

019210

SUMMARY REPORT FOR  
DY DRILL PROGRAM

WEEK ENDING  
OCTOBER 12, 1990

FOR: GREGG JILSON  
V.P. EXPLORATION  
CURRAGH RESOURCES INC.  
#117 INDUSTRIAL ROAD  
WHITEHORSE, YUKON  
YIA 2T8

BY: JOHN ZBEETNOFF  
OCTOBER 12, 1990

## PILOT HOLE

Fishing attempts are continuing in drill hole 90DY-04-DS. To date all retrievable cable down the hole has been recovered. Very little cable is expected to remain down the hole. The P-casing has been reamed to 92' which is believed to be 2' past the top of the lost drill sting. Starting late into day shift of Friday Oct. 12 fishing attempts have begun focusing on the removal of the plug which still exists loosely secured to the top of the drill string.

All down hole survey data taken from 90DY-04-DS are located in Appendix A. Analysis of the down hole survey data indicates the hole, at a depth of 2113', is an estimated 21.02' from the centerline of drill hole collar. The calculation which arrived at this value is based on sporadic survey data taken below 1917'. Potential existed where the single shot equipment could have been lost if it had become stuck in the fault. Although the sample density for surveys is low, confidence about the hole location at the 2113' depth is considered adequate to within a foot or two. Further surveys which will be taken during the next 50' of coring proposed will confirm the lowest survey, which is suspect due to significant pyrrhotite content noted in core. The current trace of the drill hole is located in Figure 1. Although the down hole motor had built significant angle to correct the hole trajectory in the interval from 1903' to 1963', the angle has been lost during the coring interval from 1963' to 2113'.

The fault intersected at the 1960'-2083' has been called the Plug Fault. Analysis of previous drill hole data has located several faults in holes near the Pilot Hole. Two strong fault zones have been intersected in 78X-10. Based on proximity to the Pilot Hole and intensity of these structures it is believed that one or possibly both of these fault zones represents the Plug structure. The upper fault occurs at 507.3m to 522.0m, the second at 550.8m to 559.3m (hole depth). Individual three point problems have been calculated using each of these intervals in conjunction with the most optimistic point of the Plug Fault in the Pilot Hole. The most optimistic point to use for the Plug Fault in the Pilot Hole is the hanging wall contact. The hanging wall contact is considered the most optimistic point because it offers the best potential to allow correlation to faults intersected in holes located to the south. The third point used in the three point problem has been provided by 78X-05, which is the closest hole to the south of the Pilot Hole. Solutions to three point problems

have generated results that give a northeast strike and very steep dips which vary from the northwest to southeast. The projected strike lines for the resultant solutions contain no supporting evidence in holes directly on trend to the south of analyzed area. This indicates the data is insufficient to determine an orientation of the Plug Fault.

Retaining the assumption that the fault or faults intersected in 78X-10 are part of the Plug structure, a very general trend of the structure can be estimated. This estimated trend gives a minimum dip of 75 degrees to the south-ish if the lower fault in 78X-10 is the Plug Fault extension. Should the upper fault be the extension of the structure the minimum dip will be approximately 80 degrees southerly. Only vague estimations can be made as to the strike direction of the structure. A general southerly dip direction can be expected but I wish to stress this could vary significantly. The volume of rock cored by drill holes to the south, which are considered to contain no correlative extensions to the structure in question, limit the degree of easterly and westerly trend for dip direction of the fault. Given these parameters, the valley to the north of the Pilot Hole collar may represent the surface expression of the Plug Fault, or a coincident structure. Figure 2 displays the proposed scenario. This scenario also provides for excellent potential for further ore reserves of the Dy Deposit displaced along the Plug Fault. This could be tested after the orientation of the Plug structure is established. Core from 78X-10 is scheduled to inspected this weekend to establish the likelihood of correlation to the fault intersected in the Pilot Hole.

Potential also exists that the two fault zones in 78X-10 are unique structures that approach convergence near DY-04-DS. To determine if this in fact is the case several three point problems will have to calculated to confirm the possibility. This analysis will be conducted over the weekend.

Geochemical analysis of core samples taken from the Pilot Hole is expected to be completed next week. A copy of the assay log is located in Appendix B. This will aid in calculating the grade of the mineralized zones intersected in this hole.

