FARO UNDERGROUND

- Kilborn
1987

6.0 FARO UNDERGROUND MINING

6.0 FARO UNDERGROUND MINING

6.1 GENERAL

Southwest of the ore being mined in the Faro Open pit is a zone of high grade lead zinc ore which will be mined by underground methods.

Mining practices at the Faro Underground will be influenced by two major factors:

a) The mineralized tabular zones dip at 15 to 25 degrees;
b) The rock comprising the footwall and the hanging wall is mineralized and the grades similar to the material being mined within the open pit.

The dip of the zones is well below the angle of repose of broken rock and gravity cannot be used to move broken ore. The dip is too steep to allow the use of rubber tired equipment within the stopes.

The competent rocks, however, allow the use of a mining method requiring relatively large areas of exposed, unsupported back.

Open stoping methods will be used. Open stopes will be mined up dip and pillars left between stopes. These pillars will be partially removed during final mining retreat to give a final overall extraction of 75 percent.

The thickness which will be mined are normally greater than 3 metres. A minimum mining height of 2.1 metres has been used.

Mine water inflows are not expected to be a major problem. The wet areas encountered within the Faro open pit appear to be associated with faults and most of the rocks have low permeability.

The mine will be operated on a two - ten hour shift, five day per week basis. Production per operating day will be 2000 tonnes. Access will be provided by a decline. Hydraulic jumbos and trackless loaders and trucks will be used to drive the decline and the access drifts to the stoping areas. Stope mining operations will be conducted with short hole, portable drills and electric slushers.

6.2 ORE RESERVES

The ore zone shown on Figure 6.2-1 is an extension of the orebody being mined by the Faro open pit. The reserves are based on surface drill holes as indicated in the figure. A geolocial reserve was calculated by the polygon method using the following parameters:

a) Minimum insitu grade 9 percent Pb + Zn.
b) Minimum mining height 2.1 metres.
c) Maximum radius of influence 46 metres.
d) Minimum pillar between underground reserves and final open pit wall is 15 metres.

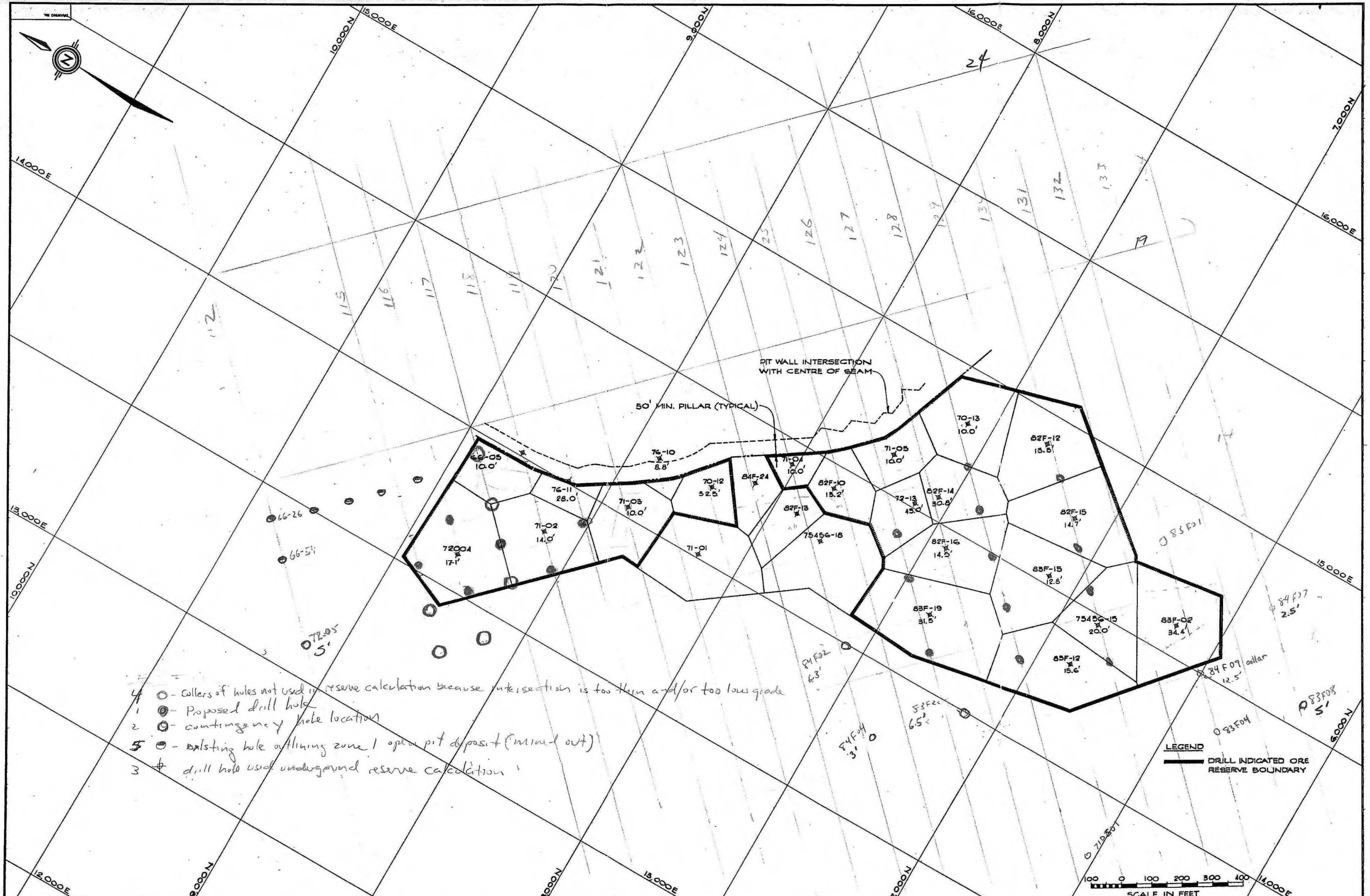
These reserves are considered to be in the probable catagory.

Geological reserves are given in table 6.2-1.

Mining reserves are calculated from geological reserves on the following parameters:

a) Dilution - 10 percent at zero grade.
b) Mining Recovery - 75 percent of inplace reserves.

Mining Reserves are given in table 6.2-1.



A	ISSUED FOR FEASIBILITY STUDY	MAR.3.87	P.A.H
No.	DESCRIPTION		
	REVISIONS		

DWG. NO. | REFERENCE DRAWINGS

SECTION:	CLIENT: CURRAGH RESOURCES	TITLE	B.O.M. No.
SCALE: 1"=100' DATE		FARO AREA DEPOSITS	PROJECT No. 3509 / DIVISION No. 19
DESIGNED BY: J.B.F. FEB.87	LOCATION: FARO, YUKON.	FARO DEPOSIT UNDERGROUND MINE	DRAWING NUMBER
DRAWN BY: P.A.H FEB.87	KILBORN	DRILL INDICATED ORE RESERVES	FIG.6.2-1 REV. A
CHECKED BY:			
APPROVED BY: JBF			

Table 6.2-1

Geological Reserves

Ore Type	Lead Percent	Zinc Percent	Silver gm/tonne	Quantity tonnes
2A	1.98	3.88	13.86	58,000
2BG	5.09	7.69	67.51	2,288,000
2H	5.21	9.26	82.17	264,000
TOTAL	5.04	7.76	67.90	2,610,000
	Mining Reserve			
TOTAL	4.59	7.00	61.29	2,014,000

6.3 MAJOR DEVELOPMENT

Major development prior to the start of production is shown on Figure 6.3-1 and comprises 3 main areas:

- Main access decline;
- Mining levels;
- Ventilation Raise.

The main access decline will be collared on the west wall of the existing open pit at 3670 ft elevation. The grade of the decline will be 15 percent. Dimensions of the decline will be 4.3 metres high by 5.2 metres wide. This decline will be positioned to permit intersection of the bottom of the ore zone at 30 metres vertical intervals. Prior to start of production 1219 metres of decline will be driven. Two main level drifts will be driven as part of the preproduction development at 3300 and 3400 ft elevations. This major drifting will amount to 1128 metres of which 579 metres will be at the 3400 ft elevation. The remaining 550 metres of pre-production development will be at the 3200 ft elevation. These drifts will have the same dimensions as the decline.

The main ventilation downcast raise will be driven from the end of the 3300 ft level to surface in a distance of 245 metres. This raise will be a 2.4 metre diameter bored raise fitted with an emergency escape manway.

10,000N
15,000E
9,000N
16,000E
8,000N
7,000N
14,000E
16,000E
15,000E
13,000E
10,000N
12,000E
9,000N
8,000N
13,000E
7,000N
14,000E
6,000N

N

3750
3710
3630
3790
3830
3850
4050
3600
3630
3670
3670
3500
3400
3300
3200
3500
3400
3300
3500

EXIT RAMP FROM PIT

PORTAL
EL. 3670'

N.W. PIT WALL

EL. 3500'

EL. 3400'

EL. 3300'

PIT WALL INTERSECTION
WITH CENTRE OF SEAM

50' MIN. PILLAR (TYPICAL)
TO PIT WALL

14'H.x15'W. DRIFTS DRIVEN
ON 3300' AND 3400' LEVELS
AS INITIAL DEVELOPMENT

VENT RAISE TO
SURFACE FROM
3300' LEVEL

14'H.x17'W.
DECLINE DRIVEN @ -15%
DOWN TO 3500' LEVEL
AS INITIAL DEVELOPMENT.

VENT EXHAUST AIR
TO PORTAL

14'H.x17'W.
DECLINE @ -15%

4050
3100
950
4050
3100
950
4050
3200
1050

100 0 100 200 300 400
SCALE IN FEET

DWG. NO.	REFERENCE DRAWINGS

No.	DESCRIPTION	CLIENT	FINAL DWG.	CHECK
A	ISSUED FOR TECHNICAL REVIEW MAR 1967			

REVISIONS

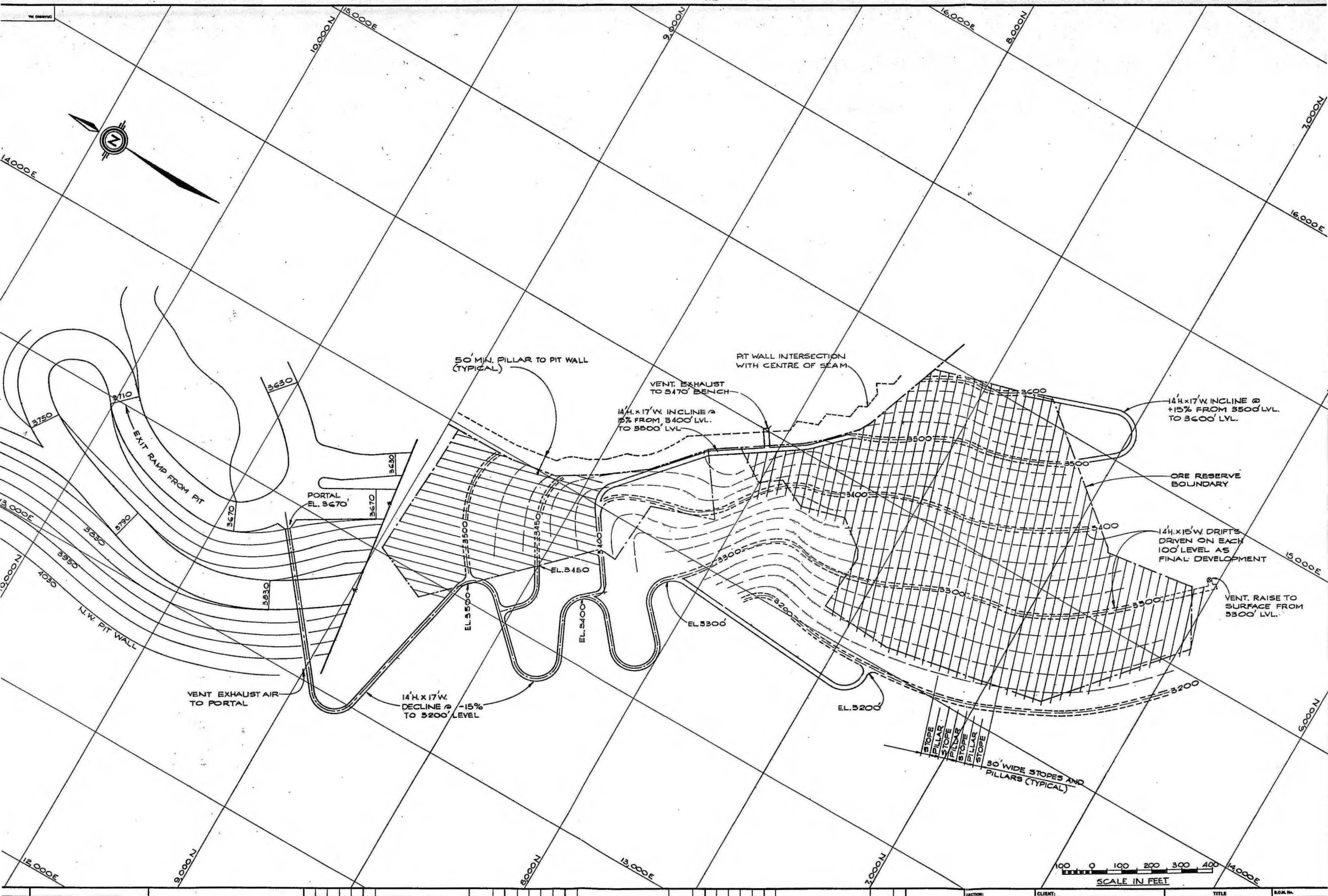
SECTION:
SCALE: 1" = 100' DATE
DESIGNED BY: J.B.F. MAR 67
DRAWN BY: P.A.H. MAR 67
CHECKED BY:
APPROVED BY: J.B.F.

