

76VW-1

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everything with S_2 dipping N
strike of S_2 is E-W.

Footage	S_1	S_2	Folding	Remarks
25'	24VW	64VW	WAA S_2	Overburden.
45'				Casing
46'	26VW	68VW	$S_1 \wedge S_2 \approx 42^\circ$	direction of S_1, S_2 at 29° in S_2 plane
52'		69 69VW		fract. $\perp S_2$ qtz healed
55'	80VW	66VW	$S_1 \wedge S_2 \approx 14^\circ$	S_2 only $S_2 > S_1$
63'	51VW	58VW	$S_1 \wedge S_2 \approx 57^\circ$	flatter $S_2 > S_1$
72'		72VW		$S_2 > S_1$
82'	27 27VW	68VW	$S_1 \wedge S_2 \approx 85^\circ$	S_2 dominate looking along strike 15W $\lambda \approx 1mm$ on S_2
88'				$S_2 > S_1$ looking along strike 22E
89'	27VW	84VW	$S_1 \wedge S_2 \approx 69^\circ$	Well frac. S_1, S_2 minor fold N03E.
101'	22VW	80VW	$S_1 \wedge S_2 \approx 78^\circ$	$S_2 > S_1$
106'	63VW	78VW	$S_1 \wedge S_2 \approx 39^\circ$	$S_2 > S_1$
111		75VW		S_2 dominant
116'		70VW		"
120'	42VW	76VW	$S_1 \wedge S_2 \approx 62^\circ$	$S_2 > S_1$ $\lambda \approx 1mm$ on S_2 looking strike 14E
130'	25VW	68VW	$S_1 \wedge S_2 \approx 87^\circ$	$S_2 > S_1$
146'	70VW	74VW	$S_1 \wedge S_2 \approx 4^\circ$	$S_2 \approx S_1$
150'		73VW		S_2 dominant $\lambda \approx 1mm$ on S_2 looking along strike 16W well fractured.
162'	65VW	75VW	$S_1 \wedge S_2 \approx 39^\circ$	$S_1 \wedge S_2$
169+172'				bodily broken.
172'		78VW		S_2 dominant
188'	~74° variable	83VW	$S_1 \wedge S_2 \approx 23^\circ$ FA. trace $\approx 86^\circ$ ch. / 07N	still bodily broken
192'			slightly brecciated in fractures.	
198'	58VW	76VW	$S_1 \wedge S_2 \approx 18^\circ$	$S_2 > S_1$
210'	66VW	82VW	$S_1 \wedge S_2 \approx 32^\circ$	$S_2 \approx S_1$
215'	80 80VW		$S_1 \wedge S_2 \approx ?$	M folding in S_1
220'	?	78VW	$S_1 \wedge S_2 \approx ?$	$S_2 > S_1$
227-239'			poor recovery badly broken along S_2	
230'		65VW		S_2 dominant w/

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Footage	S ₁	S ₂	Folding	Remarks
250	74	92	S ₁ AS ₂ = 2? □ □	S ₂ > S ₁ ^{1/2} A = 1 unit locking along GE
260		83	S ₁ AS ₂ = 2? □ □	S ₂ completely dominant
269	45	74	S ₁ AS ₂ = 31" □ □	S ₂ > S ₁
280	68	74	S ₁ AS ₂ = 39° □ □	
290		78		S ₂ dominate but S ₁ present and very visible.
300		77	S ₁ AS ₂ = 230 □ □	S ₂ > S ₁
310	steep	42	S ₁ AS ₂ = ? □	S ₁ > S ₂
320	variable	35		S ₁ > S ₂
330	?	78	FA = 50 (blank) 20. d.c.	S ₁ > S ₂
340	?	72 ?		S ₁ > S ₂
350		42		S ₂ dominant
354		35		"
360	25?	68	S ₂ AS ₁ < 87 □ □	S ₂ > S ₁
370		65 (1)	S ₁ AS ₂ = 50 (broken up poor comparison)	S ₂ dominant
380		60		S ₂ dominant
390	07	78	S ₁ AS ₂ = 85 □ □	S ₂ > S ₁
400		77		S ₂ dominant
410	41	88	S ₁ AS ₂ = 50 □ □	S ₂ > S ₁
420		72		S ₂ dominant
430		6		
426	82	65	S ₁ AS ₂ = 17 □ □	S ₁ > S ₂
440	variable	81	FA = blank	S ₂ > S ₁
450	80(?)	73	S ₁ AS ₂ = 73 □ □	S ₂ > S ₁
460	steeper?	82		S ₂ > S ₁
470		83		S ₁ dominant
480		80		"
490		75		"
500		74		"
510		33(?)	maybe S ₁	
520		76	"	
530	00	72	S ₁ AS ₂ = 72	S ₂ dominant
540		73	maybe S ₁ ?	"
550		33		"
560		72		"
570		67		"
580		70		"
590	variable	58		S ₂ > S ₁