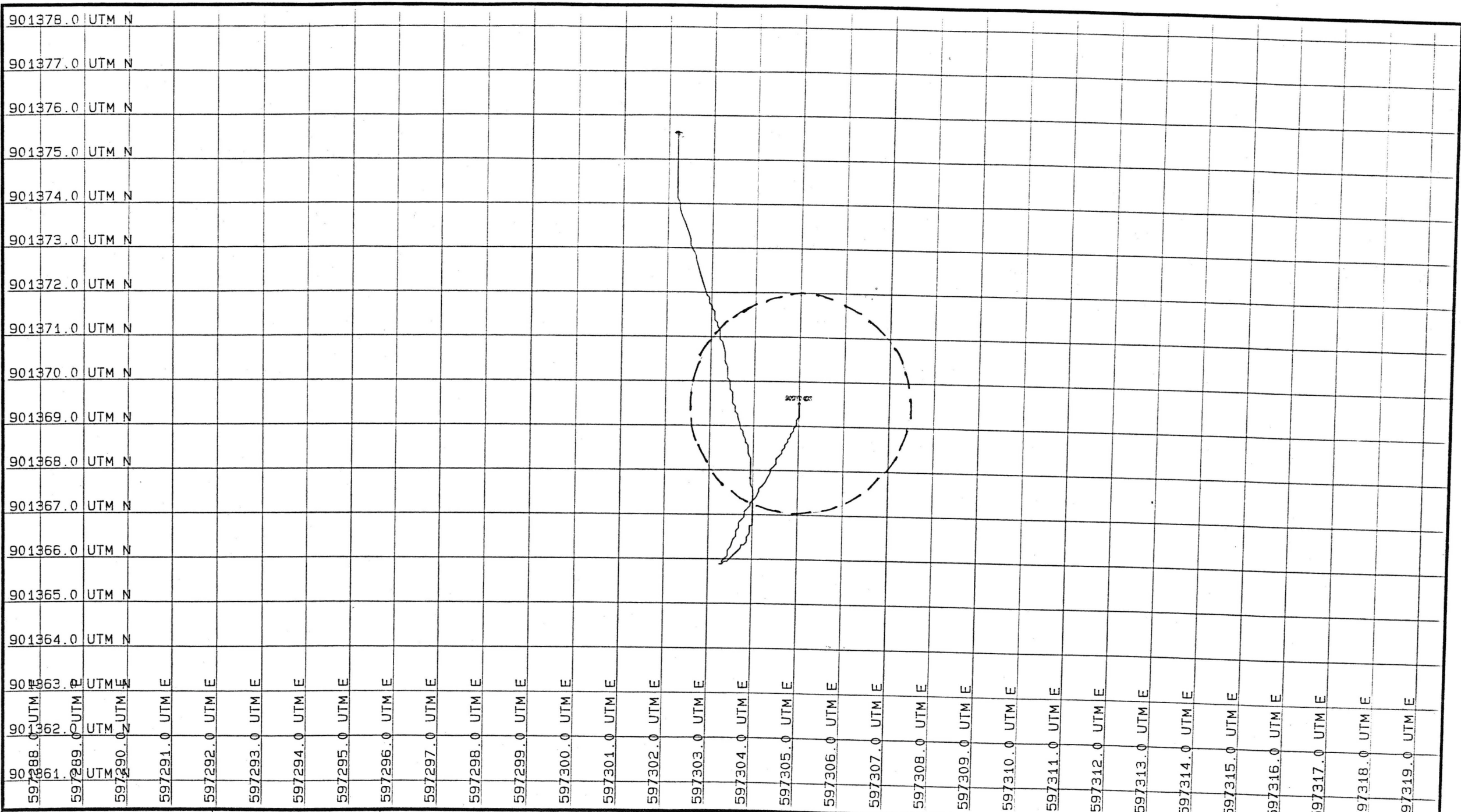
## DECLINE DRILL PROGRAM

The proposed drill targets for the Dy Decline drill program have been given letter codes A through J. The deepest hole proposed to be drilled during the 1990 Dy decline drill program has been issued code A, the shallowest hole has been given code J. A total of six drill hole collar locations have been surveyed in by Lamerton & Associates (Targets E through J). The collar location for the DY portal and the point projected to surface from the base of the ramp (Target-B) have also been spotted. Appendix C contains the target coding and the UTM co-ordinates of the surveyed locations (provided by Lamerton). A full scale plan of these proposed targets, collar location, and previous drill holes has been generated and will follow in the mail bag shortly.

Analysis of drill hole data along the trace of the proposed trace of the Dy Decline has been partially completed. Deviation patterns based on previous drill holes have proven to be erratic. A more usable database of hole deviation is hoped to be compiled during the on going drilling of the Dy Decline drill program. Appendix D contains the deviation data for previously drilled holes adjacent three of the deeper holes proposed to be drilled in 1990. Of key importance from this tabulated data is the general consistency in dogleg values for previously drilled holes.

Mineralized intersections cored along the proposed trace of the decline recorded mineralization have been analyzed and length weighted grade calculations completed. This analysis has been used in the vicinity of Target-A, B, and C. The intersections of interest have been plotted on Figure 3. The trace of the decline near Target B will pass near intersections as high as 22.36%/5.4 meters (78X-04). Target C is not located near significant mineralization, but this may be a function of a lack of drilling in that area. Related data occurs in Appendix D.

Detailed analysis of structural data for holes along the trace of the proposed decline will begin this weekend. Should the potential for significant problems with structure in the vicinity of the decline be identified, you will be notified immediately.



QUICK-PLOT  
GEMCOM Services Inc.

DATE = 11-10-90  
TIME = 16: 39: 37

Currnagh Resources Inc.  
Faro Mine

DY DEPOSIT  
CURRENT TRACE OF 90DY-04-DS  
AT 2113'  
J.Z.