CLIENT: CURRAGH RESOURCES
LOCATION: FARO, YUKON.

KILBORN

TITLE
FARO AREA DEPOSITS
FARO DEPOSIT
UNDERGROUND MINE
INITIAL DEVELOPMENT

B.O.M. No.
PROJECT No. 3509 DIVISION No. 19
DRAWING NUMBER
FIG. 6.5-1 REV. A



DWG. NO.	REFERENCE DRAWINGS

No.	DESCRIPTION	CLIENT	FINAL ENG.	CHECK
	REVISIONS			

No.	DESCRIPTION	CLIENT	FINAL ENG.	CHECK
	REVISIONS			

No.	DESCRIPTION	CLIENT	FINAL ENG.	CHECK
A	ISSUED FOR TECHNICAL REVIEW MAR.3.87			
	REVISIONS			

SECTION:		
SCALE: 1"=100'	DATE	
DESIGNED BY: J.B.F.	MAR 87	
DRAWN BY: P.A.H.	MAR 87	
CHECKED BY:		
APPROVED BY: J.B.F.		

CLIENT: CURRAGH RESOURCES

LOCATION: FARO, YUKON.

KILBORN

TITLE: FARO AREA DEPOSITS
FARO DEPOSIT
UNDERGROUND MINE
FINAL DEVELOPMENT

B.O.M. No.	
PROJECT No.	DIVISION No.
3509	19
DRAWING NUMBER	
FIG.6.3-2	REV. A

Total major development for the life of the mine is shown on Figure 6.3-2 and includes further drifting on the 3200 ft., 3400 ft. and 3500 ft. elevations. This additional ongoing development amounts to 1433 metres in length.

6.4 STOPE DEVELOPMENT

Stope development will be similar for both stopes in thick ore zones and stopes in thinner ore zones. This development for a stope, which can be seen on Figure 6.4-1, includes:

- slusher station with access raise
- drawpoint
- stope raise

Stope development will be positioned in ore to minimize the excavation of waste.

6.5 STOPING METHOD

The stoping method which will be used is up-dip open-stoping with air leg pneumatic drills and electric powered slusher/scrapers for ore removal to the stope drawpoint. Typical stopes are shown on Figure 6.4-1.

The proceedure will be as follows:

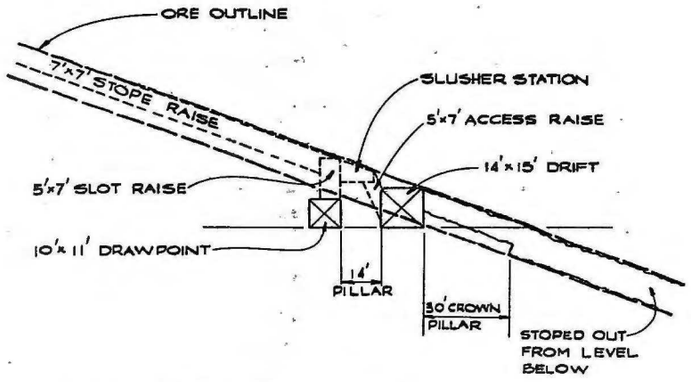
a) A slot raise will be excavated from the top of the drawpoint drift to the top of the ore.

b) An access raise from the main level drift to the slusher hoist station and the slusher hoist station will be excavated.

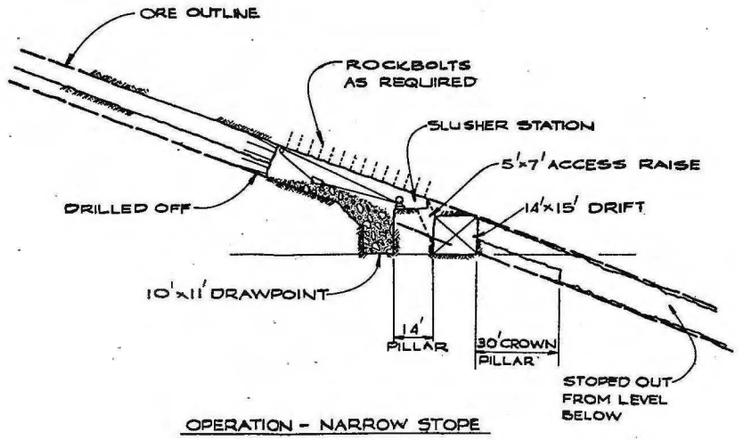
c) The slusher hoist and scraper will be installed.

d) A 2.1 metre slot raise will be driven along the back of the stope from the top of the slot raise to the level above.

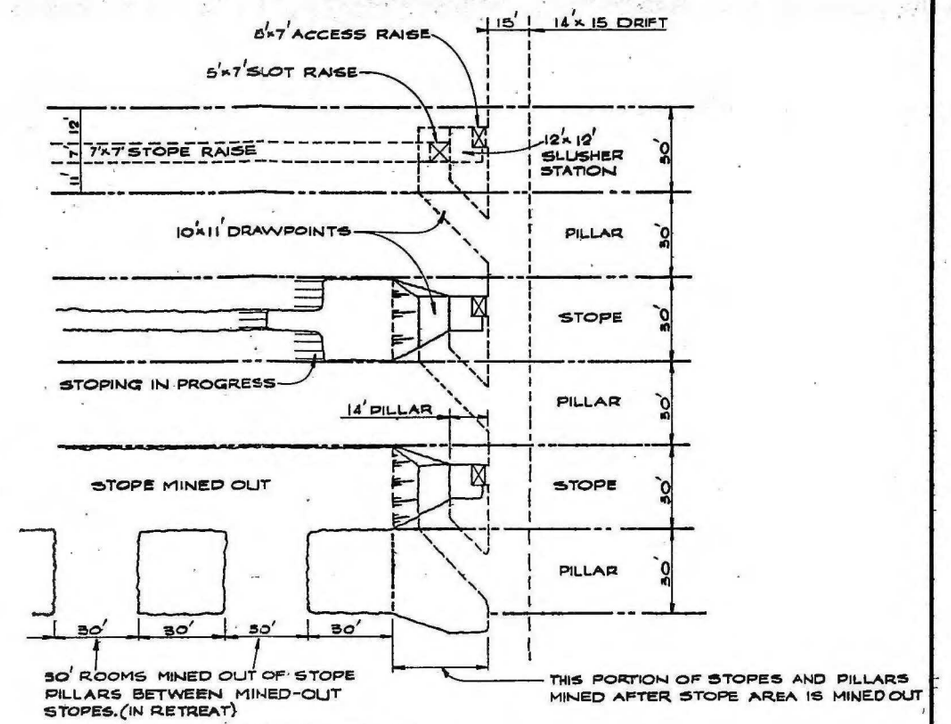
e) The ore body will be mined up dip from the slot raise to the crown pillar. Drill holes will be drilled up dip as shown on Figure 6.4-1. Hole length will be 10 feet. Initial mining height will be 3 metres or ore thickness if less than 3 metres. The stope back will be rockbolted as required.



