GJ/501

File: Vangorda Metallurgy

017898

Richard Coleman
156 Hollyrood Hts. Dr.
Mississauga, Ont.
L5G 2H4

25 January, 1989

Mr. Bill Weymark
Manager
Curragh Resources Inc.
P.O. Box 1000
Faro
Yukon Y0B 1K0

Dear Sir:

The 1988 metallurgical research conducted by Lakefield Research on the Vangorda deposit has been completed and reports have been forwarded to your people. The work started in the spring of 1988 with suites of samples for a mineralogical examination followed by the laboratory mineral dressing research between June and December.

The research confirms the complexity of the deposit but suggests that reasonable grades and recoveries of lead, zinc and precious metals can be expected. Modifications to the existing Faro concentrator layout and equipment will be essential when processing this ore. In addition finer grinds and higher reagent consumptions can be expected although plant practice may not be as severe as indicated during the research.

The majority of the research was conducted on ore types E and G with minor oxidation and of a non-porous nature. This material represents 70% of the mineral inventory and was called Composite No 3 during the testing. The flowsheet developed for this ore was utilized for research on the other types of ore available. Favorable results on all NON-POROUS types of ore including even the low grade (represented by Composite 5) were obtained. However, ore type represented by Composite 1A was the most refractory, was porous and oxidized, was carbonaceous and contained secondary copper minerals. The results in general from this material were not acceptable except that the precious metal recovery was encouraging.

General comments about the ore types and responses would include the following remarks:

<u>Composite 1A</u> Most Refractory
Carbonaceous - Porous
Poor selectivity
Good lead concentrate grades not possible
High zinc content of lead concentrate
Good recovery of gold and fair recovery of silver in lead concentrate.

Composite 2 — Course grained
Good lead, gold and silver recoveries
High zinc loss with lead concentrate
Good zinc concentrate grade but lowest recovery

Composite 3 — 70% of deposit
Good metallurgy with new flowsheet
Reagent consumption (particularly NaCN) higher

Composite 4 — Graphitic quartzite
Requires special depressant to improve lead grade
Lowest lead, gold and silver recoveries
Lowest grade tested (except for Composite 5 which may not be considered ore)
Good zinc recovery acceptable zinc grade

Composite 5 — Low grade
Good metallurgy

Composite 6 — Instructions for compositing not received. However, it is understood that material would be similar to that of Composite 5 and therefore good metallurgy could be expected with higher head assays.

General

If the samples tested are truly representative of the ores from the zones, a modified flowsheet with new reagents could be expected to produce

Lead Concentrates of	62% Pb	84% Recovery
	8% Zn	
	6 to 10 gms/T Au	62% Recovery
	700 gms/T Ag	70% Recovery
Zinc Concentrates of	1% Pb	
	54% Zn	82% Recovery
	45 gms/T Ag	

Deleterious metal contents of the concentrates may include copper, manganese, arsenic and magnesia in the lead concentrate and copper and silica in the zinc concentrate.

In the bulk scale test of material from Vangorda proceeds in the fall of 1989 with the flowsheet revisions and reagent regimes recommended, the metallurgy might be expected to be plus 61% Pb in Pb conc. 83% recovery
plus 54% Zn in Zn conc. 86% recovery

Based on their research, Lakefield have drawn certain conclusions and make specific recommendations. I support their comments. At the same time I would like to emphasize certain features when ore from the Vangorda deposit is processed.

1. Finer primary grind will benefit precious metal recovery.
2. A new lead collector is recommended.
3. More lead products should be reground.
4. Open circuit lead cleaning is essential.
5. An organic depressant for the lead circuit is required for some of the ore types.
6. High speed conditioning in the zinc circuit will be extremely beneficial.
7. During the bulk scale testing of this deposit a representative of the Lakefield research company should be present.
8. If blending with Faro 3 ore is contemplated extensive laboratory research should be done.

Further Recommendations

Some of the knowledge gained during this research project should be rested in the current milling technique on the Faro 3 ores. Specifically the collector combination A317/3418A. Regrinding of all lead rougher and scavenger concentrates, open circuit cleaning of lead concentrates, the use of DS20 depressant, and high speed zinc circuit conditioning should be tested in the laboratory and on the circuit as soon as practical.