HORIZONTAL SCALE = 1 : 100

VERTICAL SCALE = 1 : 100

FIGURE 1

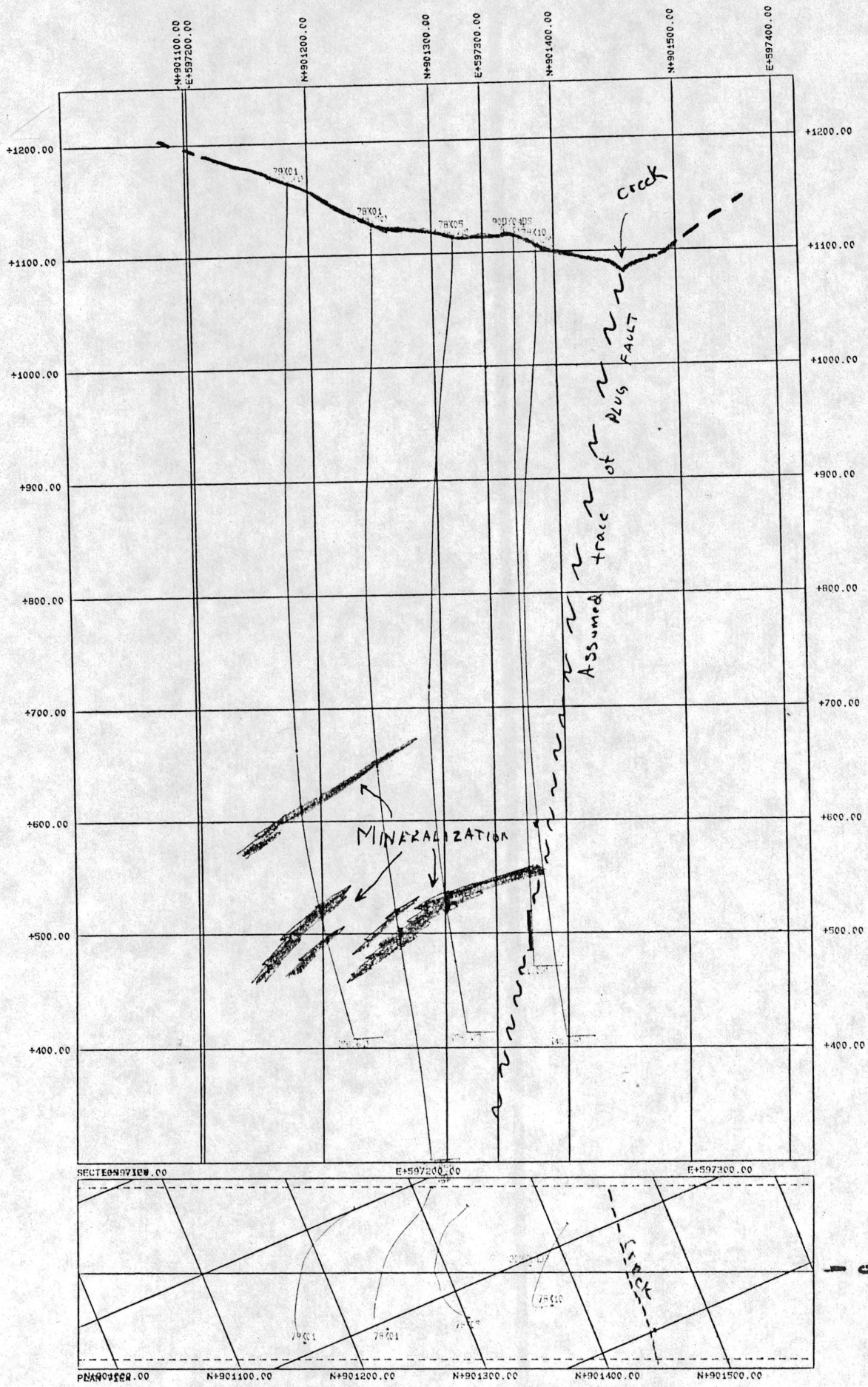
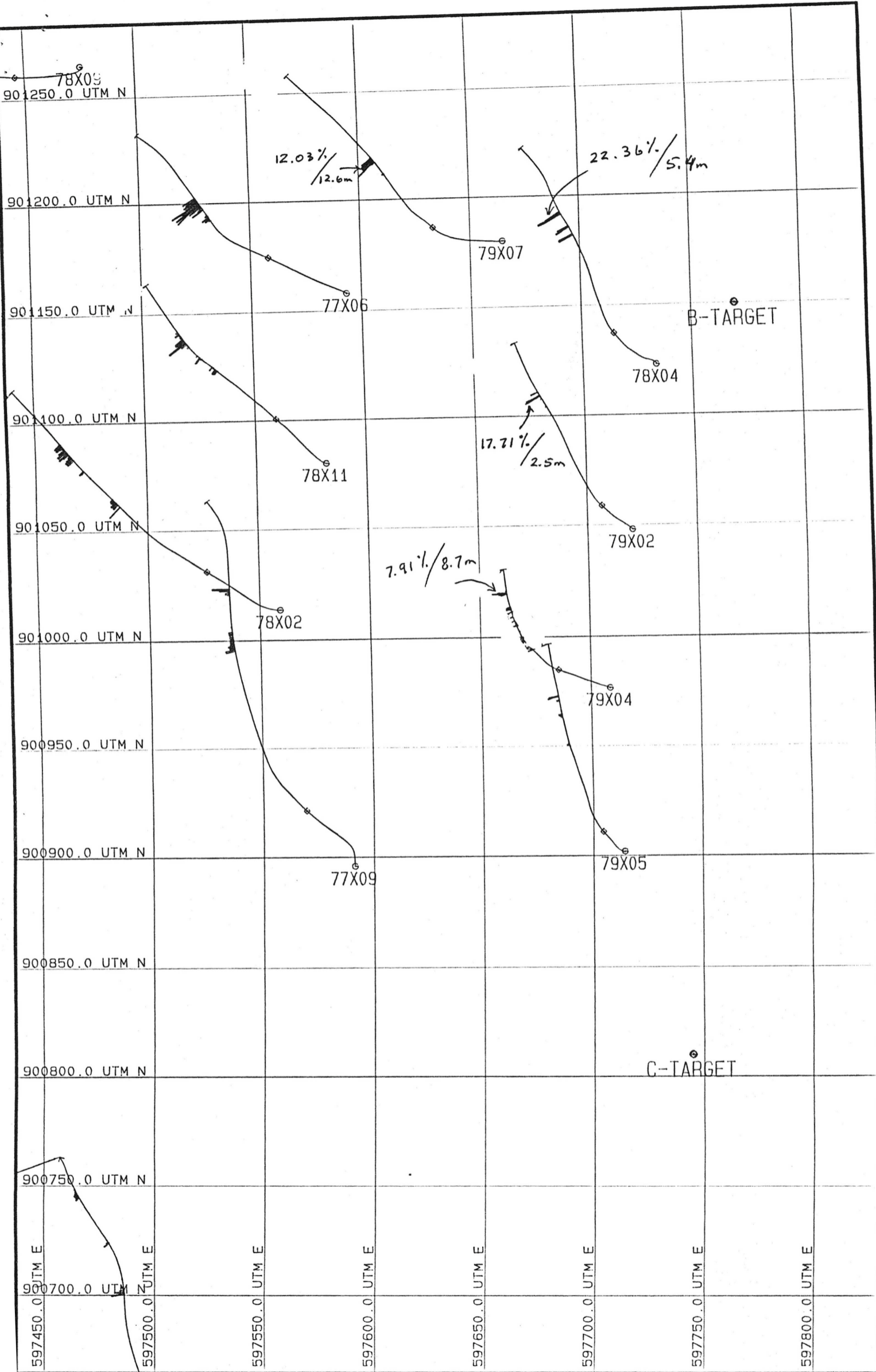


FIGURE 2

QUICK-PLOT GEMCOM Services Inc.	DATE = 13-10-90 TIME = 11:02:10	Curragh Resources Inc. Faro Mine	DY DEPOSIT OBLIQUE SECTION 023 AZ. J. A. Z.
HORIZONTAL SCALE = 1 : 5000		VERTICAL SCALE = 1 : 5000	



QUICK-PLOT  
GEMCOM Services Inc.

