

015631

OWL CLAIMS

CROWN JEM
SURVEY

OPERATORS:

J. BRITTON / R. WELLS

July / August

1970

L	STN	HIGH C	H H	Sum
LD	0	-24	+16	-8
	1N	-24	+15	-9
	2	-29	+20	-9
	3	-32	+20	-12
	4	-35	+24	-11
	5	-39	+24	-15
	6	-44	+30	-14
	7	-47	+30	-17
	8	-38	+15	-23
	9	-25	+8	-27
	10	-24	+10	-14
	11	-27	+22	-5
	12	-29	+26	-3
	13	-30	+24	-6
	14	-25	+20	-5
	15	-21	+18	-3
	16N	-17	+15	-2
	17N	-14	12	-2
	18N	-11	8	-3

	LOW		Sum difference
	chief	helper	

-24	+18	-6	
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-24	+20	-4	
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-26	+23	-3	
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-30	+22	-8	
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-33	+26	-7	
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-36	+30	-6	
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-44	+34	-10	
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-46	+34	-12	
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-37	+28	-9	
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-25	+15	-10	
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-24	+16	-8	
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-25	+24	-1	
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+26	+26	0	
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-27	+26	-1	
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-22	+22	0	
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-18	+16	-2	
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-15	+15	0	
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-13	11	-2	
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-10	10	0	
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L	STN	HIGH		Sum
		C	H	
0	19N	-15	12	-4
	20	-25	23	-2
	21	-37	35	-2
	22	-43	34	-7
	23	-26	25	-1
	24	-28	19	-9
	25	-29	20	-9
	26	-25	20	-5
	27	-27	19	-8
	28	-36	20	-16
	29	-39	+32	-7
4W	BL-0	-20	+12	-8
	1N	-18	+13	-5
	2	-30	+13	-17
	3	-31	+23	-8
	4	-30	+26	-4
	6	-35	+25	-10
	6	-36	+25	-11

LOW

C

H

SUM

C	H	SUM
-14	12	-2
-24	25	+1
-36	35	-1
-40	36	-4
-23	25	+2
-27	21	-6
-28	21	-7
-25	22	-3
-23	22	-1
-28	23	-5
-36	34	-2
-20	15	-5
-19	+13	-6
-29	+16	-13
-29	+23	-6
-31	+26	-5
-32	+30	-2
-34	+28	-6

L	STN	HIGH		Sum
		C	H	
4W	7N	-38	+26	-12
	8N	-43	+27	-16
	9	-39	+18	-21
	10	-29	+4	-25
	11	-24	+8	-16
	12	-20	+10	-10
	13	-23	+20	-3
	14	-37	+36	-1
	15	-43N	+36	-7
	16	-26	+26	0
	17	-23	+18	-5
	18	-15	+15	0
	19	-13	+12	-1
	20	-20	+12	-8
	21	-28N	+16	-12
	22	-34	+25	-9
	23	-35	+28	-7
	24	-33	+22	-11
	25	-28	+16	-12

	LOW		
L	C	H	SUM
	-35	+30	-5
	-41	+34	-7
	-42	+28	-14
	-28	+14	-14
	-20	+11	-9
	-16	+12	-4
	-19	+20	+1
	-37	+34	-3
	-39	+38	-1
	-28	+28	0
	-21	+18	-3
	-14	+14	0
	-11	+11	0
	-17	+12	-5
	-30N	+18	-12
	-31	+23	-8
	-35	+30	-5
	-31	+24	-7
	-27	+18	-9

LINE	STN	MIGHT		SUM
		C	H	
4W	26N	-32N	+12	-20
	27N	-35	+14	-21
	28N	-35	+20	-15
	29N	-34	25	-9
4W	15	-20	6	-14
	2	-19	8	-11
	3	-21	13	-8
	4	-25	12	-13
	5	-24	7	-17
	6	-26	6	-20
	7	-35	6	-29
	8	-32	0	-32
	9	-26	0	-26
	10	-36	0	-36
	11	-38	2	-36
	12	-40	14	-26
	13	-42	12	-30
	14	-43	12	-31
	15	-36	8	-28

	Low	
C	H	Sum
-31N	418	-13
-35	417	-18
-34	419	-15
-33	25	-8
-16	8	-8
-17	10	-7
-19	15	-4
-21	14	-7
-19	12	-7
-18.	14	-4
-30	17	-13
-30	18	-12
-24	8	-16
-34	10	-24
-40	20	-20
-44	26	-18
-41	25	-16
-43	25	-18
-45	28	-15

