



Resources Inc.

017743

P.O. Box 1000
Faro, Yukon
Y0B 1K0
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TELECOPIER COVER LETTER

TO:

GREGG JILSON, J.P. OF EXPLORATION
WHSE.

TELECOPIER NO. _____

FROM:

NAME: E. Sp.

CURRAGH RESOURCES INC., BOX 1000, FARO, YUKON, Y0B 1K0

TOTAL NO. OF PAGES: 3 DATE: 27/08/91 TIME: _____ OPERATOR _____
(Including Cover Letter)

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MESSAGE HELLO GREGG:

1/ OUR PRECIPITATION RECORD IS NOT COMPLETE
FOR APRIL - MAY. SECURITY WAS ASSIGNED
WEATHER - REPORTING DURING THE STRIKE
BUT WASN'T CAREFUL TO RECORD PPT. I
HAVE HOWEVER ASSEMBLED FARO AIRPORT PPT.
DATA PLUS WHAT WE HAVE ON FILE WHICH
IS COMPLETE.

2/ I HAVE APPENDED A BIOASSAY RESULT
I RECEIVED TODAY FROM B.C. RESEARCH.

TAKE CARE
— E.

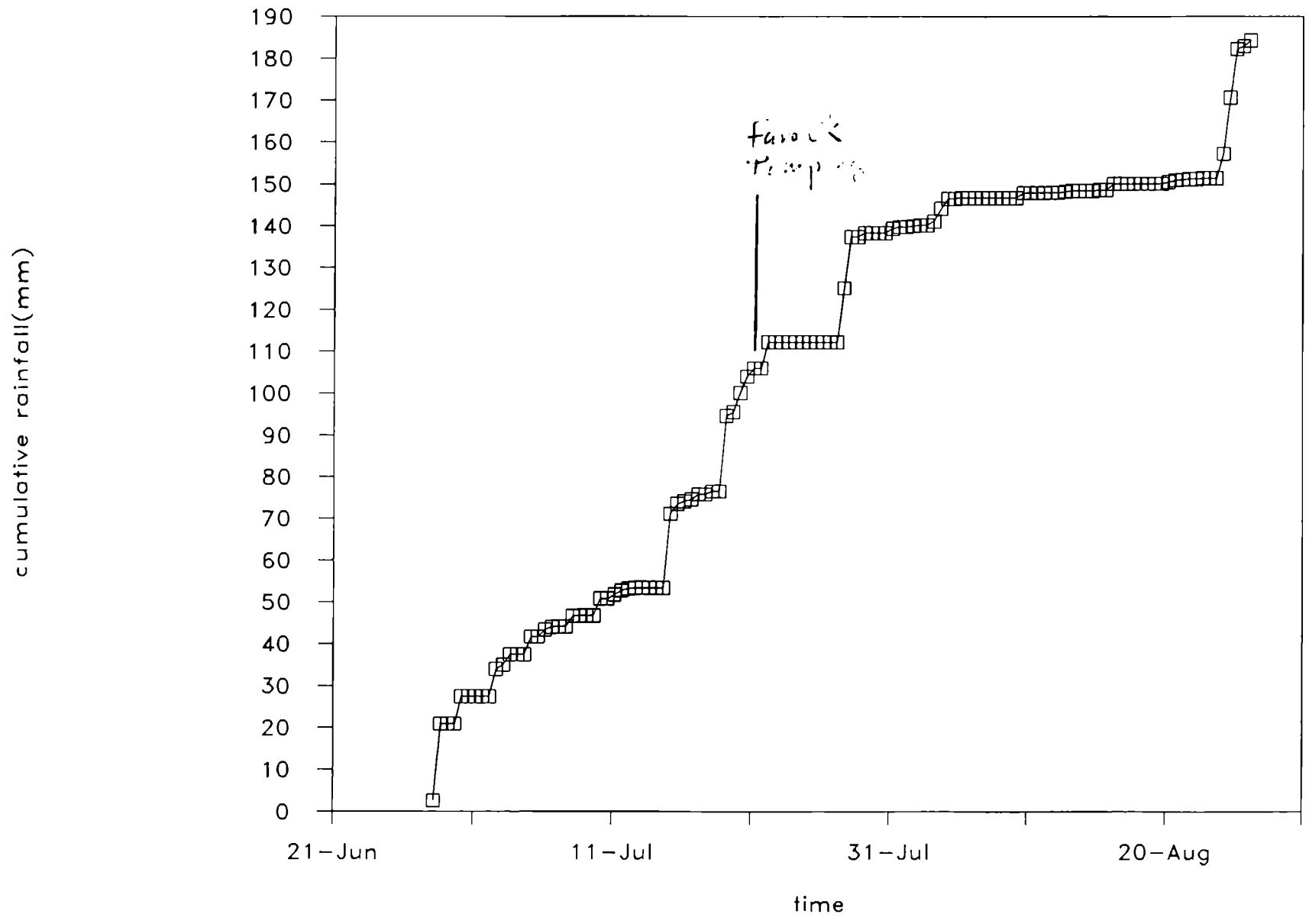
PRECIPITATION (mm)

APRIL - PRESENT 1991

<u>DATE</u>	<u>FARO AIRPORT</u>	<u>FARO MINESITE</u>
APRIL	2.8 mm	incomplete
MAY	22.4	not measured
JUNE	30.2	28.5
JULY	115.4	116.3
→ AUG 26		46.0

FARO MINE – RAINFALL

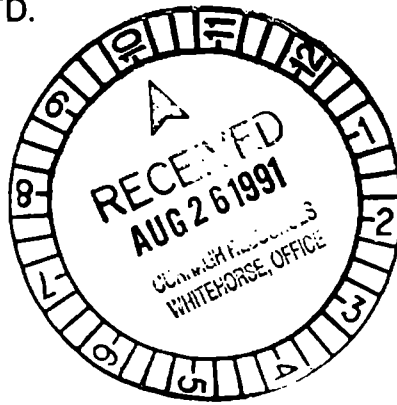
cumulative rainfall at minesite



C.O. BRAWNER ENGINEERING LTD.

Consulting Geotechnical Engineers

Ste. 502, Kapilano 100, 100 Park Royal
WEST VANCOUVER, B.C., CANADA V7T 1A2



1410 W. 14th
P.O. Box
Geotechnical
Telephone: (604) 922-3717
(604) 987-2771
Fax: (604) 925-1366
NE Wall

August 9, 1991

Mr. John Hogg
General Manager
Curragh Resources, Inc.
P.O. Box 1000
Faro, Yukon Y0B 1K0

Dear Sir:

Re: Evaluation of East Pit Wall Stability

Further to the request of Mr. Colin Benner, Vice President, the stability of the east pit wall has been inspected and evaluated.

A site inspection of the pit wall was made Wednesday, August 7, 1991. Typical site photographs are appended.

Information was provided to me by Mr. A. Stewart of Piteau Associates and Curragh Mining staff on movement monitoring and history, geology and structural geology, groundwater and surface water, blasting and the mining plan.

A summary of my comments and recommendations made to senior mining staff at the mine Thursday, August 8th is as follows:

Geology

The east wall is comprised extensively of moderately weak to weak phyllites with a high mica content and lower than normal friction angle, compared to other local rock.

2 materials
fresh hard
blocky CS
- friable altered
Chl. CS

A harder nose exists about midway along the east pit wall which is described as calc silicate rock. This rock is much more competent and is tending to act as a retaining wall to the slope.

The phyllites both north and south of the calc silicate is moving and ravelling. These zones are referred to as the north slump and south slump.

what is movement in CS saying

The major Big Indian Fault intersects the east wall at a small angle to the face and dips about 75 - 80° toward the pit. Prior to extensive movement, this fault was likely a low permeability barrier to water seeping toward the pit. This fault is about 100 feet wide.

What about fault?

Secondary shears have recently been observed which dip into the slope at about 65 - 70°. Recent toppling movement has occurred along these shears.

?

Curragh staff suggest a shear may exist at the contact of the calc silicate and underlying phyllite which is dipping about 40° toward the pit. This contact appears to have been encountered near the toe of the calc silicate slope. The location and orientation of this shear zone is very important to future stability and should be located accurately.

It is recommended that geology develop a cross-section perpendicular to the face along the center of the calc silicate block showing as much structural geologic detail as is known. This section should be forwarded to Mr. A. Stewart.