Additionally it is a good time to start the research on the Grum deposit so that results can be available for your long term planning. I continue to recommend that Lakefield Research be engaged for this purpose and I am available to assist if you wish my services.

Since carbonaceous ores may be a factor in the life of your company, it might be worthwhile for a new project to be initiated to do basic research on this type of refractory material.

Yours Very Truly

R. L. Coleman

Dick Coleman

cc. K. Forgaard
E. Beaumont
G. Jilson

Dick Coleman (416)274-6836
8 Dec 88 10:15 am

Summary of Locked Cycle

(1a) porous core with little oxidation
fine grinding ? any merit

(1b) non porous core with oxidation

		Pb	Zn	Au	Ag	
Pb con	Assay	63.9	7.17	6.17	701	head 585
	Recvy	83.5	8.3	60.0	70.8	6.1
Zinc con	Assay	1.03	57.2	0.31	38.4	0.79
		1.7	82.2	3.8	4.8	75.6

(2) EG from SE

		Pb	Zn	Au	Ag	
Pb	Ass	65.4	8.93	11.19	705	4.88
		89.3	10.8	74.4	74.1	head 5.51
Zn con		1.07	54.7	0.84	56.9	1.09
	Rec	1.7	76.9	6.5	7.0	63.4

(3) EG from west

Pb con		66.2	7.17	8.56	814	head 4.14
	Rec	88.4	7.6	65.0	75.3	5.19
Zn con		1.03	55.3	0.28	48.5	0.73
		2.0	85.6	3.2	6.5	59.7

(4) A type
Low Py low grade - problem in high Pb grade con
graphite floating
finer grinding - got improvement in recovy
78 → 85 %
zinc recvy not affected
64-68%

(5) EC low grade,
= no tests

What is plan for now and timeframe for final results

Comp 6 of higher grade EC+C one

Comm 5

Bend of 1 year material
Bend for entire deposit

end January maybe February

Table No. 8 - Impurity Analyses of Lead and Zinc Concentrate - Products from Locked Cycle Test ON VANGORDA - COMPOSITE 3

Element		Assays %, g/t	
		Lead Concentrate	Zinc Concentrate
Lead	(Pb)	68.20	1.03
Zinc	(Zn)	7.20	54.90
Iron	(Fe)	4.12	6.72
Bismuth	(Bi)	0.002	<0.002
Cadmium	(Cd)	0.011	0.069
Chromium	(Cr)	0.022	0.036
Cobalt	(Co)	<0.002	<0.002
Mercury	(Hg)	0.0050	0.0280
Nickel	(Ni)	<0.002	<0.002
Tin	(Sn)	0.002	<0.001
Arsenic	(As)	<0.001	0.007
Sulphur	(S)	17.800	33.3
Fluorine	(F)	0.093	0.11
Manganese	(Mn)	0.10	0.33
Silica	(SiO_2)	2.36	0.25
Alumina	(Al_2O_3)	0.085	0.034
Calcium	(CaO)	0.120	0.40
Acid Insol.		5.79	2.00
Magnesia	(MgO)	0.92	0.14
Antimony	(Sb)	0.23	0.006
Gold	(Au)	8.60	0.28
Silver	(Ag)	813.00	48.5

FILING

CURRAGH RESOURCES INC.

Inter-Office Memorandum

TO: Bill Weymark
General Manager
Faro Office

DATE: 1989 02 20

FROM: Gregg Jilson
Vice-President, Exploration
Whitehorse Office

RE: Vangorda Deposit Metallurgical Testing

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1. In light of the declining grade of Faro deposit it seems likely that some consideration will be given to accelerating mill feed from the Vangorda deposit to supplement that from the Faro pit. This, of course, will require testing for compatability of Faro ores with Vangorda ores and examination of the behaviour of Faro ores in the modified flow sheet required for Vangorda. The purpose of this memo is to let you know that from last years drilling program we have stored a large amount of core from the southwest end of the Vangorda deposit for possible eventual usage for metallurgical testing. The holes from last year are largely cluster in the area where the initial bulk sample would come from and from the area of the shallowest reserves where earliest production would originate. Should you decide that further testing is required and need more material these samples could be composited in very short order. Just let me know somewhat in advance when the samples are required, if at all, and I will see that they are prepared for you.

