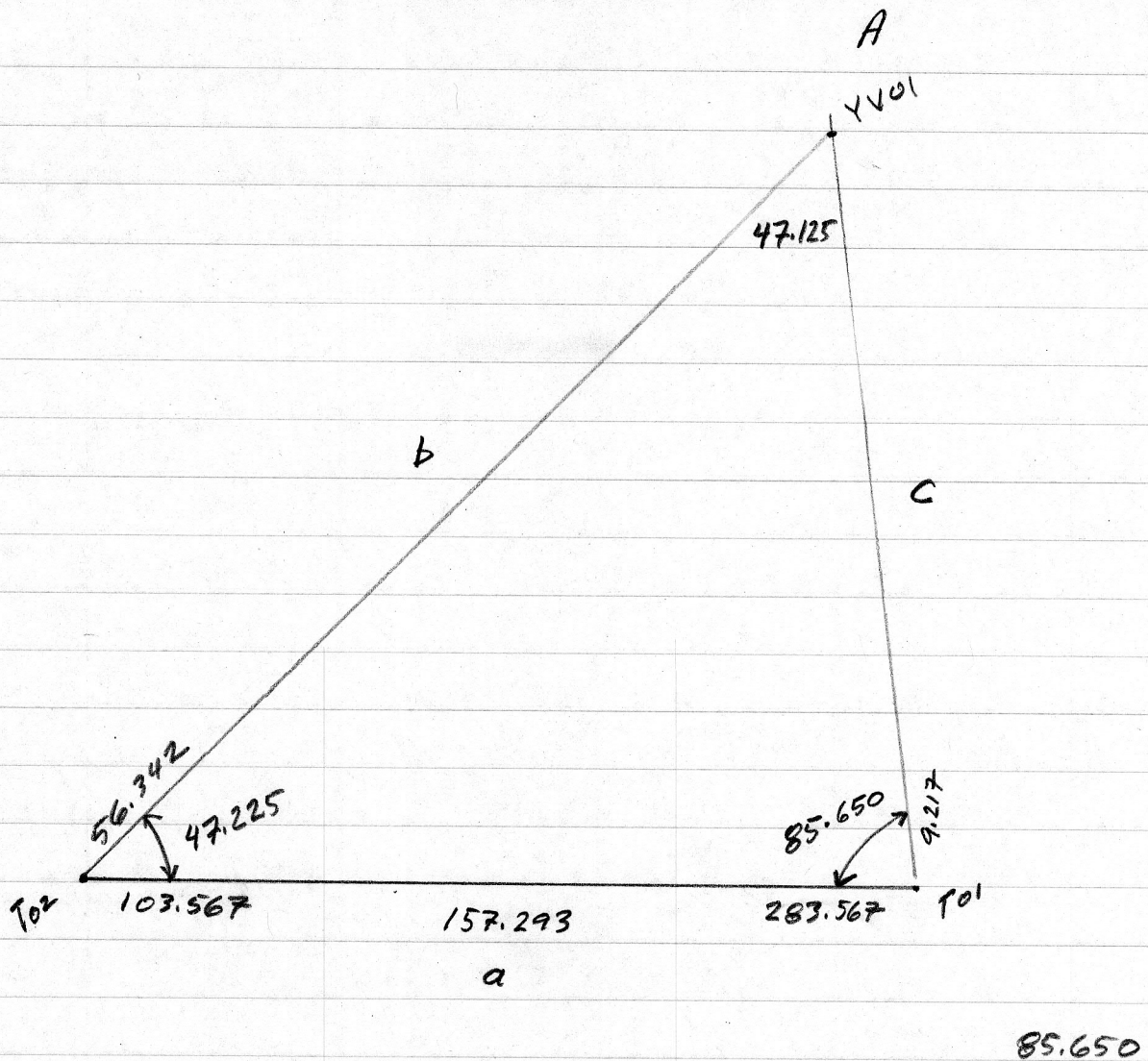
YV- DRILLING - DDH CO-ORDINATES - METERS

