

XQOV

020494

# PACIFIC WATERPROOF

MIKE BREMNER

CAB

July, Aug 1969

Product of

**DOMINION BLUEPRINT LTD.**

**1529-WEST PENDER, VANCOUVER 5, B.C. - 681-7501**

Tape distance 74.1'

Top 1.60

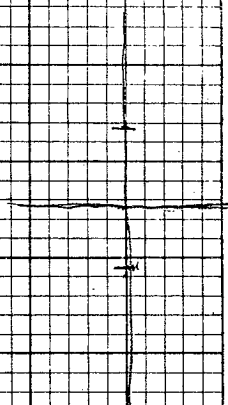
13.8 V

Mid 1.97

+8°

Bot 2.35

1.84 H



Distance

2.35

1.60

7.5

= 75 ft.

1.84

73.16



Sta. No.	Stadia interval L	Stadia height R	Inclination	H	Horiz. <sup>CONV. STADIA</sup> 100 x L x H
0	1.90	1.355	0°	0	19.00
A	1.66	6.63	+4°	.5	.83
B	1.40	4.90	-4°	.5	.70
<u>Sunday 20<sup>th</sup> July 1969 - SURVEY BASE LINE</u>					

V	Elevation F (L x V) ± R	Remarks
9.0	1.355	1.475 1.285 / 1.90 1.355 1.7
<del>6.96</del> 6.96	11.55 - 6.63 = 4.92	7.41 5.81 / 1.66 5.60 4.20 / 1.40
33.30 6.96	9.74 + (-4.90) = -4.90	-17.36 = +6.28 -1.36 = -13.28

Zero  $\frac{1.57}{1.74} / \frac{2.43}{4.61} + 3^\circ$   
 A  $\frac{1.74}{2.43} / \frac{4.61}{7.95} + 30^\circ$   
 B 7.95

Last 13.44' above zero

(A)

+ 13.44

- 7.15

+ 6.29

Sta. No.	Cross-hairs			Inclination	H	V	Stadia Interval L (V-B)	Horiz Correct. C ( <del>100</del> H x L)	Horiz Dist. D (L x 100) - C	Elevation w/ Inst. Sta.		True ELEV E Inst ± E
	T	M	B							± M	± E	
zero	1.21	2.03	2.85	-4°	.49	6.96	1.64	.80	163.20	11.47	-13.44	0
A	6.79	7.15	7.50	/	/	/	.71	/	71.00	/	-7.15	+6.29
B	5.25	6.71	8.14	-4°	.49	6.96	2.89	1.42	287.58	20.11	-26.82	-13.38
C	3.82	5.63	7.43	+4°	.49	6.96	3.61	1.77	359.23	25.13	+19.50	+32.94

MONDAY 21<sup>st</sup> July 1969

Base-line extension  
+ triangulation of X-line stars.

(A)

11.54

.95

10.59 ✓

9.67

$$\begin{array}{r} 10.59 \\ 10.07 \\ 6.31 \\ \hline 26.97 \end{array}$$

$$\begin{array}{r} 32.94 \\ 6.29 \\ \hline 26.65 \end{array}$$

$$\begin{array}{r} 33.16 \\ 6.40 \\ \hline 26.76 \end{array}$$

$$\begin{array}{r} 23.10 \\ 23.78 \\ \hline 46.88 \\ 32.94 \\ 13.88 \\ \hline 46.82 \end{array}$$

$$\begin{array}{r} 33.16 \\ 6.40 \\ \hline 9.56 \\ 33.16 \\ 13.00 \\ \hline 46.26 \end{array}$$

$$\begin{array}{r} 3.98 \\ .97 \\ \hline 3.01 \\ 1.50 \\ .97 \\ \hline 2.47 \end{array}$$

10.62

.55

$$\begin{array}{r} 26.20 \\ 2.47 \\ \hline 23.73 \\ 21.15 \\ .95 \\ \hline 22.10 \\ 3.46 \\ .99 \\ \hline 2.46 \end{array}$$

$$\begin{array}{r} 10.07 \\ 6.24 \\ 6.31 \\ \hline 42.88 \\ 6.29 \\ 22.94 \\ \hline 39.23 \end{array}$$

$$\begin{array}{r} 23.10 \\ 9.75 \\ \hline 13.35 \end{array}$$

$$\begin{array}{r} 33.16 \\ 6.40 \\ \hline 39.56 \end{array}$$

$$\begin{array}{r} 6.79 \\ 48 \\ \hline 6.31 \end{array}$$

3/2

$$\begin{array}{r} .87 \\ \hline 311 \quad 13 \end{array}$$

$$\begin{array}{r} +6.40 \\ -13.10 \\ +33.16 \end{array}$$

+6.29

.48

(C)

$$\begin{array}{r} 33.16 \\ 6.40 \\ \hline 26.56 \end{array}$$

$$\begin{array}{r} 32.94 \\ 6.29 \\ \hline 26.65 \end{array}$$

$$\begin{array}{r} 11.54 \\ .95 \\ \hline 10.59 \end{array}$$

$$\begin{array}{r} 10.62 \\ .95 \\ \hline 9.67 \end{array}$$

$$\begin{array}{r} 10.62 \\ .55 \\ \hline 10.07 \end{array}$$

$$\begin{array}{r} 182.40 \\ 1.40 \\ \hline 0.60 \end{array}$$

$$\begin{array}{r} 320 \\ 2.46 \\ \hline 317.54 \end{array}$$

$$\begin{array}{r} 6.02 \\ 2.82 \\ \hline 3.20 \\ 1.60 \\ 2.82 \\ \hline 4.42 \end{array}$$

$$\begin{array}{r} 7.88 \\ 7.06 \\ \hline 0.82 \\ 21 \\ 7.46 \\ \hline 7.6 \end{array}$$

$$\begin{array}{r} 4.23 \\ 2.41 \\ \hline 1.82 \\ 1.91 \\ 2.41 \\ \hline 3.32 \end{array}$$

$$\begin{array}{r} 3.78 \\ .66 \\ \hline 2.12 \\ 2(2.12) \\ 1.06 \\ .66 \\ \hline 3.22 \end{array}$$

$$\begin{array}{r} 13.10 \\ 6.40 \\ \hline 6.70 \\ 13.38 \\ 6.29 \\ \hline 6.09 \end{array}$$

$$\begin{array}{r} 19.15 \\ 14.01 \\ \hline 5.14 \\ 19.50 \\ 13.44 \\ \hline 6.06 \end{array}$$

~~13.44~~ A-B  
B-C  
C-A

19.50 19.67  
46.26 46.32  
26.56 26.65

Zero	2.41	3.32	4.23	-5°	.77	8.7	1.82	1.40	180.60	15.83	-19.15	0
A	7.46	7.67	7.88	7°	1.48	12.1	.42	.61	41.39	5.08	-12.75	+6.40
B	2.82	4.41	6.02	-5°	.77	8.7	3.20	2.46	317.54	27.84	-32.25	-13.10
C	.66	2.22	3.78	+3°	.28	5.2	3.12	.87	311.13	16.23	+14.01	+33.16

Tuesday, 22<sup>nd</sup> July, 1969. - Grid + X-line stars

A-C	.97	2.47	3.98	+5°	.77	8.7			26.20	+23.73		
												33.48
A-Zero	8.94	9.75	10.46	/	/	/				-9.75		46.83
												13.35
A+B	.44	1.95	3.46	-4°	.49	7.0			21.15	-23.10		

$$\begin{array}{r} 7.13 \\ 10.80 \\ \hline 17.93 \\ 2 \overline{) 35.86} \\ \underline{35.86} \\ 0.00 \end{array}$$

$$\begin{array}{r} 4.55 \\ 3.83 \\ \hline 8.38 \\ 2 \overline{) 16.76} \\ \underline{16.76} \\ 0.00 \end{array}$$

$$\begin{array}{r} 2.770 \\ 1.905 \\ \hline 4.675 \\ 2 \overline{) 9.35} \\ \underline{9.35} \\ 0.00 \end{array}$$

$$\begin{array}{r} 4.55 \\ 3.83 \\ \hline 8.38 \\ 2 \overline{) 16.76} \\ \underline{16.76} \\ 0.00 \end{array}$$

$$\begin{array}{r} 2.770 \\ 1.905 \\ \hline 4.675 \\ 2 \overline{) 9.35} \\ \underline{9.35} \\ 0.00 \end{array}$$

$$\begin{array}{r} 3.49 \\ 1.56 \\ \hline 5.05 \\ 2 \overline{) 10.10} \\ \underline{10.10} \\ 0.00 \end{array}$$

(A) = +6.33

(B) = -13.28

(C) = +33.24

ZERO	3.83	4.16	4.55	/	/	/	72	/	72.0	/	-4.16	0
A	1.905	2.340	2.770	+3°	.3	5.23	.865	.24	86.26	+4.52	+2.18	+6.34
B	1.56	2.62	3.69	-4°	.5	6.96	2.13	1.04	211.96	-14.83	-17.45	-13.29
C	7.13	8.95	10.80	+6°	1.1	10.40	3.67	4.04	362.96	+38.17	+29.22	+33.38

Tuesday 22<sup>nd</sup> July 1969 — Grid + X-line Atlas.

SURVEY BASE-LINE AVERAGES. →

(A)	(B)	(C)
+6.28	-13.28	
+6.29	-13.38	+32.94
+6.40	-13.35	+33.48
+6.34	-13.10	+33.16
+6.34	-13.29	+33.38
4125.31	5166.40	4132.96
+6.33	-13.28	+33.24

$$\begin{array}{r} 2.58 \\ 8.19 \\ \hline 1.39 \\ \hline .20 \end{array}$$

$$\begin{array}{r} 16.82 \\ 8.87 \\ \hline 25.69 \end{array}$$

$$\begin{array}{r} 6.29 \\ 6.40 \\ 6.34 \\ \hline 19.03 \\ \hline 6.37 \end{array}$$

$$\begin{array}{r} 7.37 \\ 5.36 \\ \hline 2.01 \\ \hline 1.01 \\ 5.36 \\ \hline 6.37 \end{array}$$

$$\begin{array}{r} 201 \\ 13.47 \\ \hline 187.53 \end{array}$$

$$\begin{array}{r} 50.03 \\ 6.37 \\ \hline 43.66 \\ \hline 2.03 \\ \hline 45.69 \end{array}$$

$$\begin{array}{r} 8.42 \\ 5.10 \\ \hline 3.32 \\ \hline 1.66 \\ 5.10 \\ \hline 6.76 \end{array}$$

$$\begin{array}{r} 6.75 \\ 5.97 \\ \hline .78 \end{array}$$

$$\begin{array}{r} 75.69 \\ 78 \\ \hline 74.91 \end{array}$$

$$\begin{array}{r} 7.20 \\ 4.69 \\ \hline 2.51 \\ \hline 2.26 \\ \hline 4.69 \\ \hline 5.95 \end{array}$$

$$\begin{array}{r} 251 \\ 1.23 \\ \hline 249.77 \end{array}$$

$$\begin{array}{r} 7.59 \\ 5.95 \\ \hline 11.64 \\ 32.03 \\ \hline 43.67 \end{array}$$

$$\begin{array}{r} 32.03 \\ .78 \\ \hline 31.25 \end{array}$$

$$\begin{array}{r} 6.63 \\ 4.74 \\ \hline 11.89 \\ \hline .95 \\ 4.74 \\ \hline 5.69 \end{array}$$

$$\begin{array}{r} 189 \\ 18.05 \\ \hline 170.95 \end{array}$$

$$\begin{array}{r} 55.60 \\ 5.69 \\ \hline 61.29 \\ 75.69 \\ \hline 136.98 \end{array}$$

$$\begin{array}{r} 6.98 \\ 5.28 \\ \hline 1.70 \\ \hline .85 \\ 5.28 \\ \hline 6.13 \end{array}$$

$$\begin{array}{r} 284 \\ 33.22 \\ \hline 250.78 \end{array}$$

$$\begin{array}{r} 170 \\ 3.28 \\ \hline 166.72 \end{array}$$

$$\begin{array}{r} 35.21 \\ 6.81 \\ \hline 28.40 \\ 136.98 \\ \hline 165.38 \end{array}$$

$$\begin{array}{r} 23.44 \\ 6.13 \\ \hline 29.57 \end{array}$$

$$\begin{array}{r} 9.56 \\ 5.78 \\ \hline 3.81 \\ \hline 1.91 \\ 5.15 \\ \hline 7.66 \end{array}$$

$$\begin{array}{r} 136.98 \\ 29.57 \\ \hline 107.41 \end{array}$$

$$\begin{array}{r} 9.56 \\ 6.72 \\ \hline 2.84 \\ \hline 1.42 \\ 6.72 \\ \hline 8.14 \end{array}$$

$$\begin{array}{r} 64.92 \\ 8.13 \\ \hline 56.79 \\ 136.98 \\ \hline 193.77 \end{array}$$

$$\begin{array}{r} 91.50 \\ 8.12 \\ \hline 83.38 \\ 136.98 \\ \hline 220.36 \end{array}$$

$$\begin{array}{r} 7.84 \\ 5.78 \\ \hline 2.06 \\ \hline 1.03 \\ 5.78 \\ \hline 6.81 \end{array}$$

$$\begin{array}{r} 206 \\ 6.2 \\ \hline 199.8 \end{array}$$

$$\begin{array}{r} 6.86 \\ 4.51 \\ \hline 2.35 \\ \hline 1.18 \\ 4.51 \\ \hline 5.69 \end{array}$$

$$\begin{array}{r} 8.05 \\ 5.81 \\ \hline 2.24 \\ \hline 1.12 \\ 5.81 \\ \hline 6.93 \end{array}$$

$$\begin{array}{r} 9.53 \\ 6.77 \\ \hline 2.76 \\ \hline 1.38 \\ 6.77 \\ \hline 8.15 \end{array}$$