CURRAGH RESOURCES INC.
Inter-Office Memorandum

TO: Godfrey McDonald, Vice-President, Metallurgy
Toronto Office
Dumitru Tuliu, Senior Metallurgist
Faro Minesite

FROM: Cam Reed, Geologist
Whitehorse Office

cc: Gregg A. Jilson, Vice-President, Exploration
Whitehorse Office

RE: METALLURGICAL COMPOSITING OF EARLY VANGORDA FEED FROM 1988 DDH CORE

DATE: 03 16 1990

The following pages include a list of split drillcore samples obtained from the 1988 diamond drilling program at Vangorda. The samples are selected to be representative of the type of feed expected from the first 500,000 tonnes of feed from the Vangorda pit. The samples were drilled from 9 holes between Sections 20E and 26E and are geographically located within the circled area on the accompanying drillhole plan map.

The feed from this part of the deposit is moderately oxidized and some samples are porous. JSX 550 polymer mud was used to maximized drilling recovery, so it is advisable to wash the final bucked metallurgical sample before bench testing begins.

The gangue mineralogy of the early feed material is a medium-to-fine grained, massive, pyritic/baritic, sulphide/sulphate which will contain some iron and base metal oxides. Minor pyrrhotite, magnetite, quartz, muscovite, chlorite, calcite and dolomite are common. Accessory chalcopyrite, marcasite and tetrahedrite are also present. A minor amount of dilution from altered phyllites at the hanging wall and low grade semi-massive pyritic quartzite of the footwall is expected. I have included a few samples of this material (rock types 4L and 4C) to account for this type of dilution.

The samples are located in the old kitchen of the Grum Camp. They are in labelled bags in pails labelled "B" on the lid and the sample #'s (from _ to __) on the side. There are 5-6 samples in each pail.

The samples were kept frozen up to June of last year, but were allowed to thaw when the generator was moved to an exploration camp. It is likely that the temperatures were above 0 for 2 1/2 months. The kitchen area is always cool and it is unlikely that the material would have oxidized to any noticeable degree during this period.

If there are any problems, give me a call.

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CURRAGH RESOURCES INC.
Inter-Office Memorandum

To: Gregg Jilson, V.P. Exploration
Whitehorse Office

Dave Tenney, Chief Geologist
Faro Minesite

From: Cam Reed, Exploration Geologist
Whitehorse office

RE: **Vangorda Metallurgical Composite Descriptions and Characteristics**

Date: 10 22 1990

Metallurgical composites of diamond drillcore samples from drilling projects completed in 1987 and 1988 were sent to Lakefield research for metallurgical testing. 5 composites separated on the basis of ore type, geographic location in the orebody, weathering and porosity were sampled from the 1987 DDH core and sent to Lakefield in May 1988. A description of each composite is included below.

In March 1990, an additional composite representing early more oxidized high grade feed from the SE section of the orebody located between vertical X-sections 20E and 26E was sampled from the 1988 drillcore with bench testing to be completed at Faro.

Description of 1988 Vangorda Metallurgical Composites

1a - Visibly oxidized, porous, Massive baritic/pyritic sulphides. No separation based on geographic location in the orebody, however most of the samples were taken from holes drilled in the shallow SE section of the orebody. The gangue mineralogy is medium to fine grained pyritic/baritic sulphide/sulphate which will contain significant iron and base metal oxides. Minor quartz, muscovite, chlorite, pyrrhotite, magnetite, calcite and dolomite are common. Accessory chalcopyrite, marcasite, tetrahedrite are also present. This composite is the most refractory of all the ore types.

1b - Moderately oxidized, non porous high grade ore with same mineralogy as 1a. No separation based on geographic location in the orebody. These samples were excluded from 1a because of the possible deleterious effects of drilling mud which is likely to be more abundant in the porous composite 1a.

2 - High grade massive nonporous pyritic/baritic sulphide which is moderately oxidized to fresh and located in the SE section of the orebody. Contains minor quartz, muscovite, chlorite, pyrrhotite, calcite and dolomite. Accessory magnetite, chalcopyrite, marcasite, and tetrahedrite are common. This composite represents the bulk of early feed from SE section of the vangorda orebody.