In order to develop an accurate model of the failure and failure mechanism, an accurate geologic model is required.

Failure Mechanism

Extensive slope monitoring has been performed. Figures 1 and 2 show movement results for hubs 15 and 16 about mid-height on the slope. Horizontal movement sectors are generally much larger than vertical sectors. This indicates toppling type failure. Observation from the south end of the east slope clearly indicates toppling failure with material moving in behind as a graben, which continues to apply lateral pressure.

The mechanism is described as a multiple toppling failure with the Big Indian Fault as the apparent back feature. As a result of this movement, follower slumping is occurring above and beyond the fault. The movements commenced during spring melt, accompanied with many rainy periods. On June 27th, active mining was halted due to the increased rate of ravelling.

The rate of movement between July 20 - 27 became very severe, reaching up to 3 metres per day. Extensive fracturing occurred in the central portion of the slope and major slope ravelling developed.

the calc sils.?

Material between the two shears near the top of the calc silicate zone and the Big Indian Fault is moving downward as a graben pressuring the lower toppling zone.

The Faro Creek diversion ditch has existed for many years above the crest of the east wall. Past recommendations have been to line this ditch. However, this was never effectively done. Water from this ditch has continued to seep into the east wall, creating high water pressures. On July 21, Faro Creek was diverted by pumping

water from a sump into a pipeline so the diversion seepage ceased. Within one to seven days, movements began to slow dramatically and many are now in the order of only 10 percent of the maximum movement.

Toppling failures that the writer has encountered before are at the Annaconda Twin Buttes pit south of Tuscon, Arizona (25 million cu. yds.), Cassiar and Lornex (20 million cu. yds.).

Concern regarding the calc silicate and lower phyllite shear location and possible future movement along this shear must be addressed with better geological information. Continued field mapping of newly exposed benches is required.

Factors Which Contributed to the Movements

Rock Structure

The existence of the weak phyllites, the steep dipping Big Indian Fault and the secondary shears dipping into the slope contributed to the toppling failure.

The geology and existence of weak rock is a given which cannot be changed and must be taken into account in the design.

Groundwater

The presence of groundwater in the slope has a major impact on rock stability:

- shear strength is reduced due to buoyancy forces,
- cohesion of weak rock is reduced,
- seepage forces are created by drainage flow toward the face,

- water pressure in tension cracks is developed,
- hydrodynamic shock is created by blasting below the water table.

Since the mine was developed, seepage has existed in the east wall from the Faro Creek diversion. As the pit has been deepened, the influence of groundwater on stability has generally worsened. In July, movement increased substantially. On July 21, Faro Creek was diverted into a pipeline. Except for short term heavy rains since then, seepage infiltration has been reduced. The result has been a dramatic reduction in the rates of movement in the slide area. It is concluded that seepage has been the major factor impacting on the movement.

Considerable wet areas still exist in the lower slope area. Further effort to reduce water pressures in the slope is recommended.

Blasting

Seismic acceleration forces near this face have been large. A review of blasting plans for June 27th indicated that 1,800 kg to 4,600 kg per delay were detonated below the south slump using 234 holes. Back line spacing was 12 feet with 70 kg per hole.

Prior to the strike on March 19th, 50,800 kg were blasted in front of the calc silicate block using 9 production rows, up to 2,800 kg per delay and 308 holes.

These blasts in saturated ground would be expected to generate 20 - 40 in/sec particle velocity in the final wall. This is a severe shake which would cause dynamic stress in the rock.

To maintain future stability with an existing low safety factor, future blasting energy must be reduced.

Pit Face Curvature

The east wall has a curved alignment with the calc silicate projected somewhat into the pit. For the same slope angle, concave wall slopes result in increased stress on the slope.

Stress Relief

As an excavation is developed, the rock rebounds slightly due to stress relief. This increases porosity and may open discontinuities to allow additional water to infiltrate the rock structure.

It is important to note that two of the major factors which have influenced slope stability, groundwater and blasting, can be modified to improve stability or limit the impact on stability.

Present Danger

Movements commenced during spring melt gradually increasing until major acceleration July 20 - 27. Considerable ravelling developed. Due to the ravelling danger, the mining was discontinued June 27.

On July 21, Faro Creek was diverted into a pipe. Within 1 - 2 days movements decreased rapidly. At the same time, ravelling has greatly reduced.

I have no knowledge of any large toppling failure that collapsed rapidly anywhere in the world. Al Stewart of Piteau Associates concurs with this.

We are of the opinion that the slope condition is sufficiently safe for mining to commence with precautions and procedures described in the next section.

It is our opinion that the calc silicate is acting as a retaining wall and that a smooth planar failure feature has not developed. Curragh is cautioned that the existence, location and orientation of a potential shear zone along the calc silicate contact must be determined.

A critical movement rate cannot be given. Rather, it is recommended that a program be developed to improve general stability, reduce destabilization forces, incorporate a procedure to catch occasional ravel and to reduce further movement and ravelling.

Recommended Program

1. Install six vacuum assist horizontal drains. There is still considerable seepage issuing from the wall so water pressures are still influencing the movement. In addition, mining is proposed to go considerably deeper. This will increase stresses in the slope. Maximum drainage effort is therefore strongly recommended.

The drains should be installed from the safest location available at the toe into the calc silicate. Some form of shield or wire mesh frame to protect from ravel may be required for the drill. Drains are to be fanned from one location with the first two drains to be perpendicular to this slope $+7\ 1/2^\circ$ and $-7\ 1/2^\circ$. Other drains should be fanned 15° apart.

The drains are to be 200 feet long, at a 3%+ gradient. Standard P.V.C. 1 1/2 inch diameter drain pipe is to be inserted in each hole. The inner 170 feet to be perforated with 0.02 inch slots, the outer 30 feet unperforated.

The drains are to be set up for vacuum drainage with a single vacuum manifold. Vacuum is to be applied for two weeks. Water flows are to be monitored twice daily.

Geology is to be mapped by evaluating the drill cuttings. Shear zones are to be noted. After the vacuum is discontinued, the drains are to be allowed to flow by gravity. Take off the vacuum manifold. The drains must be kept from freezing during the winter and glacial buildup must be controlled.

2. Extend the lower water interception pipe another 200 feet south to limit seepage above the south end of the south slump.
3. Clean up the talus below the north slump and construct on 6 foot high catch berm with 1 1/2:1 side slopes at the toe of the slope to catch any ravel from above.
4. Develop an 8 foot high catch berm with 1 1/2:1 side slopes below the south slump toe to catch ravelling rock. Clean out if and when required with a long boom backhoe.
5. Modify the blasting program to limit seismic acceleration forces. Typical recommendations are:
 - Reduce line hole spacing to 8 feet. Use sonotubes to better disperse explosives. Detonate this line last. Do not dig beyond this line.
 - Use three buffer lines spaced 12 feet apart with lower powder amounts.
 - Delay every production hole using 50 m/sec delays.

- Detonate rows perpendicular to the wall - maximum 50 holes per blast. This may mean multi blasts per day. If movement stops or cold, below freezing weather develops, the total number of holes per blast to be reviewed.

- 6. Continue to monitor movement. Add monitors at lower levels as the mine deepens. Continue to provide movement data to Al Stewart of Piteau Associates for evaluation. Use the same surveyor and instrument if possible. Watch for any unusual sign of bulging, crushing or spalling in the toe.

- 7. Take advantage of cold winter weather and the likely increased stability and reduced ravelling, due to reduced winter seepage. Plan for all mining to be completed by about April 1, 1992 to not extend into the spring melt period.

Experience in the past is that movements reduce or stop during winter periods.

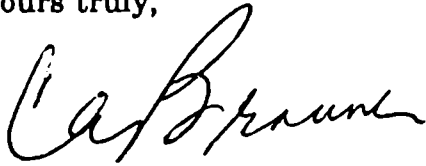
Garret Vos advised a conservative mine plan has developed which would remove 58 percent of the original ore removal program. This would use a 100 foot wide berm. It is considered that this can be reduced, particularly in the north half. The mine plan should be reviewed as each bench is developed.

It is recommended that the stability data be documented to maintain program continuity.

My involvement on the project has been as a Review Consultant. I wish to state that the work of A. Stewart is reasonable and I recommend you continue with his services.

If you have any questions please contact me.

Yours truly,

A handwritten signature in black ink, appearing to read 'C.O. Brawner', written in a cursive style.