155.

$$\begin{array}{r} 136.98 \\ 6.92 \\ \hline 130.06 \end{array}$$

$$\begin{array}{r} 276 \\ 16.01 \\ \hline 259.99 \end{array}$$

$$\begin{array}{r} 235 \\ 2.58 \\ \hline 32.42 \end{array}$$

$$\begin{array}{r} 23.98 \\ 5.61 \\ \hline 18.31 \\ 136.98 \\ \hline 155.29 \end{array}$$

I												
A	8.19	8.87	9.58	-7°	1.49	12.1	1.39	2.67	136.33	-16.82	-25.69	[6.34] +32.03
X-Line 12S terminus	5.36	6.37	7.37	+15°	6.7	25.0	2.01	13.47	187.53	+50.03	+43.66	+75.69
Slope	5.10	6.75	8.42	+1°	/	1.8	3.32	/	332.00	+5.97	-7.8	+31.25
Slope	4.69	5.95	7.20	+4°	.49	7.0	2.51	1.23	249.77	+17.59	+11.64	+43.67

II												
X-Line 12S terminus	4.74	5.69	6.63	-18°	9.55	29.4	1.89	18.05	170.95	55.60	-61.29	[75.69] +136.98
700W	5.28	6.13	6.98	-8°	1.93	13.8	1.70	3.28	166.72	-23.44	-29.57	+107.71
600W	5.78	6.81	7.84	+10°	3.01	17.1	2.06	6.20	199.80	+35.21	+28.40	+165.38
500W	(6.72) (5.75) (6.80)	(8.12) (8.16)	(9.56)	+20°	11.7	32.2	2.84	33.22	250.78	+91.50	+83.38	+220.36
X-Line 16S 600W	6.77	8.13	9.53	+14°	5.8	23.5	2.76	16.01	259.99	+61.92	+56.79	+193.77
700W	4.51	5.67	6.86	+6°	1.10	10.4	2.35	2.58	232.42	+23.98	+18.31	+155.29
800W	5.81	6.92	8.05	/	/	/	2.24	/	224.00	/	-6.92	+130.06

Wednesday 23<sup>rd</sup> July 1969

Gross Lines 1200S? W  
1600S)

$$\begin{array}{r} 7.86 \\ 5.36 \\ \hline 2.50 \\ 1.25 \\ 5.36 \\ \hline 6.61 \end{array}$$

$$\begin{array}{r} 250 \\ 24 \\ \hline 226 \end{array}$$

$$\begin{array}{r} 73.25 \\ 6.63 \\ \hline 79.87 \\ 220.36 \\ \hline 300.23 \end{array}$$

$$\begin{array}{r} 6.42 \\ 4.30 \\ \hline 52.12 \\ 1.06 \\ 4.36 \\ \hline 5.36 \end{array}$$

$$\begin{array}{r} 212 \\ 2.33 \\ \hline 209.67 \end{array}$$

$$\begin{array}{r} 22.06 \\ 5.36 \\ \hline 27.42 \end{array}$$

$$\begin{array}{r} 300 \\ 27 \\ \hline 272.8 \end{array}$$

$$\begin{array}{r} 6.47 \\ 4.25 \\ \hline 2.22 \\ 1.11 \\ 4.25 \\ \hline 5.36 \end{array}$$

$$\begin{array}{r} 222 \\ 6.68 \\ \hline 215.32 \end{array}$$

$$\begin{array}{r} 6.36 \\ 3.40 \\ \hline \end{array}$$

$$\begin{array}{r} 220.36 \\ 300.23 \\ \hline \end{array}$$

$$\begin{array}{r} 1.06 \\ 4.36 \\ \hline 5.36 \end{array}$$

$$\begin{array}{r} 8.43 \\ 6.83 \\ \hline \end{array}$$

$$\begin{array}{r} 160 \\ 49.9 \\ \hline \end{array}$$

$$\begin{array}{r} 74.98 \\ 7.63 \\ \hline 67.35 \\ 300.23 \\ \hline 367.58 \end{array}$$

$$\begin{array}{r} 1.11 \\ 4.25 \\ \hline 5.36 \end{array}$$

$$\begin{array}{r} 38.00 \\ 9.36 \\ \hline 47.36 \end{array}$$

$$\begin{array}{r} 2 \overline{) 2.96} \\ 1.48 \\ \hline 3.40 \\ 4.88 \end{array}$$

$$\begin{array}{r} 296 \\ 45 \\ \hline 251 \end{array}$$

$$\begin{array}{r} 106.49 \\ 4.89 \\ \hline 101.60 \\ 300.23 \\ \hline 401.83 \end{array}$$

$$\begin{array}{r} 1.60 \\ .80 \\ 6.83 \\ \hline 7.63 \end{array}$$

$$110.10$$

$$\begin{array}{r} 10.25 \\ 1.14 \\ \hline \end{array}$$

$$\begin{array}{r} 67.35 \\ 300.23 \\ \hline 367.58 \end{array}$$

$$\begin{array}{r} 200 \\ 8.54 \\ \hline 191.46 \end{array}$$

$$\begin{array}{r} 32.64 \\ 300.23 \\ \hline 332.87 \end{array}$$

$$\begin{array}{r} 7.60 \\ 5.11 \\ \hline 2.49 \\ 1.25 \\ 5.11 \\ \hline 6.36 \end{array}$$

$$\begin{array}{r} 249 \\ 29.18 \\ \hline 219.82 \end{array}$$

$$\begin{array}{r} 80.25 \\ 6.34 \\ \hline 73.91 \\ 300.23 \\ \hline 374.14 \end{array}$$

$$\begin{array}{r} 2.13 \\ .16 \\ \hline 1.97 \\ .99 \\ \hline 1.15 \end{array}$$

$$\begin{array}{r} 9.11 \\ 300.23 \\ \hline 309.34 \end{array}$$

$$\begin{array}{r} 197.53 \\ 196.43 \\ \hline \end{array}$$

$$\begin{array}{r} 300.23 \\ 51.55 \\ \hline 248.68 \end{array}$$

$$\begin{array}{r} 40.80 \\ 10.75 \\ \hline 51.55 \end{array}$$

$$\begin{array}{r} 11.75 \\ 9.75 \\ \hline 2.00 \\ 1.00 \end{array}$$

12+00S/500W	5.36	6.62	7.86	-18°	9.6	29.3	2.50	24.00	226.0	73.25	[220.26] -79.87	(+300.23)
400W	4.30	5.36	6.42	-6°	1.1	10.4	2.12	2.33	209.67	-22.06	-27.42	+272.81
300W	4.25	5.36	6.47	+10°	3.01	17.1	2.22	6.68	215.32	+38.00	+32.64	+332.87
200W	3.40	4.89	6.36	+23°	7.52	35.95	2.96	45.00	251.00	+106.49	+101.60	+401.83
Diorite base	6.83	7.63	8.43	+34°	31.2	46.8	1.60	49.90	110.10	+74.98	+67.35	+367.58
1600S/300W	5.11	6.34	7.60	+20°	11.7	32.2	2.49	29.18	219.82	+80.25	+73.91	+374.14
400W	0.16	1.4	2.13	+3°	.27	5.2	1.97	.53	196.43	+10.25	+9.91	+309.34
500W	9.75	10.75	11.75	-12°	4.27	20.4	2.00	8.54	191.46	-40.80	-51.55	+248.68

Wednesday 23<sup>rd</sup> July 1969

X - lines 1200S }  
1600S } W

486  
- 156  
---  
228  
114  
---  
258  
372

7.95  
3.71  
---  
4.27

136.09  
4.27  
---  
125.79

757  
539  
---  
218  
109  
---  
539  
648

218  
23.32  
---  
194.68  
11.45  
9.74  
---  
1.71

37  
19  
---  
25

67.10  
6.48  
---  
73.58

40.10  
10.60  
---  
25.79  
50.70  
---  
75.09

125.79  
73.58  
---  
52.21

863  
547  
---  
316  
158  
---  
547  
705

264  
7.02  
---  
226.78

74.25  
7.05  
---  
81.30

125.79  
81.30  
---  
44.49

87  
76  
---  
187.12

13.10  
5.06  
---  
8.04

171  
10.10  
---  
160.90

804  
408

8.37  
2.83  
---  
5.54  
2.77  
---  
2.83  
5.60

40.00  
8.11  
---  
31.89  
125.79  
---  
157.68

316  
18.65  
---  
297.35

600  
413  
---  
187  
94  
---  
413  
507

~~100~~ x 1.87 x 3.5  
17.61  
9.53  
---  
27.14

169.80  
27.14  
---  
152.66

27.14  
157.68  
---  
184.82

157.68  
169.80

554  
55.72  
---  
255  
6.90  
---  
248.10  
173.76  
---  
421.86

58.80  
73.76  
---  
332.56

164.40  
5.60  
---  
158.80  
169.80  
---  
328.60

795  
169.40  
---  
625.60

11.40  
2.60  
---  
8.80  
4.20  
---  
2.60  
6.80

-6.55  
9.53

685  
113.80  
---  
571.20

9.38  
1.43  
---  
9.95  
3.98  
---  
1.43  
5.41

325.40  
5.41  
---  
320.02

320.00  
173.76  
---  
493.76

-6.08  
157.68  
---  
173.76

Sunday 27<sup>th</sup> July 1969  
Ore body #1

I 16005/Room	2.58	3.71	4.86	+2°	.12	3.5	2.28	/	228.0	+7.78	[30.06] +4.27	(+125.70)
Rubble base	5.39	6.48	7.57	-19°	10.7	30.8	2.18	23.32	194.68	-67.10	-73.53	+52.21
Head of Claim Post	5.47	7.05	8.63	-14°	5.9	23.5	3.16	18.05	297.35	-74.25	-81.30	+44.49
Rubble base	9.74	10.60	11.45	-14°	5.9	23.5	1.71	10.10	160.90	-40.10	-50.70	+75.09
Rubble edge	6.93	8.11	9.27	+10°	3.0	17.1	2.34	7.02	226.98	+40.03	+31.89	+157.68

II Rubble edge	4.15	5.06	6.08	+4°	.49	7.0	1.87	92	186.08	+13.10	[+1.08] +8.04	+169.80
(1)				+7° 19'		12.7					(+173.76)	
(2)				+6° 28'		11.2	15.33		+173.8			+347.6
(3)				+8° 02'		13.9	14.02		+197.8			+371.6
(4)				+9° 50'		16.8	12.22		+211.8			+385.6
(5)				+11° 23'		19.3	10.98		+221.0			+394.8
(6)				+11° 50'		20.1	10.16		+212.9			+386.7

Dioxide base	2.83	5.60	8.37	+18° 10'	9.7	29.7	5.54	53.72	500.28	+164.40	+158.80	+332.56
Top dioxide ridge	2.60	6.92	11.80	+24°	16.6	37.2	6.85	113.80	571.20	+255.00	+248.10	+421.86
Top dioxide	1.43	5.41	9.38	+27° 30'	2.8	40.9	7.45	169.40	625.60	+325.40	+320.00	+493.76