DATE = 12-10-90  
TIME = 19:57:03

Curragh Resources Inc.  
Faro Mine

DY DEPOSIT  
DECLINE DRILL  
PROGRAM  
J. A. Z.

HORIZONTAL SCALE = 1 : 2000

VERTICAL SCALE = 1 : 2000

Fluids 3

APPENDIX A  
DOWN HOLE SURVEY DATA

CURRENT TREND DATA FOR 90DY-04-DS:  
SURVEYS UPTO OCT. 11, 1990

File: G:\DY\PILOTPLT.WRI

SURVEY TYPE	DEPTH (FT.)	AZIMUTH	INCLINATION	CO-ODS		HORIZONTAL
				NORTHING	EASTING	DEVIATION
GYROSCOPE	0	183.20	89.56	0	0	0.00
GYROSCOPE	25	176.60	89.45	-0.22	0	0.22
GYROSCOPE	50	176.40	89.50	-0.45	0.02	0.45
GYROSCOPE	75	189.00	89.50	-0.67	0.01	0.67
GYROSCOPE	100	195.40	89.36	-0.92	-0.05	0.92
GYROSCOPE	125	199.30	89.21	-1.22	-0.14	1.23
GYROSCOPE	150	203.60	89.13	-1.56	-0.28	1.58
GYROSCOPE	175	199.70	89.07	-1.93	-0.42	1.98
GYROSCOPE	200	198.60	89.10	-2.31	-0.56	2.38
GYROSCOPE	225	210.30	89.15	-2.65	-0.71	2.74
GYROSCOPE	250	211.20	89.00	-3	-0.92	3.14
GYROSCOPE	275	209.10	88.77	-3.43	-1.17	3.62
GYROSCOPE	300	210.60	88.73	-3.9	-1.44	4.16
GYROSCOPE	325	207.70	88.71	-4.39	-1.71	4.71
GYROSCOPE	350	203.80	88.68	-4.91	-1.96	5.29
GYROSCOPE	375	211.20	88.67	-5.42	-2.23	5.86
GYROSCOPE	400	212.30	88.66	-5.92	-2.53	6.44
GYROSCOPE	425	209.70	88.68	-6.42	-2.83	7.02
GYROSCOPE	450	213.40	88.78	-6.89	-3.12	7.56
GYROSCOPE	475	213.50	88.71	-7.35	-3.43	8.11
GYROSCOPE	500	209.70	88.70	-7.83	-3.72	8.67
GYROSCOPE	525	206.80	88.56	-8.36	-4.01	9.27
GYROSCOPE	550	202.80	88.52	-8.94	-4.27	9.91
GYROSCOPE	575	201.50	88.68	-9.5	-4.5	10.51
GYROSCOPE	600	204.10	88.52	-10.07	-4.74	11.13
GYROSCOPE	625	202.90	88.54	-10.66	-5	11.77
GYROSCOPE	637	203.80	88.55	-10.94	-5.12	12.08
GYROSCOPE	650	203.98	88.78	-11.15	-5.25	12.33
GYROSCOPE	675	211.28	88.92	-11.81	-5.58	13.06
GYROSCOPE	700	221.81	89.51	-11.81	-5.58	13.06
GYROSCOPE	725	73.88	89.76	-11.81	-5.58	13.06
GYROSCOPE	750	56.09	89.14	-11.81	-5.58	13.06
GYROSCOPE	775	49.86	88.90	-11.48	-5.25	12.63
GYROSCOPE	800	50.63	88.99	-11.15	-4.59	12.06
GYROSCOPE	825	47.57	89.00	-11.15	-4.59	12.06
GYROSCOPE	850	40.14	88.98	-10.50	-3.94	11.21
GYROSCOPE	875	30.75	89.03	-10.17	-3.94	10.91
GYROSCOPE	900	26.17	89.07	-10.17	-3.61	10.79
GYROSCOPE	925	19.04	89.08	-9.51	-3.61	10.18
GYROSCOPE	950	15.45	89.17	-9.19	-3.61	9.87
GYROSCOPE	975	6.15	89.15	-8.86	-3.28	9.45
GYROSCOPE	1000	4.61	89.18	-8.53	-3.28	9.14
GYROSCOPE	1025	356.86	89.18	-8.20	-3.28	8.83
GYROSCOPE	1050	358.29	89.22	-7.87	-3.28	8.53
GYROSCOPE	1075	357.89	89.19	-7.22	-3.28	7.93
GYROSCOPE	1100	2.55	89.08	-6.89	-3.28	7.63
GYROSCOPE	1125	355.44	89.09	-6.89	-3.28	7.63
GYROSCOPE	1150	357.27	89.11	-6.23	-3.28	7.04