C.O. Brawner, P.Eng.

COB:cg

Enclosures

cc: Mr. A. Stewart,
Piteau Associates

c:curragh.rpt

FIG. 1 - RELATIVE MOVEMENT VS TIME -- PRISM

Prism # 15

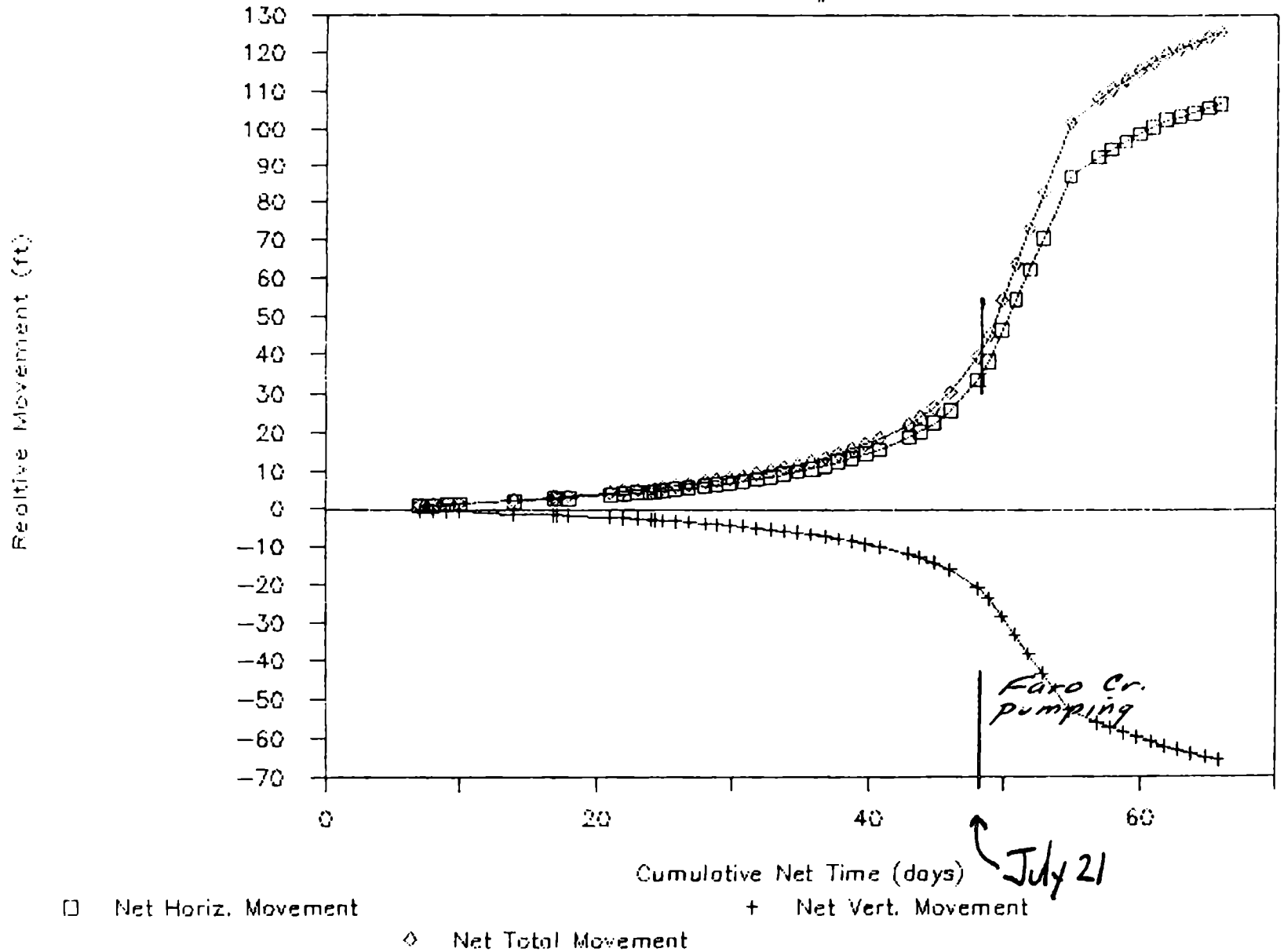
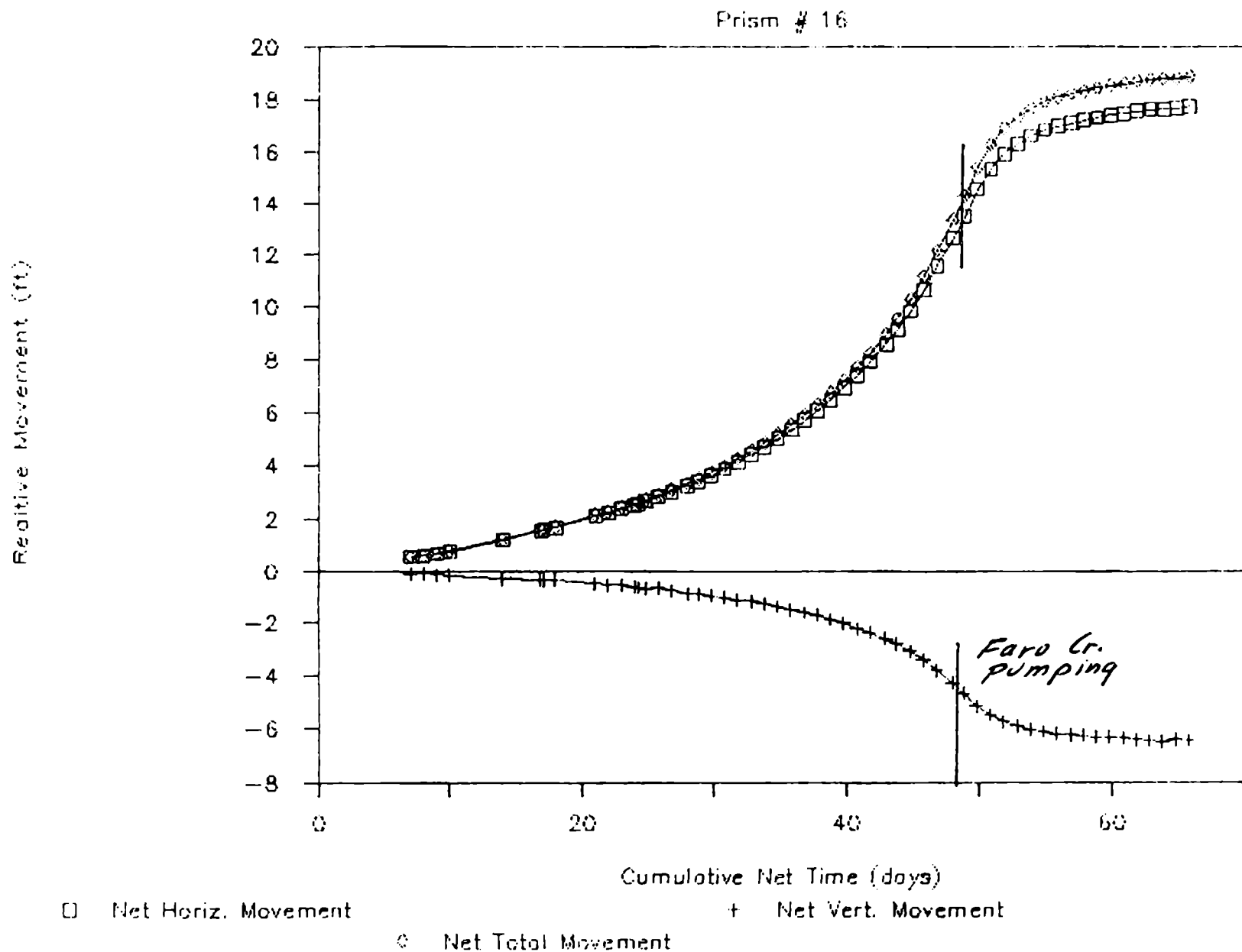