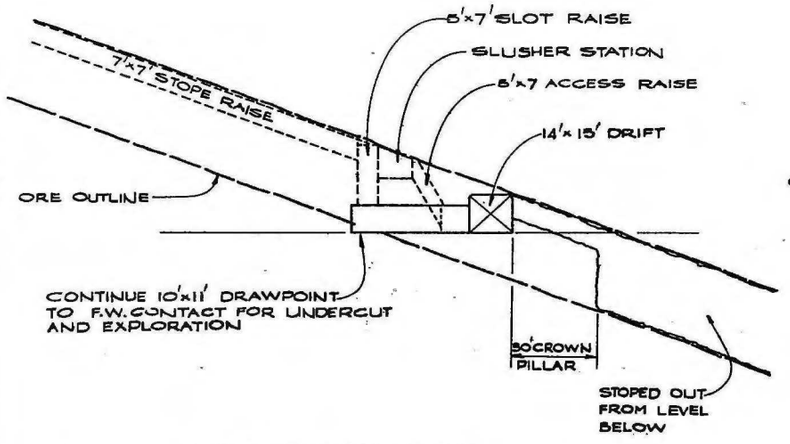
DEVELOPMENT- NARROW STOPE



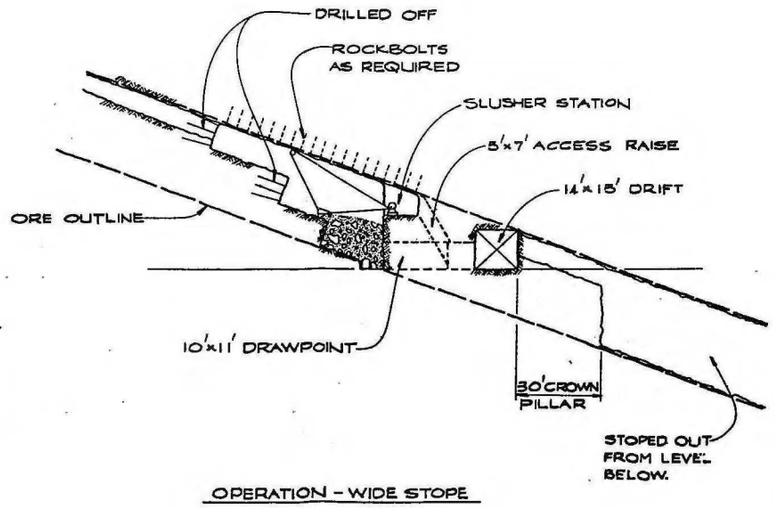
OPERATION - NARROW STOPE



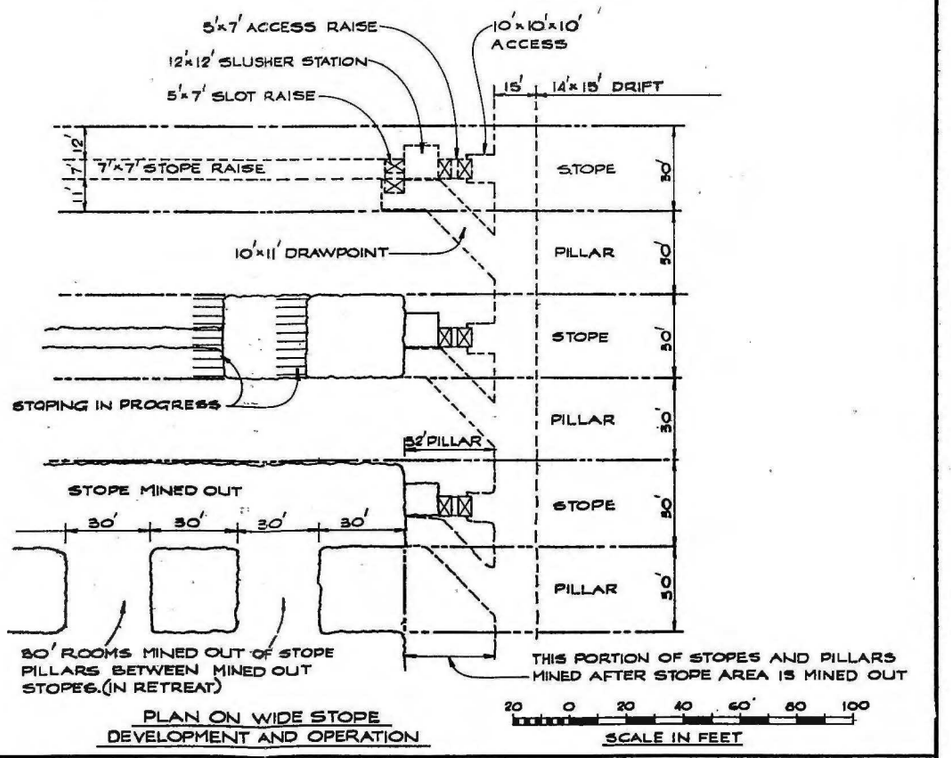
PLAN ON NARROW STOPE
DEVELOPMENT AND OPERATION



DEVELOPMENT - WIDE STOPE



OPERATION - WIDE STOPE



PLAN ON WIDE STOPE
DEVELOPMENT AND OPERATION

DWG. NO.	REFERENCE DRAWINGS

No.	DESCRIPTION	CLIENT	FIELD	CHECK
A	ISSUED FOR FEASIBILITY STUDY			

REVISIONS

SECTION:
SCALE: 1" : 20'
DESIGNED BY: J.B.F. FEB.87
DRAWN BY: R.A.H. FEB.87
CHECKED BY:
APPROVED BY: J.B.F.

CLIENT: CURRAGH RESOURCES
LOCATION: FARO, YUKON.

KILBORN

TITLE	R.O.M. No.
FARO AREA DEPOSITS	
FARO DEPOSIT UNDERGROUND MINE STOPING DETAILS	PROJECT No. 3509 / DIVISION No. 19
	DRAWING NUMBER FIG.C-4-1 / REV. A

f) If the ore is over 3 metres in thickness successive lifts of up to 3 metres will be mined from the stope.

g) Broken ore will be removed to the drawpoint with the scraper as required for mining.

h) After all ore is broken any remaining broken ore within the stope will be slushered to the drawpoint.

i) After mining of two primary stopes, the pillar will be partially mined to leave square 9.1 metres by 9.1 metres pillars and give a 75 percent mining extraction.

A total of 10 stopes operating on a two shift per day schedule will be active at any one time.

6.6 LOADING AND HAULAGE

Ore will be removed from the stope drawpoints with 4.6 m^3 LHDs and 3 35-ton trucks will be required to handle the ore produced in stoping and the material from ongoing development.

The ore will be hauled to a stockpile area immediately outside the mine portal from where it will be loaded into open pit haulage trucks and hauled to the crusher as needed.

6.7 VENTILATION AND MINE AIR HEATING

The main ventilation system, as shown on Figure 6.7.3-1, will be down the main ventilation raise from surface to the 3300 ft level and then upwards and downwards through the stoping blocks and hence exiting the mine through the decline system and exhaust drifts into the open pit.

Ventilation requirements are controlled primarily by the amount of diesel equipment operating within the mine. An allowance of 300,000 cfm is considered adequate for this operation.

19,000N
15,000E
9,000N
16,000E
8,000N
7,000N
14,000E
16,000E
13,000E
19,000N
12,000E
9,000N
8,000N
13,000E
7,000N
14,000E
15,000E
6,000N

50' MIN. PILLAR TO PIT WALL (TYPICAL)

PIT WALL INTERSECTION WITH CENTRE OF SEAM

VENT. EXHAUST TO 3470' BENCH

14'H.x17'W. INCLINE @ 5% FROM 3400' LVL. TO 3500' LVL.

14'H.x17'W. INCLINE @ +15% FROM 3500' LVL. TO 3600' LVL.

ORE RESERVE BOUNDARY

14'H.x15'W. DRIFTS DRIVEN ON EACH 100' LEVEL AS FINAL DEVELOPMENT

FRESH AIR SUPPLY VENT. RAISE TO SURFACE FROM 3300' LVL.

EXIT RAMP FROM PIT

MINE AIR EXHAUST

PORTAL EL. 3670'

EL. 3500'

EL. 3400'

EL. 3300'

EL. 3200'

N.W. PIT WALL

VENT EXHAUST AIR TO PORTAL

14'H.x17'W. DECLINE @ -15% TO 3200' LEVEL

STOPE PILLAR STOPE PILLAR STOPE PILLAR STOPE

50' WIDE STOPES AND PILLARS (TYPICAL)

VENTILATION DISTRIBUTION

100 0 100 200 300 400

SCALE IN FEET

No.	DESCRIPTION	CLIENT	PROJ. ENG.	CHECK
A	ISSUED FOR TECHNICAL REVIEW MAR.31/67			

REVISIONS

DRWG. NO. | REFERENCE DRAWINGS

SECTION:
SCALE: 1"=100' DATE
DESIGNED BY: J.B.F. MAR 67
DRAWN BY: P.A.H. MAR 67
CHECKED BY:
APPROVED BY: J.B.F.

CLIENT: CURRAGH RESOURCES
LOCATION: FARO, YUKON.

KILBORN

TITLE
FARO AREA DEPOSITS
FARO DEPOSIT UNDERGROUND MINE VENTILATION DISTRIBUTION

R.O.M. No.
PROJECT No. 3509 | DIVISION No. 19
DRAWING NUMBER FIG.6.7.3-1 | REV. A

The main ventilation fans will be located at the top of the ventilation raise and will pressurize the mine workings. Within the mine, air flows to the various working areas will be controlled with auxiliary fans and bulkheads.

Mine air will require heating during sub zero weather to ensure that waterlines and drainage systems within the mine do not freeze. Direct-fire propane heaters will be provided for this service. A propane storage system will be required near the ventilation raise.

6.8 UNDERGROUND SERVICES

Temporary underground services will be carried into the mine through the decline and level drifts until the workings are connected to the ventilation raise. When the ventilation raise is complete, mine services will be brought down the ventilation raise to service the mine. Services which will be provided include electrical power, compressed air and water. The mine has been designed with the majority of the energy requirements being for electrical and diesel powered equipment. Compressed air usage has been minimized.

Mine water drainage will be handled in sumps located at the junctions of the levels and the decline. The level drifts will be driven at a positive one percent grade to provide drainage. Unsettled water will be pumped to surface for disposal with the water from the open pit. Mine water discharge lines will be located in the decline.

Mine communications will be provided by a mine mobile radio system operating in conjunction with coaxial antenna located in the main levels and declines. A stench warning system will be provided in the mine ventilation system and compressed air system for emergencies.

Mobile equipment will be taken to the main surface shop for major maintenance. Routine maintenance will be undertaken in small shop areas within the mine workings.

6.9 RELATED SURFACE FACILITIES

The surface facilities required for the underground mine will be minimal.

Office and changehouse facilities are presently in existance and no increase in capacities will be required.

Maintenance shop facilities are available and equipped for the open pit equipment. These facilities will be used to maintain the underground equipment.

A compressor plant to provide compressed air to the mine at 100 psi will be required. Compressed air requirements are estimated to be 3500 cfm. To permit maintenance and to cover peaks 4500 cfm will be installed. A compressor house of 12.2 metres by 9.1 metres will be required to house this equipment.

Ore will be stockpiled in open piles near the decline collar. This material will be rehandled with open pit equipment.

6.10 MINE PERSONNEL

The total mine compliment is:

Supervision & Technical	14
Operating Labour	72
Maintenance Labour	14
TOTAL	100

The detailed listing are shown on Tables:

6.10-1

6.10-2

6.10-3

Table 6.10-1

Supervision & Technical

Underground Superintendent	1
U/G General Foreman	1
Shift Foreman	4
Maintenance Foreman	1
Sr. Mine Engineer	1
Mine Engineer	1
Mine Technician	1
Surveyor	1
Survey Helper	1
Geologist	1
Geological Technician	1
TOTAL	14

Table 6.10-2

Underground Operating Labour

Stope Miner	40
Development Miner	6
LHD Operator	4
Truck Driver	6
Timberman	2
Timber Helper	2
Utility	6
U/G Labour	6
TOTAL	72

Table 6.10-3

Maintenance Labour

Lead Mechanic	2
Lead Electrician	1
Mechanic	3
Electrician	2
Drill Doctor	1
Oiler	1
Maintenance Helper	4
TOTAL	14

6.11 MAJOR MINE EQUIPMENT

Major underground equipment for the mine includes:

Item	Numbers
2 Boom Hydraulic Jumbo	2
Airleg and Stoper Drills	50
LHD Units - 4.6 cu.m. Capacity	4
Trucks - 35 ton Capacity	3
Slusher Hoists c/w Scrapers	
25 Horsepower Electric	12
Service Vehicles	2
Mine Dewatering Pumps	
Various Horsepowers & Heads	5
Auxiliary Fans	15
Pumps	Lot

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
1	HOLE NO.	ROCK	FROM	TO	LENGTH	S.G	PB	ZN	SILVER	D*F	D*F*G	D*F*H	D*F*I	
2	---	---	---	---	---	---	---	---	---	---	---	---	---	
3	66-05	2A	509.0	514.0	5.0	3.09	1.28	4.00	22.10	15.45	19.78	61.80	341.44	
4		2F	514.0	519.0	5.0	4.07	5.20	9.11	65.20	20.35	105.84	185.39	1326.82	
5	---	---	---	---	---	---	---	---	---	---	---	---	---	
6	70-12	2H	566.8	567.3	.5	4.60	4.70	6.20	70.00	2.30	10.81	14.26	161.00	
7	70-12	2F	558.5	563.0	4.5	4.61	7.52	11.65	76.70	20.75	156.00	241.68	1591.14	
8		2F	563.0	566.8	3.8	4.89	6.64	9.00	59.10	18.58	123.38	167.24	1098.20	
9		2E	567.3	570.9	3.6	4.71	6.48	8.64	55.30	16.96	109.87	146.50	937.67	
10		2F	570.9	572.8	1.9	4.84	6.26	11.06	66.50	9.20	57.57	101.71	611.53	
11		2E	572.8	576.0	3.2	4.99	3.66	6.11	46.30	15.97	58.44	97.56	739.32	
12		2F	576.0	581.0	5.0	4.88	7.31	7.36	66.20	24.40	178.36	179.58	1615.28	
13		2F	581.0	586.0	5.0	4.99	7.98	11.40	73.40	24.95	199.10	284.43	1831.33	
14		2E	586.0	591.0	5.0	4.75	4.14	7.10	31.10	23.75	98.32	168.62	738.62	
15		---	---	---	---	---	---	---	---	---	---	---	---	
16		2BG	558.5	591.0	32.0	4.83	6.35	8.98	59.29	154.55	981.06	1387.33	9163.09	
17	---	---	---	---	---	---	---	---	---	---	---	---	---	
18	70-13	2D	471.0	475.0	5.0	3.49	3.28	8.82	25.20	17.45	57.24	153.91	439.74	
19		2G	475.0	479.0	5.0	4.66	6.46	7.34	81.20	23.30	150.52	171.02	1891.96	
20		---	---	---	---	---	---	---	---	---	---	---	---	
21		2BG	471.0	479.0	10.0	4.08	5.10	7.97	57.22	40.75	207.75	324.93	2331.70	
22	---	---	---	---	---	---	---	---	---	---	---	---	---	
23	70-17	2D	529.0	534.0	5.0	3.48	2.50	7.00		17.40	43.50	121.80	0.0	
24		2D	534.0	539.0	5.0	3.48	4.50	6.30		17.40	78.30	109.62	0.0	
25		2F	539.0	544.0	5.0	4.33	5.00	7.80		21.65	108.25	168.87	0.0	
26		2D	544.0	549.0	5.0	3.48	9.30	6.20		17.40	161.82	107.88	0.0	
27		2D	549.0	554.0	5.0	3.48	4.90	8.40		17.40	85.26	146.16	0.0	
28		---	---	---	---	---	---	---	---	---	---	---	---	
29		2BG	529.0	554.0	82.0	1.11	5.23	7.17	0.0	91.25	477.13	654.33	0.0	
30	---	---	---	---	---	---	---	---	---	---	---	---	---	
31	71-01	2H	615.5	616.5	1.0	3.79	2.93	6.24	58.40	3.79	11.10	23.65	221.34	
32	---	---	---	---	---	---	---	---	---	---	---	---	---	
33	71-02	2F	539.0	548.0	9.0	4.33	5.20	8.00		38.97	202.64	311.76	0.0	
34		2D	548.0	553.0	5.0	3.48	1.50	5.00		17.40	26.10	87.00	0.0	
35		---	---	---	---	---	---	---	---	---	---	---	---	