HOLE#	LAT	DEP	ELEV	DIP	AZ	GRID ORIGIN
YV86-01	506.08 505.52	2126.57 2125.24	← call'n relocated 1617.07y			LINE 21+00 E } Est elevation STA 350 N } 1645m
02	762.83	2100.00	1575.9			
03						LINE 21 E → Az 0°00'
04	290.60	1732.05	1644.5			(Defined by sight from grid origin to YV-86-02)
05	194.33	1692.05	1641.1			
06	250.26	1744.39	1643.6			
07	249.67	1744.55	1643.6			
08	349.46	2063.46	1645.1			
09	297.38	1997.98	1652.0			
				DIP	AZ	
10	224.05	1741.51	1644.88			
11	236.14	1654.15	1638.64			
12	200.28	1786.89	1645.06	-45°		
13	272.32	1997.54	1653.72	-46°	Grid N	
14	222.79	1997.18	1656.34	-48°	Grid N	check thin scan
15	271.35	1947.77	1655.70	-47°	Grid N	
16	274.49	2047.62	1653.61	-47°	Grid N	
17	412.97	2125.20	1634.33	-47°	Grid N	
18	415.29	2070.85	1635.67	-47°	Grid N	

JULY 86

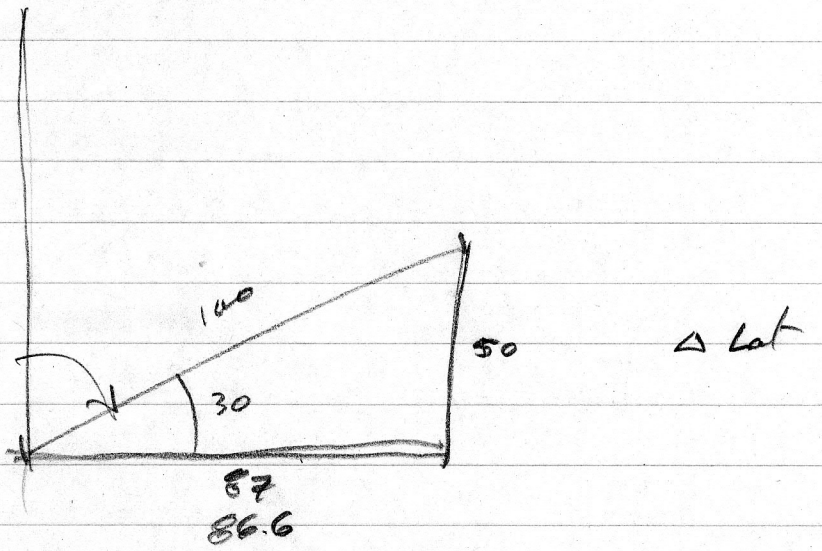
AUG / SEPT 86

②

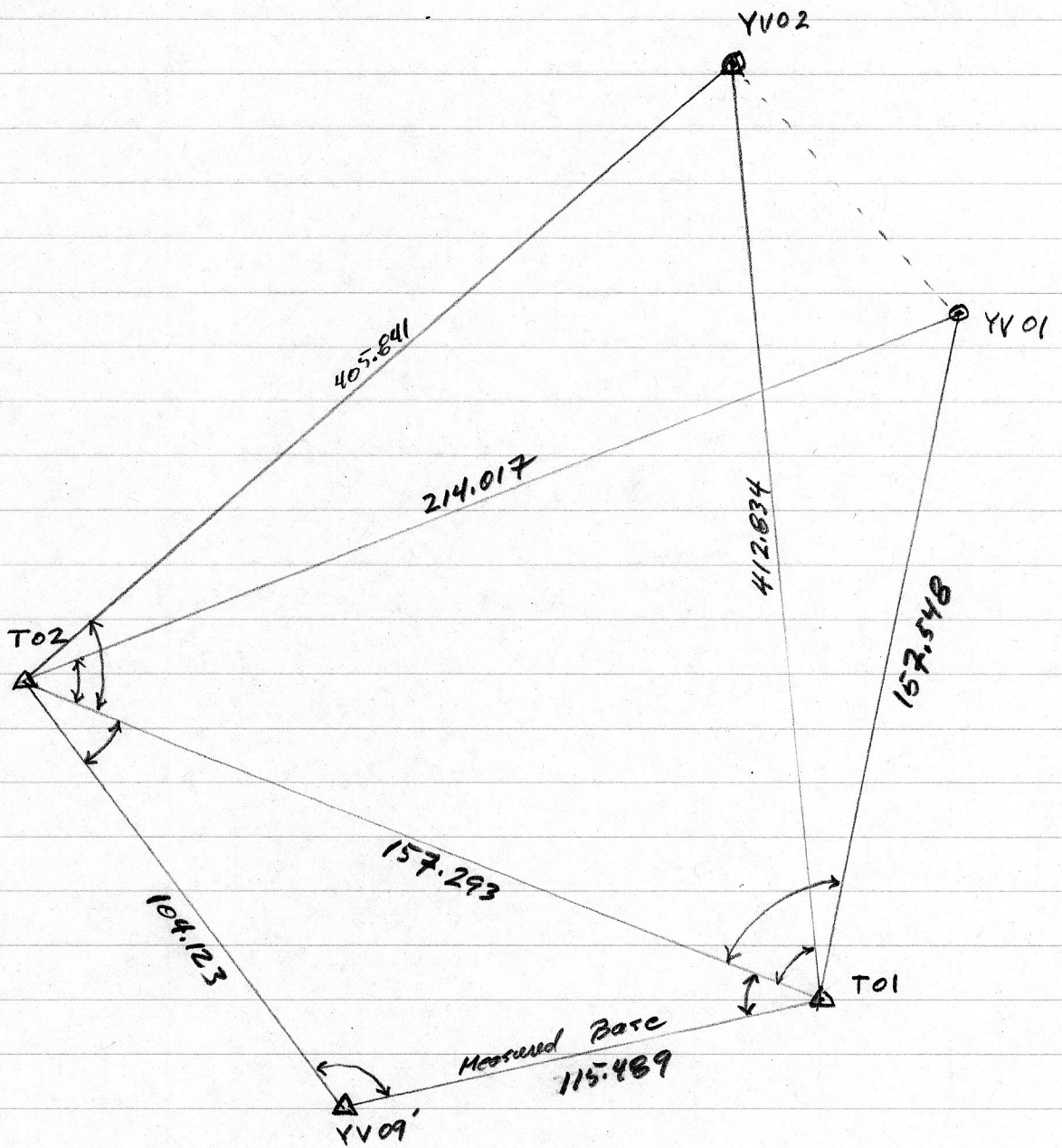


$$b = \frac{a \sin B}{\sin A} = \frac{157.293 \sin 85.650}{\sin 47.125} = 214.017$$

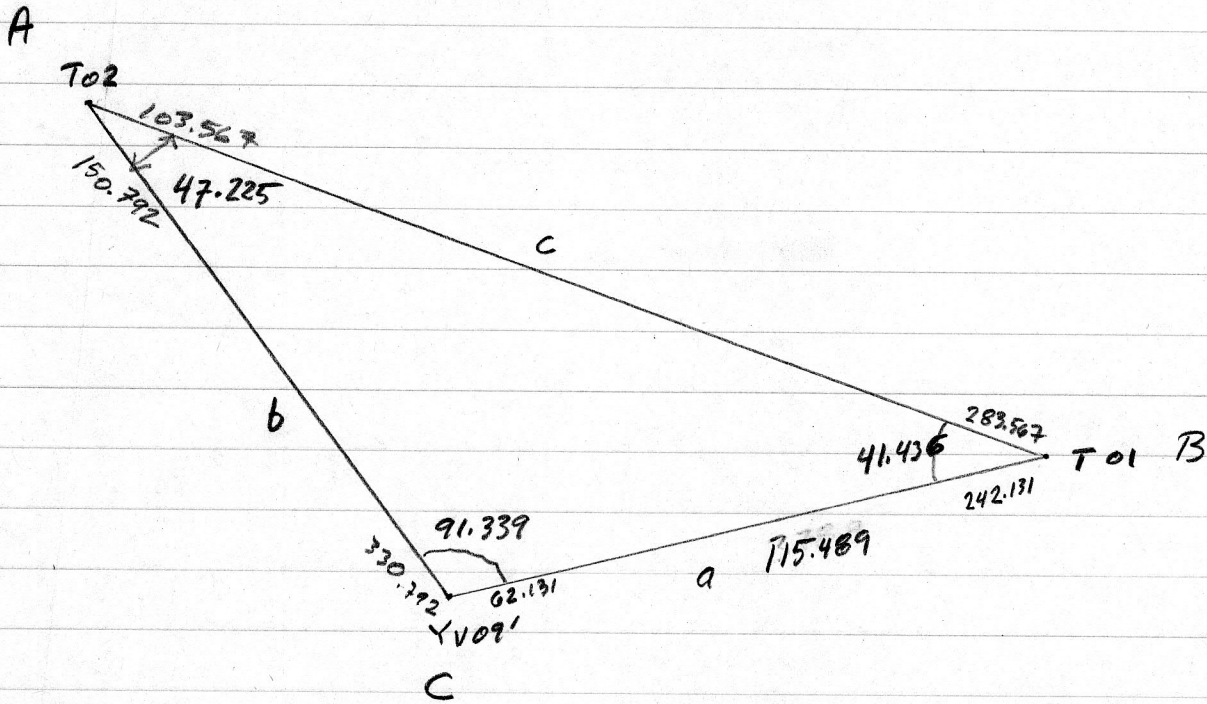
$$c = \frac{a \sin C}{\sin A} = \frac{157.293 \sin 47.225}{\sin 47.125} = 157.548$$



