JAN 22 1964

Syndicate I

BARRINGER RESEARCH LIMITED

145 BELFIELD ROAD
REXDALE, TORONTO
ONTARIO, CANADA
PHONE: CH. 7-2193
CABLE: BARESEARCH

January 21, 1964

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|---|---|---|
| | W.S.R. | |
| | K.C.G. | |
| | R.D.S. | |
| | B.C.B. | |
| ✓ | P.M.K. | ✓ |
| | G.W.M. | |
| | H.A.P. | |
| | C.K.W. | |
| | J.B.S. | |
| | C.P.R. | |
| | E.L.D. | |
| | J.I.B. | |
| | E.C.J. | |
| | D.V.B. | |
| | | |

Dr. A.E. Aho
Canex Aerial Explorations and
Silver Titan Project
328 Marine Building
355 Burrard Street
Vancouver 1, British Columbia

Re: Titan Project

Dear Aaro:

Attached are the results of soil and silt analyses from the Mayo area and comments.

I would recommend that any further mercury analyses be deferred until interferences can be eliminated. I would appreciate an okay from you before proceeding with a few trial analyses, as suggested in the attached resume.

I personally feel that the drainage reconnaissance prospecting technique has merit and I would suggest a continuation of this programme. Follow-up procedures, however, have not yet been established and consideration should be given to obtaining expert advice on the development of optimum techniques. I consider that laboratory controlled analyses are superior to field techniques in that they provide a sharper pictures.

With regard to soil geochemistry, I do not anticipate any particular difficulty in the freely drained soil areas. However, orientation studies are still required for the peat-bog areas, so let's hope that Area A proves to be amenable! Again the results suggest that laboratory analyses are preferable to field methods.

Once again I sincerely apologize for the delays caused by unavoidable laboratory down-time.

Yours sincerely,

BARRINGER RESEARCH LIMITED

D. Richard Clews

DRC/mc
Encl.

# MAYO-SILVER TITAN PROJECT

The undersigned suggested (October 7, 1963) that all stream sediment samples be analyzed for three forms of leachable copper, lead, and zinc, in order to determine (1) the most suitable analytical methods for the area and (2) the distribution pattern of the various forms of metals. It was also indicated that upon completion of the analytical programme, an interpretation and suggestions for follow-up work would be provided.

Sixty sediment samples representative of varying conditions in the area were analyzed. The number of samples (results attached) are too few to determine statistical threshold by calculation and as the geology, location, and type of mineralization is unknown the determination of threshold by inespection of the data cannot be too precise. It is therefore tentatively suggested that threshold of (i) CxHClCu is 8-10 ppm (ii) HCl-Cu is greater than or equal to 24 ppm (iii) CxZn is greater than or equal to 9 ppm and (iv) CxHClZn is greater than or equal to 25 ppm. The analytical techniques for CxCu, HClZn, CxPb, CxHClPb and HClPb appear to have little merit for stream sediments in the area sampled.

The coverage is too unsystematic to comment in detail on interpretive criteria, but the following few comments will indicate the type of information that could be obtained by a systematic sample coverage and comprehensive multi-metal analyses.

(a) POLI CREEK -

It will be noted that the values are all of the same order, suggesting a source along the stream course or in the upper catchment area. The results from streams H9, Gerlitski and E. Laysier indicate a possible source or sources of metal in the divide between H9 and Gerlitski. A further possible source is situated in the lower reaches of the E. Laysier and Gerlitski Creeks. The results from the H3 and H4 Creeks are essentially negative unless considerably stronger evidence of mineralization is obtained from the H2 and H5 Creeks.

These results would suggest that reconnaissance stream prospecting is a potent tool in this area for locating areas of potential mineralization. This technique would eliminate barren areas and focus attention on the areas of possible interest. These analytical techniques, which are laboratory procedures, appear to be considerably more definitive ("sharper") and reliable than the heavy metal field technique. Thus, for example, the results from the field heavy metal method fully justified the U.R. soil grid sampling. However, if follow-up had been planned from the Lab. results procedures would have entailed completing the drainage reconnaissance prior to deciding whether soil sampling was justified. Similarly sampling and analyses of all the drainages surrounding the H9, H10 Laysier and Gerlitski Creeks should be complete before follow-up procedures are planned.

Incidentally, the U.R. soil grid results (attached) do not indicate any areas of potential geochemical interest. The samples were analyzed for total and 3 forms of leachable Cu, Pb, and Zn.

(b) AREA A -

It was suggested that the soil samples from Area A be quantitatively analyzed for Cx, Cu, Pb and Zn in order to determine precisely the surface distribution pattern of the leachable metals. Total analyses were suggested to provide ratio data which could prove to be valuable in the interpretation when related to topography. No apparent relationship between the ratio data and the distribution pattern of Cx metal is obvious, but the writer cannot be sure of this until the topographic information is available. For instance, it is possible that the apparently confusing results on the northwest ends of lines E10 and E12 may in part be related to these factors.

Assuming that the data do not reflect a hydromorphic accumulation of metals related to topography or other similar effects, it is tentatively suggested that the axis of a zone of interest striking NE - SW is located at E4/1+50; E6/2+00 and 2+50; E8/2+00 and 2+50; E10/3+00 and 4+00; E12/4+00 and 4+50. Similarly the anomalies located on E8 (5+00 to 5+20); E9 (5+00 and 5+50); E10 (5+00, 6+00, 6+50 and 8+00); E12 (6+00, 6+50, 7+00, and 8+00) could be related to smaller NE - SW striking zones of possible interest. It will be noted that the latter zones do not appear to continue southwestwards beyond station E5/5+00.