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
36		2BG	539.0	553.0	14.0	4.03	4.06	7.07	0.0	56.37	228.74	398.76	0.0	
37	---	---	---	---	---	---	---	---	---	---	---	---	---	
38	71-03	2A	588.0	593.0	5.0	3.19	2.40	2.70		15.95	38.28	43.07	0.0	
39	71-03	2F	593.0	598.0	5.0	4.33	4.50	5.80		21.65	97.42	125.57	0.0	
40	---	---	---	---	---	---	---	---	---	---	---	---	---	
41 ✓	71-04	2E	524.0	529.0	5.0	4.33	3.20	5.60		21.65	69.28	121.24	0.0	
42		2E	529.0	534.0	5.0	4.33	3.90	5.80		21.65	84.44	125.57	0.0	
43		---	---	---	---	---	---	---	---	---	---	---	---	
44		2BG	524.0	534.0	10.0	4.33	3.55	5.70	0.0	43.30	153.72	246.81	0.0	
45	---	---	---	---	---	---	---	---	---	---	---	---	---	
46	71-05	2F	517.5	522.5	5.0	4.05	5.75	6.11	71.60	20.25	116.52	123.73	1449.90	
47		2F	522.5	527.5	5.0	4.61	5.18	5.49	83.60	23.05	119.40	126.54	1926.98	
48		---	---	---	---	---	---	---	---	---	---	---	---	
49		2BG	517.5	527.5	10.0	4.33	5.45	5.78	77.99	43.30	235.92	250.27	3376.88	
50	---	---	---	---	---	---	---	---	---	---	---	---	---	
51 ✓	72004	2J	509.0	511.5	2.5	3.79	5.04	11.90	77.80	9.47	47.75	112.75	737.15	
52		2C	511.5	516.5	5.0	2.81	1.69	3.67	34.00	14.05	23.74	51.56	477.70	
53		2B	516.5	521.0	4.5	2.69	1.41	4.73	24.60	12.11	17.07	57.26	297.78	
54		2B	521.0	526.1	5.1	2.85	3.53	7.73	60.90	14.54	51.31	112.36	885.18	
55		---	---	---	---	---	---	---	---	---	---	---	---	
56		2BG	509.0	526.1	17.1	2.93	2.79	6.66	47.80	50.17	139.88	333.93	2397.82	
57	---	---	---	---	---	---	---	---	---	---	---	---	---	
58	72-13	2E	582.0	587.0	5.0	4.07	8.53	6.63	80.40	20.35	173.59	134.92	1636.14	
59		2F	587.0	592.0	5.0	4.12	5.75	9.60	58.30	20.60	118.45	197.76	1200.98	
60		2B	592.0	597.0	5.0	3.32	4.87	6.96	56.80	16.60	80.84	115.54	942.88	
61		2F	597.0	602.0	5.0	4.56	6.18	6.55		22.80	140.90	149.34		
62		2F	602.0	607.0	5.0	4.88	6.28	6.53	87.40	24.40	153.23	159.33	2132.56	
63		2F	607.0	612.0	5.0	4.11	4.97	7.12	74.10	20.55	102.13	146.32	1522.76	
64		2B	612.0	617.0	5.0	3.30	5.30	5.88	71.20	16.50	87.45	97.02	1174.80	
65		2F	617.0	622.0	5.0	3.98	6.95	9.55	91.20	19.90	138.31	190.05	1814.88	
66		2B	622.0	627.0	5.0	3.04	11.39	2.83	192.80	15.20	173.13	43.02	2930.56	
67		---	---	---	---	---	---	---	---	---	---	---	---	
68		2BG	582.0	627.0	45.0	3.93	6.60	6.97	86.67	176.90	1168.03	1233.29	13355.56	
69	---	---	---	---	---	---	---	---	---	---	---	---	---	
70	74-17	2D	484.0	489.0	5.0	3.43	5.49	15.00	32.90	17.15	94.15	257.25	564.24	

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
71		2E	489.0	494.0	5.0	4.55	6.48	7.90	72.50	22.75	147.42	179.72	1649.38	
72		2Q	494.0	499.0	5.0	3.54	3.63	4.52	51.40	17.70	64.25	80.00	909.78	
73		2Q	499.0	504.0	5.0	2.98	.68	.94	10.00	14.90	10.13	14.01	149.00	
74		2Q	504.0	509.0	5.0	3.51	3.91	6.13	55.50	17.55	68.62	107.58	974.02	
75		2G	509.0	514.0	5.0	4.56	5.15	6.52	78.80	22.80	117.42	148.66	1796.64	
76		2G	514.0	519.0	5.0	4.58	5.76	6.43	89.00	22.90	131.90	147.25	2038.10	
77		2E	519.0	524.0	5.0	4.71	6.17	7.05	105.00	23.55	145.30	166.03	2472.75	
78		2E	524.0	529.0	5.0	4.30	5.02	6.26	80.30	21.50	107.93	134.59	1726.45	
79		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
80		2BG	484.0	529.0	45.0	4.02	4.91	6.83	67.92	180.80	887.13	1235.09	12280.35	
81	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
82	75-11	2H	505.0	510.0	5.0	3.50	4.02	5.78	35.00	17.50	70.35	101.15	612.50	
83		2H	515.0	520.0	5.0	3.81	5.19	7.89	55.49	19.05	98.87	150.30	1057.08	
84		2H	520.0	525.0	5.0	5.21	6.84	9.59	41.79	26.05	178.18	249.82	1088.63	
85		2H	525.0	530.0	5.0	3.89	6.61	9.69	68.59	19.45	128.56	188.47	1334.08	
86		2H	530.0	535.0	5.0	3.79	5.50	7.58	68.59	18.95	104.22	143.64	1299.78	
87		2H	550.0	555.0	5.0	4.17	4.98	7.17	58.29	20.85	103.83	149.49	1215.35	
88		2H	560.0	565.0	5.0	3.60	4.09	7.09	76.09	18.00	73.62	127.62	1369.62	
89		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
90		2H	495.0	565.0	35.0	4.00	5.42	7.94	57.04	139.85	757.64	1110.50	7977.04	
91	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
92	75-11	2F	495.0	500.0	5.0	3.87	3.60	6.29	33.60	19.35	69.66	121.71	650.16	
93		2F	500.0	505.0	5.0	4.30	5.50	7.08	41.79	21.50	118.25	152.22	898.48	
94		2E	510.0	515.0	5.0	2.73	.10	.08	4.79	13.65	1.36	1.09	65.38	
95		2F	535.0	540.0	5.0	4.25	5.58	8.98	61.70	21.25	118.58	190.83	1311.12	
96		2F	540.0	545.0	5.0	4.62	4.90	8.10	54.89	23.10	113.19	187.11	1267.96	
97		2F	545.0	550.0	5.0	4.00	4.96	7.78	60.39	20.00	99.20	155.60	1207.80	
98		2D	555.0	560.0	5.0	3.31	2.02	5.23	35.00	16.55	33.43	86.56	579.25	
99		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
100		2BG	495.0	565.0	35.0	3.87	4.09	6.61	44.17	135.40	553.67	895.12	5980.16	
101	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
102	75456-15	2H	729.5	731.0	1.5	4.02	6.11	9.46	91.90	6.03	36.84	57.04	554.16	
103	75456-15	2F	722.5	729.5	7.0	4.33	4.88	7.99	48.00	30.31	147.91	242.18	1454.88	
104		2E	731.0	736.5	5.5	4.33	5.09	7.05	54.70	23.82	121.22	167.90	1302.68	
105		2F	736.5	742.5	6.0	4.33	4.58	8.19	56.20	25.81	118.20	211.36	1450.34	

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
106		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
107		2BG	722.5	742.5	18.5	4.33	4.85	7.77	52.64	79.93	387.33	621.43	4207.90	
108	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
109	76-09	2H	500.0	500.7	.7	4.22	6.53	6.18	133.00	2.95	19.29	18.26	392.88	
110		2H	500.7	504.0	3.3	4.50	4.54	4.82	49.40	14.85	67.42	71.58	733.59	
111		2H	540.7	542.7	2.0	3.97	5.43	6.66	98.70	7.94	43.11	52.88	783.68	
112		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
113		2H	500.0	545.0	6.0	4.43	5.03	5.83	69.18	25.7	129.8	142.7	1910.1	
114	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
115	76-09	2E	504.0	506.5	2.5	4.81	4.32	6.06	47.30	12.02	51.95	72.87	568.78	
116		2E	506.5	508.0	1.5	4.88	4.18	3.77	30.90	7.32	30.60	27.60	226.19	
117		Q	508.0	511.0	3.0	3.94	5.68	5.23	61.70	11.82	67.14	61.82	729.29	
118		2E	511.0	514.0	3.0	3.89	3.54	6.35	49.40	11.67	41.31	74.10	576.50	
119		2E	514.0	518.4	4.4	4.74	5.04	5.80	41.10	20.86	105.11	120.96	857.18	
120		2E	518.4	519.7	1.3	4.22	5.02	4.68	66.50	5.49	27.54	25.67	364.82	
121		2E	519.7	520.3	.6	4.10	5.44	9.58	75.40	2.46	13.38	23.57	185.48	
122		2E	520.3	521.3	1.0	4.63	4.68	5.38	64.40	4.63	21.67	24.91	298.17	
123		2E	521.3	522.5	1.2	4.65	5.09	6.20	65.10	5.58	28.40	34.60	363.26	
124		2E	522.5	522.8	.3	4.35	4.00	5.00	54.90	1.30	5.22	6.52	71.64	
125		2E	522.8	524.1	1.3	4.72	7.55	8.86	236.60	6.14	46.33	54.36	1451.78	
126		2E	524.1	525.9	1.8	4.57	4.67	5.01	61.70	8.23	38.45	41.25	507.99	
127		2E	525.9	527.2	1.3	4.55	5.35	5.40	76.80	5.92	31.65	31.94	454.27	
128		2E	527.2	528.5	1.3	4.59	5.02	6.00	84.30	5.97	29.95	35.80	503.02	
129		2E	528.5	530.7	2.2	4.61	5.48	5.68	68.60	10.14	55.58	57.61	695.74	
130		2E	530.7	535.7	5.0	4.63	5.00	5.39	73.40	23.15	115.75	124.78	1699.21	
131		2E	535.7	540.7	5.0	4.57	6.10	5.80	93.90	22.85	139.38	132.53	2145.62	
132		2D	542.7	545.0	2.3	3.17	2.62	7.86	35.30	7.29	19.10	57.31	257.37	
133		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
134		2BG	500.0	545.0	39.0	4.43	5.03	5.83	69.18	172.8	868.5	1008.2	11956.3	
135	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
136	76-10	2H	529.2	530.5	1.3	4.57	6.63	9.25	94.60	5.94	39.39	54.95	562.02	
137		2H	530.5	531.3	.8	4.29	3.80	5.88	23.30	3.43	13.04	20.18	79.97	
138		2H	531.3	534.0	2.7	4.59	8.50	12.40	36.00	12.39	105.34	153.67	446.15	
139		2H	534.0	537.0	3.0	4.50	5.34	8.25	34.30	13.50	72.09	111.38	463.05	
140		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	