FIG. 2 - RELATIVE MOVEMENT VS TIME -- PRISM



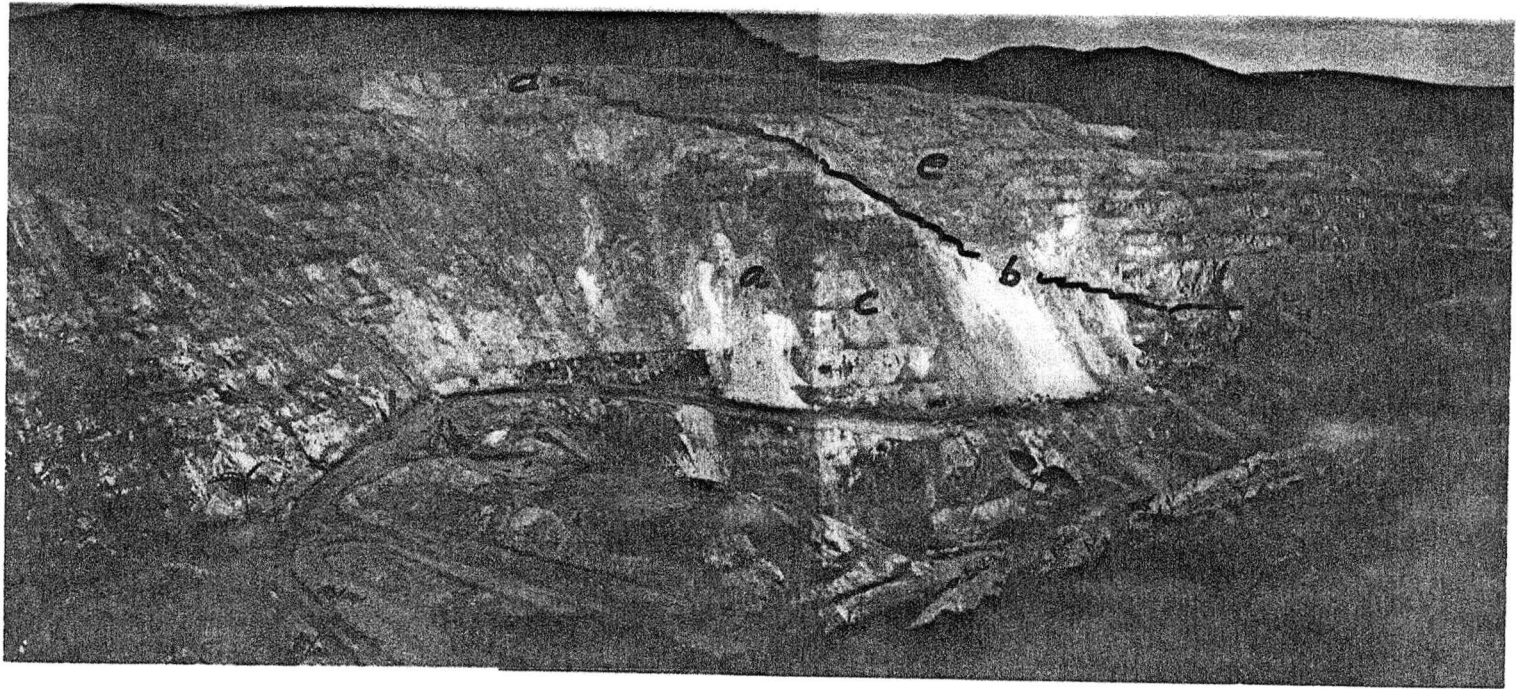


PHOTO 1: East wall of pit. The north slump and talus area (a), south slump and talus area (b) and calc silicate rock zone (c). Note negligible talus below zone c. The Big Indian Fault is behind the major talus zone (d). Upper broken moving zone behind the fault (e).

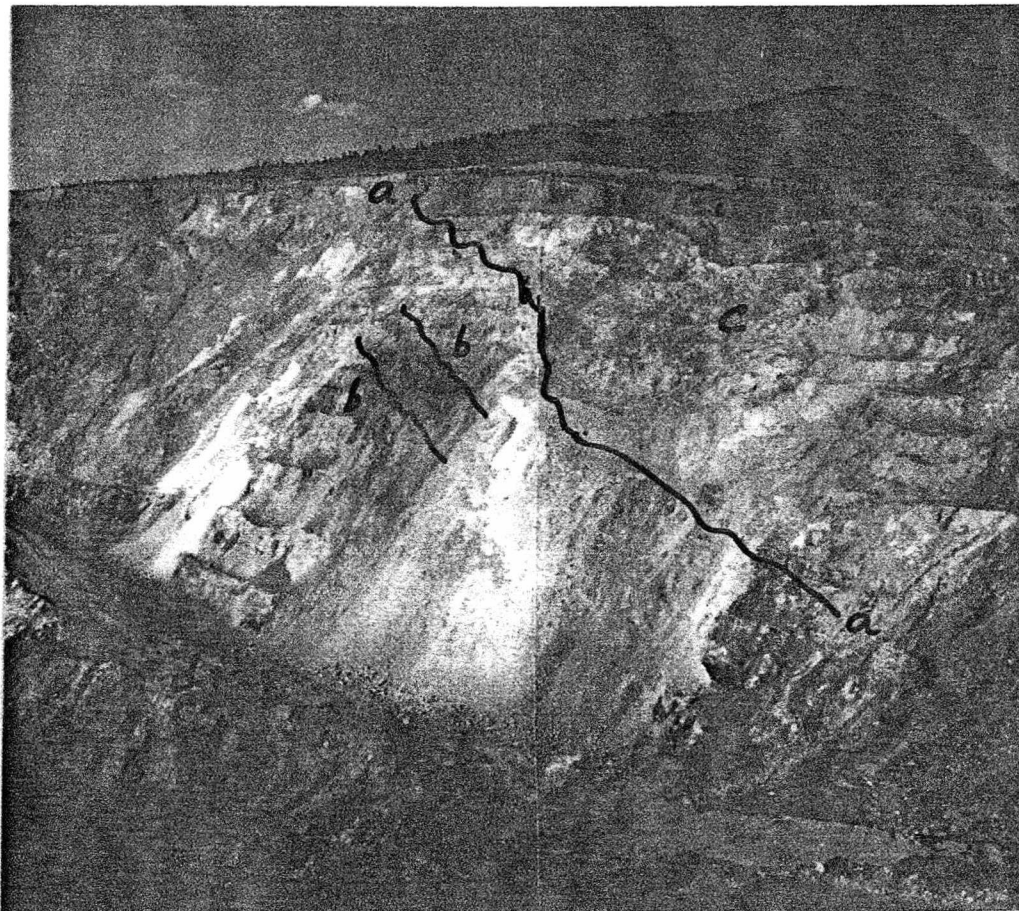


PHOTO 2: Angled view of the east slope from the south end of the pit. Note the Big Indian Fault (a) and secondary shears which dip about 70° into the pit (b) and the upper slump area (c). Note the previously blasted area on the bench (d). Greater movement has taken place in the south slump area.