SUGGESTIONS -

It is suggested that the remaining stream sediment samples which have been collected be analyzed for CxHClCu, HClCu, CxZn, CxHClZn before follow-up work is planned. Further regional drainage reconnaissance samples should also be analyzed by the same methods. It will be realized that these techniques point only to the general area within which economic mineralization may occur. Follow-up techniques which will locate the source of the anomalous metal have not yet been devised. No particular follow-up difficulty is expected in the freely drained soil areas provided the procedures are established by an experienced geologist well versed in the application of geochemical, photogeological and geophysical techniques. Follow-up techniques for the valley areas (e.g. Area A) still require basic orientation studies.

The undersigned has lost confidence in the Lemaire mercury detector due to its susceptibility to major interferences from organic and cyclic compounds. No repeat Hg analyses have therefore been attempted. Barringer Research Limited will have a laboratory instrument, without the above limitations, operative during February. It is therefore suggested that the samples from lines E8 & E10 be analyzed in order to determine the true distribution pattern of mercury. If these results are encouraging further analyses can be done.

D. Richard Clews.

DRC/mc
January 21/64.

SILVER TITAN PROJECT
MAYO - YUKON
GALENA HILL - AREA "A"
SOIL SAMPLES

| | SAMPLE NUMBER | CxCu ppm | Total Cu ppm | CxZn ppm | Total Zn ppm | Cx-Pb ppm | Total Pb ppm |
|---|---|---|---|---|---|---|---|
| AREA "A" | E2-1+50 | 6.8 | 49.0 | 11.0 | 180 | 6.0 | 20.0 |
| | 2+00 | 5.6 | 32.0 | 15.0 | 140 | 5.0 | 20.0 |
| | 2+50 | 7.2 | 40.0 | 17.0 | 140 | 5.0 | 20.0 |
| | 3+00 | 5.0 | 32.0 | 9.0 | 150 | 6.0 | 20.0 |
| | 3+50 | 5.2 | 40.0 | 10.0 | 160 | 5.6 | 30.0 |
| | 4+00 | 7.2 | 40.0 | 17.0 | 140 | 4.8 | 25.0 |
| | 4+50 | 5.6 | 56.0 | 11.0 | 200 | 8.0 | 25.0 |
| | 5+00 | 9.0 | 48.0 | 7.5 | 120 | 4.0 | 20.0 |
| | 5+50 | 7.2 | 40.0 | 12.5 | 150 | 6.0 | 25.0 |
| | 6+00 | 8.4 | 44.0 | 5.0 | 160 | 2.0 | 25.0 |
| | 6+50 | 5.0 | 32.0 | 10.0 | 120 | 6.0 | 40.0 |
| | 7+00 | 5.0 | 48.0 | 18.0 | 150 | 2.0 | 25.0 |
| | E4-1+50 | 16.0 | 40.0 | 22.0 | 180 | 4.4 | 25.0 |
| | 2+00 | 5.6 | 32.0 | 12.0 | 110 | 4.2 | 25.0 |
| | 2+50 | 7.2 | 40.0 | 13.0 | 140 | 4.4 | 30.0 |
| | 3+00 | 8.0 | 40.0 | 10.0 | 120 | 3.6 | 25.0 |
| | 3+50 | 5.6 | 40.0 | 17.0 | 150 | 5.2 | 30.0 |
| | 4+00 | 4.8 | 40.0 | 12.0 | 120 | 4.0 | 20.0 |
| | 4+50 | 6.8 | 48.0 | 13.0 | 150 | 3.2 | 20.0 |
| | 5+00 | 5.0 | 48.0 | 6.0 | 100 | 4.0 | 25.0 |
| | 5+50 | 6.4 | 40.0 | 12.5 | 180 | 3.6 | 25.0 |
| | 6+00 | 8.4 | 48.0 | 30.0 | 240 | <.2 | 5.0 |
| | 6+50 | 4.0 | 32.0 | 15.0 | 150 | <.2 | 5.0 |
| | 7+00 | 4.4 | 32.0 | 8.0 | 120 | 8.4 | 20.0 |
| | E6-2+00 | 5.0 | 40.0 | 20.0 | 220 | 4.0 | 20.0 |
| | 2+50 | 4.0 | 40.0 | 18.0 | 200 | 4.0 | 25.0 |
| | 3+00 | 6.0 | 40.0 | 17.0 | 160 | .4 | 10.0 |
| | 3+50 | 4.4 | 32.0 | 12.0 | 150 | .4 | 10.0 |
| | 4+00 | 4.8 | 40.0 | 8.0 | 120 | 4.4 | 20.0 |
| | 4+50 | 6.8 | 56.0 | 12.0 | 140 | 4.0 | 25.0 |
| | 5+00 | 3.0 | 16.0 | 3.0 | 100 | 2.0 | 10.0 |
| | 5+50 | 3.2 | 20.0 | 10.0 | 110 | 4.0 | 10.0 |
| | 6+00 | 7.0 | 32.0 | 13.0 | 140 | 5.0 | 15.0 |
| | 6+50 | 4.0 | 24.0 | 11.0 | 120 | <.2 | 5.0 |
| | 7+00 | 6.4 | 56.0 | 13.0 | 120 | .2 | 20.0 |
| | 7+50 | 7.0 | 48.0 | 10.5 | 150 | .4 | 25.0 |
| | E7-4+00 | 6.4 | 48.0 | 7.0 | 160 | .8 | 25.0 |
| | 4+10 | 4.0 | 24.0 | 11.0 | 150 | .4 | 10.0 |
| | 4+20 | 6.0 | 40.0 | 13.0 | 180 | .8 | 20.0 |
| | 4+30 | 8.4 | 40.0 | 15.0 | 180 | 1.6 | 25.0 |
| | 4+40 | 6.0 | 32.0 | 12.0 | 150 | .4 | 20.0 |
| | 4+50 | 7.2 | 56.0 | 17.0 | 160 | .4 | 25.0 |
| | 4+60 | 6.8 | 40.0 | 17.0 | 160 | .4 | 25.0 |
| | 4+70 | 4.0 | 40.0 | 12.0 | 120 | .6 | 20.0 |
| | 4+80 | 4.4 | 40.0 | 12.0 | 120 | 1.6 | 20.0 |
| | 4+90 | 5.2 | 32.0 | 15.0 | 140 | 1.6 | 20.0 |
| | 5+00 | 5.2 | 40.0 | 15.0 | 140 | 2.0 | 25.0 |