529.2

7.8 4.52 6.52 9.65 43.99

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
141		2H	542.7	538.0	7.8	4.46	4.54	7.65	42.50	35.3	229.9	340.2	1551.2	
142	76-10	2D	537.0	538.0	1.0	4.46	4.54	7.65	42.50	4.46	20.25	34.12	189.55	where is this # from?
143	---	---	---	---	---	---	---	---	---	---	---	---	---	
144	76-11	2E	516.0	521.0	5.0	4.90	4.90	7.90	56.90	24.50	120.05	193.55	1394.05	
145		2E	521.0	526.0	5.0	3.73	4.60	6.58	65.80	18.65	85.79	122.72	1227.17	
146		Q	526.0	531.0	5.0	2.90	5.33	2.20	90.90	14.50	77.28	31.90	1318.05	
147		2J	531.0	536.0	5.0	3.76	11.92	13.50	310.00	18.80	224.10	253.80	5828.00	
148		2J	536.0	541.0	5.0	4.00	12.30	16.60	384.00	20.00	246.00	332.00	7680.00	
149		2J	541.0	544.0	3.0	3.26	6.85	8.88	132.40	9.78	66.99	86.85	1294.87	
150		---	---	---	---	---	---	---	---	---	---	---	---	
151		2BG	516.0	544.0	28.0	3.79	7.72	9.61	176.43	106.23	820.21	1020.81	18742.14	
152	---	---	---	---	---	---	---	---	---	---	---	---	---	
153	77-16	2H	497.5	501.5	4.0	4.31	6.81	8.35	99.70	17.24	117.40	143.95	1718.83	
154	77-16	2F	450.0	455.0	5.0	4.56	5.73	7.21	76.60	22.80	130.64	164.39	1746.48	
155		2F	455.0	460.0	5.0	4.59	5.29	6.44	65.10	22.95	121.41	147.80	1494.04	
156		2D	460.0	463.5	3.5	3.51	3.71	4.97	53.60	12.29	45.58	61.06	658.48	
157		2D	463.5	467.0	3.5	3.36	2.36	4.23	35.00	11.76	27.75	49.74	411.60	
158		2G	467.0	472.0	5.0	4.77	5.87	6.22	82.50	23.85	140.00	148.35	1967.62	
159		2G	472.0	477.0	5.0	4.51	4.40	4.90	65.20	22.55	99.22	110.50	1470.26	
160		2G	477.0	482.0	5.0	4.55	5.76	6.59	82.40	22.75	131.04	149.92	1874.60	
161		2G	482.0	487.0	5.0	4.67	5.44	6.98	80.70	23.35	127.02	162.98	1884.35	
162		2G	487.0	492.0	5.0	4.56	5.60	5.94	90.10	22.80	127.68	135.43	2054.28	
163		2G	492.0	497.5	5.5	4.60	5.89	6.44	85.10	25.30	149.02	162.93	2153.03	
164		---	---	---	---	---	---	---	---	---	---	---	---	
165		2BG	450.0	501.5	47.5	3.28	4.22	8.01	52.88	210.4	1099.4	1293.1	15714.7	
166	---	---	---	---	---	---	---	---	---	---	---	---	---	
167	82F-10	2H	541.9	543.7	1.8	4.08	5.85	8.51	110.11	7.34	42.96	62.50	808.65	
168	82F-10	2E	530.5	533.4	2.9	4.03	4.82	6.77	79.63	11.69	56.33	79.12	930.64	
169		2E	533.4	536.6	3.2	4.26	4.97	9.14	65.32	13.63	67.75	124.60	890.44	
170		2E	536.6	539.8	3.2	4.24	5.50	9.77	78.07	13.57	74.62	132.56	1059.25	
171		2D	539.8	541.9	2.1	2.99	4.51	5.41	89.58	6.28	28.32	33.97	562.47	
172		---	---	---	---	---	---	---	---	---	---	---	---	
173		2BG	530.5	543.7	11.4	3.28	4.22	8.01	52.88	45.2	227.0	370.2	3442.8	
174	---	---	---	---	---	---	---	---	---	---	---	---	---	
175	82F-11	2A	500.8	505.0	4.2	3.19	3.11	7.43	25.51	13.40	41.67	99.55	341.78	

hole rock from to interval SG PB ZN AG int*SG int*SG*PB int*SG*Zn int*SG*Ag

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
176	82F-11	2H	515.0	519.5	4.5	4.12	4.89	5.87	90.20	18.54	90.66	108.83	1672.31	
177	82F-11	2E	505.0	510.0	5.0	4.44	5.70	5.85	79.32	22.20	126.54	129.87	1760.90	
178		2E	510.0	515.0	5.0	4.74	5.74	6.61	96.11	23.70	136.04	156.66	2277.81	
179		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
180		2BG	500.8	519.5	10.0	4.10	4.29	6.78	61.90	45.9	262.6	286.5	4038.7	
181	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
182	82F-12	2E	335.2	340.0	4.8	3.28	4.22	8.01	52.88	15.74	66.44	126.11	832.54	
183		2D	340.0	344.4	4.4	2.88	3.35	4.38	46.66	12.67	42.45	55.50	591.28	
184		2D	344.4	348.7	4.3	2.96	2.07	2.95	30.79	12.73	26.35	37.55	391.90	
185		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
186		2BG	335.2	348.7	13.5	3.05	3.29	5.33	44.13	41.14	135.24	219.16	1815.71	
187	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
188	82F-14	2H	583.0	587.6	4.6	4.27	6.46	8.28	104.82	19.64	126.89	162.64	2058.87	
189	82F-14	2F	565.5	569.4	3.9	4.35	5.40	9.53	61.90	16.96	91.61	161.68	1050.13	
190		2F	569.4	573.2	3.8	4.64	5.15	6.06	78.38	17.63	90.80	106.85	1382.00	
191		2F	573.2	578.1	4.9	4.37	4.52	6.50	71.54	21.41	96.79	139.18	1531.89	
192		2F	578.1	583.0	4.9	4.49	4.78	5.53	77.76	22.00	105.16	121.67	1710.80	
193		2E	587.6	592.0	4.4	4.26	4.89	7.18	76.83	18.74	91.66	134.58	1440.10	
194		2E	592.0	596.3	4.3	4.31	5.57	9.33	74.34	18.53	103.23	172.91	1377.74	
195		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
196		2BG	565.5	596.3	26.2	4.40	5.02	7.26	73.66	115.29	579.25	836.87	8492.66	
197	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
198	82F-15	2A	598.4	601.2	2.8	2.28	2.03	5.78	28.93	6.38	12.96	36.90	184.69	
199	82F-15	2H	609.3	610.2	.9	4.22	4.99	6.26	97.04	3.80	18.95	23.78	368.56	
200	82F-15	2D	595.5	598.4	2.9	3.28	2.39	7.46	26.44	9.51	22.73	70.96	251.50	
201		2E	601.2	605.2	4.0	4.81	4.34	4.86	60.65	19.24	83.50	93.51	1166.91	
202		2E	605.2	609.3	4.1	3.16	4.08	5.27	64.99	12.96	52.86	68.28	842.01	
203		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
204		2BG	595.5	610.2	11.0	3.79	3.81	5.58	54.20	41.7	159.1	232.7	2260.4	
205	--------	----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	
206	82F-16	2G	643.3	645.5	2.2	4.15	3.35	7.37	48.43	9.13	30.59	67.29	442.17	
207		2E	645.5	649.6	4.1	4.06	5.68	8.11	89.58	16.65	94.55	135.00	1491.15	
208		2E	649.6	653.7	4.1	4.32	5.82	8.36	87.40	17.71	103.08	148.07	1548.03	
209		2E	653.7	657.8	4.1	4.36	7.36	7.38	111.35	17.88	131.57	131.92	1990.49	
210		----	------	------	-------	------	------	------	-------	--------	--------	--------	----------	

SG Pb Zn

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
211			643.3	657.8	14.5	4.23	5.86	7.86	89.17	61.36	359.79	482.28	5471.84	
212	---	---	---	---	---	---	---	---	---	---	---	---	---	
213	83F-02	2H	728.3	730.4	2.1	4.20	5.32	8.12	88.33	8.82	46.92	71.62	779.07	
214	83F-02	2E	730.4	737.0	6.6	4.10	4.29	6.78	61.90	27.06	116.09	183.47	1675.01	
215		2Q	737.0	738.4	1.4	3.52	4.88	3.11	87.40	4.93	24.05	15.33	430.71	
216		2E	738.4	739.9	1.5	4.46	5.83	6.64	92.69	6.69	39.00	44.42	620.10	
217		2D	739.9	743.0	3.1	3.29	2.92	4.72	42.61	10.20	29.78	48.14	434.58	
218		2D	743.0	745.7	2.7	3.52	6.09	4.54	111.04	9.50	57.88	43.15	1055.32	
219		2G	745.7	749.9	4.2	4.51	4.64	5.80	67.81	18.94	87.89	109.86	1284.46	
220		2D	749.9	751.6	1.7	4.15	3.25	4.27	56.62	7.06	22.93	30.12	399.45	
221		2G	751.6	755.6	4.0	4.58	4.72	4.99	84.91	18.32	86.47	91.42	1555.55	
222		2G	755.6	759.3	3.7	4.67	5.56	6.31	94.87	17.28	96.07	109.03	1639.26	
223		2E	759.3	762.6	3.3	4.23	4.91	8.67	55.36	13.96	68.54	121.02	772.77	
224		---	---	---	---	---	---	---	---	---	---	---	---	
225		2BG	728.3	762.6	32.2	4.16	4.69	5.94	73.67	133.9	628.7	796.0	9867.2	
226	---	---	---	---	---	---	---	---	---	---	---	---	---	
227	83F-12	2H	736.6	738.6	2.0	3.89	5.12	8.79	82.11	7.78	39.83	68.39	638.82	
228	83F-12	2E	738.6	742.2	3.6	4.22	5.50	9.53	81.49	15.19	83.56	144.78	1238.00	
229		2E	742.2	744.2	2.0	3.96	4.66	8.69	74.65	7.92	36.91	68.82	591.23	
230		2E	744.2	748.0	3.8	4.25	4.37	8.05	65.01	16.15	70.58	130.01	1049.91	
231		2E	748.0	752.2	4.2	3.87	3.94	7.63	62.52	16.25	64.04	124.02	1016.20	
232		---	---	---	---	---	---	---	---	---	---	---	---	
233		2BG	736.6	752.2	13.6	4.08	4.59	8.42	70.17	55.5	255.1	467.6	3895.3	
234	---	---	---	---	---	---	---	---	---	---	---	---	---	
235	83F-15	2E	652.7	654.8	2.1	4.33	4.34	12.32	59.41	9.09	112.03	112.03	540.22	
236		2G	654.8	660.6	5.8	4.28	4.55	7.50	74.65	24.82	186.18	186.18	1853.11	
237		2D	660.6	662.3	1.7	3.72	4.78	5.08	67.50	6.32	32.13	32.13	426.87	
238		2F	662.3	666.5	4.2	3.84	4.49	6.85	87.10	16.13	110.48	110.48	1404.75	
239		---	---	---	---	---	~~4.52~~	---	---	---	---	---	---	
240		2BG	652.7	666.5	13.8	4.08	7.82	7.82	74.95	56.4	440.8	440.8	4224.9	
241	---	---	---	---	---	---	---	---	---	---	---	---	---	
242	83F-19	2H	713.2	717.5	4.3	3.87	5.96	11.00	90.82	16.64	99.18	183.05	1511.34	
243		2H	717.5	721.8	4.3	3.72	4.00	8.97	66.56	16.00	63.98	143.48	1064.69	
244		2H	721.8	726.0	4.2	3.63	5.13	10.16	78.38	15.25	78.21	154.90	1194.98	
245		---	---	---	---	---	---	---	---	---	---	---	---	