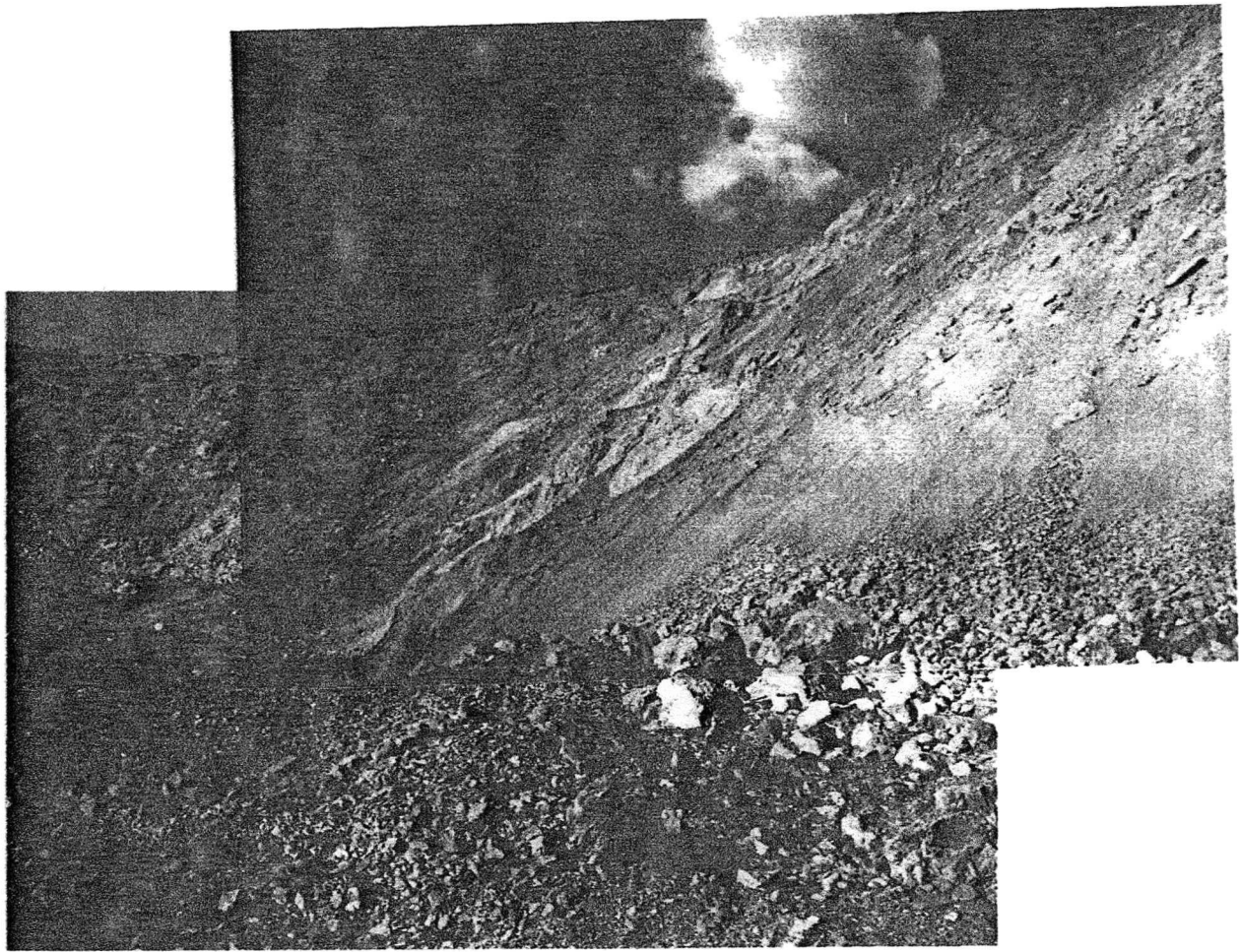


PHOTO 3: Lower area of the south slump. To protect against ravel, push up an 8 foot high pile with 1 1/2:1 side slopes along the toe of the talus. Mining excavation can then commence outside the berm.

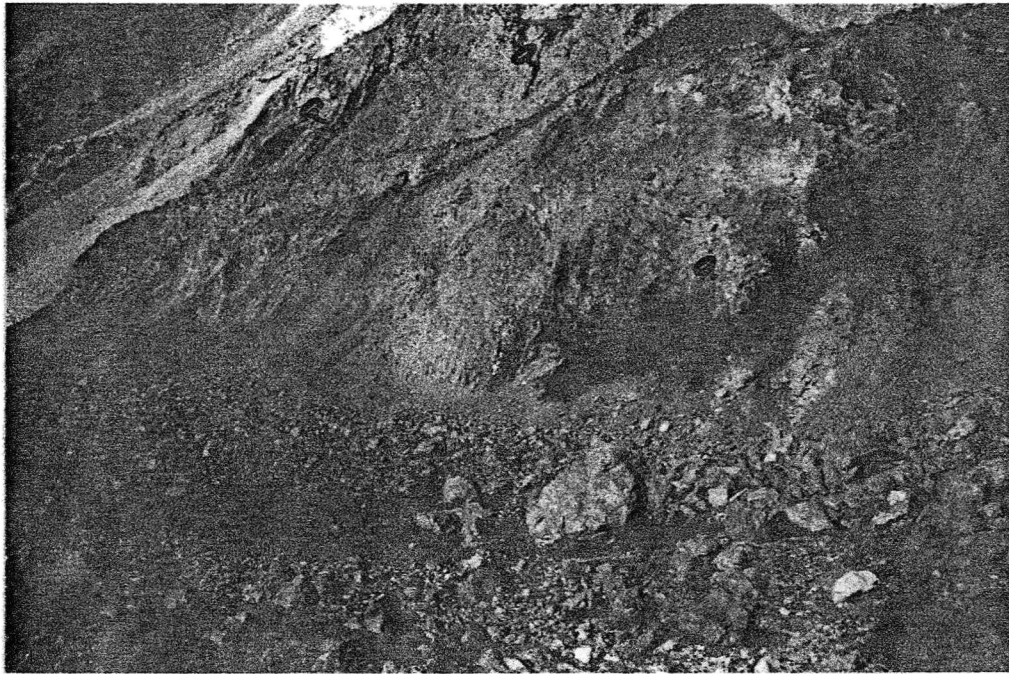


PHOTO 4: Note the numerous wet areas indicating extensive seepage (a).

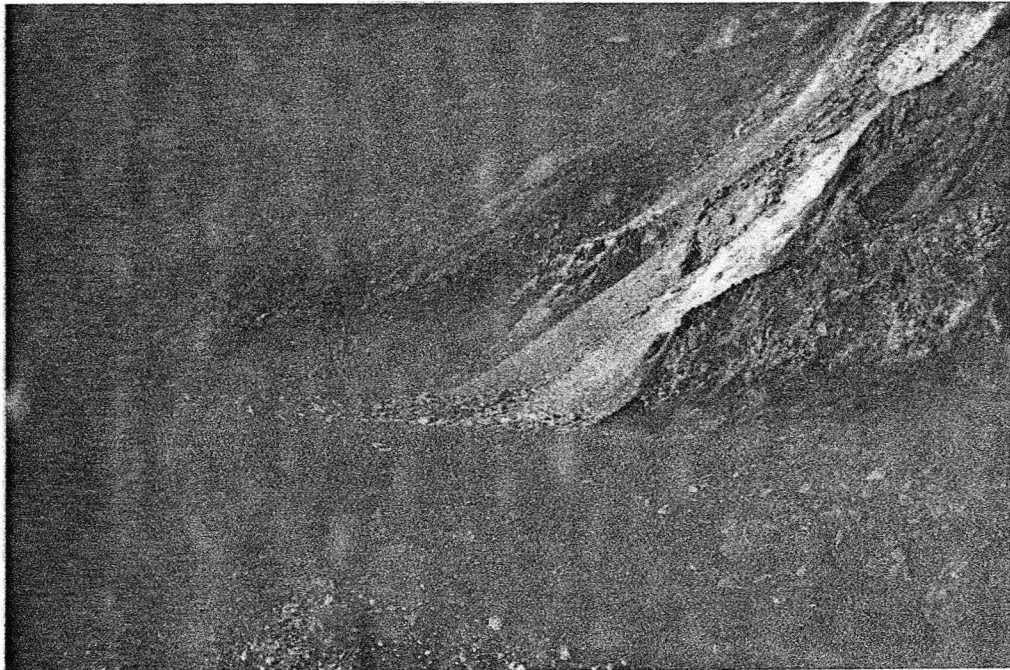


PHOTO 5: Note the zone below the calc silicate with no ravelled boulders.
Six fanned horizontal drains to be installed into the slope on plus 3% grade.

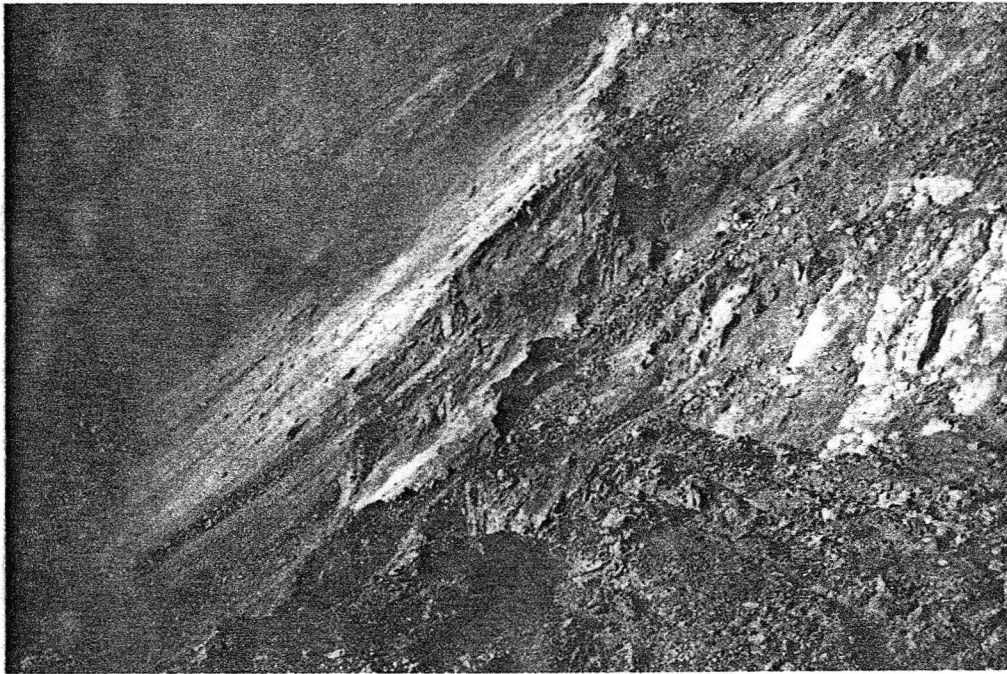


PHOTO 6: Side view of the lower east slope. Note the protruding blocks which have obviously moved in a toppling mode (a).