NO. I (continued) - January 20/64

| SAMPLE NUMBER | CxCu ppm | Total Cu ppm | CxZn ppm | Total Zn ppm | Cx-Pb ppm | Total Pb ppm |
|---|---|---|---|---|---|---|
| E7-5+10 | 5.0 | 32.0 | 13.0 | 110 | 1.6 | 25.0 |
| 5+20 | 3.2 | 24.0 | 5.0 | 100 | 2.4 | 20.0 |
| 5+30 | 4.8 | 48.0 | 6.0 | 110 | 2.0 | 20.0 |
| 5+40 | 5.2 | 40.0 | 10.0 | 100 | 2.8 | 20.0 |
| E8-2+00 | 5.0 | 40.0 | 18.0 | 160 | 3.2 | 25.0 |
| 2+50 | 7.0 | 32.0 | 18.0 | 120 | .2 | 10.0 |
| 3+00 | 4.0 | 40.0 | 10.0 | 140 | .4 | 20.0 |
| 3+50 | 5.6 | 32.0 | 14.0 | 160 | .2 | 25.0 |
| 4+00 | 5.2 | 56.0 | 15.0 | 120 | .4 | 15.0 |
| 4+30 | 4.0 | 40.0 | 14.0 | 120 | .8 | 10.0 |
| 4+40 | 4.0 | 24.0 | 13.0 | 140 | 1.0 | 20.0 |
| 4+50 (Rusty) | 2.8 | 8.0 | 17.5 | 200 | .2 | 10.0 |
| 4+50 | 2.4 | 24.0 | 6.0 | 100 | .4 | 15.0 |
| 4+60 | 5.6 | 40.0 | 14.0 | 200 | 3.0 | 10.0 |
| 4+70 | 2.4 | 40.0 | 6.0 | 140 | 10.0 | 25.0 |
| 4+80 | 3.0 | 24.0 | 7.5 | 160 | 9.6 | 20.0 |
| 4+90 | 3.0 | 40.0 | 15.0 | 160 | 12.0 | 25.0 |
| 5+00 | 6.0 | 48.0 | 20.0 | 150 | 11.0 | 20.0 |
| 5+00 | 5.2 | 48.0 | 20.0 | 180 | 7.0 | 20.0 |
| 5+10 | 2.4 | 24.0 | 6.0 | 140 | 4.0 | 20.0 |
| 5+20 | 7.2 | 48.0 | 20.0 | 110 | 3.0 | 25.0 |
| 5+30 | 4.0 | 24.0 | 10.0 | 110 | 3.6 | 20.0 |
| 5+40 | 5.0 | 40.0 | 6.0 | 120 | .4 | 10.0 |
| 5+50 | 5.2 | 32.0 | 6.0 | 110 | .4 | 10.0 |
| 5+50 | 5.0 | 32.0 | 15.0 | 120 | .8 | 10.0 |
| 5+60 | 4.4 | 32.0 | 17.5 | 160 | .4 | 10.0 |
| 5+70 | 7.0 | 24.0 | 7.0 | 120 | .8 | 20.0 |
| 6+00 | 5.6 | 40.0 | 6.0 | 140 | .8 | 20.0 |
| 6+50 | 5.0 | 40.0 | 16.0 | 140 | 1.0 | 20.0 |
| 7+00 | 6.4 | 48.0 | 11.0 | 150 | 1.0 | 20.0 |
| 7+50 | 6.0 | 32.0 | 12.0 | 120 | 1.6 | 25.0 |
| E9-4+60 | 7.6 | 32.0 | 12.0 | 140 | .8 | 20.0 |
| 4+70 | 4.0 | 48.0 | 8.0 | 150 | .8 | 25.0 |
| 4+80 | 7.0 | 48.0 | 15.0 | 160 | .4 | 15.0 |
| 4+90 | 4.0 | 24.0 | 10.0 | 110 | .8 | 25.0 |
| 5+00 | 4.4 | 40.0 | 22.0 | 200 | .8 | 25.0 |
| 5+10 | 5.5 | 24.0 | 9.0 | 120 | 3.0 | 25.0 |
| 5+20 | 6.0 | 32.0 | 12.0 | 140 | 2.0 | 25.0 |
| 5+30 | 4.4 | 32.0 | 14.0 | 150 | 4.4 | 20.0 |
| 5+40 | 4.0 | 24.0 | 17.0 | 150 | 1.0 | 20.0 |
| 5+50 | 8.0 | 48.0 | 22.0 | 240 | .2 | 5.0 |
| 5+60 | 6.8 | 32.0 | 10.0 | 140 | 2.0 | 10.0 |
| 5+70 | 4.0 | 32.0 | 11.0 | 120 | 2.0 | 5.0 |
| 5+80 | 5.2 | 40.0 | 11.0 | 140 | 3.0 | 10.0 |
| 5+90 | 4.8 | 32.0 | 3.0 | 120 | 2.0 | 5.0 |
| 6+00 | 3.6 | 40.0 | 10.0 | 150 | .2 | 10.0 |
| E10-2+50 | 4.4 | 40.0 | 10.0 | 160 | .8 | 20.0 |
| 3+00 | 6.0 | 20.0 | 26.0 | 240 | .6 | 15.0 |
| 3+50 | 4.8 | 20.0 | 7.0 | 150 | .4 | 20.0 |
| 4+00 | 40.0 | 120.0 | 34.0 | 280 | .4 | 10.0 |
| 4+50 | 5.2 | 24.0 | 8.0 | 150 | .8 | 10.0 |
| 5+00 | 16.0 | 64.0 | 18.0 | 180 | .4 | 5.0 |
| 5+50 | 6.4 | 32.0 | 15.0 | 150 | .8 | 15.0 |
| 6+00 | 16.8 | 72.0 | 24.0 | 180 | .8 | 10.0 |