9.29 2.46 6.93 3.47 2.46 5.93	37.7 5.9 8.39 3.69 4.70 2.35 3.69 6.04 6.10 3.38	6.93 1.5 578	257.90 5.94 251.96 175.76 424.82	10.09 3.72 6.37 8.19 8.7 6.91	10.03 3.75 6.25 3.13 3.75 6.88	10.03 3.75 6.28 3.14 3.75 6.89	230 6.84 223.16 173.76 396.92	8.05 2.47 5.38 2.49 2.62 5.36	5.38 63.5 474.5	173.20 5.34 167.86 173.76 341.62
3.17 13.80 305.70	2.35 3.69 6.04 6.10 3.38	470 50.3 419.7	144.90 6.04 138.86 133.76 312.62	4.54 2.65 1.89 1.95 2.65 3.60	6.61 3.61	9.45 6.26 3.19 1.50 6.26 7.26	7.84 6.26 1.58 1.61 20.19 1.5	9.45 7.84 1.61	828 55.8 272.2	
3.90 62 3.28 1.64 62 3.26	64.75 7.84 56.91 73.76 230.67 9.17 5.51 3.66 4.83 5.51 7.34	5.72 2.86 38 3.41 1.70 3.47 1.11	341.25 25.94 315.06 149.70 7.30 142.40 263.52 405.92	90.40 5.12 85.28 173.76 259.04 369 56.1 312.9 299.40 6.72 292.68 263.52 387.02 556.20	11.25 7.56 3.69 1.85 7.56 9.41	648 122.50 525.50 78.57 169.80 248.37	8.62 27.0 New 2.59 x 27.0 = 69.95 + 8.62 11.25 7.56 3.69 1.85 7.56 9.41	169.80 3.5 x 27.0 85.10 8.62 93.72 169.80 263.52 8.91 2.57 6.34 3.22 239.18 263.52 502.70 292.68 263.52 556.20	129.20 2.28 126.92 263.52 390.44 572 134.20 437.80 634 182 452 286.20 5.72 280.48 263.52 544.00	

Sunday 27th July 1969

ORE BODY #1

254  
8.67  
245.33  
263.52  
288.85  
108

Top of rivet contact	2.46	5.94	9.39	+24°	16.6	37.2	6.93	115.00	578.00	[+173.75]	+257.90	+251.06	+424.82
Top of rivet clearance	3.75	6.88	10.03	+23°30'	15.9	36.6	6.28	108.00	528.00	+230.00	+223.16	+396.92	
Top of rivet contact	2.67	5.34	8.05	+20°	11.8	32.2	5.38	63.50	474.50	+173.20	+167.86	+341.62	
Below trenches	3.69	6.04	8.39	+19°	10.7	30.8	4.70	50.50	419.70	+144.90	+138.86	+312.62	
Base of screed	2.65	3.61	4.54	+20°	/	3.5	1.89	/	189.00	+6.61	+3.00	+176.76	
Base diaphragm	6.26	7.84	9.45	+12°	4.32	20.3	3.19	13.80	305.20	+64.75	+56.91	+238.67	
Screed	3.41	5.12	6.82	+16°	7.6	26.5	3.41	25.94	315.06	+90.40	+85.28	+257.04	
													[+263.52]
III-screed LHS outcrop	0.62	2.28	3.90	+26°	19.2	39.4	3.28	55.80	272.2	+129.20	+126.92	+390.44	
Top outcrop	5.51	7.30	9.17	+27°	20.7	40.9	3.66	75.75	290.25	+149.70	+142.40	+435.92	
RHS outcrop	7.56	9.40	11.25	+23°	15.2	36.0	3.69	56.10	312.90	+132.90	+123.50	+387.02	
Bot outcrop	6.37	7.48	8.64	+20°	11.8	32.1	2.27	26.90	200.10	+72.80	+65.32	+328.84	
Screed crest	.38	3.22	6.00	+29°	23.5	42.4	5.72	134.20	437.80	+242.40	+239.18	+502.70	
Face base	/	6.72	10.15	+30°20'	25.5	43.6	6.86	175.00	511.00	+299.40	+292.48	+556.20	
"	2.57	5.72	8.91	+32°20'	28.7	45.2	6.34	182.00	452.00	+286.20	+280.48	+544.00	
Screed crest Claim Post	5.40	8.67	11.88	+25°48'	18.9	39.2	6.48	122.50	525.50	+254.00	+245.33	+568.85	

$$\begin{array}{r} 9.65 \\ 2.52 \\ \hline 7.13 \\ 3.57 \\ \hline 2.52 \\ 6.09 \end{array}$$

$$\begin{array}{r} 763 \\ 107.8 \\ \hline 605.2 \\ 254.60 \\ 6.13 \\ \hline 248.47 \\ 263.52 \\ \hline 511.99 \end{array}$$

$$\begin{array}{r} 8.81 \\ 1.98 \\ \hline 6.83 \\ 3.42 \\ \hline 1.98 \\ 5.45 \end{array}$$

$$\begin{array}{r} 683 \\ 131.10 \\ \hline 551.90 \\ 269.40 \\ 5.41 \\ \hline 263.99 \\ 263.52 \\ \hline 527.51 \end{array}$$

$$\begin{array}{r} 8.27 \\ 5.63 \\ \hline 2.64 \\ 32 \\ \hline 5.63 \\ 6.95 \\ \hline 1.32 \end{array}$$

$$\begin{array}{r} 8.27 \\ 6.63 \\ \hline 1.64 \\ 6.82 \\ \hline 6.63 \\ 7.45 \end{array}$$

$$\begin{array}{r} 164 \\ 23 \\ \hline 141 \end{array}$$

$$\begin{array}{r} 57 \\ 7.42 \\ \hline 49.58 \\ 263.52 \\ \hline 313.10 \end{array}$$

$$\begin{array}{r} 10.23 \\ 8.76 \\ \hline 1.53 \\ .77 \\ \hline 8.70 \\ 9.47 \end{array}$$

$$\begin{array}{r} 153 \\ 18 \\ \hline 135 \end{array}$$

$$\begin{array}{r} 49.30 \\ 9.47 \\ \hline 39.83 \\ 263.52 \\ \hline 303.65 \end{array}$$

$$\begin{array}{r} 7.42 \\ 5.63 \\ \hline 1.79 \end{array}$$

$$\begin{array}{r} 8.27 \\ 7.42 \\ \hline 185 \end{array}$$

$$\begin{array}{r} 9.27 \\ 5.63 \\ \hline 3.64 \\ 1.82 \\ \hline 5.63 \\ 7.45 \end{array}$$

$$\begin{array}{r} 364 \\ 51 \\ \hline 313 \end{array}$$

$$\begin{array}{r} 126.40 \\ 7.42 \\ \hline 118.98 \\ 263.52 \\ \hline 382.50 \end{array}$$

Scree valley	2.52	6.12	9.65	+22° 50'	15.1	33.15	7.13	107.80	605.20	+259.60	+298.47	+511.99		[263.52]
Ridge crest	1.98	5.41	8.81	+26°	19.2	39.40	6.89	131.10	551.90	+269.10	+263.99	+527.51		
Trench	5.63	7.42	9.27	+22°	14.0	34.75	3.64	51.00	313.00	+126.40	+118.98	+382.50		
#1 Ore body crest	8.70	9.47	10.29	+20°	11.75	32.2	1.53	8.00	135.00	+49.30	+39.83	+303.35		

SUNDAY 27<sup>th</sup> JULY 1969

OREBODY #1





1.43  
15  
1.78  
15  
1.93

1.04  
15  
89  
1.78  
15  
1.03

1.73  
1.04  
89  
8.14  
4.65  
3.49  
1.75  
4.65  
6.40

252.56  
1.04  
251.52

379  
46.4  
425.4

495  
746  
179

118.70  
6.40  
112.30  
252.56  
364.86

519  
200.20  
312.80

170  
495  
251  
126  
495  
621

254.40  
8.90  
245.50  
252.56  
498.06

31.12  
5.65  
25.47  
252.56  
278.03

251  
18.32  
232.68  
814

401  
121.02  
279.98

310  
71.60  
238.4

6530  
5.20  
60.10  
252

130.80  
8.70  
122.08  
252.56  
374.64

603  
198  
405

283.60  
8.10  
275.50  
252.56  
528.06

255  
28.96  
226.04

416  
121.04  
324.96

184  
9.13  
174.87  
252.56  
427.43

81.00  
5.09  
75.91  
252.56  
328.47

11.33  
6.87  
4.46  
2.23  
6.87  
0.10  
10.27  
7.17  
3.10  
155  
71 1/2  
87 1/2

11.15  
5.12  
6.03  
3.02  
5.12  
8.14  
6.37  
3.82  
2.55  
1.28  
3.83  
5.10

11.15  
4.58  
6.57  
3.29  
4.58  
7.87  
244  
3.95  
240.05

	2000S/600W	.15	1.04	1.93	/	/	/	1.78	/	178.0	/	[+252.51]	-1.04	+251.52
500W (above Diap)	4.95	5.20	7.46	+15°40'	7.3	26.0	2.51	18.32	232.68	+65.30	+60.10	+312.66		
400W	4.65	6.40	8.14	+21°24'	13.3	34.0	3.49	46.46	302.60	+118.70	+112.30	+364.86		
300W	6.87	9.11	11.33	+31°26'	27.15	44.5	4.46	121.04	324.96	+198.50	+189.39	+441.95		
200W	5.12	8.10	11.15	+35°	33.0	47.0	6.03	198.07	405.00	+283.60	+275.50	+528.06		
2400S/300W	4.58	7.83	11.15	+41°20'	43.60	49.78	6.57	286.60	370.40	+322.00	+319.17	+571.73	*	
400W	6.29	8.90	11.48	+39°8'	39.9	49.0	5.19	207.20	312.80	+254.40	+245.50	+498.06		
500W	7.18	9.13	11.13	+33°22'	30.2	45.9	4.01	121.02	279.98	+184.00	+174.87	+427.43		
600W	7.7	8.72	10.27	+28°48'	23.1	42.2	3.10	71.60	238.40	+130.80	+122.08	+374.64		
700W	3.82	5.09	6.37	+19°42'	11.35	31.75	2.55	28.96	226.04	+61.00	+75.91	+328.47		
800W	4.43	5.65	6.87	+7°21'	1.62	12.75	2.44	3.95	240.05	+31.12	+25.49	+278.03		

Monday 28<sup>th</sup> July 1969

- X lines 2000 } W  
2400 }

$\begin{array}{r} 7.87 \\ 3.13 \\ \hline 08 \\ -5 \\ \hline 1.54 \\ 3.42 \\ \hline 5.46 \end{array}$	$\begin{array}{r} 30.3 \\ 2.02 \\ \hline 28.28 \\ 11.17 \\ 5.80 \\ \hline 9.37 \end{array}$	$\begin{array}{r} 42.50 \\ 5.48 \\ \hline 37.02 \\ 6.27 \\ 2.08 \\ \hline 4.19 \end{array}$	$\begin{array}{r} 11.53 \\ 8.46 \\ \hline 3.07 \\ 6.33 \\ 2.06 \\ 4.15 \end{array}$	$\begin{array}{r} 35.12 \\ 10 \\ \hline 25.92 \\ 30.06 \\ \hline 175.98 \\ 175.98 \\ \hline 0 \end{array}$	$\begin{array}{r} 3.90 \\ 1.59 \\ \hline 2.31 \\ 175.98 \\ \hline 178.29 \\ 272 \\ 41.40 \\ \hline 230.60 \\ 175.98 \\ \hline 289.84 \end{array}$	$\begin{array}{r} 5.37 \\ 46.12 \\ \hline 490.88 \\ 98 \\ 4.14 \\ \hline 93.86 \\ 175.98 \\ \hline 289.84 \end{array}$	$\begin{array}{r} 150.30 \\ 8.47 \\ \hline 141.83 \\ 175.98 \\ \hline 317.81 \end{array}$	$\begin{array}{r} 421 \\ 54.75 \\ \hline 366.25 \\ 262 \\ 27.79 \\ \hline 234.21 \end{array}$	$\begin{array}{r} 142.02 \\ 6.15 \\ \hline 137.85 \\ 175.98 \\ \hline 313.83 \end{array}$
$\begin{array}{r} 5.52 \\ 2.80 \\ \hline 2.72 \\ 2.36 \\ \hline 2.80 \\ 7.1 \end{array}$	$\begin{array}{r} 2.69 \\ 5.80 \\ \hline 8.49 \\ 6.56 \\ 5.80 \\ \hline 8.49 \end{array}$	$\begin{array}{r} 2.50 \\ 2.08 \\ \hline 4.58 \\ 6.57 \\ 4.86 \\ \hline 1.71 \end{array}$	$\begin{array}{r} 11.60 \\ 8.98 \\ \hline 2.64 \\ 1.32 \\ 8.96 \\ \hline 10.28 \end{array}$	$\begin{array}{r} 70.75 \\ 10.71 \\ \hline 81.46 \\ 171 \\ 12.50 \\ \hline 158.50 \end{array}$	$\begin{array}{r} 2.06 \\ 4.21 \\ 2.11 \\ 2.06 \\ 4.17 \\ 8.94 \\ 10.24 \\ 10.50 \\ 44.48 \\ 5.77 \\ \hline 252.56 \\ 50.80 \\ \hline 202.86 \end{array}$	$\begin{array}{r} 11.56 \\ 8.94 \\ \hline 2.62 \\ 1.31 \\ 8.94 \\ \hline 10.25 \end{array}$	$\begin{array}{r} 80.75 \\ 10.24 \\ \hline 70.51 \\ 175.98 \\ \hline 246.49 \end{array}$	$\begin{array}{r} 171.10 \\ 8.46 \\ \hline 252.56 \end{array}$	