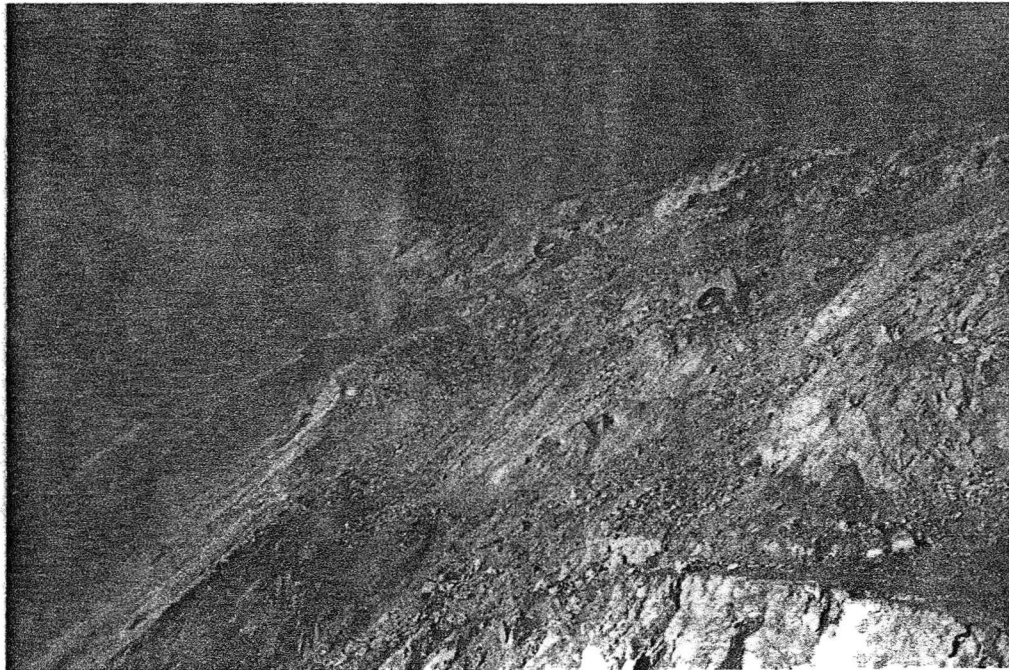


PHOTO 7: Side view of the upper slope. Note the protruding blocks which are evidence of toppling (a).



Resources Inc.

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Y0B 1K0
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TELECOPIER COVER LETTER

TO:

Gregg Sims, J.P. exple
JHS.

TELECOPIER NO. _____

FROM:

NAME: E.

CURRAGH RESOURCES INC., Box 1000, Faro, Yukon, Y0B 1K0

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MESSAGE Memo -

ppt. sheets

Cheers

-C

DAY OF MONTH	TIME OF OBSERVATION	TEMPERATURE (°C)					PRECIPITATION				TIMES OF PRECIPITATION (Calendar Day)		Weather (Calendar Day)			REMARKS		
		Maximum		Minimum		AFTER RESET	Rain		Snow		Total For Day	Began	Ended	Depth of Snow on Ground	Weather (Calendar Day)		Precipitation (mm)	Snow (cm)
		Observed	For Day	Observed	For Day		mm	mm	mm	mm								
1	A.M.																	SCAT. CLOUDS
	P.M.	-2.0												74				SCAT. CLOUDS
2	A.M.	-2.0												76				CLAR - 40% CLOUD
	P.M.	-1.5		-5.5										74				CLAR - 10% CLOUD
3	A.M.	-1.0												74				CLOUD
	P.M.	-0.5		-2.0		0.0								71				CLOUD
4	A.M.	-0.5												70				CLOUD
	P.M.	-1.0		-10.0		-1.5												
5	A.M.																	
	P.M.																	
6	A.M.																	
	P.M.																	
7	A.M.																	
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8	A.M.																	
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9	A.M.																	
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10	A.M.																	
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14	A.M.																	
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15	A.M.																	
	P.M.																	
16	A.M.																	
	P.M.																	
17	A.M.	-2.0		-13.5		7.0												SUNNY
	P.M.	18.0		-1.5		12.5												OVERCAST
18	A.M.	18.0		11.5		15.5												"
	P.M.	19.0		0		15.5												
19	A.M.	18.0		11.0		12.0												CLOUDY
	P.M.	17.0		13.5		15.0												
20	A.M.	17.0		13.5		15.0												
	P.M.	17.5		16.0		19.0												
21	A.M.	16.5		10.5		12.5												
	P.M.	19.0		12.0		19.0												CLOUDY
22	A.M.	19.0		12.0		14.0												
	P.M.	14.5		14.5		15.0												
23	A.M.	14.5		14.5		15.0												
	P.M.	12.0		13.0		18.0												
24	A.M.	12.0		14.0		11.0												
	P.M.	12.0		14.0		11.0												
25	A.M.	12.0		14.0		11.0												CLEAR - SUNNY
	P.M.	12.0		14.0		11.0												OVERCAST
26	A.M.	12.0		14.0		11.0												SCAT. CLOUDY
	P.M.	14.5		18.0		19.5												CLEAR - SUNNY
27	A.M.	10.0		11.5		14.0												
	P.M.	16.0		13.0		15.0												CLEAR
28	A.M.	17.0		15.0		16.0												
	P.M.	17.0		15.0		16.0												CLEAR
29	A.M.	17.0		15.0		16.0												
	P.M.	19.0		17.0		16.0												OVERCAST
30	A.M.	19.0		17.0		16.0												
	P.M.	19.5		17.0		16.0												
31	A.M.	19.5		17.0		16.0												
	P.M.	19.5		17.0		16.0												
SUM																		
MEAN																		

TEMPERATURE EXTREMES
 Maximum: 19.5 Date: 26th Mean Max:
 Minimum: -10.0 Date: 4th Mean Min:
 Mean:

STATION KAYE MINE SITE

Time of observation 8:00 a.m. 4:00 p.m.