	A	B	C	D	E	F	G	H	I	J	K	L	M	N
246		2H	736.6	726.0	12.8	3.74	5.04	10.05	78.75	47.9	241.4	481.4	3771.0	
247	---	---	---	---	---	---	---	---	---	---	---	---	---	
248	83F-19	2D	697.9	699.5	1.6	3.23	4.84	7.16	68.12	5.17	25.01	37.00	352.04	
249		2E	699.5	704.1	4.6	3.66	6.47	10.64	96.11	16.84	108.93	179.14	1618.11	
250		2E	704.1	708.1	4.0	3.38	8.57	16.20	114.15	13.52	115.87	219.02	1543.31	
251		2E	708.7	713.2	4.5	3.51	7.51	13.90	101.71	15.79	118.62	219.55	1606.51	
252		2E	726.0	728.0	2.0	3.83	4.08	7.81	45.10	7.66	31.25	59.82	345.47	
253		---	---	---	---	---	---	---	---	---	---	---	---	
254		2BG	697.9	728.0	16.7	3.53	6.78	12.12	92.67	59.0	399.7	714.5	5465.4	
255	---	---	---	---	---	---	---	---	---	---	---	---	---	

	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA
1	ROCK	HOLE NO	LENGTH	S.G	PB	ZN	SILVER	AREA(SQFT)	TONNES		S*W	T*W	U*W
2	------	--------	--------	--------	--------	--------	--------	----------	--------		--------	--------	----------
3	2A ✓	66-05	5.0	3.09	1.28	4.00	22.10	37665	16478		21092	65914	364174
4	✓	71-03	5.0	3.19	2.40	2.70		58281	26323		63176	71073	0
5	Not us	82F-11	4.2	3.19	3.11	7.43	25.51		0		0	0	0
6	✓	82F-15	2.8	2.28	2.03	5.78	28.93	84166	15215		30887	87944	440178
7		--------	--------	--------	--------	--------	--------	----------	--------		--------	--------	--------
8	SUM 2A				1.98	3.88	13.86		58017		115155	224931	804353
9	------	--------	--------	--------	--------	--------	--------	----------	--------		--------	--------	--------
10	2H ✓	70-12	.5	4.60	4.70	6.20	70.00	34875	2271		10676	14083	158998
11	✓	71-01	1.0	3.79	2.93	6.24	58.40	53391	5730		16789	35755	334634
12	not us	75-11	5.0	3.87	3.60	6.29	33.60		0		0	0	0
13	✓	75456-15	1.5	4.02	6.11	9.46	91.90	63086	10772		65818	101904	989957
14	not used	76-09	6.0	4.43	5.03	5.83	69.18		0		0	0	0
15	✓	76-10	7.8	4.46	4.54	7.65	42.50	5425	5344		24263	40883	227127
16	not used	77-16	4.0	4.31	6.81	8.35	99.70		0		0	0	0
17	✓	82F-10	1.8	4.08	5.85	8.51	110.11	38595	8026		46954	68304	883774
18	not used	82F-11	4.5	4.12	4.89	5.87	90.20		0		0	0	0
19	✓	82F-14	4.6	4.27	6.46	8.28	104.82	45415	25260		163180	209154	2647767
20	✓	82F-15	.9	4.22	4.99	6.26	97.04	84166	9052		45169	56665	878401
21	✓	83F-02	2.1	4.20	5.32	8.12	88.33	88661	22144		117805	179808	1955960
22	✓	83F-12	2.0	3.89	5.12	8.79	82.11	90056	19840		101581	174394	1629067
23	✓	83F-19	12.8	3.74	5.04	10.05	78.75	114701	155525		783994	1563706	12248293
24		--------	--------	--------	--------	--------	--------	----------	--------		--------	--------	--------
25	SUM 2H				5.21	9.26	83.17		263965		1376228	2444655	21953979
26	------	--------	--------	--------	--------	--------	--------	----------	--------		--------	--------	--------
27	2BG ✓	66-05	5.0	5.00	5.00	5.00	5.00	37665	26664		133321	133321	133321
28	✓	70-12	32.0	4.83	6.35	8.98	59.29	34875	152625		968860	1370074	9049130
29	✓	70-13	10.0	4.08	5.10	7.97	57.22	72541	83707		426760	667460	4789683
30		70-17	82.0	1.11	5.23	7.17	0.0		0		0	0	0
31	✓	71-02	14.0	4.03	4.06	7.07	0.0	72851	116288		471885	822617	0
32	✓	71-03	5.0	4.33	4.50	5.80	0.0	58281	35730		160786	207235	0
33	✓	71-04	10.0	4.33	3.55	5.70	0.0	17205	21096		74890	120245	0
34	✓	71-05	10.0	4.33	5.45	5.78	77.99	39060	47893		260941	276818	3735068
35	✓	72004	17.1	2.93	2.79	6.66	47.80	93156	132331		368979	880875	6325253

	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA
36	✓	72-13	45.0	3.93	6.60	6.97	86.67	37665	188676		1245783	1315383	16352181
37	not used	74-17	45.0	4.02	4.91	6.83	67.92		0		0	0	0
38	not used	75-11	35.0	3.87	4.09	6.61	44.17		0		0	0	0
39	✓	75456-15	18.5	4.33	4.85	7.77	52.64	63086.00	142792		691927	1110136	7517082
40	not used	76-09	6.0	4.43	5.03	5.83	69.18		0		0	0	0
41									0		0	0	0
42	✓	76-10	1.0	4.46	4.54	7.65	42.50	5425	685		3111	5241	29119
43	✓	76-11	28.0	3.79	7.72	9.61	176.43	20305	61080		471608	586948	10776378
44	not used	77-16	47.5	3.28	4.22	8.01	52.88		0		0	0	0
45	✓	82F-10	11.4	3.28	4.22	8.01	52.88	38595	40866		172454	327335	2160985
46		82F-11	10.0	4.10	4.29	6.78	61.90		0		0	0	0
47	✓	82F-12	13.5	3.05	3.29	5.33	44.13	82236	95812		314928	510358	4228242
48	✓	82F-14	26.2	4.40	5.02	7.26	73.66	45415	148263		744936	1076239	10921783
49	✓	82F-15	11.0	3.79	3.81	5.58	54.20	84166	99405		379180	554710	5387350
50	✓	82F-16	14.5	4.23	5.86	7.86	89.17	68200	118508		694831	931404	10567397
51	✓	83F-02	32.2	4.16	4.69	5.94	73.67	88661	336264		1578433	1998369	24772947
52	✓	83F-12	13.6	4.08	4.59	8.42	70.17	90056	141573		650487	1192520	9933633
53	✓	83F-15	13.8 (12.8)	3.74	5.04	10.05	78.75	82306	111600		562570	1122068	8789008
54	✓	83F-19	16.7	3.53	6.78	12.12	92.67	114701	191565		1298171	2320826	17751807
55		---	---	---	---	---	---	---	---		---	---	---
56	SUM 2B				5.09	7.64	66.81		2293423		11674842	17530183	153220369
57	---	---	---	---	---	---	---	---	---		---	---	---
58	TOTAL				5.03	7.72	67.29		2615404		13166224	20199769	175978701
59	---	---	---	---	---	---	---	---	---		---	---	---
60													
61													
62													
63													
64													
65													
66													
67													
68													
69													
70													

FARO UNDERGROUND 9% CUTOFF

SUMMARY OF GEOLOGIC RESERVES

	TONNES	LEAD (%)	LEAD (%)	LEAD PLUS ZINC	SILVER (g/t)	PERCENT OF TOTAL RESERVE
WEST ZONE						
A TYPE	42,801	1.97	3.20	5.17	8.5	7.4%
BG TYPE	520,083	4.92	7.82	12.74	53.1	90.2%
H TYPE	13,417	4.68	7.61	12.29	54.6	2.3%
TOTAL	576,301	4.70	7.47	12.17	49.8	
EAST ZONE						
A TYPE	15,215	2.03	5.78	7.81	28.9	0.7%
BG TYPE	1,787,645	5.10	7.51	12.61	71.6	87.1%
H TYPE	250,619	5.28	9.39	14.67	85.0	12.2%
TOTAL	2,053,479	5.10	7.73	12.83	72.9	
BOTH ZONES						
A TYPE	58,016	1.99	3.88	5.86	13.9	2.2%
BG TYPE	2,307,728	5.06	7.58	12.64	67.4	87.8%
H TYPE	264,036	5.25	9.30	14.55	83.5	10.0%
TOTAL	2,629,780	5.01	7.67	12.68	67.8	

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NOTE:

WITH A 100 FOOT RATHER THAN 50 CROWN PILLAR
AND FOLLOWING A 10 FOOT MINIMUM WIDTH THRUOUT

WEST ZONE	453,742	4.35	7.24	11.59	40.0
EAST ZONE	2,015,303	5.11	7.75	12.86	73.3
BOTH ZONES	2,469,045	4.97	7.66	12.63	67.2

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DILUTED GEOLOGIC RESERVES:

DILUTED BY THE FOLLOWING:

PERCENT DILUTION:	25 %
LEAD IN DILUTANT:	1.60 %
ZINC IN DILUTANT:	2.40 %
SILVER IN DILUTANT:	25 (g/t)

WEST ZONE	720,376	3.76	5.98	9.74	39.88
EAST ZONE	2,566,849	4.08	6.19	10.27	58.37
BOTH ZONES	3,287,225	4.01	6.14	10.15	54.32

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SAME DILUTION APPLIED TO THE RESERVES WITH CROWN PILLAR REDUCTION:

WEST ZONE	567,178	3.48	5.80	9.28	32.05
EAST ZONE	2,519,129	4.09	6.20	10.30	58.72
BOTH ZONES	3,086,306	3.98	6.13	10.11	53.82

CURRAGH RESOURCES
FARO UNDERGROUND

POLYGON	ORE TYPE	ORE TONNES	SG	LEAD (%)	ZINC (%)	SILVER (g/t)	T*PB	T*ZN	T*AG
EAST ZONE									
83F02	H	22,144	4.20	5.32	8.12	88.33	117806	179809	1955980
	BG	336,264	4.16	4.69	5.94	73.67	1577078	1997408	24772569
4567515	H	10,772	4.02	6.11	9.46	91.90	65817	101903	989947
	BG	142,792	4.33	4.85	7.77	52.64	692541	1109494	7516571
83F12	H	19,840	3.89	5.12	8.79	82.11	101581	174394	1629062
	BG	141,573	4.08	4.59	8.42	70.17	649820	1192045	9934177
83F19	H	155,525	3.74	5.04	10.05	78.75	783846	1563026	12247594
	BG	191,565	3.53	6.78	12.12	92.67	1298811	2321768	17752329
82F16	BG	118,508	4.23	5.86	7.86	89.17	694457	931473	10567358
82F15	A	15,215	2.28	2.03	5.78	28.93	30886	87943	440170
	H	9,052	4.22	4.99	6.26	97.04	45169	56666	878406
	BG	99,405	3.79	3.81	5.58	54.20	378733	554680	5387751
82F12	BG	95,812	3.05	3.29	5.33	44.13	315221	510678	4228184
7013	BG	83,707	4.08	5.10	7.97	57.22	426906	667145	4789715
82F14	H	25,260	4.27	6.46	8.28	107.82	163180	209153	2723533
	BG	148,263	4.40	5.02	7.26	73.66	744280	1076389	10921053
83F15	BG	131,225	4.08	4.52	7.82	74.95	593137	1026180	9835314
7105	BG	47,893	4.33	5.45	5.78	77.99	261017	276822	3735175
7213	BG	188,676	3.93	6.60	6.97	86.67	1245262	1315072	16352549
82F10	H	8,026	4.08	5.85	8.51	110.11	46952	68301	883743
	BG	40,866	3.28	4.22	8.01	52.88	172455	327337	2160994
7104	BG	21,096	4.33	3.55	5.70	0.00	74891	120247	0
TOTAL		2,053,479		5.10	7.73	72.90	10479846	15867931	149702172