3 - Slightly oxidized to fresh, high grade massive pyritic/baritic sulphide located in the NW section of the orebody. This composite is mineralogically similar to composite 2. This composite represents the bulk of the millfeed NW of X-section 12E.

4 - Fresh to slightly oxidized, medium grade ribbon-banded carbonaceous quartzite. No separation based on geographic location in the orebody. Pyrite content ranges from 10 to 20%. Contains the lowest concentration of copper and precious metal of all the ore types. The bulk of this ore type is located in the early benches in the NW section of the deposit. Some minor thin bands are located in the SE section. This ore type represents about 15% of the total high grade feed.

5 - Low grade, non-carbonaceous, semi-massive footwall quartzite. This material will likely make up the bulk of dilution expected in the main ore zone in both NW and SE sections. Pb+Zn is generally less than 2% with significant gold content (near 1 gram/tonne). Pyrite content ranges from 30% to 60% and is generally highest near the high grade contact. Contains minor magnetite, pyrrhotite, muscovite, and chlorite.

Table 1: Head Analyses of Composites (from lakefield research)

Composite	Assays %, g/t											
	Cu	Pb	Zn	Fe	S	Mn	Hg	Au	Ag	C(T)	C(g)	Po
Comp 1A	0.26	3.95	4.20	26.8	28.5	0.45	0.0018	0.57	49.1	1.47	0.057	11.2
Comp 1B	0.22	5.75	6.69	28.1	28.9	1.16	0.0049	0.79	77.8	1.71	0.049	17.0
Comp 2	0.20	4.75	5.70	24.5	26.8	0.79	0.0036	0.93	64.5	1.67	0.049	12.5
Comp 3	0.15	3.96	5.35	21.7	28.2	0.61	0.0043	1.57	64.8	0.20	0.015	10.3
Comp 4	0.037	2.20	3.87	7.54	8.83	0.054	0.0023	0.44	31.2	2.20	0.64	12.5
Comp 5	0.36	0.72	0.89	29.1	26.6	0.58	0.00023	1.60	12.7	1.01	0.060	9.40
Master	0.22	3.76	4.47	24.2	27.1	0.71	0.0025	0.96	57.9	1.37	0.081	17.2

Table 2: Statistics by Ore Type - V9009 Interpretation Within VIV 89 ultimate pit - Total Mineral In-situ undiluted sulphide inventory. No grade cutoff applied.