PROVINCE YUKON

Observer STACE SELDON

MONTH MAY

1952

DAY OF MONTH	TIME OF OBSERVATION	TEMPERATURE °C					PRECIPITATION					TIMES OF PRECIPITATION (Calendar Day)		Weather (Calendar Day)					REMARKS
		Maximum		Minimum		AFTER RESET	Rain		Snow		Total For Day	Began	Ended	Went to 16	Went to 17	Went to 18	Went to 19		
		Observed	For Day	Observed	For Day		mm	mm	mm	mm									
1	a.m.			+3.0		+2.0													CLOUDY
	p.m.	+10.5		+1.0		+1.5													
2	a.m.	+4.0		+5.0		+5.0													
	p.m.			+5.0		+5.0													
3	a.m.	+11.0		+2.0		+2.5													
	p.m.	+5.0		+2.0		+4.5													
4	a.m.	+5.5		+2.0		+1.0													WIND
	p.m.	+7.0		+1.0		+1.5													
5	a.m.	+7.0		+1.0		+1.5													CLEAR
	p.m.	+16.0		+2.5		+5.0													
6	a.m.	+10.5		+1.5		+2.5													CLOUDY
	p.m.																		
7	a.m.																		
	p.m.																		
8	a.m.																		
	p.m.																		
9	a.m.																		
	p.m.																		
10	a.m.																		
	p.m.																		
11	a.m.	+14.0		+1.0		+1.2													LT. SNOW
	p.m.																		
12	a.m.																		
	p.m.																		
13	a.m.																		
	p.m.																		
14	a.m.																		
	p.m.																		
15	a.m.																		
	p.m.																		
16	a.m.	+11.0		+6.0		+12.0													CLOUDY
	p.m.	+19.5		+1.0		+1.0													
17	a.m.																		
	p.m.																		
18	a.m.																		
	p.m.																		
19	a.m.	+11.0		+0.5		+3.5													OVERCAST
	p.m.																		
20	a.m.																		
	p.m.																		
21	a.m.																		
	p.m.	+10.5		+0.5		+10.0													SCANT CLOUDS + SUNNY
22	a.m.	+12.0		+0.5		+5.0													CLEAR
	p.m.																		
23	a.m.	+13.0		+2.0		+9.5													SCANT CLOUDS + SUNNY
	p.m.	+14.0		+4.0		+11.0													OVERCAST → LT. SNOW
24	a.m.	+13.0		+2.0		+3.0													CLOUDY → 90%
	p.m.																		
25	a.m.																		
	p.m.																		
26	a.m.																		
	p.m.																		
27	a.m.	+11.0		+0.5		+14.0													CLEAR → 30% CLOUD
	p.m.	+15.5		+4.0		+9.5													OVERCAST
28	a.m.	+17.0		+3.0		+6.0													CLOUDY → 80%
	p.m.	+14.0		+5.0		+12.5													CLEAR → SUNNY
29	a.m.	+13.5		+12.0		+17.0													CLOUDY → 20%
	p.m.	+18.0		+3.0		+10.0													
30	a.m.	+12.0		+9.0		+10.5													OVERCAST
	p.m.																		
31	a.m.																		
	p.m.																		
TOTAL																			

TEMPERATURE EXTREMES
 Maximum +18.0 Date 30th Mean Max.....
 Minimum -5.0 Date 2nd Mean Min.....
 Mean.....

RAPPORT DE STATION CLIMATOLOGIQUE

STATION _____

Heure de l'observation: _____ a.m. _____ p.m.

T
P

PROVINCE _____

Observateur: S. H. F. ...

MOIS June P.

JOUR DU MOIS	HEURE DE L'OBSERVATION	TEMPÉRATURE					PRÉCIPITATIONS					DURÉE DE LA PRÉCIPITATION (Jour civil)		HAUSSEUR DE NEIGE AU SOL (Jour civil)			REMARQUE		
		Maximum		Minimum		Pluie		Neige		Total de jour	Début	Fin	Enneigement	Temp. (Jour civil)					
		Observé	De jour	Observé	De jour	mm	De jour	mm	De jour					mm	mm	mm		mm	mm
1	a.m.			-1.5															OVER CAST
	p.m.																		
2	a.m.			-1.5															CLOUDY
	p.m.																		MOSTLY CLOUDY
3	a.m.			-1.5															OVERCAST
	p.m.																		
4	a.m.			-1.5															CLOUDY & WINDY
	p.m.																		
5	a.m.			-1.5															CLOUDY/SUNNY
	p.m.																		
6	a.m.			-1.5															VERY CLOUDY
	p.m.																		
7	a.m.			-1.5															OVERCAST
	p.m.																		
8	a.m.			-1.5															OVERCAST
	p.m.																		
9	a.m.			-1.5															CLOUDY
	p.m.																		SUNNY
10	a.m.			-1.5															CLOUDY & WINDY
	p.m.																		
11	a.m.			-1.5															CLOUDY & WINDY
	p.m.																		
12	a.m.			-1.5															SEMI CLOUDY
	p.m.																		
13	a.m.			-1.5															CLEAR
	p.m.																		SUNNY
14	a.m.			-1.5															CLEAR/SUNNY
	p.m.																		
15	a.m.			-1.5															SEMI CLOUDY
	p.m.																		
16	a.m.			-1.5															CLOUDY
	p.m.																		
17	a.m.			-1.5															CLOUDY
	p.m.																		PARTLY CLOUDY
18	a.m.			-1.5															PARTLY CLOUDY
	p.m.																		
19	a.m.			-1.5															CLEAR/SUNNY
	p.m.																		
20	a.m.			-1.5															CLEAR/SUNNY
	p.m.																		
21	a.m.			-1.5															SEMI CLOUDY
	p.m.																		
22	a.m.			-1.5															CLEAR & SUNNY
	p.m.																		
23	a.m.			-1.5															CLEAR
	p.m.																		
24	a.m.			-1.5															CLEAR/SUNNY
	p.m.																		
25	a.m.			-1.5															SEMI CLOUDY
	p.m.																		
26	a.m.			-1.5															CLEAR
	p.m.																		
27	a.m.			-1.5															CLEAR AT 26°C
	p.m.																		
28	a.m.			-1.5															CLOUDY & WINDY
	p.m.																		
29	a.m.			-1.5															SUNNY & SEMI CLOUDY
	p.m.																		
30	a.m.			-1.5															OVERCAST 5°C
	p.m.																		

TEMPÉRATURES EXTRÊMES Maximum

DAY OF MONTH	TIME OF OBSERVATION	TEMPERATURE (°C)				PRECIPITATION				TIMES OF PRECIPITATION (Calendar Day)		Weather Calendar Day	REMARKS
		Maximum		Minimum		Rain		Snow		Begin	Ended		
		For Day	Observed	For Day	AFTER RESET	mm	mm	cm	cm	mm	mm		
1	a.m.		18.0		13.0								CLOUDY
	p.m.	18.5	14.5		13.0								PARTLY CLOUDY & SUN
2	a.m.	17.5	7.0		15.5	0.0							PARTLY CLOUDY
	p.m.	18.0	15.0		12.5	1.0							CLOUDY & SUN
3	a.m.	19.0	6.0		14.5	2.0							PARTLY CLOUDY
	p.m.	20.5	12.5		12.0	0.0							PARTLY CLOUDY
4	a.m.	18.5	4.5		15.5	0.0							CLOUDY
	p.m.	16.5	11.0		4.0	0.0							CLOUDY
5	a.m.	18.5	8.5		12.5	0.0							CLOUDY
	p.m.	16.5	6.5		11.5	1.0							CLOUDY
6	a.m.	17.0	6.0		12.0	0.0							PARTLY CLOUDY & SUN
	p.m.	18.5	6.5		11.5	0.0							SUNNY
7	a.m.	21.5	8.5		14.5	2.5							CLOUDY
	p.m.	11.0	8.5		8.5	0.1							OVERCAST
8	a.m.	11.0	6.5		8.0	0.0							SCAR. CLOUDS
	p.m.	13.5	8.0		7.5	0.0							SUNNY, OVERCAST
9	a.m.	13.0	6.0		8.0	0.0							OVERCAST
	p.m.	13.0	6.0		8.0	0.0							OVERCAST
10	a.m.	17.5	7.0		10.5	1.0							CLEAR
	p.m.	16.0	6.0		13.5	1.0							OVERCAST
11	a.m.	15.5	8.0		14.5	0.0							CLEAR
	p.m.	14.0	11.0		14.5	0.0							PARTLY CLOUDY
12	a.m.	11.0	7.0		14.5	0.0							OVERCAST
	p.m.	14.0	7.0		14.5	0.0							PARTLY CLOUDY
13	a.m.	14.0	7.0		14.0	0.0							PARTLY CLOUDY
	p.m.	15.5	7.0		12.5	0.0							PARTLY CLOUDY
14	a.m.	14.0	7.0		14.0	0.0							PARTLY CLOUDY
	p.m.	15.5	7.0		12.5	0.0							PARTLY CLOUDY
15	a.m.	14.0	7.0		14.0	0.0							OVERCAST - LITE RAIN
	p.m.	15.5	7.0		12.5	0.0							"
16	a.m.	19.0	6.0		7.5	1.0							CLEAR
	p.m.	14.0	7.0		9.0	0.0							CLOUDY
17	a.m.	15.0	8.0		8.5	0.0							OVERCAST - DRIZZLE
	p.m.	13.5	5.5		7.5	1.0							CLOUDY 95%
18	a.m.	12.0	5.5		8.0	1.0							OVERCAST
	p.m.	10.5	7.0		8.0	0.5							SUNNY
19	a.m.	15.0	8.0		12.5	1.0							SUNNY
	p.m.	15.5	7.5		11.5	0.0							SUNNY
20	a.m.	17.5	4.5		15.0	0.0							SUNNY
	p.m.	17.0	6.5		16.5	0.0							CLEAR
21	a.m.	17.0	6.5		16.5	0.0							CLEAR
	p.m.	18.0	10.5		7.0	0.0							SCATTERED CLOUDS
22	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
23	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
24	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
25	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
26	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
27	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
28	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
29	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
30	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS
31	a.m.	17.5	14.0		12.0	0.0							SCATTERED CLOUDS
	p.m.	19.0	8.5		10.0	0.0							SCATTERED CLOUDS

Total no. of days with		TEMPERATURE	
MEANS		TEMPERATURE EXTREMES	Mean Max.
		Maximum	Date
		Minimum	Mean Min.
			Date
			Mean

CLIMATOLOGICAL STATION REPORT

STATION _____

Time of observation 9.00 a.m. 4.00 p.m.