Monday 28<sup>th</sup> July 1969 — X-lines 2000 } W  
 2400 }



# FRIDAY 1st August 1968

$\begin{array}{r} 5.31 \\ 2.21 \\ \hline 3.10 \\ 2.55 \\ 3.21 \\ \hline 5.76 \end{array}$	$\begin{array}{r} 101.60 \\ 5.75 \\ \hline 107.35 \\ 33.24 \\ \hline 140.59 \end{array}$	$\begin{array}{r} 510 \\ 20.94 \\ \hline 489.06 \\ 7.57 \\ 2.40 \\ \hline 5.17 \\ 2.59 \\ \hline 2.40 \\ 4.99 \end{array}$	$\begin{array}{r} 9.26 \\ 2.27 \\ \hline 6.99 \\ 7.00 \\ 2.27 \\ \hline 6.27 \end{array}$	$\begin{array}{r} 5.77 \\ 2.27 \\ \hline 3.50 \\ 3.50 \\ 2.27 \\ \hline 5.77 \end{array}$	$\begin{array}{r} 9.26 \\ 5.77 \\ \hline 3.49 \end{array}$	$\begin{array}{r} 58.70 \\ 5.77 \\ \hline 52.93 \\ 140.59 \\ \hline 193.52 \end{array}$	$\begin{array}{r} 517 \\ 47.5 \\ \hline 469.5 \end{array}$	$\begin{array}{r} 149.50 \\ 5 \\ \hline 144.50 \\ 140.59 \\ \hline 285.09 \end{array}$		
$\begin{array}{r} 8.66 \\ 5.37 \\ 8.29 \\ 1.65 \\ 5.37 \\ \hline 7.02 \end{array}$	$\begin{array}{r} 2.65 \\ 6.85 \\ 11.17 \\ 4.99 \\ 2.40 \\ 2.65 \\ \hline 8.57 \end{array}$	$\begin{array}{r} 2.59 \\ 2.40 \\ 4.99 \\ 11.17 \\ 2.65 \\ \hline 8.57 \end{array}$	$\begin{array}{r} 11.17 \\ 2. \\ 1.32 \\ 1018 \\ 6.58 \\ \hline 842.5 \end{array}$	$\begin{array}{r} 12.00 \\ 1.32 \\ \hline 11.68 \\ 5.84 \\ 1.32 \\ \hline 7.16 \end{array}$	$\begin{array}{r} 329 \\ 22 \\ \hline 307 \end{array}$	$\begin{array}{r} 82.25 \\ 7.00 \\ 75.25 \\ 140.59 \\ \hline 215.84 \end{array}$	$\begin{array}{r} 852 \\ 151.8 \\ \hline 700.2 \end{array}$	$\begin{array}{r} 325.8 \\ 6.85 \\ \hline 318.95 \\ 140.59 \\ \hline 459.54 \end{array}$	$\begin{array}{r} 10.75 \\ 25 \\ \hline 10.50 \\ 5.25 \\ 25 \\ \hline 5.50 \end{array}$	$\begin{array}{r} 11.50 \\ 1.32 \\ \hline 8 \end{array}$
$\begin{array}{r} 1050 \\ 214 \\ \hline 836 \end{array}$	$\begin{array}{r} 424 \\ 5.3 \\ \hline 418.7 \\ 140.6 \\ \hline 559.3 \end{array}$	$\begin{array}{r} 4.26 \\ 2.65 \\ \hline 6.91 \end{array}$	$\begin{array}{r} 12.00 \\ 12.00 \\ 45 \\ \hline 11.55 \\ 5.78 \\ 1.45 \\ \hline 6.23 \end{array}$	$\begin{array}{r} 1155 \\ 254 \\ \hline 901 \end{array}$	$\begin{array}{r} 478 \\ 6.20 \\ \hline 471.8 \\ 140.6 \\ \hline 612.4 \end{array}$	$\begin{array}{r} 11.50 \\ 1.32 \\ \hline 8 \end{array}$	$\begin{array}{r} 384.4 \\ 6.58 \\ \hline 377.8 \\ 140.6 \\ \hline 518.4 \end{array}$	$\begin{array}{r} 518.4 \end{array}$	$\begin{array}{r} 518.4 \end{array}$	$\begin{array}{r} 518.4 \end{array}$

Backsight on C	3.21	5.75	8.81	4.1	-19.9	5.10	20.94	489.06	-101.60	<sup>[130.24]</sup> -107.35	(1140.59)
On #1 screer base	2.27	5.77	9.26	7.1	+8.4	6.99	5.00	694.00	+58.70	+52.93	+193.52
"	3.00	5.00	7.00	/	+1.1	4.00	/	400.00	+4.40	-.60	+140.00
"	5.37	7.00	8.66	6.7	+25.0	3.29	22.02	306.98	+82.25	+75.25	+215.84
"	2.40	5.00	7.57	9.2	+28.9	5.17	47.50	469.50	+149.50	+144.50	+285.09
Outcrop below "A"	2.65	6.85	11.19	17.8	+38.2	8.52	151.80	700.20	+325.80	+318.95	+459.54
outcrop base right of "A"	1.32	6.58	11.50	17.25	+37.8	10.18	175.50	842.50	+384.40	+377.80	+518.40
Red powder	2.5	5.30	10.75	20.4	+40.4	10.50	214.00	836.00	+424.00	+418.70	+559.30
Outcrop middle screer	0.45	6.20	12.00	22.0	+41.4	11.53	254.00	901.00	+478.00	+471.80	+612.40

Friday 1<sup>st</sup> August - #1 showing

$$\begin{array}{r} 5.64 \\ 2.89 \\ \hline 12.75 \\ 1.38 \\ \hline 2.89 \\ \hline 4.27 \end{array}$$

$$\begin{array}{r} 308 \\ 26.8 \\ \hline 281.2 \end{array}$$

$$\begin{array}{r} 397 \\ 78.6 \\ \hline 318.4 \end{array}$$

$$\begin{array}{r} 275 \\ 55.2 \\ \hline 219.8 \\ 5.95 \\ 4.06 \\ \hline 1.89 \\ 95 \end{array}$$

$$\begin{array}{r} 5.49 \\ 9.51 \\ 98 \\ \hline 7.06 \end{array}$$

$$\begin{array}{r} 110.20 \\ 4.26 \\ \hline 105.94 \\ 527.51 \\ 633.45 \\ + 4.00 \\ \hline 637.45 \end{array}$$

$$\begin{array}{r} 76.50 \\ 641.45 \\ \hline 717.95 \end{array}$$

$$\begin{array}{r} 641.45 \\ 12.06 \\ \hline 629.4 \end{array}$$

$$\begin{array}{r} 10.02 \\ 6.05 \\ \hline 3.97 \\ 1.99 \\ \hline 804 \end{array}$$

$$\begin{array}{r} 127 \\ 10.55 \\ \hline 116.45 \end{array}$$

$$\begin{array}{r} 641.45 \\ 120 \\ \hline 521.45 \end{array}$$

$$\begin{array}{r} 641.45 \\ 14.25 \\ \hline 627.20 \\ 432 \\ 6.15 \\ \hline 425.85 \end{array}$$

$$\begin{array}{r} 3.63 \\ 2.36 \\ \hline 1.27 \end{array}$$

$$\begin{array}{r} 34.90 \\ 31.90 \\ 641.45 \\ \hline 673.35 \end{array}$$

$$\begin{array}{r} 11.63 \\ 8.33 \\ \hline 3.30 \\ 1.65 \\ 9.98 \\ \hline 51.50 \\ 5.00 \\ \hline 46.48 \\ 641.45 \\ \hline 687.93 \end{array}$$

$$\begin{array}{r} 6.70 \\ 3.60 \\ \hline 2.80 \end{array}$$

$$\begin{array}{r} 641.45 \\ 19 \\ \hline 622.45 \\ 10.90 \\ 9.10 \\ \hline 1.8 \\ .9 \end{array}$$

$$\begin{array}{r} 108 \\ 641.45 \\ \hline 744.45 \end{array}$$

$$\begin{array}{r} 275 \\ 57.75 \\ \hline 217.25 \end{array}$$

$$\begin{array}{r} 7.19 \\ 2.87 \\ \hline 4.32 \\ 2.16 \\ 2.87 \\ \hline 5.03 \end{array}$$

$$\begin{array}{r} 1.54 \\ 2 \\ \hline 3.08 \end{array}$$

$$\begin{array}{r} 280 \\ 57 \\ \hline 229 \end{array}$$

$$\begin{array}{r} 180 \\ 14.75 \\ \hline 165.25 \\ 49.40 \\ 39.40 \\ \hline 641.45 \\ \hline 680.85 \end{array}$$

$$\begin{array}{r} 9.35 \\ 6.60 \\ \hline 2.75 \\ 1.38 \\ 6.00 \\ \hline 7.98 \end{array}$$

Class. Knoll above "A"	2.89	4.26	5.64	20.1	40.1	2.75	55.20	219.80	+110.20	+105.94	+637.45
											(1641.45)
Small outcrop	4.06	5.00	5.95	/	-4.9	189.	/	189.00	-9.25	-14.25	+627.20
Creek	8.33	10.00	11.63		-2.7	3.30	/	330.00	-9.00	-19.00	+622.45
Crest exposed	2.87	5.02	7.19	1.42	+11.9	4.32	6.15	425.85	+51.50	+46.48	+687.93
Small outcrop	9.10	10.00	10.90	8.20	+27.4	1.80	14.75	165.25	+49.40	+39.40	+680.85
Basalt ridge outcrop	/	10.00	11.54	8.7	+28.1	3.08	26.80	281.20	+86.50	+76.50	+717.95
Top "	6.05	8.02	10.02	19.8	+39.8	3.97	78.60	318.90	+158.00	+150.00	+791.45
Summit atop "A"	6.40	5.00	3.60	18.2	+38.6	2.80	51.00	229.00	+108.00	+103.00	+744.45
Atop Jaky	2.36	3.00	3.63	8.3	+27.5	1.27	10.55	116.45	+34.90	+31.90	+673.35
Atop Granite	4.51	5.00	5.49	.53	-7.2	.98	.52	97.50	-7.06	-12.06	+627.40
Point ridge + outcrop	6.60	8.00	9.35	21.0	-40.7	2.75	57.75	217.25	-112.00	-120.00	+521.45

FRIDAY 1<sup>st</sup> August - #1 Showing

$$\begin{array}{r} 6.79 \\ 5.21 \\ \hline 1.58 \end{array}$$

$$\begin{array}{r} 158 \\ 1.4 \\ \hline 156.6 \end{array}$$

$$\begin{array}{r} 13.2 \\ 4 \\ \hline 9.2 \end{array}$$

$$\begin{array}{r} 764 \\ 234 \\ \hline 530 \\ 265 \\ 234 \\ \hline 99 \end{array}$$

$$\begin{array}{r} 530 \\ 4.93 \\ \hline 25.07 \end{array}$$

$$\begin{array}{r} 51.43 \\ 46.43 \\ 9.29 \\ \hline 37.29 \end{array}$$

$$\begin{array}{r} 8.02 \\ 3.99 \\ \hline 4.05 \\ 2.02 \\ 3.99 \\ \hline 5.99 \end{array}$$

$$\begin{array}{r} 60.50 \\ 9.29 \\ \hline 51.21 \\ 9.60 \\ 4.34 \\ \hline 5.26 \end{array}$$

$$\begin{array}{r} 10.08 \\ 1.95 \\ \hline 8.43 \\ 4.23 \\ 1.92 \\ \hline 6.05 \end{array}$$

$$\begin{array}{r} 10.08 \\ 1.92 \\ \hline 8.16 \\ 4.08 \\ 1.92 \\ \hline 6.00 \end{array}$$

$$\begin{array}{r} 7.05 \\ 2.95 \\ \hline 4.10 \\ 2.05 \end{array}$$

$$\begin{array}{r} 526 \\ 127.4 \\ \hline 378.6 \end{array}$$

$$\begin{array}{r} 512 \\ 123.4 \\ \hline 308.6 \end{array}$$

$$\begin{array}{r} 223.4 \\ 9.2 \\ \hline 214.2 \end{array}$$

$$\begin{array}{r} 352 \\ 271.5 \\ \hline 80.5 \end{array}$$

7.85

4.84  
7.90

$$\begin{array}{r} 410 \\ 87.4 \\ \hline 322.6 \end{array}$$

$$\begin{array}{r} 2.67 \\ 4.34 \\ 6.97 \\ \hline 7.56 \\ 2.44 \\ \hline 5.12 \end{array}$$

$$\begin{array}{r} 7.77 \\ 2.22 \\ \hline 5.55 \\ 2.78 \\ 2.22 \\ \hline 5.00 \end{array}$$

$$\begin{array}{r} 555 \\ 173.2 \\ \hline 381.8 \end{array}$$

$$\begin{array}{r} 7.56 \\ 2.44 \\ \hline 5.12 \end{array}$$

$$\begin{array}{r} 444 \\ 118.1 \\ \hline 325.9 \end{array}$$

$$\begin{array}{r} 11.00 \\ 4.84 \\ 6.16 \\ 3.08 \\ 4.84 \\ \hline 7.92 \end{array}$$

$$\begin{array}{r} 7.27 \\ 2.78 \\ 4.49 \\ 2.25 \\ 2.78 \\ \hline 5.03 \end{array}$$

$$\begin{array}{r} 5.12 \\ 2.56 \\ 2.44 \\ \hline 0.0 \\ 616 \\ 239.4 \\ \hline 376.6 \end{array}$$

$$\begin{array}{r} 7.27 \\ 2.78 \\ 4.44 \\ 2.22 \\ 2.78 \\ \hline 5.00 \\ 300 \\ 7.9 \\ \hline 292.1 \end{array}$$

$$\begin{array}{r} 6.75 \\ 3.23 \\ 3.52 \\ 1.76 \\ 2.23 \\ \hline 4.99 \end{array}$$

$$\begin{array}{r} 11.07 \\ 4.94 \\ 6.13 \\ 3.07 \\ 4.94 \\ \hline 8.01 \end{array}$$