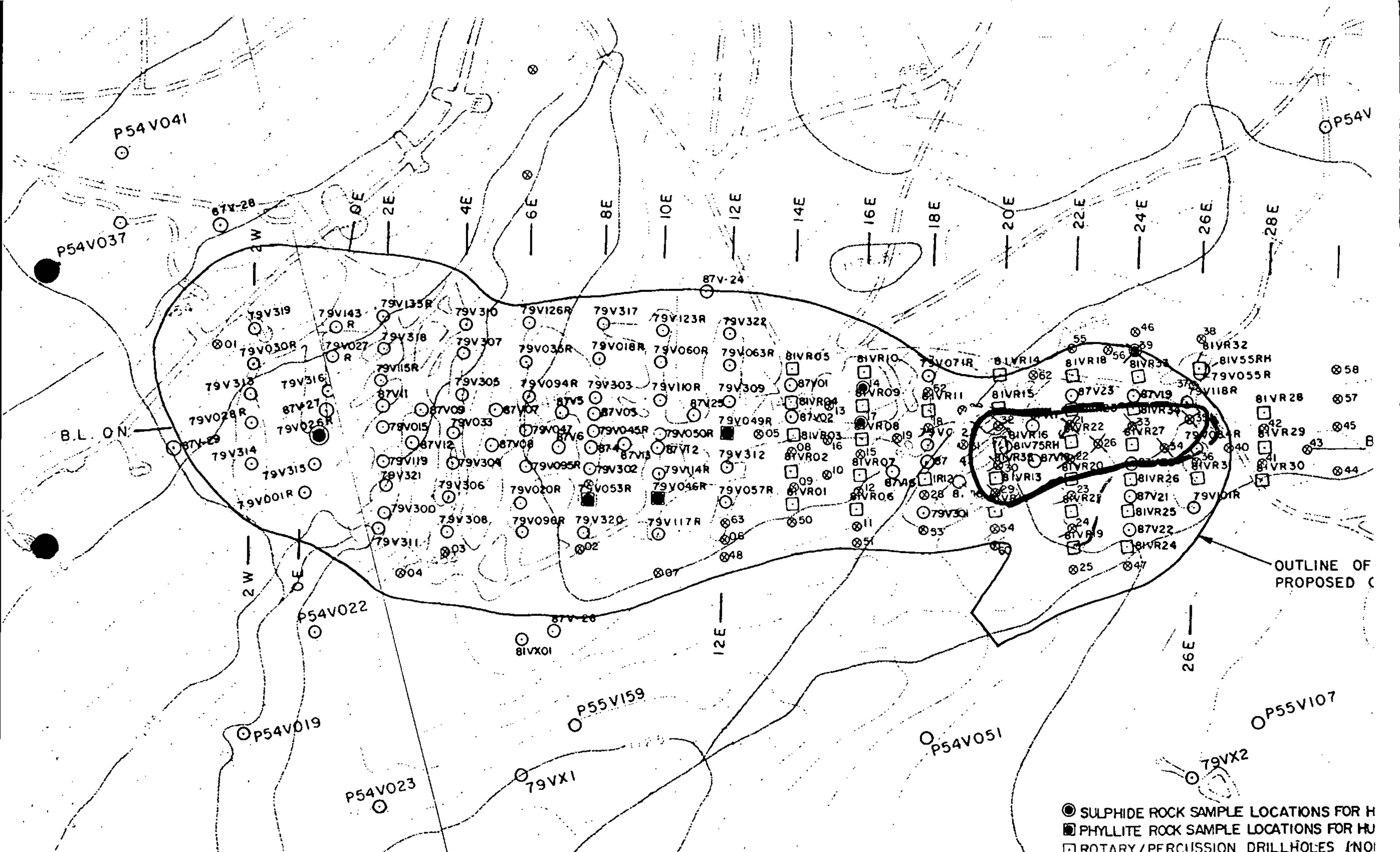
Rock Type	Tonnes	%Pb+Zn	Ag g/mt	Au g/mt	%Cu
SE SECTOR					
Massive Sulphide	1696640	10.05	56.36	0.921	0.21
Footwall noncarbonacous qtzite	1001800	2.22	18.41	0.915	0.31
Carbonaceous qtzite	174590	7.23	35.71	0.641	0.12
NW SECTOR					
Massive Sulphide	3232840	10.05	56.27	0.779	0.13
Footwall noncarbonacous qtzite	1014350	2.09	16.72	0.904	0.31
Carbonaceous qtzite	1249750	4.82	26.29	0.476	0.07
TOTAL PIT					
Massive Sulphide	4929480	10.05	56.30	0.828	0.16
Footwall noncarbonacous qtzite	2016150	2.15	17.56	0.909	0.31
Carbonaceous qtzite	1424340	5.11	27.44	0.496	0.08

VANGORDA METALLURGICAL COMPOSITE INTERVALS
1988 DIAMOND DRILLING PROGRAM

Composite Number : V90-01 February 26, 1990
Description: Early Feed Vangorda Metallurgical Composite Samples - Sections 20E to 26E
Total Intervals: 60 Approximate Weight of Composite: 240.61 kg