TRIANGULATION



①



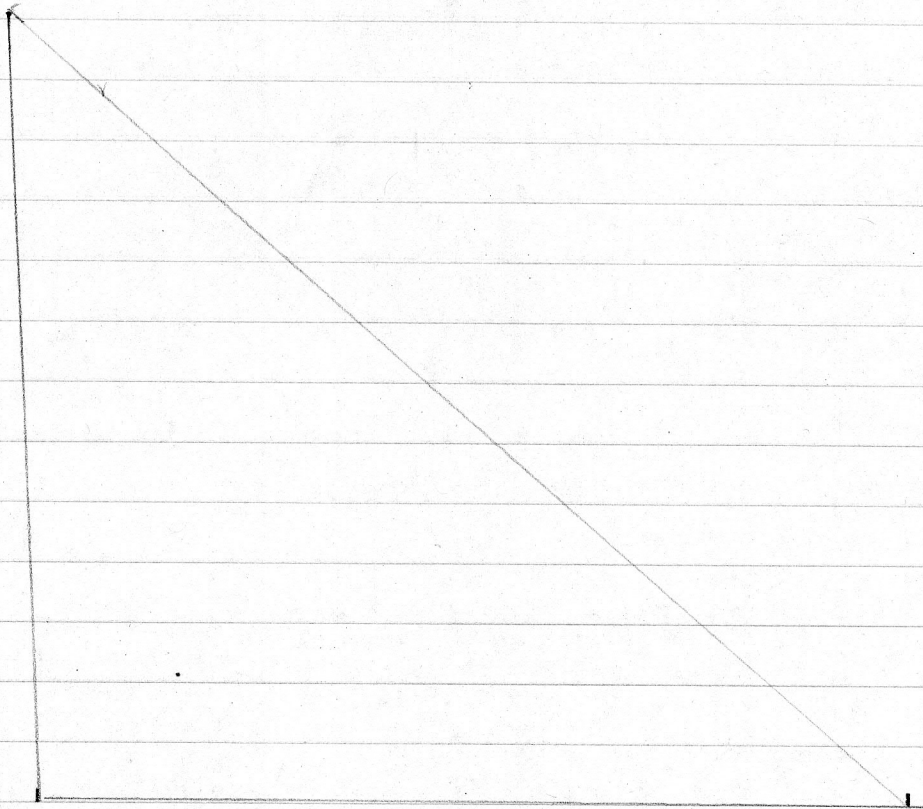
41.436
 91.339
 47.225

 180.000

$$b = \frac{a \sin B}{\sin A} = \frac{115.489 \sin 41.436}{\sin 47.225} = 104.123$$

②

$$c = \frac{a \sin C}{\sin A} = \frac{115.489 \sin 91.339}{\sin 47.225} = 157.293$$