From B Clock Band	5.21	6.00	6.79	.89	-9.3	1.58	1.41	156.6	-14.70	-20.70	-29.10
$\Delta$ 4005/800W	2.33	5.00	7.62	.93	+9.7	5.30	4.93	525.07	+51.48	+46.93	+37.23
$\Delta$ 8005/800W	3.97	6.00	8.02	2.69	+16.4	4.05	10.90	404.10	+66.50	+66.50	+51.30
Slope	1.92	6.00	10.08	8.7	+28.1	8.16	70.90	745.1	+229.40	+223.40	+214.20
4005/100W	2.95	5.00	7.05	2.3	+4.0	4.10	87.40	322.6	+168.00	+163.00	+381.00
$\Delta$ 2005	4.34	7.00	9.60	28.0	+44.9	5.26	147.40	378.6	+236.20	+229.20	+447.20
$\Delta$ 8005	2.22	5.00	7.77	31.2	+46.4	5.55	173.20	381.8	+251.90	+252.90	+470.90
8005/100W	2.44	5.00	7.56	28.0	+44.9	5.12	143.40	368.6	+230.00	+225.00	+443.00
"/200W	2.78	5.00	7.22	26.6	+44.2	4.44	118.10	325.9	+174.00	+169.00	+387.00
"/300W	3.23	5.00	6.75	22.85	+42.0	3.52	80.5	291.5	+148.00	+143.00	+361.00
Buttress	4.84	7.90	11.00	38.8	+48.7	6.16	239.4	376.6	+300.00	+292.10	+510.10

218.00

SATURDAY 2nd Aug. X lines 400W  
800W

$$\begin{array}{r} 2.40 \\ 1.80 \\ \hline 6.80 \\ 2.80 \\ \hline 1.80 \\ \hline 4.60 \end{array}$$
$$\begin{array}{r} 580 \\ 6.5 \\ \hline 573.5 \\ 9.42 \\ 6.57 \\ \hline 285 \\ 143 \\ \hline 657 \\ 800 \end{array}$$
$$\begin{array}{r} 680 \\ 7.62 \\ \hline 572.38 \\ 11.17 \\ 6.88 \\ \hline 4.29 \\ 214 \\ \hline 688 \\ 902 \end{array}$$
$$\begin{array}{r} 6.65 \\ 3.37 \\ \hline 3.28 \\ 1.64 \\ \hline 3.37 \\ 5.01 \end{array}$$
$$\begin{array}{r} 328 \\ 8.2 \\ \hline 319.8 \\ 7.56 \\ 2.46 \\ \hline 510 \\ 250 \end{array}$$
$$\begin{array}{r} 6.99 \\ 2.99 \\ \hline 4. \\ 2. \\ \hline 2. \\ 429 \\ 75.5 \\ \hline 453.5 \end{array}$$
$$\begin{array}{r} 400 \\ 31.6 \\ \hline 368.4 \end{array}$$
$$\begin{array}{r} 429 \\ 75.5 \\ \hline 353.5 \end{array}$$

SATURDAY 2nd Aug

X - lines 4000 } W  
8000 }

II

Buttress to Quad	1.00	5.00	8.40	11.12	-10.5	6.80	7.61	572.39	-68.40	-73.40	440.35
400S/100E	6.57	8.00	9.42	/	2.0	2.85	/	285.00	-5.70	-13.70	500.05
400S/200E	3.37	5.00	6.65	2.5	+15.6	3.28	8.20	319.80	+51.70	+46.10	559.85
4 / 300E	2.99	5.00	6.99	7.9	+27.0	4.00	31.60	368.40	+108.00	+103.00	616.75
800S/300E	5.02	6.01	7.01	10.0	+30.0	2.00	20.00	180.00	+60.00	+54.00	567.75
	5.40	6.00	6.60	1.72	+13.0	1.20	2.60	117.40	+15.60	+9.60	523.35
	2.06	5.00	7.56	/	0.2	5.10	/	510.00	-110.2	-6.02	507.73
High Ridge	6.88	9.00	11.17	17.6	+38.1	4.29	75.50	353.5	+163.40	+154.40	668.5
											(-672.25)
①					-11.1						
②											
③			8°45'		-15.0	21.59			-331.1		341.2
④			8°12'		-14.1	21.93			-316.7		355.6
⑤			7°25'		-12.8	23.41			-304.7		367.6
⑥			7°25'		-12.8	24.52			-319.3		383.0

$$\begin{array}{r} 6.61 \\ 5.39 \\ \hline 1.22 \\ \end{array}$$

$$\begin{array}{r} 3.76 \\ 2.23 \\ \hline 1.53 \\ \end{array}$$

$$\begin{array}{r} 4.18 \\ .82 \\ \hline 2.36 \\ 1.18 \\ \hline 0 \\ \end{array}$$

$$\begin{array}{r} 6.00 \\ 1.22 \\ \hline 4.78 \\ \end{array}$$

$$\begin{array}{r} 8.59 \\ 5.38 \\ \hline 3.21 \\ 1.69 \\ \hline 6.99 \\ \end{array}$$

$$\begin{array}{r} 672.25 \\ 4.78 \\ \hline 667.47 \\ \end{array}$$

$$\begin{array}{r} 321 \\ 10.3 \\ \hline 310.7 \\ \end{array}$$

$$\begin{array}{r} 9.69 \\ 6.30 \\ \hline 3.39 \\ 1.20 \\ \end{array}$$

$$\begin{array}{r} 672.25 \\ 55.7 \\ \hline 616.55 \\ \end{array}$$

$$\begin{array}{r} 6.48 \\ 3.50 \\ \hline 2.98 \\ \end{array}$$

$$\begin{array}{r} 10.77 \\ 7.28 \\ \hline 3.54 \\ 1.77 \\ \hline 9.00 \\ \end{array}$$

$$\begin{array}{r} 298 \\ 34 \\ \hline 264 \\ \end{array}$$

94.8

$$\begin{array}{r} 354 \\ 2516 \\ \hline 32884 \\ \end{array}$$

4005/400E	5.39	6.00	6.61	/	+1.0	1.22	/	122.00	+1.22	+9.78	+667.47		
base KPI	6.30	8.00	9.69	/	+3.1	3.39	/	339.00	+10.50	+2.50	+674.25		
Crest n	3.50	5.00	6.48	11.4	+31.8	2.98	34.00	264.00	+94.80	+89.80	+762.05		
4005/500E	2.23	3.00	3.76	/	-1.9	1.53	/	153.00	-2.82	-5.82	+646.43		
n / 600E	1.82	3.00	4.18	.91	-9.15	2.36	2.14	233.86	-22.40	-25.40	+646.85		
n / 700E	5.38	7.00	8.59	3.2	-17.1	3.21	10.30	310.90	-48.70	-55.70	+616.55		
Base 100W	7.23	9.00	10.77	7.1	-26.7	3.59	25.6	328.39	-91.00	-82.00	-590.25		

(+672.26)

SATURDAY 2<sup>nd</sup> Aug

X - lines 400N  
800N W

11.62  
7.13  
4.46  
2.23  
9.39

10.12  
1.87  
8.25  
4.13  
6.00

10.47  
1.52  
8.95  
4.48  
5.80

101.8  
9.39  
92.4  
862  
62.9  
799.1

92.4  
4  
571.73  
668.10

446  
24.6  
421.4

825  
21.45  
803.55  
340  
19  
321

10.70  
1.8  
9.52  
4.76  
5.94

11.72  
6.37  
5.35  
2.68  
5

10.32  
1.70  
8.62  
4.31  
6.01  
11.69  
8.29  
3.40  
20

7.16  
2.84  
4.32  
2.16  
5.00

10.94  
7.06  
3.88  
1.94  
9.00

7.34  
2.66  
4.68  
2.34  
5.00

11.74  
6.33  
5.41  
2.71  
9.24

672.50  
44.64  
627.86

10.18  
9.81  
37  
19  
11.38  
6.62  
6.74  
2.37

474  
388  
435.2

6.83  
3.17  
3.66  
183

4.68  
2  
9.36

11.69  
8.29  
3.40  
1.70  
9.99

11.69  
7.35  
55.9  
67.9.1

936  
89.9  
946.1

MONDAY  
4th AUGUST 69

EAST CAIRNS (672.50)

RIDGE cairns  
S of 1200S

(24) - 29.1

(16) - 41.5

(8) - 23.8

(20) - 39.5

(12) - 33.8

(4) - 10.0

From													
2400S/300W	7.16	9.39	11.62	5.5	+22.8	4.46	24.6	421.4	+191.8	+92.4	+668.10		
1200S/100E	1.87	6.00	10.12	2.6	15.9	8.25	21.45	803.55	-131.10	-131.10	+535.40	(672.50)	
✓ 300E	1.52	6.00	10.47	6.15	-24.0	8.95	55.00	840.00	-214.40	-220.40	+452.10		
✓ 400E	1.18	5.92	10.70	9.25	-49.0	9.52	88.00	864.00	-276.00	-281.92	+390.58		
✓ 100W	1.70	6.00	10.32	7.3	-26.0	8.62	62.90	799.10	-224.00	-230.00	+42.50		
A 1600S	2.84	5.00	7.16	6.0	-23.8	4.32	25.90	406.10	-102.90	-107.90	564.60		
11/100W	2.66	5.00	7.34	13.9	-34.5	4.68	65.10	402.90	-161.60	-166.60	505.90		
11/200W	6.33	9.00	11.74	21.8	-41.25	5.41	118.00	423.00	-223.40	-282.40	440.10		
A 2000S	9.18	10.00	10.18	1.46	-12.0	.37	.54	36.46	-3.94	-13.94	658.56		
2400S/300W	7.06	9.00	10.92	86	9.2	3.88	3.34	385	-35.64	-44.64	627.86		
11/100W	3.7	5.00	6.83	74	+8.7	3.66	2.71	3.63	+31.84	+26.84	699.34		
A 2400S-(34)	8.29	10.00	11.69	5.6	+23	3.40	19.05	(321) 345.	+78.25	+68.25	740.75		
2500S	6.62	9.00	11.38	8.2	+27.5	4.74	38.80	435.2	+130.20	+12.20	793.70		
Knife 2000	1.32	5.00	8.67	7.6	+26.6	7.35	55.90	699.10	+195.80	+190.80	863.30		
11	.32	5.00	/	9.6	+29.4	9.36	89.90	946.10	+275.40	+270.40	942.90		