AVERAGES FOR ORE TYPES

ORE TYPE=	T	A T*PB	T*ZN	T*AG
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	15215	30886	87943	440170
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
	0	0	0	0
TOTAL	15215	30886	87943	440170
AVERAGE		2.03	5.78	28.93

WEST ZONE

6605	A	16,478	3.09	1.28	4.00	22.10	21092	65912	364164		16478	21092	65912	364164
	BG	21,704	4.07	5.20	9.11	65.20	112861	197723	1415101		0	0	0	0
72004	BG	132,331	2.93	2.79	6.66	47.80	369203	881324	6325422		0	0	0	0
7102	BG	116,288	4.03	4.06	7.07	0.00	472129	822156	0		0	0	0	0
7611	BG	61,080	3.79	7.72	9.61	176.43	471538	586979	10776344		0	0	0	0
7103	A	26,323	3.19	2.40	2.70	0.00	63175	71072	0		26323	63175	71072	0
	BG	35,370	4.33	4.50	5.80	0.00	159165	205146	0		0	0	0	0
7610	H	5,416	4.52	6.52	9.65	43.99	35312	52264	238250		0	0	0	0
	BG	685	4.46	4.54	7.65	42.50	3110	5240	29113		0	0	0	0
7012	H	2,271	4.60	4.70	6.20	70.00	10674	14080	158970		0	0	0	0
	BG	152,625	4.83	6.35	8.98	59.29	969169	1370573	9049136		0	0	0	0
7101	H	5,730	3.79	2.93	6.24	58.40	16789	35755	334632		0	0	0	0
TOTAL		576,301		4.69	7.48	49.78	2704217	4308226	28691131	TOTAL	42801	84267	136984	364164
										AVERAGE		1.97	3.20	8.51

BOTH ZONES

ORE TONNES	SG	LEAD (%)	ZINC (%)	SILVER (g/t)	ORE TYPE=A TONNES	LEAD (%)	ZINC (%)	SILVER (g/t)
2,629,780		5.01	7.67	67.84	58,016	1.98	3.88	13.86

CURRAGH RESOURCES
FARO UNDERGROUND

WITH A 100 RATHER THAN 50 FOOT CROWN PILLAR

POLYGON	ORE TYPE	ORE TONNES		SG	LEAD (%)	ZINC (%)	SILVER (g/t)
EAST ZONE							
83F02	H	22,144		4.20	5.32	8.12	88.33
	BG	336,264		4.16	4.69	5.94	73.67
4567515	H	10,772		4.02	6.11	9.46	91.90
	BG	142,792		4.33	4.85	7.77	52.64
83F12	H	19,840		3.89	5.12	8.79	82.11
	BG	141,573		4.08	4.59	8.42	70.17
83F19	H	155,525		3.74	5.04	10.05	78.75
	BG	191,565		3.53	6.78	12.12	92.67
82F16	BG	118,508		4.23	5.86	7.86	89.17
82F15	A	15,215		2.28	2.03	5.78	28.93
	H	9,052		4.22	4.99	6.26	97.04
	BG	99,405		3.79	3.81	5.58	54.20
82F12	BG	95,812		3.05	3.29	5.33	44.13
7013	BG	75,336	*	4.08	5.10	7.97	57.22
82F14	H	25,260		4.27	6.46	8.28	107.82
	BG	148,263		4.40	5.02	7.26	73.66
83F15	BG	131,225		4.08	4.52	7.82	74.95
7105	BG	33,525	*	4.33	5.45	5.78	77.99
7213	BG	188,676		3.93	6.60	6.97	86.67
82F10	H	7,223	*	4.08	5.85	8.51	110.11
	BG	36,779		3.28	4.22	8.01	52.88
7104	BG	10,548	*	4.33	3.55	5.70	0.00
TOTAL		2,015,303			5.11	7.75	73.34

****

POLYGON	ORE TYPE	ORE TONNES		SG	LEAD (%)	ZINC (%)	SILVER (g/t)
WEST ZONE							
6605	A	9,887	*	3.09	1.28	4.00	22.10
	BG	13,022	*	4.07	5.20	9.11	65.20
72004	BG	132,331		2.93	2.79	6.66	47.80
7102	BG	116,288		4.03	4.06	7.07	0.00
7611	BG	24,432	*	3.79	7.72	9.61	176.43
7103	A	21,058	*	3.19	2.40	2.70	0.00
	BG	28,296	*	4.33	4.50	5.80	0.00
7610	H	0	**	4.52	6.52	9.65	43.99
	BG	0	**	4.46	4.54	7.65	42.50
7012	H	1,590	*	4.60	4.70	6.20	70.00
	BG	106,838	*	4.83	6.35	8.98	59.29
7101	H	0	**	3.79	2.93	6.24	58.40
TOTAL		453,742			4.35	7.24	40.00

* CROWN PILLAR REDUCTION
**LESS THAN 10 FEET THICK

****

BOTH ZONES	ORE TONNES	SG	LEAD (%)	ZINC (%)	SILVER (g/t)
	2,469,045		4.97	7.66	67.21

****

COMPOSITING OF 83F-15

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG
2.1	4.34	12.32	4.33	39.46	112.03	9.093	59.41	540.2151
5.8	4.55	7.50	4.28	112.95	186.18	24.824	74.65	1853.111
1.7	4.78	5.08	3.72	30.23	32.13	6.324	67.5	426.87
4.2	4.49	6.85	3.84	72.41	110.48	16.128	87.1	1404.748
13.80	4.52	7.82	4.08	255.06	440.81	56.37	74.95	4224.95

TONNAGE FOR 83F-15

A	L	SG	mA	mL	mV	mT
82,306	13.8	4.08	7,646	4.21	32,163	131,225

****

COMPOSITING OF 66-05

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG
5	1.28	4.00	3.09	19.78	61.80	15.45	22.1	341.445
5	5.20	9.11	4.07	105.82	185.39	20.35	65.2	1326.82
10.00	3.51	6.90	3.58	125.60	247.19	35.80	46.60	1668.27

TONNAGE FOR 66-05

A	L	SG	mA	mL	mV	mT	
37,665	5.0	3.09	3,499	1.52	5,333	16,478	A
37,665	5.0	4.07	3,499	1.52	5,333	21,704	BG

****

COMPOSITING OF 76-10

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG
1.3	6.63	9.25	4.57	39.39	54.95	5.941	94.6	562.0186
0.8	3.80	5.88	4.29	13.04	20.18	3.432	23.3	79.9656
2.7	8.50	12.40	4.59	105.34	153.67	12.393	36	446.148
3	5.34	8.25	4.50	72.09	111.38	13.5	34.3	463.05
7.80	6.52	9.65	4.52	229.86	340.18	35.27	43.99	1551.18

TONNAGE FOR 76-10

A	L	SG	mA	mL	mV	mT
5,425	7.8	4.52	504	2.38	1,198	5,416
5,425	1.0	4.46	504	0.30	154	685

****

CURRAGH RESOURCES
FARO UNDERGROUND

AVERAGES FOR ORE TYPES

POLYGON	ORE TYPE	ORE TONNES	ORE VOLUME	SG	LEAD (%)	ZINC (%)	SILVER (g/t)	T*PB	T*ZN	T*AG		ORE TYPE= T	A T*PB	T*ZN	T*AG
EAST ZONE															
83F02	H	22,144	5,272	4.20	5.32	8.12	88.33	117806	179809	1955980		0	0	0	0
	BG	336,264	80,833	4.16	4.69	5.94	73.67	1577078	1997408	24772569		0	0	0	0
4567515	H	10,772	2,680	4.02	6.11	9.46	91.90	65817	101903	989947		0	0	0	0
	BG	142,792	32,977	4.33	4.85	7.77	52.64	692541	1109494	7516571		0	0	0	0
83F12	H	19,840	5,100	3.89	5.12	8.79	82.11	101581	174394	1629062		0	0	0	0
	BG	141,573	34,699	4.08	4.59	8.42	70.17	649820	1192045	9934177		0	0	0	0
83F19	H	155,525	41,584	3.74	5.04	10.05	78.75	783846	1563026	12247594		0	0	0	0
	BG	191,565	54,268	3.53	6.78	12.12	92.67	1298811	2321768	17752329		0	0	0	0
82F16	BG	118,508	28,016	4.23	5.86	7.86	89.17	694457	931473	10567358		0	0	0	0
82F15	A	15,215	6,673	2.28	2.03	5.78	28.93	30886	87943	440170		15215	30886	87943	440170
	H	9,052	2,145	4.22	4.99	6.26	97.04	45169	56666	878406		0	0	0	0
	BG	99,405	26,228	3.79	3.81	5.58	54.20	378733	554680	5387751		0	0	0	0
82F12	BG	95,812	31,414	3.05	3.29	5.33	44.13	315221	510678	4228184		0	0	0	0
7013	BG	83,707	20,516	4.08	5.10	7.97	57.22	426906	667145	4789715		0	0	0	0
82F14	H	25,260	5,916	4.27	6.46	8.28	107.82	163180	209153	2723533		0	0	0	0
	BG	148,263	33,696	4.40	5.02	7.26	73.66	744280	1076389	10921053		0	0	0	0
83F15	BG	131,225	32,163	4.08	4.52	7.82	74.95	593137	1026180	9835314		0	0	0	0
7105	BG	47,893	11,061	4.33	5.45	5.78	77.99	261017	276822	3735175		0	0	0	0
7213	BG	188,676	48,009	3.93	6.60	6.97	86.67	1245262	1315072	16352549		0	0	0	0
82F10	H	8,026	1,967	4.08	5.85	8.51	110.11	46952	68301	883743		0	0	0	0
	BG	40,866	12,459	3.28	4.22	8.01	52.88	172455	327337	2160994		0	0	0	0
7104	BG	21,096	4,872	4.33	3.55	5.70	0.00	74891	120247	0		0	0	0	0
TOTAL		2,053,479	522,549	3.93	5.10	7.73	72.90	10479846	15867931	149702172	TOTAL	15215	30886	87943	440170
											AVERAGE		2.03	5.78	28.93
WEST ZONE															
6605	A	16,478	5,333	3.09	1.28	4.00	22.10	21092	65912	364164		16478	21092	65912	364164
	BG	21,704	5,333	4.07	5.20	9.11	65.20	112861	197723	1415101		0	0	0	0
72004	BG	132,331	45,164	2.93	2.79	6.66	47.80	369203	881324	6325422		0	0	0	0
7102	BG	116,288	28,856	4.03	4.06	7.07	0.00	472129	822156	0		0	0	0	0
7611	BG	61,080	16,116	3.79	7.72	9.61	176.43	471538	586979	10776344		0	0	0	0
7103	A	26,323	8,252	3.19	2.40	2.70	0.00	63175	71072	0		26323	63175	71072	0
	BG	35,370	8,169	4.33	4.50	5.80	0.00	159165	205146	0		0	0	0	0
7610	H	5,416	1,198	4.52	6.52	9.65	43.99	35312	52264	238250		0	0	0	0
	BG	685	154	4.46	4.54	7.65	42.50	3110	5240	29113		0	0	0	0
7612	H	2,271	494	4.60	4.70	6.20	70.00	10674	14080	158970		0	0	0	0
	BG	152,625	31,599	4.83	6.35	8.98	59.29	969169	1370573	9049136		0	0	0	0
7101	H	5,730	1,512	3.79	2.93	6.24	58.40	16789	35755	334632		0	0	0	0
	N	0		0	0	0	0	0	0	0		0	0	0	0
	N	0		0	0	0	0	0	0	0		0	0	0	0
	N	0		0	0	0	0	0	0	0		0	0	0	0
	N	0		0	0	0	0	0	0	0		0	0	0	0
	N	0		0	0	0	0	0	0	0		0	0	0	0

