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Introduction

This report summarizes the results of a sectional hand calculation of the reserves of phase A of the Faro deposit. Phase A includes most of the first years mining reserves according to the latest mining plans. The major purpose of the calculation was to report reserves by bench and by ore type in order to compare with existing reserve estimates. This is currently the only estimate that uses 1984 fill in drilling as a data source.

Other reserve estimates for the phase A area are the F3 block model that has been used for mine planning by Cyprus Anvil in the past, and the T3 model that has been used for the evaluation of the Faro mine project by Kilborn Engineering. These models are described elsewhere in detail; both are based on data collected up to and including 1981, are based on the same geologic interpretation, use the same 50′x 50′x 20′ high blocks and the same bench composites. The models differ in the manner of interpolation, F3 uses no geologic control on interpolation while T3 restricts its choice of assay composites to appropriate ore types.

Methods

At the outset a strictly routine sectional calculation similar to that done for Faro by Hall and Slack in 1984 was anticipated. This method while intuitive and uncomplicated makes it very difficult to report reserves by bench and especially difficult to quote a meaningful grade for a given bench.

An alternative approach that would make it possible to report results by bench was selected, this method sacrifices some of the selectivity normally possible in a sectional calculation but because of the geometry of the deposit should nonetheless give a reasonable approximation of tonnage and grade by bench.*

The geometry of the deposit was modeled by interpretation of the relevant cross-sections. The distribution of grade rather than simply lithofacies was used as a means of correlation between drillholes. To do this each drillhole log was examined for sections that met the criteria of being over 6% Pb + Zn over 20 feet or more thickness. The results showed that the deposit generally consists of an upper and lower band of qualifying high grade mineralization separated by lower grade sulphides and/or phyllitic waste. A basal unit of low grade quartzose sulphides is generally present. The deposit was only modeled between the high grade bands and the basal zone was ignored. On each section the deposit consists of a southwest area rich in high grade sulphides and with relatively minor (but not insignificant) waste, and a thicker northeast area with three high grade bands within an overall very low grade mineralized body. The northeast portion is in the upthrown block of a major east - west trending and south dipping fault (or more likely, a set of faults) on several of the sections and in plan (Fig. 1) forms a triangular area which will be referred to as the northeast wedge. The bulk of the reserves are in the southwestern area. An important diorite dyke, apparently intruded along the fault that separates zone 3 from zone 1, trends sub-parallel to and is just northwest of section 118+000. A smaller quartz-feldspar porphyry body occurs in the northeast wedge. This interpretation has generally ignored the late stage folds that crenulate the deposit in favor of the simpler concept of nearly flat lying ore layers largely because computations are simpler and realistic handling of the folds was not possible in the time available with the current density of drilling. These folds are present and will have to be delt with in mining but for the purposes of reserve estimation are left to be treated in the F4 model. The effect of these folds is to introduce a great deal of uncertainty into the bench reserves without dramatically influencing the overall reserves. It is important to realize that the models to be compared to the present calculation <u>have</u> attempted to deal with these folds.

For the purposes of computation the overall deposit geometry and limits outlined above was superimposed on a plot of the planned mining benches. The length, in cross section, along the mid-bench line from a given drillhole half way to the next hole or to the interpreted margin of the deposit (or the phase) plus the length to the next hole or edge of deposit in the opposite direction along section was measured. Similarly the strike length northwest and southeast of the section was estimated. For most cases this strike length was half way to the next section but at the edges of the phase A pit and particularly northwest of section 118+000 a shorter length was used depending on the local geometry. The volume of a portion of the deposit on a given bench to be influenced by a given drillhole was estimated by computing the product of the cross-sectional length, the sum of the northwest and southeast strike lengths and the bench height (which in most cases was 20 feet but at the top or bottom of the deposit might be less depending on the local situation). All measurements recorded in feet and the volumes converted to cubic meters. The tonnage of these volumes was calculated by multiplying the volume by the measured pulp specific gravity. These data and calculations are given in Tables 1A to 1C. This method produces a crude approximation to the volume of the deposit. It must be borne in mind that this S.G. in always greater than the insitu rock S.G. since there is no allowance for porosity. Studies on the Anvil District deposits suggests that the overestimation of S.G. is on the order of 5% but can average as high as 10% for the more vuggy massive sulphides. This correction to tonnage is not accounted for directly in any of the mine models quoted here and is one of the major factors contributing to the various corrections that have been applied to Anvil District reserves over the years.