LINE	STN	HIGH		sum
		C	M	
4W	16 S	-55	26	-29
	17	-40	14	-26
	18	-46	28	-18
	19	-60	52	-8
	20	(-72)	68	(-4)
	21	—	—	—
	22	—	—	—
	23	-70	60	-10
	24	-70	70	0
	25	-55	58	+3
	26	-42	30	-10
	27	-1	0	-1
	28	-5	4	-1
	29	-23	18	-5
	30	—	—	—
0	30 ^S	—	—	—
	28 ^S	-24	25	+1
	27 ^S	-35	35	0
	26 ^S	-55	55	0

		LOW	
	C	H	SUM
	-56	40	-16
	-43	32	-11
	-50	38	-12
	-64	60	-4
	-70	68	-2
	—	—	—
	—	—	—
	-70	66	-4
	-68	70	+2
	-56	56	-0
	-37	30	-7
	-2	0	-2
	-6	4	-2
	-20	20	0
	—	—	—
	—	—	—
	-24	23	-1
	-36	35	-1
	-56	56	0

) LINE
ERROR

LINE	STN	HIGH		SUM
		C	H	
0	-			
	25	-70	72	
	24	—	—	
	23	(7)	70	
	22	-69	68	-1
	21	-66	64	-2
	20	-64	56	-8
	19	-55	44	-11
	18	-52	30	-22
	17	-42	15	-27
	16	-43	12	-31
	15	-45	14	-31
	14	-43	10	-33
	13	-39	13	-26
	12	-36	-1	-37
	11	-33	-4	-37
	10	-24	0	-24
	9	-19	-2	-21
	8	-24	0	-24

	c	L0 H	SUM.
	(T)	72	
	—	—	
	(T)	70	
	-70	68	-2
	-65	62	-3
	-58	56	-2
	-56	52	-4
	-53	42	-11
	-44	28	-16
	-46	23	-23
	-45	34	-21
	-44	30	-14
	-41	28	-13
	-37	20	-17
	-34	5	-29
	-25	2	-23
	-26	+4	-22
	-28	10	-18

LINE	STN	M1 C	H	SUM
0	75	-25	0	-25
	6	-21	10	-11
	5	-24	12	-12
	4	-26	18	-8
	3	-29	16	-13
	2	-25	15	-10
	1	-25	15	-10
8W	86-0	-19	5	-14
	15	-17	7	-10
	25	-23	11	-12
	35	-29	18	-11
	4	-26	15	-11
	5	-34	15	-19
	6	-36	20	-16
	7	-33	6	-27
	8	-32	6	-26
	9	-36	11	-25
	10	-45	14	-21
	11	-42	15	-26

		Lo			
	C	H	from		
	-25	10	-15		
	-19	13	-6		
	-20	15	-5		
	-26	18	-8		
	-27	19	-8		
	-22	18	-4		
	-23	16	-7		
	-18	9	-9		
	-15	11	-4		
	-19	15	-4		
	-23	21	-2		
	-21	15	-6		
	-26	20	-6		
	-28	23	-5		
	-27	23	-4		
	-30	18	-12		
	-36	26	-10		
	-45	34	-11		
	-40	25	-15		

LINE	STN	HIGH		SUM
		C	H	
8W	125	-35	7	-28
	13	-42	13	-29
	14	-47	18	-29
	15	-50	18	-32
	16	-50	24	-26
	17	-45	22	-23
	18	-45	25	-20
	19	-66	56	-10
	20	—	—	—
	21	—	—	—
	22	—	—	—
	23	—	—	—
	24	-44	44	0
	25	-34	34	0
	26	-35	32	-3
	27	-36	35	-1
	28	-28	26	-2
	29	-18	18	0
	30	—	—	—

	C	LOW M	SUM.		
	-34	22	-12		
	-41	25	-16		
	-47	29	-18		
	-50	35	-15		
	-49	38	-11		
	-50	35	-15		
	-52	43	-9		
	-66	+62	-4		
	-	-	-	OFF	SCALE
	-	-	-	"	"
	-	-	-	"	"
	-	-	-	"	"
	- 410	12	0		
	-34	34	0		
	-34	33	-1) LINE ERROR	
	-35	35	-1		
	-30	28	-2		
	-17	18	+1		
	-	-	-		