NO. I - (continued) - January 20/64

| SAMPLE NUMBER | CxCu ppm | Total Cu ppm | CxZn ppm | Total Zn ppm | Cx-Pb ppm | Total Pb ppm |
|---|---|---|---|---|---|---|
| E10-6+50 | 12.8 | 40.0 | 16.0 | 160 | .8 | 15.0 |
| 7+00 | 5.0 | 48.0 | 15.0 | 140 | .8 | 15.0 |
| 7+50 | 4.0 | 24.0 | 12.5 | 100 | 2.0 | 10.0 |
| 8+00 | 7.0 | 56.0 | 24.0 | 120 | 3.0 | 10.0 |
| E12-2+50 | 6.8 | 32.0 | 7.5 | 140 | 1.0 | 5.0 |
| 3+00 | 9.0 | 48.0 | 10.0 | 160 | 1.0 | 25.0 |
| 3+50 | 4.0 | 20.0 | 8.0 | 110 | 4.0 | 15.0 |
| 4+00 | 3.6 | 16.0 | 25.0 | 120 | 1.0 | 10.0 |
| 4+50 | 6.0 | 20.0 | 25.0 | 140 | 2.0 | 10.0 |
| 5+50 | 5.2 | 24.0 | 17.0 | 140 | 3.0 | 20.0 |
| 6+00 | 6.0 | 64.0 | 20.0 | 200 | 4.0 | 20.0 |
| 6+50 | 6.8 | 24.0 | 25.0 | 220 | 3.2 | 15.0 |
| 7+00 | 5.6 | 48.0 | 22.0 | 180 | 3.0 | 10.0 |
| 7+50 | 4.4 | 20.0 | 11.0 | 120 | 4.0 | 20.0 |
| 8+00 | 6.4 | 20.0 | 32.0 | 200 | 1.0 | 20.0 |