A set of assay (including measured pulp S.G.) composites by bench had already been generated for the interim computer model of Zone 3 (the FI model). These composites were used for this reserve estimate as well. The composites use all available drill data and are calculated by weighting assays by length of an assay interval within a given bench and the measured specific gravity of the individual assay intervals. The composites are based on the length along the drillhole and only consider the portion of the drillhole that is within sulphides, thus most composites are over a length of 20 feet but in a few inclined holes may be marginally longer and at the margins of the deposit the composites are generally shorter than 20 feet. Where internal waste is less than a bench height the waste is assigned zero assay values and these values are used to compute the composite grades. In order to avoid biasing a large volume of ore by an unusually high assay the top 5% of the assays were reduced to the 95th percentile; similarly once the composites were calculated they were rolled back to the 95th percentile. All computer based mine models of the Faro deposit follow a similar proceedure. The composite data used in this calculation is listed in Tables 1A thru 1C; a complete listing of the composites can be found in the planned documentation for the Faro interim model.

The computations were carried out on a spreadsheet that was capable of summing the tonnage of blocks above a given Pb + Zn grade and computing an average grade of this tonnage. The results of these calculations are presented in terms of cutoff grade.

Results

The result of this calculation is presented in Table 2 and compared to the results of other reserve estimates for the same volume of the deposit. On the basis of total contained metal this calculation compares fovorably to the T3 model, this is due to indicating a smaller number of tonnes of higher grade. On a bench by bench basis the two estimates do not compare well; below the 3550 bench (where 74% of the tonnage is) the current estimate tends to show both a smaller tonnage of ore and a slightly smaller total contained metal content than the other models. Above that area largely in the area of the northeast wedge, there is a larger tonnage and correspondingly larger amount of contained metal.

The striking lateral zoning of the deposit is quite apparent in the cross sections. The northeast portion of the deposit poses difficult questions for the overall economics of the deposit since the cost of incremental stepouts to the northeast is high due to increasingly uncertain and likely difficult ground conditions as well as the lower slope already used there. The viability of the northeast part of the deposit is clearly a question for a pit optimization program and work is already underway that will held evaluate this area. The northwestern part of the northeast edge of the deposit (on sections 118 and 119) shows much better development of high grade zones than the sections toward the southeast. These volumes are relatively close to the present pit surface (beneath the present west ramp) and can contribute significantly to the first years production however the analogous volumes on sections 120 and 121 may not be worth extraction.

The geometry and asymmetry of grade distribution in the deposit suggested at first glance that it would be desireable to shift phase A southwest by about 200 ft (to the southwest ultimate pit limit). This appears to be reasonable in cross section from a stripping ratio and grade view but it looks to be very difficult to maintain access to a pit and may not be viable.

There is a relative abundance of phyllitic waste in the upper half of the central part of the deposit. This material is weakly mineralized and has been logged variously as 2CD, 2B6, 1D4, 2L, 1H4* or 1F; a characteristic of this material is that it contains a low but definitely unusually elevated BaO content. Much of this material appears to be an altered mafic sill, such a rock type should be expected to contain talc and this waste type may create problems in the mill. The rock will be light colored like the bleached schist surrounding the deposit and should be easily distinguished from ore. It may be necessary to take special measures to avoid milling or stockpiling this material on the 3550 through 3450 benches of phase A. Some of this rock type was included in the 2BCD ore type in the F3/T3 model thus blocks of that ore type especially if containing an elevated BaO content should be viewed with caution. This rock type will be found throughout the Zone 3 pit and equates to the waste bands between horizons 2 and 3 in the F4 modeled part of the deposit but is thicker there.

Pyrrhotitic ore types (2H) proved to be suprisingly abundant in the upper part of the southwest portion of the deposit (particularly between long. sections 20 and 22). This ore type appears to be spatially related to the waste rocks mentioned above but reaches its maximum development a few hundred feet to the southwest. The T3/F3 models predict about 8% of the reserves in the A phase to be pyrrhotite bearing. Overall this looks reasonable but locally there will be a higher percentage (perhaps as high as 30%) particularly in the deeper benches of the southwest part of the phase. This part of phase A does not appear to be significantly different from the extended JB phase in its pyrrhotite content (nor from the remainder of Zone 3).

In summary there appears to be no indication that the previous computer models have grossly misrepresented the reserves of the A phase. There are problematic ore and waste types in the phase but they are not peculiar to this part of the deposit and the phasing does not appear to have unduly increased exposure to this material (although it would be possible to inadvertently do so). The banded and assymetric nature of grade distribution in the deposit comes through clearly on the sections and I can only reiterate previous recommendations about the need for careful grade control and the hazards of viewing the Faro deposit as a homogenous mass of ore.