[571.73]

$$\begin{array}{r} +37.23 \\ + 3.77 \\ \hline 41.00 \end{array}$$

$$\begin{array}{r} 8.24 \\ 3.78 \\ \hline 4.46 \\ 2.22 \\ \hline 6.11 \end{array}$$

$$\begin{array}{r} 8.22 \\ 3.78 \\ \hline 4.44 \\ 2.22 \\ \hline 6.00 \end{array}$$

$$\begin{array}{r} 41.00 \\ 14.88 \\ \hline 26.12 \\ 11.62 \\ 6.40 \\ \hline 5.22 \\ 2.61 \\ \hline 9.01 \end{array}$$

$$\begin{array}{r} 10.52 \\ 5.97 \\ \hline 5.05 \\ 2.53 \\ \hline 8.00 \end{array}$$

$$\begin{array}{r} 5.05 \\ 8.5 \\ \hline 496.5 \end{array}$$

$$\begin{array}{r} 73.10 \\ 78.00 \\ \hline 32.10 \end{array}$$

$$\begin{array}{r} 10.09 \\ 5.91 \\ \hline 4.08 \\ 2.04 \\ \hline 7.95 \end{array}$$

$$\begin{array}{r} 520.4 \\ 11.95 \\ \hline 508.45 \end{array}$$

$$\begin{array}{r} 10.07 \\ 5.90 \\ \hline 0.7 \end{array}$$

$$\begin{array}{r} 10-10 \\ 5.90 \\ \hline 4.20 \\ 2.10 \\ \hline 0.00 \end{array}$$

$$\begin{array}{r} 8.52 \\ 1.47 \\ \hline 7.05 \\ 3.53 \\ \hline 5.00 \end{array}$$

$$\begin{array}{r} 9.39 \\ 2.57 \\ \hline 6.82 \\ 3.41 \\ \hline 5.90 \end{array}$$

$$\begin{array}{r} 114.56 \\ 41 \\ \hline 73.5 \end{array}$$

$$\begin{array}{r} 705 \\ 6.05 \\ \hline 698.94 \end{array}$$

$$\begin{array}{r} 682 \\ 29.65 \\ \hline 652.35 \end{array}$$

$$\begin{array}{r} 520.40 \\ 20.40 \\ \hline 499.56 \end{array}$$

$$\begin{array}{r} 134 \\ 91 \\ \hline 93 \end{array}$$

$$\begin{array}{r} 10.38 \\ 1.62 \\ \hline 8.76 \\ 4.38 \\ \hline 6.00 \end{array}$$

$$\begin{array}{r} 8.61 \\ 3.41 \\ \hline 5.20 \\ 2.60 \\ \hline 0.01 \end{array}$$

$$\begin{array}{r} 10.10 \\ 1.96 \\ \hline 8.20 \end{array}$$

$$\begin{array}{r} 11.55 \\ 4.53 \\ \hline 7.02 \\ 9.51 \\ \hline 8.09 \end{array}$$

$$\begin{array}{r} 876 \\ 33.3 \\ \hline 842.7 \end{array}$$

$$\begin{array}{r} 173.50 \\ 4 \\ \hline 132.50 \end{array}$$

$$\begin{array}{r} 702 \\ 92.6 \\ \hline 609.4 \end{array}$$

$$\begin{array}{r} 10.08 \\ 1.92 \\ \hline 8.06 \\ 2.23 \\ \hline 5.95 \end{array}$$

$$\begin{array}{r} 6.73 \\ 3.26 \\ \hline 3.47 \\ 1.74 \\ \hline 510.0 \end{array}$$

209 - 100 ft

300 - 20

20 =  $\frac{100}{1} \times \frac{20}{20}$

15  
 $\frac{200}{20}$

1500 ft

From #100 (600)

(\$41.00)

Oct 1 A Snow	3.78	6.00	8.22	/	-1.2	4.44	/	444	-8.88	-14.88	+26.12
Risky Claim posts	5.27	8.00	10.52	1.68	-12.9	5.05	8.49	496.50	-65.10	-73.10	-32.10
Waterfall	5.90	8.00	10.10	3.99	-9.15	4.20	16.75	403.25	-82.00	-90.00	-49.00
Cutaway Claim posts	6.40	9.00	11.67	4.20	-20.2	5.22	22.44	499.56	-105.50	-114.50	-73.50
Cliff tongue base	1.47	5.00	8.52	.86	-9.1	7.05	6.06	698.74	-64.10	-69.10	-28.10
Creek/cliff	2.57	6.00	9.39	3.52	-18.8	6.82	24.65	657.35	-128.20	-134.20	-93.20
'	1.62	6.00	10.38	3.8	-19.1	8.76	33.30	842.70	-167.50	-173.50	-132.50
Ridge for waterfall	3.41	6.00	8.61	2.3	-15.0	5.20	11.95	508.05	-28.00	-34.00	-43.00
A 4-way/snow	1.90	6.00	10.10	/	+3.0	8.20	/	820.00	+24.60	+18.60	+59.60
2 way outcrop.	4.53	8.00	11.53	13.2	+33.9	7.02	92.60	609.40	+240.40	+232.40	+273.40
GD outcrop middle	3.26	5.00	6.73	14.4	+35.1	3.47	50.00	297.00	+122.00	+117.00	+158.00

Sat 9th Aug 1969

Valley below Camp.

11.90  
1.10  
10.80  
5.20  
6.36

11.90  
1.05  
10.95  
5.

59.60  
3.40  
62.00

1080  
71.3  
1008.7

269

275.5  
62  
213.5

11.05  
.95  
10.10  
5.05  
6.00

10.80  
3.18  
7.62  
3.81  
6.99

1010  
63.6  
946.4  
9.60  
2.40  
7.20  
3.60

762  
55.3  
706.7  
156.5  
62  
94.5

205.10  
60  
143.10

11.20  
2.80  
8.40  
4.20  
7.00  
259  
17.6  
241.4

840  
72.2  
767.8

445  
71.4  
373.4

355  
107.2  
247.8

10.31  
7.72  
2.59  
1.30  
9.02

11.50  
10  
1.54  
30.8

308  
12.1  
295.9

11.77  
0.22  
3.55  
1.78  
10.00

11.22  
6.77  
4.45  
2.23  
9.00

Creek from town/boom	7.10	6.50	11.90	6.6	-24.9	10.80	71.3	1008.3	-269.00	-275.50	-213.50
"	95	6.00	11.05	6.3	-24.2	10.10	63.6	916.4	-244.10	-250.10	-188.10
channel	3.18	7.00	10.80	7.25	+26.0	7.62	55.3	706.7	-198.10	-205.10	-143.10
"	2.80	7.00	11.20	8.6	-28.1	8.40	72.2	767.8	-236.00	-243.00	-181.00
Slope	2.40	6.00	9.00	4.58	-20.9	7.20	33.0	687.0	-150.50	-156.50	-94.50
Slope base	7.72	9.00	10.31	6.8	-25.2	2.59	17.60	241.4	-65.30	-74.30	-12.30
Δ Boom/boom	/	10.00	11.54	3.9	+19.3	3.08	12.10	295.9	+59.50	+49.50	+111.50
outcrop boom	6.77	9.00	11.22	16.1	+36.8	4.45	71.60	373.4	+163.90	+154.90	+216.90
Slope	8.22	10.00	11.77	30.2	+46.0	3.55	107.20	247.8	+163.30	+153.30	+215.30

Monday 11<sup>th</sup> Aug 1969 - End of creek in valley.

$$\begin{array}{r} 10.73 \\ 7.24 \\ \hline 3.49 \\ 1.75 \\ \hline 8.99 \end{array}$$

$$\begin{array}{r} 59.60 \\ 2.40 \\ \hline 63.00 \\ 10.52 \\ 5.53 \\ \hline 4.90 \\ 3 \end{array}$$

$$\begin{array}{r} 1.73 \\ 2 \\ \hline 3.46 \\ 10.51 \\ 5.53 \\ \hline 4.98 \\ 2.49 \\ \hline 8.02 \end{array}$$

$$\begin{array}{r} 59.60 \\ 69.90 \\ \hline 498 \\ 127.8 \\ \hline 370.2 \end{array}$$

$$\begin{array}{r} 59.60 \\ 11.31 \\ \hline 70.91 \\ 190 \\ 16.7 \\ \hline 473.3 \end{array}$$

$$\begin{array}{r} 71. \\ 68.6 \\ \hline 2.4 \end{array}$$

$$\begin{array}{r} 4.2 \\ 260.8 \\ 180.9 \\ \hline 79.9 \end{array}$$

$$\begin{array}{r} 7.72 \\ 2.24 \\ \hline 5.48 \end{array}$$

$$\begin{array}{r} 548 \\ 88.3 \\ \hline 459.7 \end{array}$$

$$\begin{array}{r} 9.47 \\ 4.57 \\ \hline 4.90 \\ 2.45 \\ \hline 7.02 \end{array}$$

$$\begin{array}{r} 4.98 \\ 2.49 \\ \hline 8.02 \end{array}$$

$$\begin{array}{r} 436 \\ 364 \\ \hline 72 \end{array}$$

$$\begin{array}{r} 72 \\ 3.5 \\ \hline 58.5 \end{array}$$

$$\begin{array}{r} 666 \\ 119.2 \\ \hline 546.8 \end{array}$$

$$\begin{array}{r} 264.8 \\ 156.8 \\ \hline 108.0 \end{array}$$

$$\begin{array}{r} 9.33 \\ 2.67 \\ \hline 6.66 \\ 2.33 \\ \hline 6.00 \end{array}$$

$$\begin{array}{r} 2.74 \\ 4.98 \end{array}$$

$$\begin{array}{r} 10.67 \\ 1.32 \\ \hline 9.35 \\ 4.68 \end{array}$$

$$\begin{array}{r} 2.90 \\ 2.45 \\ \hline 7.02 \end{array}$$

$$\begin{array}{r} 9.34 \\ 2.69 \\ \hline 6.65 \end{array}$$

$$\begin{array}{r} 329.9 \\ 156.8 \\ \hline 273.1 \end{array}$$

$$\begin{array}{r} 260.8 \\ 156.8 \\ \hline 104.0 \\ 186.90 \\ 156.80 \\ \hline 30.10 \end{array}$$

$$\begin{array}{r} 9.11 \\ 6.63 \\ \hline 2.78 \\ 1.39 \end{array}$$

$$\begin{array}{r} 556 \\ 57.2 \\ \hline 488.8 \end{array}$$

$$\begin{array}{r} 10.42 \\ 7.61 \\ \hline 2.81 \\ 1.41 \end{array}$$

$$\begin{array}{r} 7.78 \\ 2.72 \\ \hline 5.56 \\ 2.78 \\ \hline 2.78 \\ 25.3 \\ \hline 252.7 \end{array}$$

$$\begin{array}{r} 281 \\ 7.9 \\ \hline 273.1 \end{array}$$

$$30.10$$

$$8.02$$

Slope from 400N/Brown	7:24	9:20	10:73	/	+4.1	3.49	/	3.49	+14.60	+5.60	68.60
Backlight	/	10:29	12:00		-3	3.46			-1.04	-11.31	(77.00)
Outcrop	5:53	8:00	10:52	25.6	+43.6	4.98	127.80	370.2	+217.40	+209.40	280.40
"	2:24	5:00	7:72	16.1	+36.8	5.48	88.30	459.7	+202.00	197.00	268.00
Slope	4:57	7:00	9:47	3.4	+18.1	4.90	16.70	473.3	+88.60	81.60	152.60
										(6.20)	(156.80)
1200N/Brown	3:64	4:00	4:36	18.7	+39.0	.72	13.50	58.5	+28.10	24.10	180.90
Glacial	2:67	6:00	9:33	17.9	-38.25	6.66	119.20	546.8	-254.80	-260.80	-104.00
Clamp post Risky 9:00/12	2:69	6:00	9:34	18.5	-38.8	6.65	123.00	542.00	-258.00	-264.80	-108.00
Glacial	1:32	6:00	10:67	13.9	-34.6	9.35	130.00	905.00	-323.90	-329.90	-173.10
Slope	2:22	5:00	7:78	12.1	-32.7	5.56	67.20	488.8	-181.90	-186.90	-30.70
"	7:61	9:00	10:42	2.8	-16.5	2.81	7.90	273.1	-46.50	-55.50	101.30
"	6:63	8:00	9:41	9.1	+28.9	2.78	25.30	252.7	+80.40	72.40	227.20

Saturday 16<sup>th</sup> Aug 1969

1200N }  
1600N } W

+ valley outcrops.

$$\begin{array}{r} 5.81 \\ 14.19 \\ \hline .62 \end{array}$$

$$\begin{array}{r} 7.53 \\ 6.49 \\ \hline 10.4 \end{array}$$

$$\begin{array}{r} .52 \\ 7.01 \end{array}$$

$$\begin{array}{r} 1.29 \\ 2 \\ \hline 2.78 \end{array}$$

$$\begin{array}{r} 236 \\ 75.4 \\ \hline 160.6 \end{array}$$

$$\begin{array}{r} 104 \\ 19.98 \\ \hline 84.02 \end{array}$$

$$\begin{array}{r} 233.20 \\ 7.04 \\ \hline 226.16 \end{array}$$

$$\begin{array}{r} 7.52 \\ 0.40 \\ \hline 3.12 \\ 156 \\ \hline 596 \end{array}$$

$$\begin{array}{r} 200 \\ 25.8 \\ \hline 174.2 \end{array}$$

$$\begin{array}{r} 312 \\ 100.4 \\ \hline 211.6 \end{array}$$

$$\begin{array}{r} 11.05 \\ 8.94 \\ \hline 2.11 \\ 1.26 \\ \hline 9.50 \end{array}$$

$$\begin{array}{r} 233.20 \\ 77.90 \\ \hline 155.3 \end{array}$$

$$\begin{array}{r} 6.16 \\ 3.86 \\ \hline 2.36 \\ 1.18 \\ \hline 4.98 \end{array}$$

$$\begin{array}{r} 233.20 \\ 10.35 \\ \hline 222.85 \end{array}$$

$$\begin{array}{r} 211 \\ 1.43 \\ \hline 209.57 \end{array}$$

1600N/700W	4.19	5.00	5.81	/	-3.3	1.67	/	162.00	-5.35	-10.35	222.85
from slope											
" 800W	/	11.00	12.00	12.9	-33.4	2.00	25.80	174.20	-66.90	-77.90	155.30
Slope	/	10.00	11.39	.78	+8.8	2.78	2.16	275.84	+24.44	11.44	247.64
Outcrop	6.49	7.00	7.53	19.2	+39.5	1.04	19.98	84.02	+41.08	36.08	269.28
1600N/400W	4.19	6.00	7.52	32.2	+46.7	3.12	100.40	211.6	+145.90	139.90	373.10
Outcrop	3.80	5.00	6.16	31.9	+45.9	2.36	75.40	160.6	+108.20	103.20	336.40
"	8.94	10.00	11.65	.67	+8.1	2.11	1.43	209.57	+17.10	7.10	240.30

Saturday 16<sup>th</sup> August 1969 - 1200N? 1600N } W + valley outcrops.