NO. 1 - Jan. 20/64

SILV TITAN PROJECT
MA.. - YUKON
GRID SAMPLES

| SAMPLE NUMBER | CxCu ppm | Cx-HC1Cu ppm | HC1-Cu ppm | Total Cu ppm | Cx-Zn ppm | Cx-HC1-Zn ppm | HC1-Zn ppm | Total Zn ppm | Cx-Pb ppm | Total Pb ppm |
|---|---|---|---|---|---|---|---|---|---|---|
| UR74-BL | 5.0 | 14.0 | 38 | 40 | 3.0 | 18 | 100 | 140 | 4.0 | 40.0 |
| " "-0+50E | 6.8 | 16.8 | 36 | 40 | 5.0 | 20 | 110 | 140 | 6.0 | 30.0 |
| 1+00E | 4.8 | 15.2 | 38 | 40 | 4.0 | 20 | 100 | 140 | 5.0 | 35.0 |
| 1+50E | 6.4 | 16.0 | 50 | 56 | 3.0 | 16 | 110 | 150 | 4.0 | 37.5 |
| 2+00E | 6.0 | 14.0 | 40 | 64 | 4.0 | 16 | 110 | 160 | 3.0 | 45.0 |
| 2+50E | 1.0 | 7.0 | 30 | 56 | 2.5 | 14 | 100 | 140 | 5.0 | 40.0 |
| 3+00E | 1.0 | 8.0 | 30 | 40 | 2.0 | 6 | 90 | 150 | 5.0 | 50.0 |
| 3+50E | 4.4 | 14.0 | 50 | 72 | 6.0 | 18 | 120 | 150 | 4.0 | 55.0 |
| 4+00E | 2.8 | 4.0 | 18 | 20 | 5.0 | 18 | 80 | 100 | 3.0 | 40.0 |
| UR76-BL | 6.0 | 14.0 | 36 | 40 | 3.0 | 16 | 90 | 120 | 2.5 | 50.0 |
| " " -0+50E | 4.4 | 9.2 | 26 | 28 | 2.5 | 16 | 80 | 120 | 3.0 | 40.0 |
| 1+00E | 6.0 | 12.8 | 30 | 32 | 6.0 | 18 | 90 | 120 | 5.0 | 50.0 |
| 1+50E | 8.0 | 16.8 | 40 | 40 | 3.0 | 15 | 90 | 120 | 4.0 | 45.0 |
| 2+00E | 7.4 | 19.2 | 50 | 60 | 4.0 | 16 | 105 | 120 | 4.0 | 70.0 |
| 2+50E | 1.6 | 11.2 | 40 | 40 | 3.0 | 18 | 110 | 150 | 5.0 | 65.0 |
| 3+00E | 14.4 | 17.6 | 52 | 72 | 6.0 | 16 | 80 | 120 | 4.0 | 40.0 |
| 3+50E | 1.2 | 8.0 | 34 | 32 | 3.0 | 15 | 100 | 120 | 5.0 | 40.0 |
| 4+00E | 5.2 | 8.8 | 32 | 32 | 4.0 | 20 | 120 | 150 | 3.0 | 37.5 |
| UR78-BL | 6.4 | 13.6 | 40 | 56 | 6.0 | 20 | 100 | 120 | 2.5 | 45.0 |
| " "-0+50E | 3.6 | 8.0 | 20 | 20 | 6.0 | 15 | 70 | 100 | 2.5 | 40.0 |
| 1+00E | 5.0 | 8.4 | 24 | 32 | 7.0 | 15 | 80 | 100 | 2.0 | 45.0 |
| 1+50E | 6.0 | 13.6 | 44 | 48 | 6.0 | 18 | 120 | 150 | 3.0 | 70.0 |
| 2+00E | 3.0 | 4.8 | 22 | 24 | 6.0 | 18 | 80 | 120 | 6.0 | 65.0 |
| 2+50E | 4.0 | 7.0 | 22 | 40 | 5.0 | 20 | 90 | 140 | 5.0 | 55.0 |
| 3+00E | 2.0 | 6.0 | 25 | 24 | 3.0 | 15 | 80 | 100 | 5.0 | 65.0 |
| 3+50E | 4.0 | 8.0 | 32 | 60 | 5.0 | 18 | 100 | 140 | 4.0 | 62.5 |
| 4+00E | 2.0 | 7.6 | 22 | 24 | 2.5 | 18 | 80 | 110 | 6.0 | 75.0 |
| UR-80-BL | 6.8 | 13.6 | 28 | 32 | 4.0 | 18 | 90 | 120 | 3.0 | 40.0 |
| " "-0+50E | 2.0 | 8.0 | 21 | 20 | 3.0 | 14 | 80 | 120 | 5.0 | 50.0 |
| 1+00E | 3.0 | 10.4 | 25 | 24 | 2.5 | 18 | 100 | 120 | 4.0 | 65.0 |
| 1+50E | 2.4 | 6.4 | 21 | 20 | 2.5 | 15 | 85 | 120 | 5.0 | 105.0 |
| 2+00E | 3.0 | 5.2 | 24 | 24 | 3.0 | 16 | 90 | 120 | 6.0 | 75.0 |
| 2+50E | 4.0 | 6.4 | 28 | 24 | 4.0 | 20 | 100 | 140 | 5.0 | 60.0 |
| 3+00E | 5.6 | 8.0 | 27 | 32 | 7.0 | 30 | 120 | 150 | 4.0 | 45.0 |
| 3+50E | 1.0 | 4.0 | 36 | 40 | 3.0 | 30 | 120 | 150 | 5.0 | 65.0 |
| 4+00E | 1.2 | 4.0 | 45 | 40 | 2.5 | 12 | 120 | 140 | 4.0 | 87.5 |
| 4+50E | 4.8 | 12.0 | 45 | 48 | 5.0 | 16 | 110 | 160 | 5.0 | 87.5 |
| UR-82-BL | 9.2 | 15.2 | 35 | 32 | 5.0 | 15 | 75 | 120 | 4.0 | 95.0 |
| " "-0+50E | 7.0 | 13.6 | 34 | 32 | 3.0 | 16 | 90 | 120 | 5.0 | 75.0 |
| 1+00E | 3.0 | 8.4 | 35 | 40 | 2.0 | 12 | 110 | 120 | 2.5 | 90.0 |
| 1+50E | 4.8 | 12.8 | 46 | 48 | 2.5 | 18 | 140 | 150 | 5.0 | 75.0 |
| 2+00E | 8.0 | 15.2 | 45 | 40 | 4.0 | 20 | 140 | 150 | 5.0 | 80.0 |
| UR-82-2+50E | 2.8 | 7.2 | 20 | 20 | 4.0 | 18 | 90 | 140 | 6.0 | 87.5 |
| 3+00E | 3.0 | 7.0 | 16 | 16 | 3.0 | 15 | 70 | 100 | 5.0 | 70.0 |
| 3+50E | 4.0 | 8.0 | 30 | 32 | 3.0 | 15 | 110 | 140 | 4.0 | 75.0 |
| 4+00E | 3.6 | 10.0 | 28 | 24 | 2.5 | 12 | 90 | 120 | 2.5 | 60.0 |
| 4+50E | 3.0 | 6.8 | 16 | 20 | 3.0 | 12 | 85 | 120 | 5.0 | 85.0 |
| 5+00E | 2.4 | 8.0 | 34 | 40 | 3.0 | 12 | 90 | 140 | 4.0 | 87.5 |