Footage	S ₁	S ₂	Folding	Remarks
600	67	70	S ₁ AS ₂ ≈ 57°	S ₁ > S ₂
610	70	82	S ₁ AS ₂ ≈ 72°	S ₁ > S ₂
620	variable	75		S ₁ ≈ S ₂
630	"(≈ 38)	68	S ₁ AS ₂ ≈ 30°	S ₁ ≈ S ₂
634			slightly decciated over	~ 1.5' Thick
640	sub II	72		S ₂ > S ₁
650	79	80	S ₁ AS ₂ ≈ 6°	S ₂ > S ₁
660	83	72		
670	variable	76	L. (stam) in S ₂ looking along strike E-W	S 13 E
680	78	88	S ₁ AS ₂ = 10°	S ₁ > S ₂
690	73	80	S ₁ AS ₂ ≈ 7°	S ₁ > S ₂
700	?	82		S ₂ > S ₁
710		75	light and dark bands	S or S ₂ ?
717	51	76		S ₁ AS ₂
730	58	58		S ₁ = S ₂
740		82		S ₁ = S ₂ , S ₁ dominant
752	72	78	S ₁ AS ₂ = 30°	S ₁ > S ₂
760	75	75		S ₁ = S ₂
765	78	85	S ₁ AS ₂ = 17°	S ₂ > S ₁
774	77	89	S ₁ AS ₂ = 14°	S ₂ > S ₁
780	70	80	S ₁ AS ₂ = 30°	S ₂ > S ₁
790	variable	78	small M-fold in S ₁	
800	"	86	FA - 70° clockwise - 10° dip N 8°	S ₁ = S ₂
810	72	78	S ₁ AS ₂ ≈ 60°	S ₁ = S ₂
820	variable	79		S ₁ = S ₂
830	70	80	S ₁ AS ₂ ≈ 10°	S ₁ = S ₂
840	variable	80	FA - 70° clockwise - 12° dip	
850	73	81	S ₁ AS ₂ = 26°	S ₁ = S ₂
860	variable	83		S ₁ ≈ S ₂
870	"	79		S ₂ > S ₁
880	"	81		S ₂ > S ₁
890	(58)	84	S ₁ AS ₂ = 20°	S ₂ > S ₁
900	78	86	S ₁ AS ₂ = 16°	S ₂ = S ₁
910	variable	79		S ₂ ≈ S ₁
920	"	78		S ₂ > S ₁
930	77	87	S ₁ AS ₂ = 10°	S ₂ > S ₁

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(A)

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Remarks

Footage	S ₁	S ₂	Folding	Remarks
940	Variable	75		S ₂ > S ₁
950	"	82		S ₂ > S ₁
960		83		S ₂ dominant
970	Variable	78		S ₂ > S ₁
972	"	82	F ₁ - check 72 dip 14	S ₂ > S ₁
980	76	86	S ₁ / S ₂ ≈ 14° <input type="checkbox"/> <input type="checkbox"/>	S ₁ < S ₂
990	Variable	83	L ₁ (N 40 W) on S ₂ looking along strike E is 0°	S ₁ < S ₂
1000	80	81	S ₁ / S ₂ ≈ 1° <input type="checkbox"/> <input type="checkbox"/>	S ₁ > S ₂ (?)
1001-			shot through with	qtz rough cly
1003		38(?)	probably S ₂	
1007	80	80	S ₁ / S ₂ ≈ 20° <input type="checkbox"/> <input type="checkbox"/>	S ₂ > S ₁