* Table 4 compares the cross-sectional areas of volumes considered to be +6% mineralization by this method with ~~those~~ the area interpreted using the criteria that a qualifying drillhole ore intersection must be +6% over 20' or more and these intersections are connected to define volumes of +6% ore. The grade and SG of this mineralization is expected to be higher than the average of +6% bench composites thus overall the two methods probably would compare favorably. This additional sectional calculation could be finished in a few days but I haven't been able to get enough disk space on the computer to calculate the composites and elected to give priority to the interim Faro model.

Table 4

Comparison of Planimitered cross-sectional area of selectively defined high grade bands with cross sectional area of bench defined rectangular ~~outcrops~~ blocks ~~of~~ corresponding to composites of greater than 6% Pb+Zn

Section No.	Area (ft²) by rectangles	Area (ft²) by planimiter	Δ (sq ft)	Δ %
118	97280	88650	-8630	-8.9
119	62801	49475	-13326	-21.2
120	38400	35960	-2440	-6.4
121	27462	25275	-2187	-7.7
Total	225943	199360	-26583	-11.8%

/ FARUCALC.5

JB PHASE

BENCH	WASTE BCY	3D WASTE BCY	SULPHIDE WASTE BCY	TOTAL WASTE BCY	TOTAL WASTE + 6% ORE TONNES
3830	24741		20370	45111	54606
3850	65949		12556	78505	60315
3870	76493		9852	86345	16324
3890	55333		5541	60874	37976
TOTAL	222516	0	48319	270835	169221

BENCH	2UD TONNES	2UD PB	2UD ZN	2UD AG	2A TONNES	2A PB	2A ZN	2A AG	2BCD TONNES	2BCD PB	2BCD ZN	2BCD AG
3830									8879	3.181	3.736	60.949
3850	5012	2.610	4.540	38.000	4955	3.900	5.580	70.000	4800	3.190	5.410	48.000
3870	5380	3.600	4.970	53.000					4757	2.690	3.540	46.000
3890									17717	3.608	4.468	53.312
TOTAL	10392				4955				36153			

BENCH	2CE TONNES	2CE PB	2CE ZN	2CE AG	2EF TONNES	2EF PB	2EF ZN	2EF AG	2EG TONNES	2EG PB	2EG ZN	2EG AG	2EH TONNES	2EH PB	2EH ZN	2EH AG
3830													45727	4.583	8.180	53.188
3850													45548	4.463	7.896	52.509
3870													6187	3.570	5.790	46.000
3890					20259	3.804	5.268	53.523								
TOTAL	0				20259				0				97462			

A PHASE

− : FI<T3
+ : FI>T3
+ = FI≥HC
− : FI<HC

BENCH	WASTE BCY	3D WASTE BCY	SULPHIDE WASTE BCY	TOTAL WASTE BCY	Δ	TOTAL WASTE + 6% ORE TONNES (FI)	T3	F3	HC	Δ
3430	8685		20852	29537	−	229753	271237	~~2?????~~ 286967	177981	+
3450	21907		14093	36000	−	343589	374355	362634	353783	−
3470	38352		30944	69296	+	412027	322654	380842	289557	+
3490	40963		43963	84926	+	445170	412494	403816	412470	+
3510	90463		15945	106408	−	636069	642474	710269	480848	+
3530	167111		30427	197538	−	501346	565072	622830	458958	+
3550	307463		63259	370722	+	311310	290243	261109	271218	+
3570	399464		80759	480223	+	105225	55998	71019	78134	+
3590	420833		44331	465164	−	101074	104642	165734	91123	+
3610	430731		16779	447510	−	183210	232847	237398	177798	+
3630	461834		27648	489482	−	89897	125757	62143	76508	+
3650	487714		48129	535843	+	48866	40082	17187	69732	−
3670	536338		46297	582635	−	47131	53235	54597	22460	+
3690	529842		22222	552064	−	57180	65437	87205	112172	−
3710	584727			584727	−	68573	92654	117362	115269	−
3730	587836			587836	−	11831	18975	18975	83045	−
3750	633776	3852		637628	+	3063	0	0	19261	−
3770	616077	8000		624077		0				
3790	622257	34667		656924		0				
3810	612225	46833		659058		0				
3830	556466	133521		689987		0				
3850	442309	218576		660885		0				
3870	212352	90759		303111		0				
3890	191574	73679		265253		0				
3910	66284			66284		0				
TOTAL	9067583	609887	505648	10183118		3595314				