NO. I - January 20/64

| SAMPLE NUMBER | CxCu ppm | Cx-HClCu ppm | HCl-Cu ppm | Total Cu ppm | Cx-Zn ppm | Cx-HCl-Zn ppm | HCl-Zn ppm | Total Zn ppm | Cx-Pb ppm | Total Pb ppm |
|---|---|---|---|---|---|---|---|---|---|---|
| UR-84-BL | 2.4 | 4.0 | 12 | 12 | 2.0 | 12 | 55 | 100 | 2.5 | 80.0 |
| -0+50E | 14.0 | 18.4 | 40 | 40 | 6.0 | 20 | 120 | 150 | 2.5 | 100.0 |
| 1+00E | 7.0 | 14.0 | 34 | 40 | 4.0 | 20 | 110 | 140 | 2.0 | 100.0 |
| 1+50E | 6.8 | 12.8 | 40 | 32 | 4.0 | 20 | 125 | 140 | 5.0 | 105.0 |
| 2+00E | 9.0 | 20.0 | 45 | 48 | 6.0 | 22 | 130 | 160 | 7.0 | 100.0 |
| 3+00E | 8.8 | 16.8 | 32 | 32 | 5.0 | 18 | 100 | 120 | 8.5 | 100.0 |
| 3+50E | 8.0 | 16.0 | 38 | 40 | 5.0 | 16 | 105 | 140 | 8.0 | 105.0 |
| 4+00E | 1.2 | 6.0 | 45 | 40 | 3.0 | 12 | 110 | 180 | 6.0 | 110.0 |
| 4+50E | 7.2 | 12.8 | 46 | 40 | 3.0 | 12 | 105 | 140 | 5.0 | 105.0 |
| 5+00E | 1.0 | 3.2 | 45 | 64 | 2.5 | 10 | 130 | 160 | 8.0 | 90.0 |
| 5+50E | 2.4 | 7.0 | 32 | 56 | 2.5 | 10 | 105 | 150 | 6.0 | 87.5 |
| 6+00E | .8 | 2.4 | 28 | 32 | 1.0 | 10 | 90 | 120 | 4.0 | 87.5 |
| UR-86-2+00E | 2.8 | 6.0 | 18 | 20 | 3.0 | 30 | 110 | 140 | 12.0 | 90.0 |
| 2+50E | 9.2 | 17.6 | 38 | 60 | 5.0 | 26 | 100 | 140 | 6.0 | 100.0 |
| 3+00E | 7.2 | 15.2 | 35 | 32 | 7.0 | 25 | 100 | 140 | 5.0 | 100.0 |
| 3+50E | 4.8 | 8.0 | 38 | 40 | 4.0 | 18 | 125 | 150 | 5.0 | 90.0 |
| 4+00E | 5.2 | 9.2 | 42 | 48 | 2.5 | 16 | 125 | 160 | 9.0 | 95.0 |
| 4+50E | 4.4 | 9.0 | 42 | 60 | 2.0 | 15 | 120 | 120 | 4.0 | 112.5 |
| 5+00E | 3.2 | 8.0 | 32 | 32 | 2.0 | 12 | 100 | 140 | 10.0 | 25.0 |
| 5+50E | 4.0 | 7.2 | 37 | 72 | 2.5 | 11 | 110 | 140 | 5.0 | 25.0 |
| 6+00E | 3.0 | 4.8 | 16 | 16 | .5 | 6 | 90 | 100 | 7.5 | 25.0 |
| 6+50E | 5.6 | 8.8 | 48 | 60 | 2.0 | 11 | 125 | 150 | 9.0 | 45.0 |
| 7+00E | 1.6 | 5.6 | 50 | 64 | 1.0 | 10 | 120 | 180 | 5.0 | 37.5 |
| UR-88-1+00E | 4.0 | 5.6 | 22 | 24 | 5.0 | 18 | 80 | 120 | 7.0 | 45.0 |
| 1+50E | 2.8 | 3.6 | 11 | 16 | 4.0 | 16 | 75 | 120 | 9.0 | 62.5 |
| 2+00E | 3.6 | 4.8 | 16 | 24 | 3.0 | 10 | 70 | 120 | 7.5 | 60.0 |
| 2+50E | 13.6 | 17.6 | 50 | 60 | 5.0 | 24 | 125 | 160 | 6.0 | 45.0 |
| 3+00E | 5.0 | 8.0 | 25 | 24 | 6.0 | 28 | 110 | 150 | 6.0 | 37.5 |
| 3+50E | 2.0 | 3.6 | 35 | 32 | .5 | 12 | 110 | 150 | 10.0 | 35.0 |
| 4+00E | 8.0 | 16.0 | 44 | 56 | 3.0 | 24 | 110 | 150 | 7.0 | 37.5 |
| 4+50E | 6.4 | 14.4 | 30 | 32 | 8.0 | 25 | 100 | 160 | 7.5 | 45.0 |
| 5+00E | 7.2 | 16.0 | 45 | 60 | 8.0 | 28 | 125 | 180 | 5.0 | 50.0 |
| 5+50E | 4.8 | 9.0 | 45 | 72 | .5 | 12 | 125 | 160 | 5.0 | 40.0 |
| 6+00E | 2.0 | 3.2 | 22 | 20 | .5 | 12 | 75 | 140 | 4.0 | 37.5 |
| 6+50E | 2.0 | 2.0 | 15 | 24 | .5 | 4 | 60 | 140 | 5.0 | 40.0 |
| 7+00E | 2.0 | 5.6 | 40 | 40 | .5 | 10 | 120 | 180 | 7.5 | 50.0 |
| 7+50E | 2.8 | 6.0 | 45 | 64 | 2.5 | 12 | 120 | 200 | 8.0 | 50.0 |
| 8+00E | 2.4 | 5.2 | 40 | 48 | .5 | 5 | 70 | 120 | 4.0 | 50.0 |
| UR-90-BL | 12.0 | 21.0 | 52 | 80 | 6.0 | 32 | 130 | 200 | 6.0 | 50.0 |
| " "0+50E | 14.0 | 16.8 | 38 | 32 | 7.0 | 32 | 120 | 180 | 5.0 | 45.0 |
| 1+00E | 5.2 | 7.0 | 24 | 24 | 4.0 | 26 | 100 | 140 | 7.0 | 50.0 |
| 1+50E | 4.0 | 7.0 | 30 | 40 | 2.0 | 16 | 110 | 160 | 6.0 | 40.0 |
| 2+00E | 5.2 | 10.4 | 26 | 24 | 6.0 | 16 | 110 | 140 | 5.0 | 45.0 |
| 2+50E | 2.4 | 3.6 | 16 | 16 | 2.0 | 6 | 60 | 120 | 6.0 | 50.0 |
| 3+00E | 5.6 | 12.8 | 34 | 32 | 2.5 | 20 | 100 | 150 | 4.0 | 62.5 |
| 3+50E | 2.0 | 2.4 | 36 | 40 | 2.5 | 12 | 105 | 160 | 5.0 | 50.0 |
| 4+00E | 2.4 | 3.6 | 30 | 32 | 1.0 | 5 | 100 | 150 | 21.0 | 80.0 |
| 4+50E | 11.2 | 18.0 | 60 | 72 | 5.0 | 18 | 125 | 200 | 8.0 | 62.5 |
| 5+00E | 1.2 | 1.6 | 42 | 64 | .5 | 2 | 100 | 140 | 6.0 | 50.0 |
| 5+50E | 3.0 | 5.2 | 36 | 40 | 1.0 | 5 | 110 | 140 | 12.5 | 55.0 |
| 6+00E | 2.8 | 5.6 | 38 | 48 | 1.0 | 6 | 110 | 120 | 6.0 | 50.0 |
| 0+50W | 2.4 | 8.4 | 40 | 40 | 2.0 | 15 | 110 | 200 | 5.0 | 55.0 |
| 1+00W | 4.4 | 7.2 | 18 | 20 | 4.0 | 25 | 90 | 140 | 6.0 | 55.0 |
| 1+50W | 4.4 | 4.0 | 16 | 20 | 7.0 | 36 | 150 | 220 | 12.0 | 65.0 |