CURRENT TREND DATA FOR 90DY-04-DS:  
SURVEYS UPTO OCT. 11, 1990

File: G:\DY\PILOTPLT.WR1

SURVEY TYPE	DEPTH (FT.)	AZINITH	INCLINATION	CO-ODS		HORIZONTAL
				NORTHING	EASTING	DEVIATION
GYROSCOPE	1175	358.98	89.07	-5.91	-3.28	6.76
GYROSCOPE	1200	359.9	89.11	-5.58	-3.28	6.47
GYROSCOPE	1225	356.93	89.11	-5.25	-3.61	6.37
GYROSCOPE	1250	358.44	89.07	-4.59	-3.61	5.84
GYROSCOPE	1275	351.08	89.07	-3.94	-3.61	5.34
GYROSCOPE	1300	348.34	88.99	-3.61	-3.61	5.10
GYROSCOPE	1325	348.25	88.98	-2.95	-3.61	4.66
GYROSCOPE	1350	342.65	88.81	-2.30	-3.94	4.56
GYROSCOPE	1375	341.77	88.71	-1.97	-3.94	4.40
GYROSCOPE	1400	337.03	88.74	-1.31	-3.94	4.15
GYROSCOPE	1425	338.86	88.82	-0.98	-4.27	4.38
GYROSCOPE	1450	341.53	88.83	-0.66	-4.59	4.64
GYROSCOPE	1475	342.64	88.96	0.00	-4.59	4.59
GYROSCOPE	1500	343.62	88.94	0.33	-4.59	4.60
GYROSCOPE	1525	348.08	88.82	0.98	-4.92	5.02
GYROSCOPE	1550	345.48	88.84	1.31	-5.25	5.41
GYROSCOPE	1575	349.46	88.79	1.97	-5.25	5.61
GYROSCOPE	1600	349.37	88.68	2.62	-5.25	5.87
GYROSCOPE	1625	351.1	88.57	2.95	-5.25	6.02
GYROSCOPE	1650	346.34	88.50	3.61	-5.58	6.64
GYROSCOPE	1675	347.79	88.28	4.27	-5.58	7.02
GYROSCOPE	1700	347.59	88.27	4.92	-5.58	7.44
GYROSCOPE	1712	345.42	88.25	5.25	-5.91	7.90
SPERRY SUN IOL/6 Deg. COMPASS	1752	342	87.9	5.25	-6.23	8.15
SPERRY SUN 6 Deg. COMPASS	1802	341	87.3	8.53	-6.89	10.97
SPERRY SUN IOL/ASSUMED AZ.	1862	341	87.4	11.15	-7.87	13.65
SPERRY SUN IOL/6 Deg. COMPASS	1892	341.1	86.9	12.14	-8.20	14.65
SPERRY SUN IOL/6 Deg. COMPASS	1917	341	87.15	13.45	-8.50	15.91
SPERRY SUN IOL/6 Deg. COMPASS	2008	5	88.25	16.73	-9.19	19.09
SPERRY SUN IOL/6 Deg. COMPASS	2105	356	88.17	19.69	-9.19	21.73
ASSUMED TREND	2113	356	88.17	20.01	-9.19	22.02

APPENDIX B

ASSAY SHEET FOR 90DY-04-DS



APPENDIX C

TARGET CODING FOR PROPOSED DRILL HOLES  
AND  
SURVEY LOCATIONS CO-ORDINATES OF  
POINTS LOCATED BY LAMERTON

FILE: TARGET.ASC

TARGET CODE	EASTING	NORTHING	GROUND EST. ELEV.	HOLE DEPTH
"A-TARGET"	597282.00	901255.00	1132.00	850.0
"B-TARGET"	597770.00	901150.00	1029.35	570.0 *
"C-TARGET"	597745.00	900810.00	1045.00	500.0
"D-TARGET"	597702.00	900394.00	1012.00	380.0
"COLLAR-E"	597687.00	900096.90	963.28	290.0
"COLLAR-F"	597653.60	899673.90	884.39	110.0 *
"COLLAR-G"	597645.80	899574.40	874.22	75.0 *
"COLLAR-H"	597641.40	899519.10	865.03	60.0 *
"COLLAR-I"	597637.90	899474.60	860.38	40.0 *
"COLLAR-J"	597635.60	899444.80	854.95	30.0 *
"P-COLLAR"	597632.00	899400.00	843.39	N/A *

\* LOCATIONS SURVEYED BY LAMERTON

Appended sheet provided by Lamerton & Assc.

POINT	NORTHING	EASTING	ELNV	CODE
1	6897493.926	599458.978	1266.526	1439 as measured
2	6899358.384	597307.686	935.430	1449
3	6900432.898	597666.333	1021.306	Fd.'69 Post
4	6898953.008	597354.100	823.603	
5	6899178.387	597549.888	813.419	
6	6899093.925	597562.148	790.571	
7	6899126.292	597530.927	799.378	
8	6899406.670	597842.292	846.181	
10	6899411.784	597723.837	848.070	
12	6899512.121	597767.034	877.738	
13	6899426.113	597634.059	853.315	
14	6899551.165	597643.921	872.127	
17	6900123.177	597700.479	970.958	
18	6900096.926	597686.996	963.276	
19	6900061.112	597626.079	967.368	
20	6900036.341	597540.892	973.231	
21	6900044.761	597514.330	979.760	
22	6900120.670	597565.290	991.020	
23	6900267.936	597620.416	1005.447	
24	6900492.967	597717.251	1027.267	
25	6900660.868	597786.258	1038.139	
26	6900839.258	597747.209	1044.379	
27	6900972.355	597673.372	1054.904	
28	6901044.431	597609.396	1063.719	
29	6901187.216	597571.009	1078.041	
30	6901149.985	597770.009	1029.353	
32	6901171.918	598013.247	1040.552	
39	6897494.701	599458.084	1266.526	1439
50	6899400.000 <i>portal</i>	597632.000	843.387	Dye Collar <i>oct 6</i>
51	6900096.926 <i>E</i>	597686.996	963.276	on Road <i>oct 7</i>
52	6901149.985 <i>B</i>	597770.009	1029.353	Ramp Bottom <i>oct 10, 11</i>
53	6899444.820 <i>J</i>	597635.534	854.949	+46 from portal <i>oct 6</i>
54	6899474.565 <i>I</i>	597637.880	860.384	+75 <i>oct 6</i>
55	6899519.045 <i>H</i>	597641.388	865.025	+120 <i>oct 6</i>
56	6899574.463 <i>G</i>	597645.758	874.225	+175 <i>oct 7</i>
57	6899673.966 <i>F</i>	597653.604	884.925	+275 <i>oct 8</i>
100	6899400.000 <i>portal</i>	597632.003	843.387	

APPENDIX D  
DEVIATION DATA  
AND  
LENGTH WEIGHTED GRADE CALC'S

GYROSCOPIC DOWN HOLE SURVEY DATA  
FROM PREVIOUS DY DRILLING

TO BE USED TO DETERMINE APPROXIMATE DEVIATION TREND  
FOR 1990 DY DECLINE DRILL PROGRAM

FILE: DEVIATE.WR1  
J. ZBEETNOFF  
OCT. 11, 1990

=====

\*\*\*\*\* TARGET B \*\*\*\*\*  
BOTTOM OF THE RAMP (CORNER)  
TARGET LOCATION: 6901149.985 N ESTIMATED HOLE LENGTH: 570m  
597770.009 E  
476.5 Elev.  
1029.353 TOPOGRAPHIC ELEVATION ABOVE TARGET (SURVEYED)  
\*\*\*\*\*