BENCH	2UD TONNES	2UD PB	2UD ZN	2UD AG	2A TONNES	2A PB	2A ZN	2A AG	2BCD TONNES	2BCD PB	2BCD ZN	2BCD AG
3430									4871	2.370	4.890	22.000
3450					77659	3.519	4.403	72.650	5822	2.308	4.582	22.935
3470					33697	2.637	3.672	53.149	47475	2.968	5.699	29.311
3490									39696	2.954	5.592	50.718
3510									16254	5.582	5.348	51.407
3530									66122	3.518	5.058	65.176
3550									110117	3.675	5.321	70.094
3570									17178	4.830	5.611	61.816
3590									26087	2.519	4.628	30.392
3610					2068	1.908	4.874	20.438	43891	2.476	5.637	15.878
3630					28182	2.012	5.198	21.883	10973	2.416	5.579	16.000
3650												
3670									4545	2.350	5.410	46.000
3690					12850	2.870	6.870	29.000	18916	3.358	3.184	56.466
3710					9204	3.230	7.570	30.000	22809	3.720	2.749	63.451
3730									4474	3.680	2.490	63.000
TOTAL	0				163660				439230			
PERCENT OF EACH ORE TYPE					5				12			

BENCH	2CE TONNES	2CE PB	2CE ZN	2CE AG	2EF TONNES	2EF PB	2EF ZN	2EF AG	2EG TONNES	2EG PB	2EG ZN	2EG AG	2EH TONNES	2EH PB	2EH ZN	2EH AG
3430					212139	3.812	5.733	46.814	12743	2.714	4.500	3.469				
3450					260108	3.825	5.783	48.905								
3470	4146	3.130	3.370	59.000	280327	4.177	5.432	45.418	25372	5.084	5.840	72.491	21010	5.497	6.463	77.000
3490	21954	3.017	5.373	32.000	283815	4.364	6.097	47.507	68541	4.904	5.475	75.408	31164	5.613	6.768	78.678
3510	54981	3.427	6.736	30.874	440047	3.820	5.596	43.420	74570	4.782	5.736	71.515	50217	5.335	6.681	76.386
3530	125580	3.162	6.476	25.912	237346	3.900	5.468	44.620	47068	5.254	6.350	77.776	25230	3.869	4.709	60.138
3550	77085	3.250	5.386	31.505	94196	3.467	5.527	39.603	7329	5.605	6.772	84.550	22583	4.566	6.853	74.715
3570	51730	2.238	5.472	19.636					18732	4.690	5.390	63.000	17585	4.520	7.160	81.000
3590	50096	2.676	6.321	13.110	12403	2.872	4.336	23.565	12488	4.690	5.390	63.000				
3610	75151	2.360	6.073	13.723	37124	4.591	5.284	52.676	24976	4.690	5.390	63.000				
3630	1470	2.710	5.350	27.000	12063	5.404	6.257	60.486	37209	5.450	5.450	71.000				
3650	15050	2.222	4.039	22.631	15212	4.154	4.668	44.305	18604	5.450	5.450	71.000				
3670					16761	4.479	5.582	47.819	25825	3.960	6.020	49.000				
3690					5649	2.220	3.920	28.000	19765	3.889	6.114	51.021				
3710	2262	2.860	5.330	68.000	24726	2.075	4.553	28.833	9572	4.445	6.270	65.431				
3730									7357	3.982	6.206	57.614				
3750									3063	6.500	5.940	105.000				
TOTAL	479505				1931916				413214				167789			
PERCENT OF EACH ORE TYPE	13				54				11				5			