SIL R TITAN PROJECT
MAYO - YUKON
STREAM SEDIMENTS

| SAMPLE NUMBER | CxCu ppm | CxHCl-Cu ppm | HCl-Cu ppm | Cx-Zn ppm | CxHCl-Zn ppm | HCl-Zn ppm | CxPb ppm | CxHClPb ppm | HClPb ppm |
|---|---|---|---|---|---|---|---|---|---|
| H-3-0 | 2.4 | 4.0 | 14 | 3.0 | 12 | 75 | 5.0 | 14.0 | 60 |
| 1 | 2.4 | 4.8 | 14 | 3.0 | 12 | 75 | 3.0 | 8.0 | 40 |
| 2 | 2.8 | 4.8 | 12 | 2.5 | 8 | 70 | 3.0 | 9.0 | 40 |
| 3 | 2.8 | 5.2 | 12 | 3.5 | 13 | 80 | 4.0 | 11.0 | 50 |
| 5 | 3.0 | 3.2 | 20 | 5.0 | 10 | 85 | 5.0 | 15.0 | 50 |
| 6 | 4.0 | 5.6 | 22 | 8.0 | 15 | 90 | 6.0 | 16.0 | 70 |
| 7 | 3.6 | 3.6 | 15 | 17.0 | 25 | 85 | 4.0 | 12.0 | 60 |
| 8 | 1.8 | 1.0 | 2 | 3.0 | 5 | 40 | 3.0 | 8.0 | 50 |
| 9 | 2.8 | 4.8 | 15 | 3.0 | 12 | 90 | 4.0 | 9.0 | 60 |
| 10 | 5.6 | 9.0 | 24 | 5.0 | 12 | 90 | 5.0 | 17.0 | 70 |
| 11 | 4.4 | 8.0 | 20 | 5.5 | 14 | 80 | 4.0 | 11.0 | 60 |
| H-4-C-1 | 3.2 | 6.0 | 15 | 3.0 | 8 | 70 | 5.0 | 13.0 | 50 |
| 2 | 2.4 | 4.8 | 11 | 2.5 | 8 | 50 | 3.0 | 8.0 | 40 |
| 3 | 3.6 | 5.0 | 15 | 3.0 | 11 | 85 | 4.0 | 9.0 | 50 |
| 4 | 3.6 | 6.4 | 16 | 4.0 | 11 | 75 | 4.0 | 10.0 | 50 |
| 5 | 3.2 | 4.0 | 15 | 3.5 | 10 | 85 | 6.0 | 8.0 | 60 |
| 6 | 4.0 | 7.6 | 18 | 5.0 | 15 | 80 | 5.0 | 6.0 | 50 |
| 7 | 2.0 | 6.8 | 15 | 3.0 | 12 | 75 | 6.0 | 7.0 | 60 |
| 8 | 1.6 | 6.4 | 16 | 3.0 | 8 | 60 | 4.0 | 10.0 | 50 |
| 9 | 2.4 | 4.4 | 12 | 2.5 | 10 | 60 | 5.0 | 14.0 | 70 |
| 10 | 3.2 | 8.0 | 15 | 5.0 | 16 | 80 | 6.0 | 15.0 | 70 |
| 11 | 4.4 | 8.4 | 12 | 8.0 | 15 | 80 | 4.0 | 13.0 | 50 |
| H-9-1 | 3.0 | 6.0 | 16 | 3.0 | 10 | 80 | 6.0 | 20.0 | 75 |
| 2 | 3.0 | 5.6 | 14 | 3.0 | 10 | 50 | 5.0 | 14.0 | 70 |
| 3 | 4.0 | 6.8 | 32 | 4.0 | 11 | 75 | 5.5 | 14.0 | 60 |
| 5 | 4.4 | 10.4 | 26 | 6.0 | 15 | 85 | 5.0 | 13.0 | 75 |
| 6 | 4.4 | 11.2 | 30 | 6.0 | 15 | 90 | 5.0 | 11.0 | 50 |
| 7 | 6.4 | 13.6 | 44 | 7.5 | 18 | 105 | 6.0 | 14.0 | 75 |
| 8 | 6.0 | 12.0 | 30 | 7.5 | 16 | 100 | 6.0 | 16.0 | 75 |
| T.C.-0 | 5.2 | 6.0 | 15 | 28.0 | 52 | 150 | 7.0 | 16.0 | 80 |