STADIA

est from 1:50,000 TOPO MAP → DATUM

Add
1.27 ↓
El₂

Sta	Sto	Lat.	Dep ¹	El.	HI	Rod	SI _{x100}	Az	V _x	Leat ₂	Dep ₂	El ₂
T04	S-01	282.49	1790.02	1645	4.2	6.7	354	232.08	86.21	216.5	1655.2	1637.4
N	E											
1.5	16.5			1645		5.3	465	222.23	87.06	178.1	1644.7	1637.5
				+1.27								
1.5	16					4.8	569	235.34	86.59	184.7	1597.4	1635.7
1.5	15.5					5.0	688	246.07	86.52	197.8	1548.8	1633.3
2	15.5					5.0	635	260.54	85.14	252.1	1550.2	1628.7
2.25	16.5					4.0	340	253.24	84.41	253.1	1641.6	1635.5
2.5	17					2.0	150	263.31	84.42	277.4	1695.0	1641.5
	T05					2.0	176	309.043	83.21	315.9	1698.9	1639.5
3.25	17.5					2.0	224	5.19	89.55	350.5	1746.3	1645.6
3.5	18					5.0	342	31.34	92.17	371.2	1794.5	1648.9
	T03					3.0	455	83.55	94.04	297.11	1877.23	1655.2
					Check →					297.21	1878.10	
3.25	18.5					5.0	414	60.48	94.01	343.7	1849.6	1653.6
2.25	18.5					5.0	385	109.44	92.51	243.0	1850.2	1650.6
2	18					5.0	267	136.54	90.26	223.1	1795.6	1645.4
1.75	17.5					8.0	270	175.06	88.28	200.6	1747.0	1641.6
1.5	17					5.0	369	202.43	87.11	179.0	1696.7	1639.2

Aug 30 Stadia

T04		282.49	1740.01	1646.27	4.45	9.0						
	518 ✓					9.0	142	132.21	90.55	253.3	1772.0	1645.6
	519					7.0	202	147.14	89.57	230.7	1773.3	1645.4
	520					7.0	251	120.50	91.29	243.3	1805.7	1647.5
	521					8.0	269	131.44	90.24	227.9	1801.2	1645.8
	522					6.0	146	212.46	84.09	245.5	1716.2	1641.3
	523					7.0	379	262.08	84.18	266.8	1626.7	1634.1
D9'	524	296.00	1997.91	1652.35	4.0	9.0	95	284.54	90.54	303.4	1969.9	1651.3
	525					4.0	189	276.34	91.13	302.6	1940.7	1653.6
	526					6.0	192	279.57	91.38	306.1	1940.3	1653.4
	527					8.0	152	312.12	90.13	327.1	1963.6	1651.3
	528					9.0	88	330.05	87.13	319.2	1984.6	1649.5

STADIA ("STAD")

STO	1	2	3	4	5	6	7	8				
At	To	Lat.	Dep.	EL	HI	Red	SIx100	Az	Vx	Lat ₂	Dep ₂	EL ₂
T-02		386.88	1947.10	1655.96	4.0							
	534					8.0	152	234.27	90.47	360.0	1909.4	1655.4
	535					9.0	128	203.00	87.50	351.0	1931.9	1653.0
	536					6.0	138	249.11	91.29	371.9	1907.8	1656.4
	537					7.0	132	254.31	91.30	376.1	1908.4	1656.1
	538					6.0	125	281.50	90.03	394.7	1909.8	1655.4
	539					5.0	120	341.01	79.34	420.3	1935.6	1649.1
	540					7.0	220	329.38 229.38	83.46	444.7	1913.6	1647.8
	541					6.0	176	273.07	90.33	389.8	1893.5	1655.9
	542					7.0	237	262.06	89.46	377.0	1875.5	1654.8
	543					8.0	323	266.31	89.55	380.9	1848.8	1654.6
	544					8.0	307	278.10	88.23	400.2	1854.5	1652.1
	545					8.0	84	142.46	86.12	366.6	1962.5	1653.0