T
P

PROVINCE _____

Observer _____

MONTH AUGUST

DAY OF MONTH	TIME OF OBSERVATION	TEMPERATURE (°C)					PRECIPITATION				TIME OF PRECIPITATION (CAVIM Day)		Depth of Snow on Ground	Wettest Calendar Day	REMARKS	
		Maximum		Minimum		Wettest	Snow	Total For Day	Begin	End						
		Observed	Feeling	Observed	Feeling						mm	cm				mm
1	a.m.			6.5		7.5										OVERCAST
	p.m.	11		6.5		11	0.2									OVERCAST
2	a.m.	12		7.0		9.5	0.2									OVERCAST
	p.m.	16.5		9.5		15.5	0									OVERCAST - LTR RAIN
3	a.m.	16.5		1.5		9.5	0									CLOUDS - RAIN
	p.m.	14		14.0		4.0	3.0									OVERCAST
4	a.m.	13.5		4.0		7.5	0									CLOUDY 3/8
	p.m.	14.0		1.5		9.5	0.2									OVERCAST
5	a.m.	11.5		2.0		11.0	0									OVERCAST
	p.m.	18.5		5.0		1.0	0									OVERCAST
6	a.m.	14.5		1.5		8.5	0									OVERCAST
	p.m.	17.5		9.5		17.0	0									OVERCAST
7	a.m.	17.5		9.5		9.5	0									OVERCAST
	p.m.	20.5		9.5		16.5	0									OVERCAST
8	a.m.	19.0		11.0		15.5	0									OVERCAST
	p.m.	19.0		11.0		15.5	0									OVERCAST
9	a.m.	16.5		11.0		11.0	0									OVERCAST
	p.m.	13.0		11.0		11.0	0									OVERCAST
10	a.m.	16.5		11.0		11.0	0									OVERCAST
	p.m.	13.0		11.0		11.0	0									OVERCAST
11	a.m.	19.5		13.5		14.5	0									OVERCAST
	p.m.	22.0		13.5		14.5	0									OVERCAST
12	a.m.	21.0		13.0		19.0	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
13	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
14	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
15	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
16	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
17	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
18	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
19	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
20	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
21	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
22	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
23	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
24	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
25	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
26	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
27	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
28	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
29	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST
30	a.m.	16.5		11.0		14.5	0									OVERCAST
	p.m.	16.5		11.0		14.5	0									OVERCAST

Total no. of days with: _____

TEMPERATURE EXTREMES

Maximum Date Mean Max.

Minimum Date Mean Min.

Minimum Date Mean


*Fas Mune
Ges hebs
NWall*

TIME	Temperatures				R.H.		Precip.		Wind		Max. Wind		Max. Gust						
	Max.	Min.	Mean	HO	GDD	Max	Min	Total	Snow	Mean	Pre.	Spd.	Dir.	Spd.	Dir.	Gust	Spd.	Dir.	Hour
8 1	16.0	9.0	12.5	5.5	7.5	81.6	51.2	0.0	***	4.4	90	8.0	190	0.0	***	***	***	***	***
8 2	18.0	9.0	13.5	4.5	8.5	87.4	39.4	.8	***	2.1	45	4.0	270	0.0	***	***	***	***	***
8 3	18.0	9.0	13.5	4.5	8.5	87.6	63.1	4.0	***	7.4	110	10.0	130	0.0	***	***	***	***	***
8 4	15.0	6.0	10.5	7.5	5.5	50.3	43.8	-.1	***	3.8	155	7.0	200	0.0	***	***	***	***	***
8 5	15.0	2.0	8.5	9.5	3.5	87.0	44.1	0.0	***	.2	335	2.0	330	0.0	***	***	***	***	***
8 6	17.0	3.0	10.8	9.0	5.0	93.2	44.4	-.1	***	1.7	90	4.0	240	0.0	***	***	***	***	***
8 7	22.0	3.0	12.5	5.5	7.5	93.2	30.5	0.0	***	2.6	155	5.0	150	0.0	***	***	***	***	***
8 8	22.0	6.0	14.0	4.0	9.0	93.3	35.4	1.6	***	4.0	90	10.0	100	0.0	***	***	***	***	***
8 9	19.0	6.0	12.5	5.5	7.5	93.6	72.2	0.0	***	2.7	90	5.0	110	0.0	***	***	***	***	***
8 10	17.0	12.0	14.5	3.5	9.5	87.6	48.3	0.0	***	1.3	65	3.0	140	0.0	***	***	***	***	***
8 11	18.0	10.0	14.0	4.0	9.0	76.7	52.0	0.0	***	.5	315	3.0	310	0.0	***	***	***	***	***
8 12	20.0	10.0	15.0	3.0	10.0	87.5	59.5	-.1	***	2.9	110	6.0	160	0.0	***	***	***	***	***
8 13	23.0	13.0	18.0	6.0	13.0	87.6	43.7	0.0	***	2.1	90	6.0	140	0.0	***	***	***	***	***
8 14	25.0	14.0	19.5	0.0	14.5	59.5	36.0	0.0	***	7.6	270	10.0	270	17.0	17.0	270	1300	1300	1300
8 15	20.0	9.0	14.5	3.5	9.5	87.5	55.9	1.4	***	1.3	65	3.0	60	0.0	***	***	***	***	***
8 16	23.0	0.0	15.5	2.5	10.5	93.5	43.4	0.0	***	1.3	45	4.0	50	0.0	***	***	***	***	***
8 17	25.0	10.0	17.5	.5	12.5	93.5	41.2	0.0	***	4.9	110	8.0	120	0.0	***	***	***	***	***
8 18	17.0	11.0	14.0	4.0	9.0	71.2	41.4	-.1	***	8.0	270	10.0	270	22.0	22.0	270	1300	1300	1300
8 19	16.0	5.0	10.5	7.5	5.5	87.1	47.7	-.1	***	3.3	270	10.0	270	0.0	***	***	***	***	***
8 20	15.0	6.0	10.5	7.5	5.5	93.4	50.9	.8	***	1.0	270	6.0	270	0.0	***	***	***	***	***
8 21	16.0	4.0	10.0	8.0	5.0	101.0	58.2	.6	***	2.1	315	5.0	320	0.0	***	***	***	***	***
8 22	16.0	4.0	10.0	8.0	5.0	93.2	38.8	0.0	***	6.1	270	12.0	280	0.0	22.0	40	1500	1500	1500
8 23	15.0	7.0	11.0	7.0	6.0	70.8	44.1	.4	***	12.7	270	16.0	260	27.0	28.0	260	1500	1500	1500
8 24	13.0	7.0	10.0	8.0	5.0	81.5	62.2	9.0	***	6.0	315	10.0	270	18.0	18.0	270	1400	1400	1400
8 25	5.0	4.0	4.5	13.5	0.0	100.0	93.2	13.0	***	3.5	315	4.0	320	0.0	***	***	***	***	***
9 25	5.0	4.0	2.5	15.5	0.0	108.0	93.1	3.8	***	5.6	110	8.0	90	0.0	***	***	***	***	***
8 27	5.0	2.0	3.5	14.5	0.0	100.0	88.6	2.2	***	8.2	110	10.0	120	16.0	16.0	120	1000	1000	1000
8 28	3277.0	1.0	3277.0	***	***	86.6	50.7	3277.0	***	3.0	90	5.0	90	0.0	***	***	***	***	***

USE Avg. DATA WITH CAUTION.

NOTE -.1 in Pcpw is a TRACE.

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