LINE	STN	HI C	M	SUM
12W	305	—	—	—
	29	-49	46	-1
	28	-44	43	-1
	27	-34	33	-1
	26	-5	4	-1
	25	-2	-2	-4
	24	-40	40	0
	23	-56	51	-4
	22	—	—	—
	21	—	—	—
	20	-64	56	-8
	19	-66	59	-7
	18	-61	52	-9
	17	-49	27	-22
	16	-45	25	-20
	15	-45	27	-18
	14	-50	24	-26
	13	-42	14	-28
	12	-42	15	-27

	C	LO W	SUM	
	-	-	-	
	-45	44	-1	
	-42	43	+1	
	-31	31	0	
	-4	4	0	
	-2	-2	-4	
	-38	40	+2	
	-55	52	-3	
	-	-	-	700
	-	-	-	STEEP
	-59	57	-2	
	-66	62	-4	
	-61	57	-4	
	-54	38	-16	
	-47	36	-11	
	-51	36	-15	
	-52	37	-15	
	-42	26	-16	
	-39	25	-14	

LINE	STN	H1 C	M	SUM
12W	11S	-42	16	-26
	10	-35	14	-21
	9	-26	4	-22
	8	-24	14	-20
	7	-37	17	-20
	6	-36	22	-14
	5	-38	20	-18
	4	-30	15	-15
	3	-31	14	-17
	2	-28	11	-17
	1	-26	11	-15
	-BL-0	-25	8	-17
12W	1N	-25	14	-9
	2N	-26	13	-13
	3	-25	10	-15
	4	-24	10	-14
	5	-27	10	-17
	6	-27	14	-13
	7	-27	16	-11

$r^2 c$	LO H	SUM
-40	26	-14
-37	26	-11
-32	16	-16
-26	11	-15
-30	17	-13
-34	29	-5
-30	25	-5
-26	21	-5
-27	25	-2
-25	18	-7
-24	14	-10
-21	8	-13
-20	15	-5
-22	16	-6
-20	14	-6
-20	13	-7
-25	18	-7
-26	16	-10
-25	19	-6

LINE	SPN	H1 C	H	SUM
12W	8A	-29	16	-13
	9	-28	18	-10
	10	-27	18	-9
	11	-25	18	-7
	12	-20	16	-4
	13	-16	14	-2
	14	-15	13	-2
	15	-15	15	0
	16	-20	20	0
	17	-39	38	-1
	18	-39	38	-1
	19	-26	25	-1
	20	-24	25	+1
	21	-25	22	-3
	22	-26	15	-11
	23	-18	14	-4
	24	-29	26	-3
	25	-38	36	-2
	26	-42	36	-6

H	L O C	Sum
-26	20	-6
-26	20	-6
-24	22	-2
-24	20	-4
-17	16	-1
-14	14	0
-15	13	-2
-14	15	+1
-20	20	0
-38	38	0
-37	38	+1
-26	24	-2
-23	25	+2
-22	22	0
-26	13	-13
-17	14	-3
-26	28	+2
-36	35	-1
-38	36	-2

LINE	STN	HIGH		Sum
		C	H	
12W	27N	-48	44	-4
	28	-47	36	-11
	29	-35	13	-12
	30	-	-	-
8W	30N	-	-	-
	29	-45	44	-1
	28	-52	46	-6
	27	-42	32	-10
	26	-28	20	-8
	25	-34	26	-8
	24	-35	31	-4
	23	-26	24	-2
	22	-19	16	-3
	21	-16	14	-2
	20	-14	10	-4
	19	-15	14	-1
18	-23	20	-3	
17	-35	32	-3	
16	-42	38	-4	

	C	L0 H	SUM
	-47	45	-2
	-45	32	-13
	-29	23	-6
	-	-	-
	-	-	-
	-45	44	-1
	-50	48	-2
	-40	33	-7
	-28	20	-6
	-31	28	-3
	-32	31	-1
	-24	22	-2
	-17	16	-1
	-15	13	-2
	-12	12	0
	-15	14	-1
	-21	20	-1
	-35	31	-4
	-29 39	39	0