SEPT GEOL FROM T-02

Aug 21 - VIC DRILLING - TRANSIT SURVEY - COMPILATION

uncorrect

DDH

↓

Elev

Sta	Sight	Az decc	Vx decc	Red	H Dist ft	H Dist M	Δ Lat	Δ Dep	SH	LAT(N)	DEP (E)	Elev	
TO1	YV02									350N	2100E	1643.93	
HI=4	YV02	00	-9.667	0 ^{1.22}	Δ	412.83	412.83	0.0	-69.10	762.83	2100E	⊙	
1.22	Camp	24.350	-8.333	0 ^{1.22}	Δ	X							
	YV01	9.217	-10.333	3.0 ^{.30}	Δ	157.55	155.52	25.24	-28.43	505.52	2125.24	⊙	
	YV08	269.150	+1.83	4.0 ⁰	Δ	119.9	36.55	-54	-36.54	+1.2	349.46	2063.46	⊙
	YV09	242.131	+3.308	2.0 ^{.61}	Δ	378.9	115.489	-53.99	-102.09	7.28	296.01	1,997.91	1651.21
	TO2	283.567	+3.608	0 ^{1.22}	Δ	157.29	36.90	-152.90	11.14	386.90	1947.10		
YV09'										296.01	1,997.91	1651.21	
HI=4	TO1	62.191	-3.625	3.0 ^{.30}	Δ	378.9	115.49	53.99	102.09	-7.01	350.00	2100.00	
	TO2	330.792	+1.483	1.0 ^{.91}	Δ	104.12	90.88	-50.81	3.61	386.89	1947.10	1654.82	
	TO3	270.575	+2.100	5.0 ^{.30}	Δ	393.1	119.82	1.20	-119.81	4.09	297.21	1878.10	1655.30
	YV09	3.000	000	5.0 ^{.30}	Δ	4.5	1.37	1.37	.07	-30	297.38	1997.98	⊙
TO2	YV09'									386.90	1947.10	1654.82	
HI=4	YV09'	150.792	-2.783	0 ^{1.22}	Δ	393.1	104.12	-90.88	50.81	3.84	296.02	1997.91	1650.98
	TO1	107.767	-4.558	0 ^{1.22}	Δ	157.29	-36.90	152.90	11.32	350.00	2100.00		
	YV01	56.742	-10.833	0 ^{1.22}	Δ	214.02	118.62	178.14	39.73	505.52	2125.24	⊙	
	YV02	22.173	-11.308	0 ^{1.22}	Δ	405.84	375.93	152.90	79.93	762.83	2100.00	⊙	
TO3										297.21	1878.10	1655.30	
HI=4	YV09'	90.575	-2.267	2.0	Δ	397.1	119.82	-1.20	119.81	4.13			
	TO4	263.917	-4.742	0	Δ	455.6	138.87	-14.72	-138.08	-10.30	282.49	1740.02	1645.3
TO4										282.49	1740.02	1645.0	
HI=4.2	TO3	83.917	3.683	0	Δ	455.6	138.87	14.72	138.08	10.22	297.21	1878.10	1646.27
	YV04	315.525	-6.058	6.0	Δ	37.3	11.37	8.11	-7.97	-1.77	290.60	1732.05	⊙ 1643.2 1644.5
	YV05	208.558	-3.325	2.0	Δ	329.3	100.37	-88.16	-47.98	-5.16	194.33	1692.04	⊙ 1639.8
	YV06	172.275	-6.933	0	Δ	106.7	32.52	-32.23	4.37	-2.67	250.26	1744.39	⊙ 1642.3
	YV07	172.133	-6.833	0	Δ	108.7	33.13	-32.82	4.53	-2.69	249.67	1744.55	⊙ 1642.3

6400

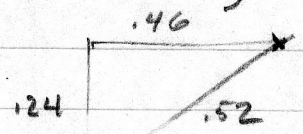
* Arb elev at T01 (from Topo map)

STO → 1 2 3 4 5 6 7 8

AT	To	Lot 1	Dep 1	El 1	H 1	Red	H	A 2	V 2	Lot 2	Dep 2	El 2
T01	D9'	350	2100	1645*	4.2	2.0'	378.9	242.073	93.183	296.00	1997.91	1652.35
D9'	T03	296.00	1997.91	1654.55	4.2	5.0	393.1	270.343	92.06	297.20	1878.10	1656.50
T03	T04	297.2	1878.1	1657.9	4.2	0	455.6	263.55	85.153	282.49	1740.01	1646.27
T04	T06	282.49	1740.01	1651.86	4.1	0	386.0	195.384	87.04	169.19	1708.29	1641.50
T06	T07	169.19			4.35	0	409.1	109.160	88.180	128.05	1826.00	1639.13
T07	T08				4.5	0	461.9	85.542	93.302	138.10	1966.42	1649.14
T08	T09				4.45	0	464.6	79.262	94.342	164.05	2105.64	1661.82
T09	T10				4.30	0	189.4	29.422	89.17	214.20	2134.24	1662.41
T10	T01				4.15	1.0	459.1	345.382	82.290	349.76	2099.54	1645.20
										350.00	2100.00	
T04	D10	282.49	1740.01	1646.27	4.2	0	191.8	178.732	87.23	224.05	1741.51	1644.88
	D11				4.1	0	320.1	241.362	84.48	236.14	1654.15	1638.64
	D12				4.45	3.0	310.5	150.163	89.00	200.28	1786.89	1645.06
	T5				4.2	0	175.3	307.043	82.413	314.70	1697.38	1640.70
	D11fs				4.45	0	296.3	255.16	83.59	259.52	1652.67	1638.11
	D12fs				4.45	0	194.0	126.42	89.43	245.52	1786.16	1647.33