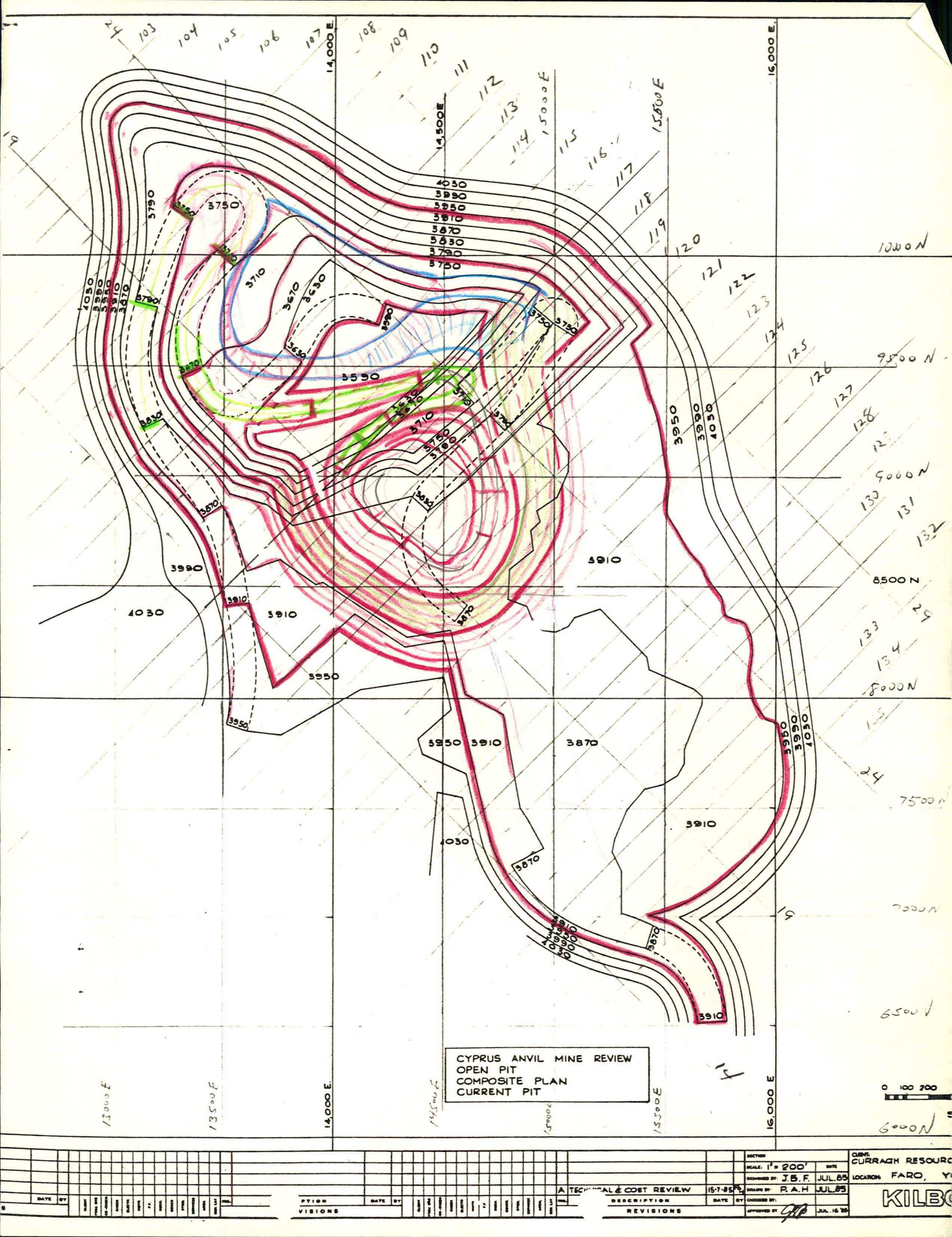
B PHASE

BENCH	WASTE BCY	3D WASTE BCY	SULPHIDE WASTE BCY	TOTAL WASTE BCY	TOTAL WASTE + 6% ORE TONNES
3350	21019		16463	37482	99027
3370	3648		32185	35833	234249
3390	9963		25185	35148	387148
3410	11444		7407	18851	636436
3430	76722		16278	93000	546027
3450	22963		25074	48037	505892
3470	6907		37185	44092	716947
3490	58574		77666	136240	398390
3510	138463		112055	250518	241024
3530	223426		67408	290834	278189
3550	359668		20722	380390	212305
3570	431131		11740	442871	168416
3590	463762		31019	494781	26354
3610	429587		21537	451124	0
3630	523651		8426	532077	0