LINE	STN	HIGH		SUM	
		C	H		
8'W	15N	-34	32	-2	
	14	-24	20	-4	
	13	-16	15	-1	
	12	-19	2	-17	
	11	-22	5	-17	
	10	-30	9	-21	
	9	-38	15	-23	
	8	-34	18	-16	
	7	-30	18	-12	
	6	-30	20	-10	
	5	-35	25	-10	
	4	-28	22	-6	
	3	-26	16	-10	
	2	-22	11	-11	
	1	-20	9	-11	RAID
20'W	BL-0	-30	2	-28	.465
	1S	-35	16	-19	.262
	2S	-37	32	-5	
	3S	-36	30	-6	

		LOW	
	C	H	SUM
	-32	32	0
	-22	20	-2
	-14	15	+1
	-15	7	-8
	-20	9	-11
	-31	16	-15
	-36	21	-15
	-31	22	-9
	-28	22	-6
	-26	22	-4
	-32	26	-6
	-26	22	-4
	-22	18	-4
	-18	14	-4
	-16	9	-7
	-28	15	-13
	-35	30	-5
	-38	35	-3
	-36	32	-4

LINE	SPN	HIGH		SUM	(RATIO)
		C	H		
20W	45	-30	25	-5	
	5	-26	25	-1	
	6	-35	31	-4	
	7	-42	38	-4	
	8	-50	48	-2	
	9	-48	45	-3	
	10	-37	24	-13	.308
	11	-35	24	-11	.091
	12	-39	25	-14	.285
	13	-45	25	-20	.250
	14	-40	28	-28	.357
	15	-35	14	-21	.525
	16	-40	23	-17	.765
	17	-52	25	-27	.630
	18	-60	33	-27	.333
	19	-53	34	-19	.526
	20	-60	37	-23	.565
	21	-70	61	-11	
	22	-	-	-	

		LOW	
	C	H	SUM
	-27	25	-2
	-24	25	+1
	-32	30	-2
	-38	38	0
	-50	47	-3
	-46	44	-2
	-32	28	-4
	-32	31	-1
	-42	38	-4
	-43	38	-5
	-35	25	-10
	-31	20	-11
	-45	32	-13
	-60	43	-17
	-62	53	-9
	-60	56	-10
	-66	53	-13
	-72	72	0
	-	-	-

] BLACK
 SHALE
 9/C.P.

LINE	STN	HIGH		SUM	RATIO	
		C	H			
Now	235	-	-	-		
	245	-	-	-		
	25	-	-	-		
	26	-15	14	-1		
	27	+10	-10	0		
	28	-11	+9	-2		
	29	-28	29	+1		
	16W	295	-56	58	+2	
		28	-53	53	0	
27		-56	56	0		
26		-54	54	0		
25		-51	48	-3		
24		-50	50	0		
23		-57	50	-7		
22		-54	51	-3		
21		-54	37	-17	.235	
20		-51	33	-18	.500	
19	-49	33	-16	.500		

	Low		
	C	H	SUM
	-	-	-
	-	-	-
	-	-	-
	-14	16	+2
	+8	-15	-7
	-14	+10	-4
	-28	29	+1
	-56	56	0
	-53	53	0
	-56	55	-1
	-54	54	0
	-49	48	-1
	-49	50	+1
	-57	50	-7
	-55	51	-4
	-54	50	-4
	-55	45	-9
	-51	43	-8

LINE	SDN	HIGH C	M	SUM	RATIO
L20W	185	-46	15	-21	.950
	17	-46	21	-25	.520
	16	-42	19	-23	.696
	15	-47	25	-22	.455
	14	-46	26	-20	.500
	13	-40	26	-14	.930
	12	-38	24	-14	.572
	11	-40	26	-14	.428
	10	-48	40	-8	.375
	9	-46	38	-8	.375
	8	-40	34	-6	
	7	-36	25	-11	.184
	6	-35	25	-10	.100
	5	-36	22	-14	.224
	4	-40	19	-21	.333
	3	-35	15	-20	.300
	2	-28	1	-29	.345
	1	-26	5	-21	.525
BL-0		-26	1	-25	.680

	C	LOW H	W/M
	-50	31	-19
	-49	36	-13
	-48	32	-16
	-50	40	-10
	-44	34	-10
	-36	33	-13
	-34	26	-8
	-36	30	-6
	-46	43	-3
	-43	40	-3
	-36	34	-2
	-31	29	-2
	-29	28	-1
	-30	27	-3
	-35	28	-7
	-33	27	-6
	-25	15	-10
	-24	13	-11
	-25	8	-17