HOLE-ID	NORTHING	EASTING	ELEV.	INCL.	INCL.	AZIMITH	HORIZONTAL DEVIATION			VERTICAL DRILLED		
							DOGLEG	NORTHING	EASTING	DISPLACEMENT	DEPTH	LENGTH
78X04	901123.0	597733.6	1039.1	-90	0	360	0	0.00	0.00	0.00	0.00	0.00
78X04	901123.3	597733.6	1008.6	-89	1	357.9	0.999	0.30	0.00	0.30	30.50	30.50
78X04	901124.1	597732.8	978.1	-86	4	304	3.502	1.10	-0.80	1.36	60.96	61.00
78X04				-86	4	282.9	1.467					91.40
78X04				-86.6	3.4	283.2	0.599					121.90
78X04				-85	5	298.3	1.930					152.40
78X04				-83.9	6.1	305.7	1.309					182.90
78X04				-83.8	6.2	304.5	0.162					213.40
78X04				-81.7	8.3	318.4	2.728					243.80
78X04				-82	8	319.5	0.337					274.30
78X04				-81.5	8.5	323.8	0.793					304.80
78X04				-80.9	9.1	337.4	2.158					335.30
78X04				-78.5	11.5	342.5	2.563					365.80
78X04				-79.2	10.8	340.3	0.821					396.20
78X04				-78.1	11.9	345.7	1.527					426.70
78X04				-76.4	13.6	343.5	1.766					457.20
78X04				-73	17	337.1	3.788					487.70
78X04	901181.0	597697.4	527.6	-72.3	17.7	335	0.938	58.00	-36.20	68.37	511.48	518.20
78X04	901189.4	597693.1	498.5	-74.1	15.9	326.3	3.095	66.40	-40.50	77.78	540.57	548.60
78X04	901196.8	597689.2	469.2	-74.1	15.9	337.6	3.089	73.80	-44.40	86.13	569.91	579.10
78X04	901204.8	597686.3	439.9	-73.3	16.7	342	1.469	81.80	-47.30	94.49	599.18	609.60
78X04	901213.0	597682.1	410.9	-71	19	324.9	5.694	90.00	-51.50	103.69	628.21	640.10
78X04	901220.2	597676.3	385.1	-69.7	20.3	317.3	3.186	97.20	-57.30	112.83	654.01	667.50

HOLE-ID	NORTHING	EASTING	ELEV.	INCL.	INCL.	AZIMUTH	DOGLEG=====			VERTICAL DRILLED		
							/100'	NORTHING	EASTING	DISPLACEMENT	DEPTH	LENGTH
79X07	901180.0	597665.0	1052.7	-90	0	0	0	0.00	0.00	0.00	0.00	0.00
79X07	901179.9	597663.8	1022.8	-85.5	4.5	265.9	4.572	-0.10	-1.20	1.20	29.95	30.00
79X07	901179.9	597661.3	992.9	-84.9	5.1	273.5	0.887	-0.10	-3.70	3.70	59.85	60.00
79X07	901180.1	597658.3	963.0	-83.5	6.5	273.5	1.422	0.10	-6.70	6.70	89.69	90.00
79X07	901180.3	597654.7	933.2	-82.7	7.3	273.9	0.814	0.30	-10.30	10.30	119.47	120.00
79X07				-83	7	272.7	0.340					150.00
79X07				-82.9	7.1	280.1	0.927					180.00
79X07				-82.5	7.5	282.3	0.495					210.00
79X07				-83	7	291.9	1.329					240.00
79X07				-82.5	7.5	297.4	0.868					270.00
79X07				-83.7	6.3	314	2.352					300.00
79X07				-83.9	6.1	312.1	0.291					330.00
79X07				-82.5	7.5	305.1	1.650					360.00
79X07				-82.7	7.3	308.5	0.489					390.00
79X07				-84.5	5.5	320.4	2.262					420.00
79X07				-83.7	6.3	325.4	0.965					450.00
79X07				-79.9	10.1	322.9	3.876					480.00
79X07	901205.9	597615.4	546.5	-79	11	327.1	1.202	25.90	-49.60	55.96	506.25	510.00
79X07	901210.9	597615.2	517.1	-77.9	12.1	326.7	1.120	30.90	-49.80	58.61	535.64	540.00
79X07	901216.3	597608.4	487.8	-76.9	13.1	324	1.178	36.30	-56.60	67.24	564.92	570.00
79X07	901221.8	597604.0	458.6	-75.9	14.1	318	1.755	41.80	-61.00	73.95	594.08	600.00
79X07	901227.5	597598.9	429.6	-74.3	15.7	318.4	1.628	47.50	-66.10	81.40	623.07	630.00
79X07	901233.4	597593.6	400.7	-75	15	318.7	0.715	53.40	-71.40	89.16	651.99	660.00
79X07	901239.1	597588.3	371.8	-74.7	15.3	314.6	1.130	59.10	-76.70	96.83	680.95	690.00