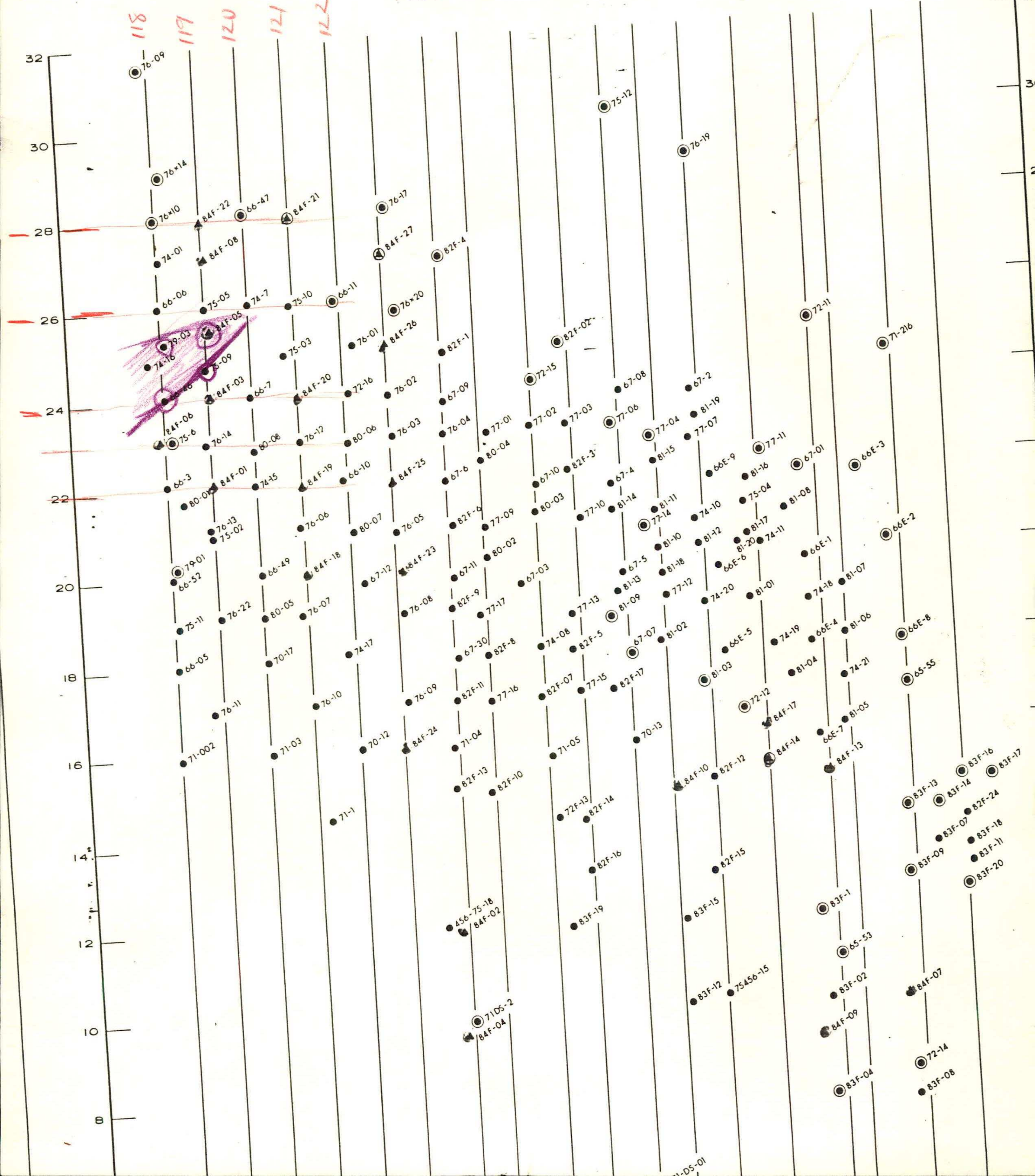
BENCH	2A TONNES	2A PB	2A ZN	2A AG	2BCD TONNES	2BCD PB	2BCD ZN	2BCD AG
3350	27243	2.807	5.006	46.818	45	2.850	5.330	50.000
3370	9795	3.443	5.968	44.296	14854	2.883	5.115	51.527
3390	2059	2.485	4.192	36.693	27800	3.780	2.642	83.653
3410					7372	3.327	2.978	78.522
3430					4602	3.110	5.470	65.000
3450	11412	5.040	6.340	62.000	68573	3.356	4.548	70.819
3470					132271	3.720	5.330	64.981
3490	25425	3.040	4.731	52.009	46213	3.616	5.220	66.389
3510	4446	2.720	4.580	55.000				
3530					49452	3.623	4.410	64.017
3550					8003	3.481	3.993	52.758
3570					22988	2.700	4.616	32.703
3590					3332	2.940	3.908	33.254