11.70  
10.30  
1.40  
2.52  
9.40

140  
44.8  
95.2

7.93  
3.13  
4.80  
2.40  
5.53

244.5  
78.3  
68.2  
386  
127  
259

7.93  
4.27  
3.86  
1.73  
5.50

244.5  
187.7  
56.8

44.20  
244.50

9.40  
2.52  
6.88  
3.44  
5.96

688  
291.4  
476.6

396  
101.4  
294.6

323.00  
244.5  
78.5

11.98  
8.02  
3.96

6.67  
3.33  
3.34  
3  
334  
21.72  
312.28

244.5  
182.9  
61.6

244.5  
87.8  
156.7

2000N/800W (Highway)	10.30	11.00	11.70	32.0 - 46.6	1.40	44.80	95.2	-65.30	-76.30	168.20
Durcrop	4.07	6.00	7.93	32.9 - 17.0	3.86	127.00	259.00	-181.70	-187.70	56.80
2400N/800W	2.52	6.00	9.40	30.7 - 46.1	6.88	211.40	476.6	-317.00	-323.00	-78.50
Creek/ Highway	8.02	10.00	11.98	25.6 - 43.6	3.96	101.40	294.6	-172.90	-182.90	61.6
Durcrop ridge	3.33	5.5.00	6.67	6.5 - 24.8	3.34	21.72	312.28	-82.80	-87.80	156.7

SUNDAY 17<sup>th</sup> Aug 1969 — 2400N/800W

$$\begin{array}{r} 4.49 \\ 5.54 \\ \hline 11.5 \\ 4.5 \\ \hline 0.2 \end{array}$$

$$\begin{array}{r} 4.48 \\ 3.55 \\ \hline 9.3 \\ 4.7 \\ \hline 0.2 \end{array}$$

$$\begin{array}{r} 9.3 \\ 2.4 \\ \hline 6.9 \end{array}$$

$$\begin{array}{r} 2.5 \\ 3 \\ \hline 7.5 \end{array}$$

$$\begin{array}{r} 11.20 \\ 4.85 \\ \hline 6.35 \\ 3.10 \\ \hline 8.03 \end{array}$$

$$\begin{array}{r} 6.35 \\ 16.2 \\ \hline 47.3 \end{array}$$

$$\begin{array}{r} 7.45 \\ 2.54 \\ \hline 4.89 \\ 2.45 \\ \hline 5.0 \end{array}$$

$$\begin{array}{r} 2.47 \\ 36.60 \\ \hline 28.10 \end{array}$$

$$\begin{array}{r} 7.40 \\ 4.61 \\ \hline 2.79 \end{array}$$

$$\begin{array}{r} 7.12 \\ 2.88 \\ \hline 4.24 \end{array}$$

$$\begin{array}{r} 4.89 \\ 50.2 \\ \hline 438.8 \end{array}$$

$$\begin{array}{r} 7.24 \\ 4.74 \\ \hline 2.48 \end{array}$$

$$\begin{array}{r} 4.24 \\ 35.6 \\ \hline 388.4 \end{array}$$

$$\begin{array}{r} 285.5 \\ 113.2 \\ \hline 248 \end{array}$$

$$\begin{array}{r} 6.67 \\ 3.32 \\ \hline 3.35 \end{array}$$

$$\begin{array}{r} 200 \\ 12.8 \\ \hline 187.2 \end{array}$$

$$\begin{array}{r} 9.52 \\ 6.47 \\ \hline 3.05 \end{array}$$

$$\begin{array}{r} 21.0 \\ 0.0 \\ \hline 1.87 \end{array}$$

$$\begin{array}{r} 3.35 \\ 12.9 \\ \hline 322.1 \end{array}$$

$$\begin{array}{r} 7.74 \\ 7.74 \\ \hline 768.26 \end{array}$$

$$\begin{array}{r} 30.5 \\ 2.3 \\ \hline 0.2 \end{array}$$

$$\begin{array}{r} 11.7 \\ 236.3 \\ \hline 248 \end{array}$$

$$\begin{array}{r} 264.6 \\ 84.5 \\ \hline 182.1 \end{array}$$

$$\begin{array}{r} 11.18 \\ 8.82 \\ \hline 2.36 \\ 1.68 \end{array}$$

$$\begin{array}{r} 11.25 \\ 0.75 \\ \hline 2.50 \end{array}$$

$$\begin{array}{r} 8 \\ 3.87 \\ 2 \\ \hline 7.74 \end{array}$$

$$\begin{array}{r} 11.41 \\ 6.62 \\ 4.74 \\ \hline 2.80 \\ 2.52 \\ 2.40 \\ \hline 0.2 \end{array}$$

$$\begin{array}{r} 11.24 \\ 7.8 \\ \hline 10.46 \\ 5.23 \\ \hline 6.01 \end{array}$$

$$\begin{array}{r} 10.46 \\ 6.8 \\ \hline 9.78 \\ 11.40 \\ 6.6 \end{array}$$

$$\begin{array}{r} 2.36 \\ 52.6 \\ \hline 183.4 \end{array}$$

$$108.20$$

$$\begin{array}{r} 4.79 \\ 96.60 \\ \hline 382.40 \end{array}$$

$$\begin{array}{r} 1.18 \\ 201.00 \\ 6.20 \\ \hline 194.80 \end{array}$$

Top outcrop	3.55	4.00	4.48	25.8	+43.7	93	24.00	69.00	+40.60	+36.60	281.10
A											(285.50)
1600N	4.85	8.00	11.20	25.5	+43.6	6.35	162.00	473.00	+276.50	268.50	553.00
Kopje base	2.56	5.00	7.45	12.9	+33.5	4.89	50.20	438.80	+163.90	158.90	444.40
A											
2000N	2.88	5.00	7.12	8.4	+27.9	4.24	35.60	388.4	+118.20	113.20	398.70
Middle creek channel	4.76	6.00	7.24	4.7	+21.2	2.48	11.70	236.3	+52.50	46.50	332.00
Outcrop	4.61	6.00	7.40	0.4	-6.2	2.79	1.10	277.90	-17.30	-23.30	262.20

MONDAY 18<sup>th</sup> Aug - W side Koppes.

(266.60)

Kopje base	3.32	5.00	6.67	3.84	+19.2	3.35	12.90	322.1	+64.40	59.40	326.00
A											
2000N	6.47	8.00	9.52	7.5	-8.7	3.95	2.30	302.7	-26.60	-34.60	232.00
Outcrop	/	8.00	11.87	1.0	-9.9	7.74	7.74	766.26	-76.50	-84.50	182.1
2000N	7.8	6.00	11.24	6.5	-24.7	10.46	68.00	978.00	-258.40	-264.40	2.20
End outcrop	9.00	10.00	11.00	6.4	-24.4	2.00	12.80	189.2	-48.80	-58.80	-52.60
5000N	8.32	10.00	11.18	22.3	-41.6	2.36	52.60	183.4	-98.20	-108.20	-102.20
"	8.15	10.00	11.25	3	+5.0	2.50	17.00	249.00	+12.5	2.15	8.70
"	6.63	9.00	11.4	20.2	-40.1	4.79	46.50	382.40	-192.00	-201.00	-194.80

(6.20)

11.67  
6.37  

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5130  
265  
~~8.82~~

530  
89  

---

541  
441

197.80  
4.4  

---

197  
-190.40  

---

207.20  

---

-397.60

Knoll 6.34 9.00 11.67 14.8 -37.4 5.30 89.00 44.00 -198.20 -207.20 -397.60

MONDAY 18<sup>th</sup> Aug - W side Kopjes.

$$\begin{array}{r} 9.07 \\ 6.92 \\ \hline 2.15 \\ \hline 1.08 \\ \hline 8.00 \end{array}$$

$$\begin{array}{r} 215 \\ 19.2 \\ \hline 195.6 \end{array}$$

$$\begin{array}{r} 9.58 \\ 6.02 \\ \hline 3.16 \end{array}$$

$$\begin{array}{r} 7.26 \\ 4.73 \\ \hline 2.53 \end{array}$$

$$\begin{array}{r} 316 \\ 19 \\ \hline 297 \end{array}$$

$$\begin{array}{r} 39.8 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 108.06 \\ 3 \\ \hline 111.60 \\ 69.00 \\ \hline 42.00 \end{array}$$

$$\begin{array}{r} 253 \\ 22.8 \\ \hline 230.2 \end{array}$$

$$\begin{array}{r} -99.10 \\ 66.90 \\ \hline 32.20 \end{array}$$

$$\begin{array}{r} 693 \\ 151 \\ \hline 542 \end{array}$$

$$\begin{array}{r} 672 \\ 105 \\ \hline 567 \end{array}$$

$$\begin{array}{r} 28.6 \\ 4 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 101.37 \\ 3.65 \\ \hline 6.72 \\ \hline 3.36 \\ \hline 7.01 \end{array}$$

$$\begin{array}{r} 11.12 \\ 4.90 \\ \hline 6.22 \end{array}$$

$$\begin{array}{r} 8.47 \\ 1.54 \\ \hline 6.93 \\ \hline 3.47 \\ \hline 5.01 \end{array}$$

$$\begin{array}{r} 278.00 \\ 97.10 \\ \hline 178.90 \end{array}$$

$$\begin{array}{r} 236.90 \\ 99.10 \\ \hline 137.80 \end{array}$$

$$\begin{array}{r} 171.20 \\ 99.10 \\ \hline 72.10 \end{array}$$

$$\begin{array}{r} 22.6 \\ -24.6 \\ \hline 39.8 \\ \hline -24.6 \\ \hline 15.2 \end{array}$$

$$\begin{array}{r} -108.00 \\ 3 \\ \hline -105.00 \\ -69.50 \\ \hline 174.50 \end{array}$$

$$\begin{array}{r} 11.48 \\ 4.52 \\ \hline 6.96 \end{array}$$

$$\begin{array}{r} 696 \\ 51.5 \\ \hline 644.5 \end{array}$$

$$\begin{array}{r} 4.14 \\ 1.85 \\ \hline 3.27 \\ 1.64 \\ \hline 5.1 \end{array}$$

$$\begin{array}{r} 622 \\ 56 \\ \hline 566 \end{array}$$

$$\begin{array}{r} 73 \\ 99.1 \\ \hline 73.9 \end{array}$$

$$\begin{array}{r} 228 \\ 1.9 \\ \hline 216.1 \end{array}$$

$$\begin{array}{r} 174.50 \\ 4.5 \\ \hline 179.00 \\ 66.90 \\ \hline 245.90 \end{array}$$

$$\begin{array}{r} 11.80 \\ 6.21 \\ \hline 5.59 \end{array}$$

$$\begin{array}{r} 99.10 \\ 16.70 \\ \hline 82.40 \end{array}$$

$$\begin{array}{r} 5.65 \\ 4.35 \\ \hline 1.30 \end{array}$$

$$\begin{array}{r} 4.14 \\ 1.86 \\ \hline 2.28 \\ 1.64 \\ \hline 3.90 \end{array}$$

$$\begin{array}{r} 4.14 \\ 1.86 \\ \hline 2.28 \\ 1.14 \end{array}$$

$$\begin{array}{r} -78.50 \\ 2.5 \\ \hline -76.0 \\ 47.4 \\ \hline -28.6 \end{array}$$

$$\begin{array}{r} -174.50 \\ 4.50 \\ \hline -170.00 \\ 66.90 \\ \hline -103.10 \end{array}$$

$$\begin{array}{r} 30 \\ 17.9 \\ \hline 112.1 \end{array}$$

$$\begin{array}{r} 6.42 \\ 3.58 \\ \hline 2.84 \end{array}$$

$$\begin{array}{r} 284 \\ 30.7 \\ \hline 253.3 \end{array}$$

$$\begin{array}{r} 83 \\ -24.6 \\ \hline 58.4 \end{array}$$

$$\begin{array}{r} -103.10 \\ 4.00 \\ \hline 99.10 \end{array}$$

TUESDAY 19<sup>th</sup> Aug 68 - 2000N/BOON + outcrops.