HOLE-ID	NORTHING	EASTING	ELEV.	INCL.	INCL.	AZIMUTH	DOGLEG =====			VERTICAL DRILLED		
							/100'	NORTHING	EASTING	DISPLACEMENT	DEPTH	LENGTH
79X02	901048.0	597720.6	1036.4	-90	0	0	0	0.00	0.00	0.00	0.00	0.00
79X02	901048.0	597720.7	1005.4	-89.8	0.2	117.9	0.196	0.00	0.10	0.10	31.00	31.00
79X02	901048.3	597720.4	975.4	-88.5	1.5	314.1	1.720	0.30	-0.20	0.36	60.99	61.00
79X02	901048.9	597719.6	944.4	-87.2	2.8	305.8	1.311	0.90	-1.00	1.35	91.97	92.00
79X02	901049.9	597718.2	914.5	-86.3	3.7	306.4	0.915	1.90	-2.40	3.06	121.92	122.00
79X02	901051.1	597716.6	884.5	-86.2	3.8	301.6	0.334	3.10	-4.00	5.06	151.86	152.00
79X02				-84.6	5.4	300.7	1.574					183.00
79X02				-84.3	5.7	307.3	0.716					213.00
79X02				-84.5	5.5	314.3	0.699					244.00
79X02				-84.6	5.4	313.7	0.116					274.00
79X02				-84.6	5.4	312	0.157					305.00
79X02				-84.5	5.5	324.6	1.217					335.00
79X02				-83.1	6.9	328.7	1.442					366.00
79X02				-81.1	8.9	331.3	2.063					396.00
79X02				-79.3	10.7	332.9	1.789					427.00
79X02				-78.7	11.3	334.7	0.702					457.00
79X02				-78.3	11.7	338	0.756					488.00
79X02	901089.6	597689.9	522.1	-77.6	12.4	337.4	0.722	41.60	-30.70	51.70	514.29	518.00
79X02	901096.1	597687.1	491.9	-76.1	13.9	335	1.569	48.10	-33.50	58.62	544.48	549.00
79X02	901103.3	597683.3	463.1	-72.6	17.4	330.3	3.779	55.30	-37.30	66.70	573.35	579.00
79X02	901111.8	597678.4	433.6	-70.6	19.4	329.9	1.970	63.80	-42.20	76.49	602.76	610.00
79X02	901120.6	597674.0	405.3	-70.7	19.3	337.1	2.424	72.60	-46.60	86.27	631.07	640.00
79X02	901129.9	597670.3	376.0	-71.8	18.2	339.6	1.339	81.90	-50.30	96.11	660.42	671.00

DY PROPERTY  
LENGTH WEIGHTED GRADE CALC'S

File: ASSYDAT.WR1

HOLE-ID	FROM (m)	TO (m)	INTERVAL	ROCK CODE	SG-PULP	Pb%	Zn%	Pb+Zn%	Ag(g/t)	Au(g/t)	
79X07	544	545.8	1.8	4A0	-1	1.51	3.28	4.79	28	-1	
79X07	545.8	568.4	22.6	WASTE	-1	-1	-1	-1	-1	-1	
79X07	568.4	570.2	1.8	4A0	-1	0.26	0.49	0.75	4	-1	
79X07	570.2	572.2	2	4A0	-1	0.02	0.03	0.05	1	-1	
79X07	572.2	574.2	2	4A0	-1	0.32	0.45	0.77	4	-1	
79X07	574.2	576.1	1.9	4G0	4.1	1.87	4.55	6.42	32	0.34	12.198
79X07	576.1	577.8	1.7	4G0	4.2	2.13	5.88	8.01	34	0.48	13.617
79X07	577.8	578.6	0.8	4G0	4.4	6.78	16.2	22.98	150	1.2	18.384
79X07	578.6	580.3	1.7	4D4	3.3	2.17	4.7	6.87	35	0.51	11.679
79X07	580.3	581.4	1.1	4D4	3.0	3.61	7.76	11.37	83	0.34	12.507
79X07	581.4	583.3	1.9	4D4	4.3	6.76	9.52	16.28	104	1.44	30.932
79X07	583.3	585.2	1.9	4D4	3.0	4.41	9.85	14.26	3	0.1	27.094
79X07	585.2	586.8	1.6	4A14	3.9	5.51	10.2	15.71	80	0.65	25.136
79X07	586.8	588.8	2	5A0	-1	0.37	0.77	1.14	5	-1	151.547
79X07	588.8	792.7	203.9	WASTE	-1	-1	-1	-1	-1	-1	12.6

12.03% /12.6m

DY PROPERTY  
LENGTH WEIGHTED GRADE CALC'S

File: ASSYDAT.WR1

HOLE-ID	FROM (m)	TO (m)	INTERVAL	ROCK CODE	SG-PULP	Pb%	Zn%	Pb+Zn%	Ag(g/t)	Au(g/t)	
78X04	518.4	520.6	2.2	4G4	4.3	5.38	12.19	17.57	92	0.62	
78X04	520.6	532.3	11.7	WASTE	-1	-1	-1	-1	-1	-1	
78X04	532.3	533.4	1.1	4J0	3.4	4.42	12.45	16.87	49	0.14	
78X04	533.4	533.9	0.5	WASTE	-1	-1	-1	-1	-1	-1	
78X04	533.9	534.5	0.6	4J0	3.9	3.77	10.82	14.59	43	0.07	
78X04	534.5	556.6	22.1	WASTE	-1	-1	-1	-1	-1	-1	
78X04	556.6	558.6	2	4E0	4.4	11.28	15.25	26.53	192	0.89	53.06
78X04	558.6	560	1.4	4E9	3.8	8.72	13.04	21.76	134	1.58	30.464
78X04	560	562	2	4E0	4.2	8.23	10.39	18.62	122	1.08	37.24
78X04	562	675	113	WASTE	-1	-1	-1	-1	-1	-1	120.764

22.36% /5.4m

5.4



DY PROPERTY  
LENGTH WEIGHTED GRADE CALC'S

File: ASSYDAT.WR1

HOLE-ID	FROM (m)	TO (m)	INTERVAL	ROCK CODE	SG-PULP	Pb%	Zn%	Pb+Zn%	Ag(g/t)	Au(g/t)	
79X04	365.5	367	1.5	4L76	-1	0.05	0.03	0.08	2	-1	
79X04	367	390.6	23.6	WASTE	-1	-1	-1	-1	-1	-1	
79X04	390.6	391.9	1.3	4A0	-1	0.05	0.04	0.09	2	-1	
79X04	391.9	392.3	0.4	WASTE	-1	-1	-1	-1	-1	-1	
79X04	392.3	394.5	2.2	4A0	-1	0.05	0.03	0.08	3	-1	
79X04	394.5	396.5	2	4K1	-1	0.03	0.01	0.04	6	-1	
79X04	396.5	398.8	2.3	4C79	-1	0.04	0.01	0.05	-1	-1	
79X04	398.8	400	1.2	4A0	-1	0.02	0.01	0.03	3	-1	
79X04	400	400.5	0.5	4E0	-1	0.01	0.02	0.03	7	-1	
79X04	400.5	582.2	181.7	WASTE	-1	-1	-1	-1	-1	-1	
79X04	582.2	584.2	2	4D57	-1	2.21	5.19	7.4	50	-1	
79X04	584.2	586.2	2	4A4	-1	0.68	1.03	1.71	12	-1	
79X04	586.2	588.2	2	4A4	-1	3.62	3.41	7.03	46	-1	
79X04	588.2	590	1.8	4A4	-1	2.64	3.34	5.98	40	-1	
79X04	590	625.8	35.8	WASTE	-1	-1	-1	-1	-1	-1	
79X04	625.8	626.8	1	4G0	4.0	4.79	11.95	16.74	90	0.55	16.74
79X04	626.8	627.8	1	4A41	3.0	2.72	5.93	8.65	47	0.34	8.65
79X04	627.8	629.1	1.3	4A41	3.0	3.6	7.13	10.73	66	0.55	13.949
79X04	629.1	630.6	1.5	4C0	3.3	3.66	6.87	10.53	56	0.93	15.795
79X04	630.6	632.6	2	4A1	-1	1.18	2.11	3.29	21	-1	6.58
79X04	632.6	634.5	1.9	4A1	-1	1.7	2.03	3.73	25	-1	7.087
79X04	634.5	689.1	54.6	WASTE	-1	-1	-1	-1	-1	-1	68.801