N	0	0	0	0	0	0	0	0	0	0	0	0	0
N	0	0	0	0	0	0	0	0	0	0	0	0	0
N	0	0	0	0	0	0	0	0	0	0	0	0	0
N	0	0	0	0	0	0	0	0	0	0	0	0	0
N	0	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	576,301	152,178	3.79	4.69	7.48	49.78	2704217	4308226	28691131	TOTAL	42801	84267	136984	364164
										AVERAGE	1.97	3.20	8.51	

****

BOTH ZONES

^^^^^^^^^^

ORE TONNES	ORE VOLUME	SG	LEAD (%)	ZINC (%)	SILVER (g/t)
2,629,780	674,728	3.90	5.01	7.67	67.84

ORE TYPE=A

TONNES	LEAD (%)	ZINC (%)	SILVER (g/t)
58,016	1.98	3.88	13.86

****

COMPOSITING OF 83F-15

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG
2.1	4.34	12.32	4.33	39.46	112.03	9.093	59.41	540.2151
5.8	4.55	7.50	4.28	112.95	186.18	24.824	74.65	1853.111
1.7	4.78	5.08	3.72	30.23	32.13	6.324	67.5	426.87
4.2	4.49	6.85	3.84	72.41	110.48	16.128	87.1	1404.748
13.80	4.52	7.82	4.08	255.06	440.81	56.37	74.95	4224.95

TONNAGE FOR 83F-15

A	L	SG	mA	mL	mV	mT
82,306	13.8	4.08	7,646	4.21	32,163	131,225

****

COMPOSITING OF 66-05

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG
5	1.28	4.00	3.09	19.78	61.80	15.45	22.1	341.445
5	5.20	9.11	4.07	105.82	185.39	20.35	65.2	1326.82
10.00	3.51	6.90	3.58	125.60	247.19	35.80	46.60	1668.27

TONNAGE FOR 66-05

A	L	SG	mA	mL	mV	mT	
37,665	5.0	3.09	3,499	1.52	5,333	16,478	A
37,665	5.0	4.07	3,499	1.52	5,333	21,704	BG

****

COMPOSITING OF 76-10

L	PB	ZN	SG	L*SG*PB	L*SG*ZN	L*SG	AG	L*SG*AG

1.3	6.63	9.25	4.57	39.39	54.95	5.941	94.6	562.0186
0.8	3.80	5.88	4.29	13.04	20.18	3.432	23.3	79.9656
2.7	8.50	12.40	4.59	105.34	153.67	12.393	36	446.148
3	5.34	8.25	4.50	72.09	111.38	13.5	34.3	463.05
7.80	6.52	9.65	4.52	229.86	340.18	35.27	43.99	1551.18

TONNAGE FOR 76-10

A	L	SG	∝A	∝L	∝V	∝T
5,425	7.8	4.52	504	2.38	1,198	5,416
5,425	1.0	4.46	504	0.30	154	685

****

A	ISSUED FOR TECHNICAL REVIEW	FEB. 87	Z.A.
No.	DESCRIPTION		
	REVISIONS		

DWG. NO. | REFERENCE DRAWINGS

SECTION MINING		CLIENT: CURRAGH RESOURCES	
SCALE 1" = 100'	DATE	LOCATION. FARO, YUKON	
DESIGNED BY J.B.F.	FEB 87	KILBORN	
DRAWN BY Z.A	FEB 87		
CHECKED BY			
APPROVED BY J.B.F.			

TITLE	B.O.M. No.	
FARO AREA DEPOSITS	PROJECT No. 3509	DIVISION No. 19
FARO DEPOSIT OPEN PIT PLAN END OF 1992 - ULTIMATE	DRAWING NUMBER FIG. 5.6.5-7	REV. A

DWG. NO.	REFERENCE DRAWINGS

No.	DESCRIPTION	CLIENT	PROJ. ENG.	CHECK
	REVISIONS			

No.	DESCRIPTION
	REVISIONS

No.	DESCRIPTION		
A	ISSUED FOR TECHNICAL REVIEW	MAR. 87	ZA
	REVISIONS		

SECTION: MINING

SCALE: 1" = 100'	DATE
DESIGNED BY: J.B.F	MAR. 87
DRAWN BY: Z.A	MAR. 87
CHECKED BY:	
APPROVED BY: JBF	

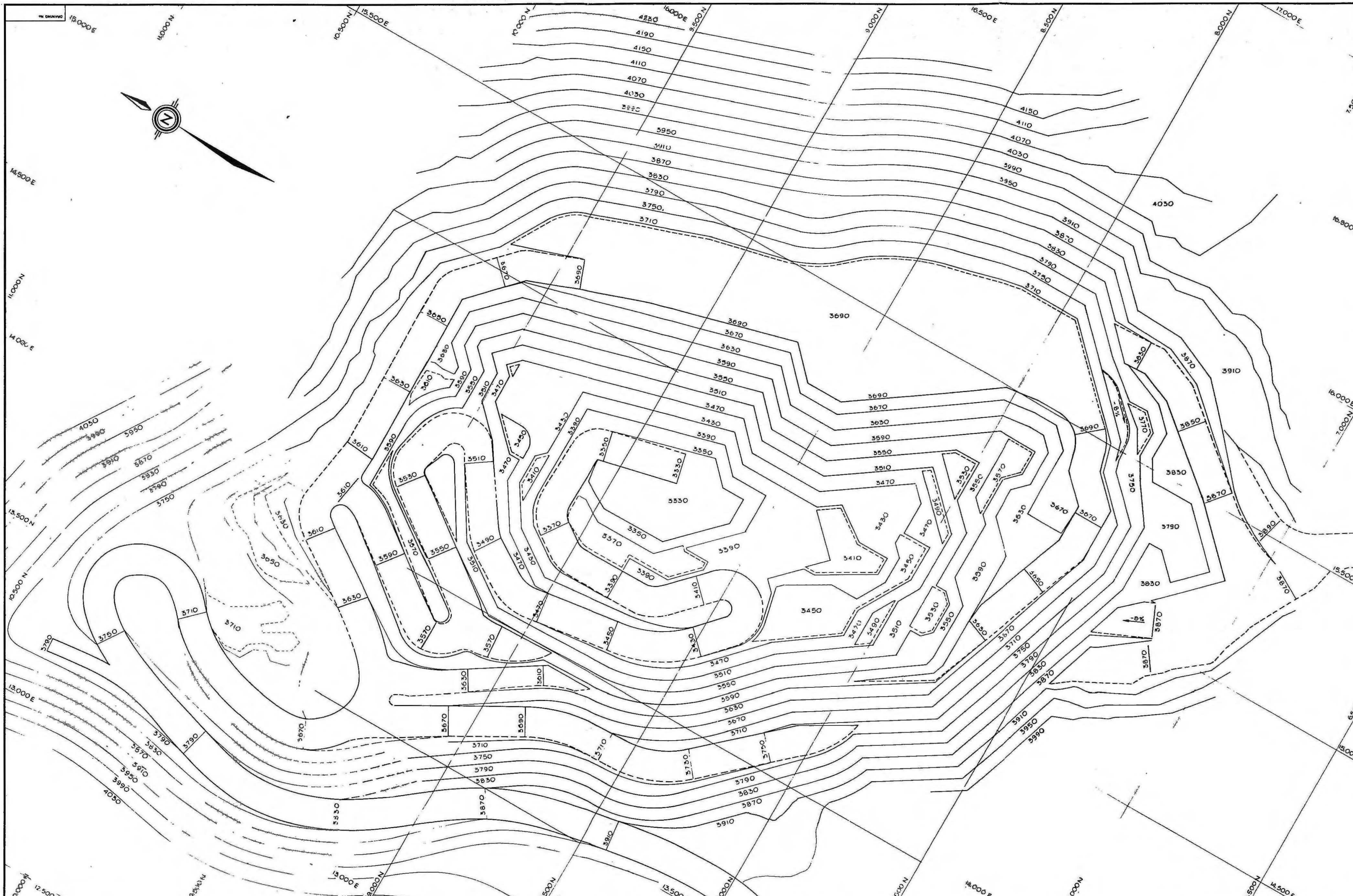
CLIENT: CURRAGH RESOURCES

LOCATION: FARO, YUKON

KILBORN

TITLE
FARO AREA DEPOSITS
FARO DEPOSIT
OPEN PIT PLAN
END OF 1991

B.O.M. No.	
PROJECT No.	DIVISION No.
3509	19
DRAWING NUMBER	
FIG. 5.6.5-6	REV. A



SECTION: MINING		CLIENT: CURRAGH RESOURCES	TITLE: FARO AREA DEPOSITS
SCALE: 1" = 100'	DATE		PROJECT No. 3509 / DIVISION No. 19
DESIGNED BY: J.B.F.	MAR.87	LOCATION: FARO, YUKON	FARO DEPOSIT OPEN PIT PLAN END OF 1990
DRAWN BY: Z.A.	MAR.87	KILBORN	DRAWING NUMBER: FIG.5.6.5-5
CHECKED BY:			REV. A
APPROVED BY: JBF			

REVISIONS

No.	DESCRIPTION		
A	ISSUED FOR TECHNICAL REVIEW	MAR 87	ZA

DWG. NO. — REFERENCE DRAWINGS

DWG. NO.	REFERENCE DRAWINGS

No.	DESCRIPTION	CLIENT	FINAL ENG.	CHECK
	REVISIONS			

No.	DESCRIPTION	CLIENT	FINAL ENG.	CHECK
	REVISIONS			

No.	DESCRIPTION			
A	ISSUED FOR TECHNICAL REVIEW	MAR.87	ZA	
	REVISIONS			

SECTION: MINING	
SCALE: 1" = 100'	DATE
DESIGNED BY: J.B.F.	MAR 87
DRAWN BY: Z.A	MAR. 87
CHECKED BY:	
APPROVED BY: JBF	

CLIENT: CURRAGH RESOURCES
LOCATION. FARO. YUKON

KILBORN

TITLE
FARO AREA DEPOSITS
FARO DEPOSIT
OPEN PIT PLAN
END OF 1989

R.O.M. No.	
PROJECT No.	DIVISION No.
3509	19
DRAWING NUMBER	
FIG.5.6.5-4	REV. A

SECTION: MINING		CLIENT: CURRAGH RESOURCES	TITLE: FARO AREA DEPOSITS
SCALE: 1" = 100'	DATE	LOCATION: FARO, YUKON	FARO DEPOSIT OPEN PIT PLAN END OF 1988
DESIGNED BY: J.B.F.	MAR. 87	KILBORN	
DRAWN BY: Z.A.	MAR. 87		
CHECKED BY:			
APPROVED BY: JBF			

D.O.H. No.

PROJECT No.	DIVISION No.
3509	19

DRAWING NUMBER: FIG. 5.6.5 -3 | REV. A

No.	DESCRIPTION		
A	ISSUED FOR TECHNICAL REVIEW	MAR. 87	Z.A.

REVISIONS

DWG. NO. | REFERENCE DRAWINGS