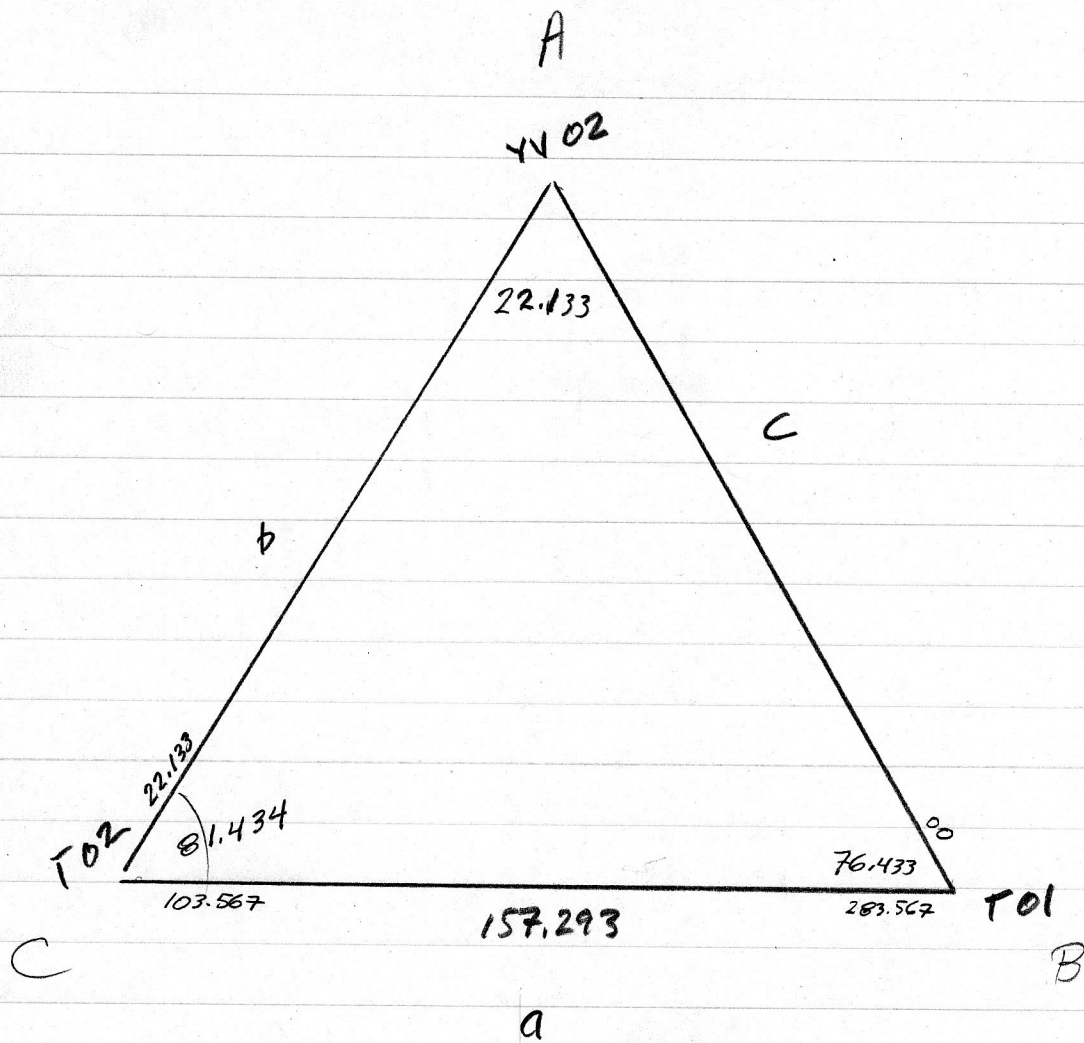
Closed transit survey - Vic Claims

2 closure 10 sec
 Lin closure lat .24 m
 dep .46 m } .52 m



		Lot 1	Dep 1	El 1	H 1	Red	H	A 2	V 2	Lot 2	Dep 2	El 2
D9'	D13	296.00	1997.91	1652.35	4.0	0	177.7	180.53	90.22	272.32	1997.54	1653.72
	D14					0	240.2	180.343	92.10	222.79	1997.18	1656.34
	D15					0	183.3	243.49	92.11	271.35	1947.77	1655.70
	D16					0.5	177.7	113.24	90.12	274.49	2047.62	1653.61
T01	T11	350	2100	1645	3.7	0	286.1	344.343	81.03	434.06	2076.81	1632.39
T11	D-17	434.06	2076.81	1632.39	4.0	0	173.2	113.37	90.47	412.97	2125.20	1634.33
	D-01					0	287.2	34.383	79.18	506.08	2126.57	1617.07
D9'	T02	296.00	1997.91	1652.35	4.0	1.0	341.61	330.473	91.29	386.88	1947.10	1655.96
T11	D-18	434.06	2076.81	1632.39	4.0	0	64.5	197.37	95.59	415.29	2070.85	1635.67