BENCH	2CE TONNES	2CE PB	2CE ZN	2CE AG	2EF TONNES	2EF PB	2EF ZN	2EF AG	2EG TONNES	2EG PB	2EG ZN	2EG AG	2EH TONNES	2EH PB	2EH ZN	2EH AG
3350	7726	2.918	4.458	36.959	64013	2.789	5.055	22.540								
3370	12126	2.490	5.264	17.941	197474	2.894	4.794	25.946								
3390	12290	2.639	5.750	27.613	344999	3.013	4.641	27.806								
3410					629064	3.152	4.965	30.011								
3430	4630	2.610	5.070	0.000	509428	3.764	5.449	40.088					27367	3.790	6.040	67.000
3450	31388	4.162	5.264	55.241	311977	3.888	5.429	46.873	6570	2.830	3.330	43.000	75972	5.305	7.479	67.398
3470	56360	4.521	5.870	63.227	385880	4.116	5.772	51.861	58163	3.439	4.946	45.626	84273	4.887	6.785	58.178
3490	31578	4.417	5.869	68.850	214365	4.550	6.112	61.467	50830	4.997	6.557	65.454	29979	4.264	6.459	52.837
3510	70989	3.707	5.015	63.968	57892	4.361	5.794	61.623	60851	5.063	6.351	76.744	46846	3.168	4.733	56.448
3530	44649	3.319	4.663	53.748	30872	2.875	4.602	45.940	115412	5.268	6.238	79.570	37804	3.876	4.441	60.159
3550	35563	2.937	3.716	47.057	43736	3.421	4.314	50.251	119934	4.857	5.202	68.126	5069	3.130	4.510	53.000
3570	1290	3.310	4.680	28.000	17061	3.934	4.001	55.632	94937	4.866	5.638	55.748	32140	3.603	5.504	52.761
3590									23022	4.038	5.253	63.593				

3650	536776		2815 [unclear]	539591 [unclear]	7444 [unclear]	
3670	559698	5556	1661	566915	0	
3690	560555	11111		571666	0	
3710	572014	24870		596884	0	
3730	568012	31833		599845	0	
3750	530062	56870		586932	0	
3770	471384	120111		591495	0	
3790	405280	219648		624928	0	
3810	357331	267407		624738	0	
3830	407703	269424		677127	0	
3850	438453	242437		680890	0	
3870	51630	83111		134741	0	
3890	44744	77966		122710	0	
3910	37566			37566	0	
	8322136	1410344	514826	10247306	4457848	0


CYPRUS ANVIL MINE REVIEW
OPEN PIT
COMPOSITE PLAN
CURRENT PIT
14,000 E.
14,500E
15,000 E
15,500 E
16,000 E.
10000 N
9500 N
9000 N
8500 N
8000 N
7500 N
7000 N
6500 N
6000 N
13000 E
13500 E
4030
3990
3950
3910
3870
3830
3790
3750
3710
3670
3630
3590
0 100 200
SCALE: 1" = 200'
DESIGNED BY: J.B.F. JUL.85
DRAWN BY: P.A.H. JUL.85
CHECKED BY:
APPROVED BY: JUL.16 '85
A TECHNICAL & COST REVIEW 15-7-85
DESCRIPTION
REVISIONS
DATE
BY
CLIENT: CURRAGH RESOURC
LOCATION: FARO, Y
KILBO

FARO DEPOSIT Zone 3



Bench	UNKN S= Tons	Yds	ORE Yds	Tons	Pb	Zn	Ag	Cu
3750	7110	1917	—	—				
3730	—	—	6115	20916	4.00	4.82	58.4	0.11
3710	—	—	30128	102133	3.08	5.80	40.7	0.14
3690	1154	465	21988	72131	3.38	5.81	43.6	.10
3670	—	—	16351	58681	4.06	5.45	43.8	.17
3650	12571	4531	12378	44182	3.87	4.58	46.0	0.19
3630	6001	2113	40341	138622	3.31	4.85	37.0	0.13
3610	680	274	79677	256667	2.84	5.13	25.2	0.13
3590	32673	12368	34943	115346	2.84	5.73	21.7	0.11
3570	22816	7407	20032	61724	2.41	5.14	23.3	0.11
3550	6482	1852	98280	319935	3.36	5.33	41.4	0.18
3530	—	—	184233	622879	3.67	5.55	39.8	0.17
3510	—	—	201212	708199	4.01	5.75	46.4	0.17
3490	—	—	125799	454692	4.38	5.74	52.5	0.20
3470	—	—	104906	355662	4.17	5.71	53.2	0.18
3450	—	—	124984	412652	3.39	4.95	42.7	0.19
3430	5259	1852	84283	298984	2.98	4.45	31.8	0.24
	94744	32779	1,185,649	4,043,406	3.63	5.37	41.9	0.17