ROSTY
CREEK

LINE	SPN	HIGH		SUM	RATIO
		C	H		
20W	1N	-26	-6	-32	.625
	2	-27	-2	-25	.720
	3	-27	-2	-29	.552
	4	-28	1	-27	.370
	5	-28	3	-25	.360
	6	-26	0	-26	.385
	7	-25	0	-25	.520
	8	-30	3	-27	.592
	9	-28	9	-19	.474
	10	-26	15	-11	.545
	11	-24	14	-10	.400
	12	-24	20	-4	
	13	-32	27	-5	
	14	-35	30	-5	
	15	-30	30	0	
	16	-19	14	-5	
	17	-17	16	-1	
	18	-20	19	-1	
	19	-24	24	0	

	C	L O H	SUM	
	-24	44	-20	SWAMP.
	-25	7	-18	
	-24	8	-16	
	-20	10	-10	
	-22	13	-9	
	-22	12	-10	
	-23	10	-13	
	-24	8	-16	
	-25	16	-9	
	-24	18	-6	
	-20	16	-4	
	-22	15	-7	
	-29	26	-3	
	-32	32	0	
	-30	29	-1	
	-16	16	0	
	-15	14	-1	
	-20	19	-1	
	-22	24	+2	

LINE	STN	HIGH		SUM	
		C	M		
20W	20N	-28	25	-3	
	21	-30	29	-1	
	22	-30	28	-2	
	23	-29	26	-3	
	24	-34	25	-9	.445
	25	-26	6	-20	.600
	26	-10	-2	-12	.500
	27	-34	16	-18	.278
	28	-50	40	-10	.100
16W	27N	-54	45	-9	
	26	-49	45	-4	
	25	-36	30	-6	
	24	-20	18	-2	
	23	-16	16	0	
	22	-16	16	+2	
	21	-22	20	-2	
	20	-25	20	-5	
	19	-28	27	-2	

	C	LOW H	SUM
	-26	26	0
	-30	32	-2
	-29	26	-3
	-30	25	-5
	-30	26	-4
	-24	12	-12
	-6	0	-6
	-24	19	-5
	-48	47	-1
	-50	50	0
	-48	47	-1
	-34	30	-4
	-18	17	-1
	-16	14	-2
	-16	15	-1
	-19	20	+1
	-23	22	-1
	-28	26	-2

O/C/P IN
CREEK

GREEN SHALE
WITH PYRITE

2650' N
BLACK GRAPH.
SHALE
CONTACT

LINE	SPN	HIGH		SUM	RATIO
		C	H		
16W	18N	-35	30	-5	
	17	-26	26	0	
	16	-20	20	0	
	15	-17	19	+2	
	14	-15	12	-3	
	13	-20	18	-2	
	12	-21	18	-3	
	10	-21	20	-1	
	10	-26	17	-9	.555
	9	-28	15	-13	.462
	8	-28	12	-16	.625
	7	-26	8	-18	.555
	6	-27	7	-20	.450
	5	-24	7	-17	.353
	4	-25	5	-20	.550
	3	-28	5	-23	.522
	2	-28	6	-22	.500
	1	-30	5	-25	.360

	LOW		
C	H	SUM	
-34	30	-4	
-26	25	-1	
-18	20	+2	
-17	17	0	
-14	12	-2	
-18	17	-1	
-21	20	-1	
-19	18	-1	
-24	19	-5	
-25	19	-6	
-26	16	-10	
-25	15	-10	
-24	15	-9	
-20	14	-6	
-21	10	-11	
-27	12	-12	
-26	15	-11	↓ RUSTY ↓ CREEK
-25	16	-9	

LINE	SPN	HIGH		SUM	
		C	H		
24W	BL-0	-29	6	-23	.348
	15	-38	26	-12	
	25	-39	33	-6	
	3	-30	28	-2	
	4	-29	29	0	
	5	-31	29	-2	
	6	-33	31	-2	
	7	-43	41	-2	
	8	-48	50	+2	
	9	-43	36	-7	
	10	-30	26	-4	N
	11	-36	26	-10	.100
	12	-36	30	-6	
	13	-35	25	-10	.200
	14	-35	15	-20	.300
	15	-42	27	-15	.532
	16	-53	43	-10	.400
	17	-59	48	-9	.445
	18	-70	63	-7	