3



$$b = \frac{a \sin B}{\sin A} = \frac{157.293 \cdot \sin 76.433}{\sin 22.133} = 405.841$$

$$c = \frac{a \sin C}{\sin A} = (\quad) \sin 81.434 = 412.834$$

DATA INPUT

Program "TRAN"

1 Lbl "TRAN"

2 Rel 07 $\left[\begin{array}{l} xco \\ \alpha \\ HR \\ \alpha \end{array} \right.$

3 HR

4 Sto 07

5 Rel 08

6 HR $\alpha = DMS \text{ to Dec Deg}$

7 90

8 -

9 Sto 08 (Vert \times Dec $^{\circ} \pm$)

10 Rel 06

11 Rel 14 } ft \rightarrow m

12 x

13 Sto 06 - H in meters

14 Rel 07

15 Rel 06

16 \square P \rightarrow R

17 Sto 09 (Δ Lat)

18 $x \div y$

19 Sto 10 (Δ dep)

20 Rel 01

21 Rel 09

22 +

23 R/s Display Lat 2

24 Rel 02

25 Rel 10

26 +

27 R/s Display Dep 2

28 Rel 08 \sqrt{x} dec.

29 Tan

30 Rel 06 H

31 x Δ H ft

32 Rel 03 Stall EL 2

33 + Stall

34 Sto 11

35 Rel 04

36 Rel 05

37 -

38 Rel 14. Display EL 2

39 x

40 Rel 11

41 +

42 Sto 11

STA 1	STORE
Lat 1 M	01
Dep 1 M	02
EL 1 M	03
HI ft	04
SIGHT ON STA 2	
ROD Reading ft	05
HOR DIST ft	06
Az DMS	07
V \times DMS ($H_{\alpha} = 90^{\circ}$)	08

Storage reg 14 has
ft \rightarrow m conversion factor

Stadia sight from T04 - Aug 26 HI = 4.2 ft

Sta	Az	Vs	Red	SI	Hs	Vs	ΔV	ΔLat	ΔDep	Lat	Dep
DDH 10	178.53	-2.62	0.0	3.54	191.8	8.8	-8.8				
S.01	232.13	-3.65	6.7	3.54	353.2	-22.5	-25.0	216.43	278.32	66.06 96.75	1461.70 1744.94
S.02	222.38	-2.90	5.3	4.65	464.8	-23.5	-24.6				
S.03	235.57	-3.02	4.8	5.69	567	-29.9	-30.5				
S.04	246.12	-3.13	5.0	6.88	686	-37.5	-38.3				
S.05	260.90	-4.77	5.0	6.35	631	-52.6	-53.4				
S.06	253.40	-5.32	4.0	3.40	337	-31.4	-31.2				
S.07	263.52	-5.30	2.0	1.50	149	-13.8	-11.6				
T05	307.08	-7.31	0.0		175.3						
T05s	^{307.043} 307.08	-6.65	2.0	1.76	174	-20.2	-18.0	104.91	-138.82	387.40	1601.20
S.08	05.32	-0.08	2.0	2.24	224	-0.3	+1.90				
S.09	31.57	+2.28	5.0	3.42	341	+13.6	+12.8				
T03	83.92	+4.07	3.0	4.55	453	+32.2	+31.0	48	450.5	330.5	2190.5
S.10	60.80	+4.02	5.0	4.14	412	+28.9	+28.1				
S.11	109.73	+2.85	5.0	3.85	384	+19.1	+18.3				
S.12	136.90	+0.43	5.0	2.67	267	+2.0	+1.2				
S.13	175.10	-1.53	8.0	2.70	267	-7.1	-10.9				
S.14	202.72	-2.82	5.0	3.69	368	-18.1	-18.9				

5.7
2.5