Tons metal = 363,908

T3 at 6.00% Phase A

3.63
5.37
9.00

A phase

Bench	Comments		
3830	nothing		
3810	v. minor 117 → 118		
3790	nothing at all!		
3770	minor 117 → 118 + 3 blocks on 119 (@10%)		
3750	minor low grade 117 → 118		
3730	NE ENDS of 117 → 120 v.v. patchy basically the upper band		
3710	NE ENDS of 117 → ~~[illegible]~~ 120 ~~[illegible]~~ (v. patchy)		
3690	NE ENDS of 117 → 121 (could live w/o 121)		possible ore SE of dike on 117 2 blk HG
3670	NE ENDS of 117 → 121 (could live w/o 121)		" 4 blk HG
3650	NE ENDS of 117 → 121		
3630	NE ends of all sections from 117 → 122		
3610	NE ends " "	part of wedge NE of pit	minor low grade 116 ~~[illegible]~~ 117 SE of dike at SW end
3590	" " " "		
3570	" " "	Starting to skim top of main zone	2 blocks of H grade on 117 middle of main
3550	most sections 117 → 122 S ends of 118 → 120 still above ore)		leaving some good grade NE of ramp hairpin
3530	most sections 117-122 (S ends of 118 → 120 still above ore)		hairpin on good grade!
3510	all sections have lots of ore (but S ends of 119 + 120)		lots of grade under and N of hairpin
3490	all sections solid ore (but for a bit of 120)		grade below hairpin area now drops to zilch
3470	all sections 118 → 121 in solid ore	Some +6% under ramp	NE wedge dying + low grade
3450	"	"	"
3430	"		NE wedge basically shit but for basal band
3410	"		"
3390	118 bu is all ore but below A phase.		4 blocks of >4% in NE wedge
3370	118 → 124 in ore but below A phase		NE wedge basically gone.

Left margin brackets: "Northeast Wedge" (benches 3730–3590); "Hairpin Area problem" (benches 3550–3450) extended JB tonnages (3890 – 3750 incl)

① F4 model + blastholes on 3890

		Pb	Zn	Ag
3890 – 3750	858,887 SDT	3.8	6.1	52.4

② F3 model *1,03,9506 SDT

extended JB ore composition from F4 model + blastholes (%)

	A	A+BCD	H+EH	CE	EF+G
3890	18.5	44.7	—	—	55.3
3870	4.4	54	26	—	20
3850	15.4	36	55	9	~~9~~
3830	6.2	39	55	—	6
3810	6.9	52	33	—	15
3790	12.1	37	19	—	44
3770	9.3	34	31	—	35
3750	0.7	21	45	—	34

F-3 ORE SUMMARY 1 Phase NE Wedge 6% c/o

bench	(7) 2A	(8) 2BCD	(9) 2EC	(10) 2EF	(11) 2H	(12) 2G	Total
3750	—	—	—	—	—	[illegible]	—
3730	—	7064@8.1	—	—	—	13852@10.7	20916@9.8
3710	9919@8.0	16278@7.3	16383@8.5	51623@7.8	—	25165@11.4	129368@8.6
3690	20547@9.5	[illegible]	27762@7.9	27038@7.9	—	20779@9.1	96126@8.5
3670	—	—	—	39403@10.9	—	20779@7.3	60182@9.7
3650	—	5426@11.8	—	13519@7.2	—	[illegible]	18945@8.5
3630	11586@6.7	8262@8.3	7428@7.1	13519@9.8	—	27705@8.6	68500@8.3
3610	1423@8.3	59825@7.6	111896@8.7	60835@9.0	—	27705@9.0	261684@8.6
3590	20177@7.9	59685@6.6	75789@9.5	27038@8.1	—	—	182689@8.2
	73652	156540	239258	232975	—	135985	838410
	8.9%	18.7%	28.5%	27.8%	0%	16.2%	

T-3

bench	2A	2BCD	2EC	2EF	2H	2G	Total
3750	—	—	—	—	—	—	—
3730	—	7064@6.5	—	—	—	13852@10.0	20916@8.8
3710	19919@10.4	5426@6.3	—	51623@8.0	—	25165@10.0	102133@8.9
3690	19296@8.8	—	11779@8.3	20278@9.2	—	20779@10.0	72131@9.2
3670	—	5426@6.9	—	39403@10.4	—	13852@8.1	58681@9.5
3650		5426@8.9	—	24904@8.7		13852@7.7	44182@8.4
3630	—	2836@7.3	60432@6.4	33797@8.8		41557@10.2	138622@8.1
3610		81528@7.1	100118@7.4	47316@9.4	—	27705@10.2	256667@8.0
3590	—	5426@6.7	75789@8.6	20278@7.6	—	13852@10.2	115346@8.5
	39215	113132	248118	237599	—	170614	808678
	4.8%	14.0%	30.7%	29.4%	0%	21.1%	