		LOW	
	C	H	SUM
	-30	22	-8
	-35	35	0
	-34	32	-2
	-28	27	-1
	-29	28	-1
	-30	29	-2
	-30	31	+1
	-41	41	0
	-49	49	0
	-39	40	+1
	-28	28	0
	-30	29	-1
	-33	32	-1
	-30	28	-2
	-31	25	-6
	-35	27	-8
	-48	44	-4
	-58	54	-4
	-65	65	-5

LINE	SPN	HIGH		SUM
		C	M	
24W	195	—	—	—
	205			
	21			
	22			
	23			
	24			
	25			
	26			
	27	-18	17	+
	28	+20	-20	0
	29	+17	-17	0
28W	29	-2	+2	0
	28	-1	0	-1
	27	10	-11	-1
	26	10	-11	-1
	25	-32	32	0
	24	—	—	—
	23	—	—	—

LINE	SPN	HIGH C	H	sum	
L28W	225	-	-	-	
	21	-	-	-	
	20	-70	70	0	
	19	-65	55	-10	.600
	16	-70	68	-2	
	15	-64	55	-9	.223
	14	-43	35	-8	.375
	13	-33	26	-7	N
	12	-31	29	-2	N
	:				
	1	?			
	11	-34	34	0	
	10	-32	31	-1	
	9	-30	28	-2	
	8	-29	26	-3	
	7	-47	40	-2	
	6	-48	44	-4	
	5	-40	40	0	
	4	-34	30	-4	

	C	cow H	sum
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-	-	-	-
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-	-	-	-
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-68	67	-1
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-63	57	-6
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-70	69	-1
-----	----	----

-60	58	-2
-----	----	----

-43	40	-3
-----	----	----

-28	25	-3
-----	----	----

-28	26	-2
-----	----	----

-31	32	+1
-----	----	----

-31	30	-1
-----	----	----

-28	28	0
-----	----	---

-28	27	-1
-----	----	----

-41	42	+1
-----	----	----

-46	45	-1
-----	----	----

-40	39	-1
-----	----	----

-30	30	0
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LINE	STN	HIGH		SUM	
		C	H		
28 W	35	-30	26	-4	
	2	-31	24	-7	N
	1	-30	16	-14	N [286
	BL-0	-33	12	-21	286
24 W	1 N	-28	2	-26	.424
	2	-30	5	-25	.440
	3	-35	8	-27	.481
	4	-30	8	-32	N [.312
	5	-28	6	-22	.454
	6	-27	4	-23	.435
	7	-26	0	-26	.424
	8	-22	-4	-26	.546
	9	-25	0	-25	.800
	10	-25	4	-21	.670
	11	-22	8	-14	.430
	12	-20	15	-5	
	13	-20	18	-2	
	14	-20	15	-5	

		Low	
	C	H	Sum
	-26	26	0
	-27	24	-3
	-26	22	-4
	-29	23	-6
	-26	15	-11
	-27	16	-11
	-29	16	-13
	-25	15	-10
	-25	15	-10
	-24	14	-10
	-20	9	-11
	-20	6	-14
	-21	4	-20
	-24	10	-14
	-16	10	-6
	17	15	-2
	-18	4	0
	-17	15	-2

LINE	STN	C	M	Sum	
24W	15N	-14	10	-4	
	16	-2	0	-2	
	17	10	-11	-1	
	18	-6	5	-1	
	19	-22	20	-2	
	20	-24	24	0	
	21	-34	30	-4	
	22	-34	33	-1	
	23	-37	35	-2	
	24	-36	35	-1	
	25	-38	30	-8	.625
	26	-28	22	-6	
	27	-25	13	-12	.583
	28	-24	10	-14	.285
	29	-32	20	-12	.915
	30	-42	33	-9	.334
	31	-52	40	-12	.425
	32	-45	30	-15	.465
	33	-12	0	-12	.583

	C	H	Sum
	-12	10	-2
	0	0	0
	10	-10	0
	-4	4	0
	-20	20	0
	-24	24	0
	-28	29	+1
	-32	33	+1
	-36	35	-1
	-40	35	-1
	-37	32	-5
	-30	23	-7
	-23	16	-7
	-19	15	-4
	-26	15	-11
	-39	36	-3
	-50	45	-5
	-40	30	-7
	-10	13	-7