7.91% / 8.7m

8.7

BY PROPERTY  
LENGTH WEIGHTED GRADE CALC'S

File: ASSYDAT.WR1

HOLE-ID	FROM (m)	TO (m)	INTERVAL	ROCK CODE	SG-PULP	Pb%	Zn%	Pb+Zn%	Ag(g/t)	Au(g/t)	
78X11	464.9	467.2	2.3	4E89	-1	1.33	0.96	2.29	27	-1	
78X11	467.2	468.6	1.4	WASTE	-1	-1	-1	-1	-1	-1	
78X11	468.6	470.6	2	4E819	-1	0.69	1	1.69	17	-1	
78X11	470.6	471.8	1.2	4E819	-1	0.32	0.6	0.92	14.5	-1	
78X11	471.8	473.8	2	4E819	-1	0.21	0.19	0.4	14.5	-1	
78X11	473.8	475.8	2	4E819	-1	0.23	0.2	0.43	15	-1	
78X11	475.8	477.8	2	4E819	-1	0.24	0.09	0.33	16	-1	
78X11	477.8	479.4	1.6	4E819	-1	0.16	0.06	0.22	10	-1	
78X11	479.4	550.2	70.8	WASTE	-1	-1	-1	-1	-1	-1	
78X11	550.2	552.2	2	4A4	2.7	2.12	5.22	7.34	37	0.5	14.68
78X11	552.2	554.1	1.9	4A4	2.7	2.1	5.05	7.15	36	0.58	13.585
78X11	554.1	556.2	2.1	4A4	2.6	3.56	4.63	8.19	53	0.34	17.199
78X11	556.2	558.3	2.1	4A0	-1	1.62	1.54	3.16	21	-1	6.636
78X11	558.3	560.1	1.8	4A0	-1	1.04	2.34	3.38	18	-1	6.084
78X11	560.1	561.2	1.1	4A0	-1	0.78	2.03	2.81	14.5	-1	3.091
78X11	561.2	562.3	1.1	4A4	-1	2.31	4.77	7.08	37	-1	7.788
78X11	562.3	583.1	20.8	WASTE	-1	-1	-1	-1	-1	-1	69.063
78X11	583.1	584.1	1	4A1	-1	1.27	2.44	3.71	14.5	-1	
78X11	584.1	586.1	2	4A1	-1	1.68	2.59	4.27	20	-1	
78X11	586.1	587.5	1.4	4A14	-1	4.7	5.2	9.9	67	-1	
78X11	587.5	589.5	2	4A0	-1	0.92	1.14	2.06	12	-1	
78X11	589.5	591.5	2	4A0	-1	0.86	1.8	2.66	11	-1	
78X11	591.5	592.5	1	4A0	-1	1.3	3.27	4.57	17	-1	
78X11	592.5	594.2	1.7	4A0	-1	0.64	1.61	2.25	7	-1	
78X11	594.2	607.3	13.1	WASTE	-1	-1	-1	-1	-1	-1	
78X11	607.3	609.3	2	4A0	-1	0.17	0.26	0.43	4	-1	
78X11	609.3	611.3	2	4A0	-1	1.84	3.05	4.89	28	-1	
78X11	611.3	613.3	2	4A0	-1	0.91	0.85	1.76	14.5	-1	
78X11	613.3	615.3	2	4A0	-1	1.74	2.83	4.57	26	-1	
78X11	615.3	617.2	1.9	4A4	2.9	3.41	5.64	9.05	53	0.69	17.195
78X11	617.2	618.3	1.1	4E0	4.2	7.83	7.45	15.28	142	0.96	16.808
78X11	618.3	619.6	1.3	4G4	4.0	6.83	14.84	21.67	106	0.69	28.171
78X11	619.6	621.6	2	4D4	3.1	3.47	5.11	8.58	54	0.62	17.16
78X11	621.6	623.6	2	4D4	3.1	4.31	7.69	12	76	0.82	24
78X11	623.6	625.2	1.6	4D4	3.7	4.48	7.05	11.53	69	0.69	18.448
78X11	625.2	627.2	2	4A0	-1	0.92	2.21	3.13	17	-1	6.26
78X11	627.2	629.2	2	4A0	-1	1.31	2.82	4.13	21	-1	8.26
78X11	629.2	631.2	2	4A0	-1	0.92	2.62	3.54	18	-1	7.08
78X11	631.2	632.2	1	4A0	-1	1.06	2.66	3.72	20	-1	3.72
78X11	632.2	634.1	1.9	4A0	-1	2.44	4.77	7.21	38	-1	13.699
78X11	634.1	636	1.9	5A1	-1	0.36	0.76	1.12	5	-1	2.128
78X11	636	638	2	4A0	-1	2	3.01	5.01	35	-1	10.02
78X11	638	716.2	78.2	WASTE	-1	-1	-1	-1	-1	-1	51.167

5.71% /12.1m

12.1

12.30% /9.9m

9.9

4.00% /12.8m

12.8