| 1 | 4.4 | 4.8 | 18 | 17.0 | 30 | 120 | 5.0 | 13.0 | 60 |
| 2 | 4.4 | 6.4 | 22 | 13.5 | 26 | 110 | 5.0 | 12.0 | 75 |
| 3 | 4.2 | 4.8 | 22 | 68.0 | 90 | 175 | 3.0 | 9.0 | 50 |
| 4 | 4.4 | 4.4 | 25 | 28.0 | 35 | 125 | 5.0 | 9.0 | 60 |
| 5 | 3.6 | 5.0 | 20 | 12.5 | 18 | 80 | 4.0 | 10.0 | 70 |
| 6 | 2.0 | 4.8 | 16 | 3.0 | 10 | 75 | 5.0 | 11.0 | 55 |
| 7 | 2.8 | 6.4 | 22 | 3.0 | 10 | 75 | 4.0 | 8.0 | 50 |
| 8 | 4.4 | 6.4 | 22 | 4.0 | 20 | 80 | 6.0 | 13.0 | 60 |
| 9 | 4.8 | 10.0 | 20 | 4.0 | 32 | 80 | 5.0 | 10.0 | 75 |
| E.L.C. | 3.2 | 3.6 | 16 | 3.0 | 11 | 70 | 6.0 | 13.0 | 75 |
| E.L.C.-1 | 3.2 | 7.0 | 35 | 14.0 | 66 | 120 | 5.0 | 11.0 | 70 |
| 2 | 3.2 | 2.0 | 8 | 4.0 | 10 | 70 | 5.0 | 10.0 | 50 |
| 3 | 2.8 | 4.8 | 15 | 3.0 | 12 | 60 | 5.0 | 9.0 | 60 |
| 4 | 3.6 | 5.6 | 18 | 4.0 | 11 | 75 | 5.0 | 9.0 | 50 |
| 5 | 4.0 | 5.6 | 20 | 4.0 | 16 | 80 | 4.0 | 10.0 | 50 |
| 6 | 3.2 | 4.4 | 20 | 3.0 | 15 | 75 | 5.0 | 12.0 | 55 |
| 7 | 4.0 | 5.0 | 20 | 4.0 | 15 | 80 | 4.0 | 11.0 | 50 |
| 8 | 3.6 | 6.0 | 18 | 3.5 | 10 | 80 | 5.0 | 15.0 | 70 |
| P.C.-1 | 6.4 | 12.8 | 34 | 16.0 | 30 | 130 | 6.0 | 17.0 | 75 |
| 2 | 7.6 | 11.2 | 28 | 28.0 | 50 | 130 | 6.0 | 16.0 | 75 |

| SAMPLE NUMBER | CxCu ppm | CxHCl-Cu ppm | HCl-Cu ppm | Cx-Zn ppm | CxHCl-Zn ppm | HCl-Zn ppm | CxPb ppm | CxHClPb ppm | HClPb ppm |
|---|---|---|---|---|---|---|---|---|---|
| P.C.-3 | 4.0 | 6.0 | 20 | 9.0 | 18 | 110 | 5.0 | 18.0 | 70 |
| 4 | 5.6 | 12.0 | 24 | 12.0 | 26 | 100 | 4.0 | 11.0 | 75 |
| 5 | 6.4 | 12.0 | 24 | 13.0 | 30 | 120 | 4.0 | 10.0 | 60 |
| 6 | 9.6 | 16.8 | 28 | 15.0 | 32 | 125 | 5.0 | 11.0 | 60 |
| 7 | 7.6 | 12.6 | 26 | 14.0 | 28 | 110 | 3.0 | 9.0 | 50 |
| 8 | 6.4 | 10.0 | 34 | 13.0 | 20 | 120 | 4.0 | 12.0 | 60 |
| 9 | 5.2 | 8.0 | 25 | 11.0 | 30 | 140 | 4.0 | 10.0 | 55 |
| 10 | 5.6 | 12.8 | 26 | 13.0 | 28 | 125 | 5.0 | 11.0 | 55 |
| 11 | 5.0 | 9.2 | 25 | 10.5 | 26 | 125 | 4.0 | 13.0 | 70 |
| 12 | 6.4 | 11.2 | 30 | 14.0 | 26 | 125 | 6.0 | 15.0 | 70 |

Jan. 20/64