LINE#	SPN	M/GH c	M	Sum	L/M Ratio
29 W	31	-50	-15	-65	.154
	30	-43	15	-28	.535
	29	-40	6	-34	.540
	28	-35	0	-35	.545
	27	-28	0	-28	.680
	26	-36	22	-14	.570
	25	-43	35	-8	
	24	-50	45	-5	
	23	-50	50	0	
	22	-40	36	-4	
	21	-20	19	-1	
	20	-15	14	-1	
	19	-16	13	-3	
	18	-5	4	-1	
	17	12	-15	-3	
	16	0	-5	-5	
	15	-10	10	0	
	14	-10	10	0	
	13	-18	6	-12	.500

	C	LOW M	SUM
	-50	40	-10
	-45	30	-15
	-30	20	-18
	-29	10	-19
	-29	10	-19
	-38	30	-8
	-40	40	0
	-49	43	-6
	-46	50	+4
	-38	35	-3
	-18	19	+1
	-2	11	0
	-15	15	0
	-3	3	0
	10	-15	-5
	+3	-4	-1
	-8	8	0
	-8	12	-5
	-15	9	-6

LINE	STN	HIGH		SUM	
		C	H		
29W	12N	-24	8	-16	.560
	11	-20	-2	-22	.820
	10	-20	-5	-25	.840
	9	-25	-4	-29	.760
	8	-25	-9	-34	.735
	7	-29	-5	-34	.620
	6	-30	0	-30	.660
	5	-32	4	-28	.429
	4	-38	7	-31	.484
	3	-40	12	-28	.500
	2	-36	10	-26	.540
	1	-30	7	-23	.435
<hr/>					
32E	BL-0	-25	9	-16	N .25
	15	-26	11	-15	.266
	2	-28	15	-13	.23
	3	-36	15	-21	.43
	4	-35	16	-19	↓ .105
	5	-41	20	-21	.525

	Low	H	Sum	
	-19	10	-9	
	-20	2	-18	
	-22	1	-21	
	-25	3	-22	
	-26	1	-25	
	-29	8	-21	
	-29	9	-20	
	-26	14	-12	
	-35	20	-15	
	-39	25	-14	
	-35	21	-14	
	-30	20	-10	
<hr/>				
	-20	16	-4	N
	-20	16	-4	N
	-21	18	-3	N
	-28	19	-9	N
	-29	27	-2	N
	-38	27	-11	

WF	SPN	C	HIGH M	SUM	
32E	65	-47	19	-13	.54
	7	-45	24	-21	.38
	8	-46	24	-22	.23
	9	-47	24	-23	.39
	10	-39	5	-34	.38
	11	-38	18	-20	.45
	12	-38	8	-30	N .93
	13	-34	6	-28	.39
	14	-20	3	-17	1.0
	15	-28	8	-20	N 1.06
	16	-26	-5	-31	.935
	17	-26	-12	-39	.925
	18	-26	-10	-36	.89
	19	-34	0	-34	.59
	20	-34	10	-29	.76
	21	-36	5	-31	.39
	22	32	4	-28	.54
	23	-30	9	-21	.62
	24	-31	8	-23	.52

	Low	Sum
-40	33	-7
-42	34	-8
-43	38	-5
-45	36	-9
-37	24	-13
-35	26	-9
-42	14	-28
-35	14	-11
-21	4	-17
-31	10	-21
-30	1	-29
-30	-5	-35
-25	-7	-32
-34	13	-20
-40	18	-22
-35	13	-12
-30	15	-15
-30	17	-13
-30	18	-12

LINE	STN	H/BAH C	H	SUM	
32E	255	-30	6	-24	.41
	26	-27	13	-14	.86
	27	-35	15	-20	.60
	28	-34	24	-10	.90
	29	-38	29	-9	.33
28E	29	-35	32	-3	
	28	-41	35	-6	
	27	-41	21	-20	.30
	26	-30	15	-15	.465
	25	-25	4	-21	.525
	24	-32	3	-29	.69
	23	-25	7	-18	.835
	22	-23	-5	-28	.93
	21	-30	-10	-40	.875
	20	-20	-13	-33	.94
	19	-16	-11	-27	1.02
	18	-19	-10	-29	.88
	17	-18	-16	-34	.94