SAMPLE	DDHID	FROM (ft)	TO (ft)	INT. (ft)	REC. (ft)	REC. (%)	ROCK TYPE	PULP S.G.	% Pb+Zn	% Pb	% Zn	Ag (g/tnn)	Au (g/tnn)
16657	88V-21	48.2	49.9	1.6	1.4	85	4C0	3.1	4.68	1.44	3.24	32	0.41
16658	88V-21	49.9	53.1	3.3	3.3	100	4G4 &#	4.3	14.71	5.70	9.01	106	1.37
16659	88V-21	53.1	57.4	4.3	4.3	100	4C3	3.8	1.20	0.61	0.59	21	1.51
16384	88V-22	23.0	27.6	4.6	4.6	100	4G4	4.5	14.60	7.20	7.40	97	0.55
16385	88V-22	27.6	31.5	3.9	3.9	100	4G0	4.3	7.31	3.27	4.04	50	0.75
16386	88V-22	31.5	35.8	4.3	4.3	100	4G4	4.2	13.03	5.18	7.85	75	0.93
16388	88V-22	38.4	40.4	2.0	2.0	100	4E4	4.1	2.01	1.36	0.65	36	1.17
16389	88V-22	40.4	44.9	4.6	4.6	100	4E4	4	12.69	4.44	8.25	67	0.27
16390	88V-22	44.9	47.9	3.0	3.0	100	4A4	4	12.01	2.92	9.09	51	0.55
16391	88V-22	64.6	69.6	4.9	4.9	100	4L1	3.2	0.59	0.04	0.55	2	0.07
16392	88V-22	91.9	95.1	3.3	3.3	100	4G4	2.9	14.27	5.07	9.20	82	0.69
16393	88V-22	95.1	98.4	3.3	3.3	100	4E0 &1	3.9	1.48	0.72	0.76	24	1.23
16394	88V-22	98.4	103.3	4.9	4.8	98	4C0	3.6	0.81	0.32	0.49	10	0.82
16639	88V-26	36.7	40.4	3.6	3.3	91	4E4	3.5	6.25	3.16	3.09	48	0.34
16640	88V-26	40.4	46.6	6.2	3.9	63	4E4	3.8	10.56	6.02	4.54	66	1.30
16641	88V-26	46.6	48.6	2.0	2.0	100	4E4 &1	3	7.16	2.05	5.11	28	0.27
16642	88V-26	71.9	76.1	4.3	4.3	100	4G4 &#	4	12.18	3.93	8.25	66	0.55
16643	88V-26	76.1	80.1	3.9	3.9	100	4G0 &#	4.1	8.83	3.32	5.51	40	1.44
16644	88V-26	80.1	84.0	3.9	3.9	100	4E1 &#	4.2	3.43	1.75	1.68	22	1.51
16645	88V-26	84.0	87.9	3.9	3.9	100	4E1 &#	4.3	0.90	0.52	0.38	19	4.77
16337	88V-29	25.9	28.5	2.6	2.6	100	4G4#	4.2	12.87	5.67	7.20	78	0.86
16338	88V-29	28.5	32.5	3.9	3.9	100	4G0	4.2	3.00	1.81	1.19	28	1.23
16339	88V-29	32.5	37.1	4.6	4.6	100	4G0	4.6	3.90	2.12	1.78	32	0.79
16340	88V-29	37.1	42.0	4.9	4.9	100	4A4	2.9	13.82	4.75	9.07	70	0.58
16341	88V-29	42.0	46.9	4.9	4.9	100	4A4	3.1	16.10	5.10	11.00	82	0.58
16342	88V-29	46.9	52.5	5.6	4.5	80	4A4	3.1	15.32	5.12	10.20	82	0.45
16343	88V-29	135.5	137.8	2.3	2.3	100	4L24 &	2.8	1.71	0.73	0.78	8	0.05
16344	88V-29	137.8	141.7	3.9	2.6	66	4G0#8	4.1	8.48	3.46	5.02	49	0.82
16345	88V-29	141.7	146.3	4.6	4.6	100	4E0	4.2	3.26	1.67	1.59	29	3.19
16346	88V-29	146.3	151.2	4.9	4.1	84	4E0	4.2	2.31	1.12	1.19	21	0.79
16347	88V-29	151.2	155.8	4.6	4.6	100	4L124	2.9	0.55	0.04	0.51	0	0.07
16133	88V-30	72.2	75.8	3.6	3.6	100	4G4#	4.1	13.93	5.13	8.80	77	1.03
16134	88V-30	75.8	79.7	3.9	3.9	100	4G4#	4.3	13.97	5.14	8.83	79	1.03
16135	88V-30	79.7	86.3	6.6	6.6	100	4E486	4.3	18.17	6.57	11.60	88	1.58
16136	88V-30	86.3	89.6	3.3	3.3	100	4G4#	4	20.32	8.52	11.80	106	2.23
16137	88V-30	89.6	93.8	4.3	4.3	100	4G4#	4.3	16.90	6.40	10.50	86	1.71
16138	88V-30	93.8	97.4	3.6	3.6	100	4G4#	3.4	9.50	3.40	6.10	63	1.61
16139	88V-30	97.4	104.3	6.9	6.9	100	4C3	3.4	1.14	0.56	0.58	12	1.23
16627	88V-32	32.2	36.4	4.3	1.8	42	4E1	3.6	0.50	0.30	0.20	14	0.55
16628	88V-32	36.4	40.0	3.6	3.4	95	4E8 &4	4.3	7.94	3.86	4.08	32	1.71
16629	88V-32	40.0	42.0	2.0	2.0	100	4G4	4.6	13.15	5.46	7.69	48	0.82
16630	88V-32	42.0	44.0	2.0	2.0	100	4E0	4	1.99	0.94	1.05	23	0.75
16631	88V-32	44.0	47.9	3.9	3.7	95	4E8	3.4	2.79	1.55	1.24	27	1.03
16632	88V-32	47.9	51.5	3.6	3.5	97	4E48	3.5	7.13	4.26	2.87	54	2.19
16633	88V-32	51.5	55.4	3.9	3.9	100	4C3	3.6	2.38	0.98	1.40	16	1.92
16399	88V-33	91.5	95.5	3.9	3.9	100	4G4	4.5	16.65	7.69	8.96	97	0.62