	C	H	SV An.
	-30	20	-10
	-29	17	-12
	-30	18	-12
	-34	25	-9
	-35	32	-3
	-34	39	0
	-38	35	-3
	-36	30	-6
	-29	22	-7
	-25	14	-11
	-30	10	-20
	-26	11	-15
	-26	0	-26
	-30	-5	-35
	-22	-9	-31
	-19	-10	-29
	-23	-10	-33
	-18	-14	-32

L	STN	HIGH		SUM	
		C	H		
28F	165	-17	-13	-30	1.1
	15	-24	-6	-30	1.06
	14	-30	5	-25	1.04
	13	-30	9	-21	1.14
	12	-35	10	-25	.56
	11	-37	14	-23	.35
	10	-40	13	-27	.298
	9	-40	15	-25	.200
	8	-46	24	-22	.36
	7	-45	24	-21	.24
	6	-45	18	-27	.26
	5	-44	16	-28	.32
	4	-35	16	-19	.16
	3	-42	24	-18	.27
	2	-50	30	-20	.30
	1	-40	20	-20	.35
	BL-0	-24	6	-18	.28
	1				

	c	Low H	Sum
	-18	-15	-33
	-22	-10	-32
	-36	10	-26
	-34	13	-24
	-39	15	-14
	-40	32	-8
	-42	34	-8
	-39	34	-5
	-44	36	-8
	-41	36	-5
	-40	33	-7
	-40	31	-9
	-35	32	-3
	-40	35	-5
	-50	44	-6
	-38	31	-7
	-20	15	-5

L	SPN	HOGH C	H	SJM	
28E	1N	-25	5	-20	.5
	2	-26	5	-21	.33
	3	-20	6	-24	.46
	4	-20	6	-24	.50
	5	-26	3	-23	.75
	6	-26	2	-24	.625
	7	-29	8	-21	.63
	8	-28	14	-14	.64
	9	-29	20	-9	.55
	10	-34	19	-15	.87
	11	-28	18	-10	.88
	12	-26	15	-11	.73
	13	-30	23	-7	.57
	14	-29	20	-9	.55
	15	-30	20	-10	.60
	16	-38	23	-15	.46
	17	-38	15	-23	.82
	18	-35	6	-30	.60
	19	-33	2	-31	.55

	C	Low H	Sum
	-20	10	-10
	-21	14	-7
	-25	14	-11
	-26	14	-12
	-26	9	-17
	-25	10	-15
	-28	15	-13
	-26	17	-9
	-28	23	-5
	-33	20	-13
	-28	20	-8
	-26	18	-8
	-27	23	-4
	-26	21	-5
	-27	21	-6
	-35	28	-7
	-37	25	-12
	-34	16	-18
	-32	15	-17

L	STN	HIGH		SUM	
		C	H		
28.E	20N	-34	7	-27	
	21	-36	14	-22	
	22	-30	17	-13	
	23	-25	11	-14	
	24	-23	13	-10	
	25	-10	2	-8	
	26	-25	21	-4	
	27	-60	54	-6	
	...				
32E	29N				
	28				
	27				
	26				
32E	25	-46	27	-19	.26
	24	-36	30	-6	
	23	-30	28	-2	
	22	-22	17	-5	
	21	-30	20	-10	.50
	20	-34	20	-14	.57

		Low		
	c	M	Sum	
	-30	20	-10	
	-32	25	-7	
	-28	20	-8	
	-20	14	-6	N
	-18	12	-6	
	-7	3	-4	
	-24	22	-2	
	-56	54	-2	

	-40	35	-5	
	-35	31	-4	
	-26	28	+2	
	-20	20	0	
	-26	21	-5	
	-30	22	-8	

L	SPN	H.IGH		SUM	
		C	H		
32E	19N	-35	14	-11	.91
	18	-26	3	-23	.61
	17	-26	11	-15	.87
	16	-34	12	-22	.45
	15	-34	18	-16	.56
	14	-30	16	-14	.50
	13	-28	15	-13	.92
	12	-32	15	-17	.59
	11	-31	20	-11	.64
	10	-27	22	-.5	:
	9	-30	23	-7	.29
	8	-31	22	-9	.77
	7	-30	15	-15	.80
	6				
	5				
	4				
	3				
	2				
	1				