16400	88V-33	95.5	100.7	5.2	5.2	100	4G4	4.6	21.39	9.79	11.60	164	1.23
16401	88V-33	100.7	104.3	3.6	3.6	100	4G4	4.3	16.70	6.80	9.90	111	1.65
16402	88V-33	104.3	107.6	3.3	3.3	100	4E4	4.4	13.16	4.45	8.71	49	1.51
16403	88V-33	107.6	110.9	3.3	3.3	100	4E4	4.1	6.07	3.67	2.40	34	1.37
16404	88V-33	110.9	114.8	3.9	3.4	87	4E0	4	1.73	0.64	1.09	22	0.41
16405	88V-33	114.8	117.8	3.0	3.0	100	4E0	4.1	0.61	0.08	0.53	16	1.03
16724	88V-34	104.7	108.3	3.6	3.6	100	4G4	3.9	15.90	5.70	10.20	98	0.82
16725	88V-34	108.3	111.2	3.0	3.0	100	4G4	4.3	12.92	5.74	7.18	108	1.23
16726	88V-34	111.2	115.8	4.6	4.6	100	4E1 &8	4.1	2.69	1.00	1.69	20	1.75
16149	88V-35	32.2	37.1	4.9	4.4	89	4G0	3.8	9.91	4.14	5.77	82	1.44
16150	88V-35	37.1	42.0	4.9	3.1	63	4G0	4.3	7.80	3.54	4.26	57	1.10
16151	88V-35	42.0	44.6	2.6	2.6	100	4G0	4.3	9.37	3.96	5.41	74	1.23
16152	88V-35	44.6	47.6	3.0	3.0	100	4E1	3.5	0.50	0.29	0.21	11	0.89
				233.6	221.5				8.91	3.64	5.27	55.5	1.18



P54V041
P54V037
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87V-24
79V319
79V143
79V135R
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79V126R
79V317
79V123R
79V322
79V318
79V307
79V030R
79V027 R
79V036R
79V018R
79V060R
79V063R
81VR05
81VR10
79V071R
81VR14
81VR18
81VR32
81V55RH
79V055R
79V115R
79V313
79V316
79V305
79V094R
79V303
79V110R
79V309
87V01
81VR09
81VR11
81VR15
87V23
87V19
79V118R
81VR28
87V11
87V27
87V09
87V07
87V5
87V05
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81VR04
81VR34
79V028R
79V026R
79V015
79V033
79V047
79V045R
79V050R
79V049R
87V02
81VR08
81VR16
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79V314
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87V12
79V312
81VR03
81VR02
81VR07
81V75RH
81VR38
81VR20
81VR3
81VR30
79V315
79V119
79V304
79V095R
79V302
79V114R
79V321
79V306
79V020R
79V053R
79V046R
79V057R
81VR01
81VR06
81VR12
81VR13
81VR26
87V21
79V101R
79V001R
79V300
79V308
79V096R
79V320
79V117R
79V301
81VR21
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OUTLINE OF
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79VX2
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