Slope from clamp	6.90	8.00	9.51	9.0	-28.6	2.15	19.4	195.6	-61.50	+69.50	-174.00
Slope	6.42	8.00	9.59	6.0	+23.7	3.16	19.00	297.00	+74.90	+66.90	-103.10
Slope	4.73	6.00	7.16	9.0	+28.8	2.53	22.80	230.20	+72.90	+66.90	<u>+99.10</u> -32.20
Top 1000 outcrop	1.514	5.00	8.51	21.8	+41.25	6.93	151.00	542.00	+283.00	+278.00	+178.90
"	3.165	7.00	10.37	15.6	+36.25	6.72	105.00	562.00	+243.90	+236.90	+187.80
2000N/Draw	4.90	8.00	11.12	9.0	+28.8	6.22	56.00	566.00	+179.20	+171.20	+72.10
End outcrop	4.52	8.00	11.48	7.14	+26.4	6.96	51.50	649.5	+181.00	+173.00	+73.90
Slope	6.21	9.00	11.80	7.2	+4.6	5.59	11.00	558.00	+25.70	+16.70	-82.40
.....											
Slope from 2000N/Draw	1.80	3.00	4.16	5.2	+22.1	2.28	11.90	216.10	+50.40	+47.40	-28.6
2000N/Draw from slope	4.35	5.00	5.65	13.8	+34.5	1.30	17.90	112.10	+44.80	+39.80	+15.2
Slope from slope	3.58	5.00	6.42	10.8	+31.0	2.84	30.70	253.3	+88.00	+83.00	+58.70

$$\begin{array}{r} 6.36 \\ 3.62 \\ \hline 2.74 \\ 1.37 \\ \hline 4.99 \end{array}$$

$$\begin{array}{r} 274 \\ 27.4 \\ \hline 246.6 \\ 11.22 \\ 8.77 \\ \hline 245 \\ 1.23 \\ \hline 10.00 \end{array}$$

$$\begin{array}{r} 10.81 \\ 9.19 \\ \hline 1.62 \end{array}$$

$$\begin{array}{r} 11.17 \\ 6.95 \\ \hline 4.22 \end{array}$$

$$\begin{array}{r} 422 \\ 62.8 \\ \hline 359.2 \end{array}$$

$$\begin{array}{r} 121 \\ 62.5 \\ \hline 58.5 \end{array}$$

$$\begin{array}{r} 62.5 \\ 8.1 \\ \hline 54.4 \end{array}$$

$$\begin{array}{r} 58.4 \\ 4.1 \\ \hline 62.5 \\ 77.2 \\ \hline 139.7 \end{array}$$

$$\begin{array}{r} 11.22 \\ 8.77 \\ \hline 245 \\ 1.23 \\ \hline 10.00 \end{array}$$

$$\begin{array}{r} 10.66 \\ 1.27 \\ \hline 9.39 \\ 4.80 \\ \hline 59.7 \end{array}$$

$$\begin{array}{r} 159.00 \\ 62.5 \\ \hline -96.5 \end{array}$$

$$\begin{array}{r} 10.66 \\ 1.32 \\ \hline 9.38 \end{array}$$

$$\begin{array}{r} 938 \\ 230.8 \\ \hline 707.2 \end{array}$$

$$\begin{array}{r} 410 \\ 62.5 \\ \hline 347.5 \end{array}$$

$$\begin{array}{r} 10.09 \\ 1.93 \\ \hline 8.11 \\ 4.06 \\ \hline 5.99 \end{array}$$

$$\begin{array}{r} 6.56 \\ 3.45 \\ \hline 3.11 \end{array}$$

$$\begin{array}{r} 10.54 \\ 1.45 \\ \hline 9.09 \end{array}$$

$$\begin{array}{r} 694 \\ 38.7 \\ \hline 655.3 \end{array}$$

$$\begin{array}{r} 311 \\ 10.6 \\ \hline 296.4 \end{array}$$

$$\begin{array}{r} 811 \\ 17.7 \\ \hline 793.3 \end{array}$$

$$\begin{array}{r} 909 \\ 19.8 \\ \hline 889.2 \end{array}$$

$$\begin{array}{r} 9.47 \\ 2.53 \\ \hline 6.94 \end{array}$$

$$\begin{array}{r} 555 \\ 135.8 \\ \hline 419.2 \end{array}$$

$$\begin{array}{r} -550.8 \\ 4.2 \\ \hline -50 \end{array}$$

$$\begin{array}{r} 9.27 \\ 2.53 \\ \hline 8.94 \\ 3.47 \\ \hline 6.00 \end{array}$$

$$\begin{array}{r} 7.67 \\ 2.33 \\ \hline 5.34 \end{array}$$

$$\begin{array}{r} 5.00 \\ 1.64 \\ \hline 3.36 \end{array}$$

$$\begin{array}{r} 6.37 \\ 1.64 \\ \hline 4.73 \\ 2.37 \\ \hline 4.01 \end{array}$$

$$\begin{array}{r} 8.39 \\ 1.64 \\ \hline 6.73 \\ 3.37 \\ \hline 5.01 \end{array}$$

$$\begin{array}{r} 673 \\ 61.2 \\ \hline 611.8 \end{array}$$

$$\begin{array}{r} 9.90 \\ 6.10 \\ \hline 3.80 \end{array}$$

$$\begin{array}{r} 7.63 \\ 4.37 \\ \hline 5.26 \end{array}$$

Tuesday 26<sup>th</sup> Aug — Creek Junctions.

(+12.5)

Outcrop floor	5.62	5.00	6.36	10.0	+30.0	2.74	27.10	246.6	+82.20	17.20	139.7
"	9.19	10.00	10.81	/	+1.2	1.64	/	162.0	+1.90	-8.10	54.4
Top burn	6.45	9.00	11.17	14.9	-35.5	4.22	62.80	359.2	-150.00	-159.00	-96.5
Outcrop	8.77	10.00	11.27	28.6	-45.3	2.45	70.00	175.00	-111.00	-121.00	-58.5
Slope	11.32	6.00	10.66	24.6	-43.0	9.38	230.8	707.20	-404.00	-410.00	-327.5
											(-352.0)
Slope	3.45	5.00	6.56	4.7	-21.1	3.11	14.6	296.4	-65.60	-70.60	-422.60
Valley floor	1.43	6.00	10.04	2.78	-14.6	8.11	17.7	793.3	-118.50	-124.50	-476.50
Split check	1.45	6.00	10.54	2.18	-14.5	9.09	19.8	889.2	-131.80	-137.80	-489.80
Creek	2.52	6.00	9.47	6.3	-24.1	6.94	38.7	655.3	-167.10	-173.10	-525.10
"	1.64	5.00	8.37	9.1	-28.8	6.73	61.20	611.8	-193.80	-198.80	-550.80
											(-555.00)
Slope	2.33	5.00	7.67	7.5	+26.3	5.34	40.00	494.00	+140.80	+135.80	-419.20
"	6.10	8.00	9.90	76	+8.7	3.80	3.00	377.0	+33.20	+25.00	-530.00
Other side creek	4.37	6.00	7.63	.89	+9.2	3.26	3.00	323.0	+30.00	+24.00	-531.00
"	3.19	5.00	6.80	/	-1.6	3.61	/	261.0	-5.80	-10.80	-565.80

$$\begin{array}{r} 7.73 \\ 14.28 \\ \hline 345 \end{array}$$

$$\begin{array}{r} 345 \\ 5.5 \\ \hline 2395 \end{array}$$

$$\begin{array}{r} 600 \\ 6.6 \\ \hline 593.4 \end{array}$$

$$\begin{array}{r} 3.66 \\ 2.34 \\ \hline 1.32 \end{array}$$

$$\begin{array}{r} 132 \\ 4.5 \\ \hline 127.5 \end{array}$$

$$\begin{array}{r} 120 \\ 14.8 \\ \hline 105.2 \end{array}$$

$$\begin{array}{r} 11.46 \\ 8.53 \\ \hline 2.93 \end{array}$$

$$\begin{array}{r} 293 \\ 9.7 \\ \hline 283.3 \end{array}$$

$$\begin{array}{r} 783 \\ 46.2 \\ \hline 736.8 \end{array}$$

$$\begin{array}{r} 5.82 \\ 4.77 \\ \hline 1.65 \end{array}$$

$$\begin{array}{r} 619.5 \\ 178 \\ \hline 441.5 \end{array}$$

$$\begin{array}{r} 165 \\ 2.7 \\ \hline 162.3 \end{array}$$

$$\begin{array}{r} 9.92 \\ 2.09 \\ \hline 7.83 \\ 3.92 \\ \hline 6.6 \end{array}$$



$$\begin{array}{r} 1156 \\ 843 \\ \hline 313 \\ 157 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 313 \\ 63.2 \\ \hline 249.8 \end{array}$$

$$\begin{array}{r} 790 \\ 410 \\ \hline 380 \end{array}$$

$$\begin{array}{r} 380 \\ 8.5 \\ \hline 371.5 \end{array}$$

$$\begin{array}{r} 444.5 \\ 62.6 \\ \hline 381.9 \end{array}$$

$$\begin{array}{r} 8.22 \\ 1.78 \\ \hline 644 \\ \hline 322 \end{array}$$

$$\begin{array}{r} 322 \\ 20.6 \\ \hline 301.4 \end{array}$$

$$\begin{array}{r} 475.55 \\ \$4.15 \\ \hline 444.50 \\ \hline 135.90 \\ \hline 308.60 \end{array}$$

$$\begin{array}{r} 435 \\ 40 \\ \hline 395 \end{array}$$

$$\begin{array}{r} 644 \\ 23.3 \\ \hline 620.7 \end{array}$$

$$\begin{array}{r} 444.5 \\ 126 \\ \hline 318.5 \end{array}$$

$$\begin{array}{r} 6.61 \\ 2.39 \\ \hline 3.22 \end{array}$$

$$\begin{array}{r} 208 \\ 50 \\ \hline 158 \end{array}$$

$$\begin{array}{r} 480 \\ 43.2 \\ \hline 436.8 \end{array}$$

$$\begin{array}{r} 7.8 \\ 2.83 \\ \hline 4.35 \end{array}$$

$$\begin{array}{r} 9.88 \\ 6 \\ \hline 388 \\ \hline 776 \end{array}$$

$$\begin{array}{r} 7.04 \\ 4.96 \\ \hline 2.08 \end{array}$$

$$\begin{array}{r} 569.50 \\ 94.80 \\ \hline 464.70 \end{array}$$

$$\begin{array}{r} 8.22 \\ 3.78 \\ \hline 4.44 \end{array}$$

$$41$$

$$\begin{array}{r} 790 \\ 83 \\ \hline 707 \end{array}$$

$$\begin{array}{r} 11.67 \\ 4.34 \\ \hline 7.33 \\ \hline 367 \\ \hline 801 \end{array}$$

$$\begin{array}{r} 9.95 \\ 2.05 \\ \hline 790 \\ \hline 395 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 9.54 \\ 48 \\ \hline 906 \\ \hline 453 \\ \hline 501 \end{array}$$

$$\begin{array}{r} 733 \\ 7.7 \\ \hline 725.7 \end{array}$$

$$\begin{array}{r} 9.42 \\ 4.62 \\ \hline 4.80 \\ \hline 2.40 \\ \hline 702 \end{array}$$

$$\begin{array}{r} 906 \\ 65.2 \\ \hline 840.8 \end{array}$$

$$\begin{array}{r} 246 \\ 68.7 \\ \hline 227.3 \end{array}$$

$$\begin{array}{r} 250 \\ 51.2 \\ \hline 198.8 \end{array}$$

$$\begin{array}{r} 7.94 \\ 4.06 \\ \hline 388 \end{array}$$

$$\begin{array}{r} 388 \\ 40.4 \\ \hline 347.6 \end{array}$$

$$\begin{array}{r} 748 \\ 4.52 \\ \hline 296 \\ \hline 148 \end{array}$$

$$\begin{array}{r} 9.25 \\ 6.75 \\ \hline 2.50 \end{array}$$

Wednesday 27<sup>th</sup> Aug 400, 800, 1200 Base line  
+ Kopjes.

(+444.50)

Outcrop from 2500	8.43	10.00	11.58	20.2	-40.2	3.13	63.20	249.8	-125.90	-135.90	308.60
"	4.10	6.00	7.95	2.24	-14.9	3.80	8.50	371.5	-56.60	-62.60	387.90
"	1.78	5.00	8.22	3.62	-18.8	6.44	23.30	620.70	-121.00	-126.00	318.50
"	3.34	5.00	6.61	6.40	+24.3	3.22	20.60	301.40	+78.20	+73.20	517.70
Slope	2.83	5.00	7.18	9.2	+28.9	4.35	40.00	395.00	-125.80	+120.80	565.30
(1569.50)											
A 400 N from slope	4.96	6.00	7.04	26.00	-42.7	2.08	50.00	158.00	-88.80	-94.80	464.70
800 N before down	3.78	6.00	8.22	.45	-4.8	4.41	2.00	442.00	+30.20	-36.20	533.30
Chir Basal	4.37	6.00	9.88	/	+4.8	7.76	/	776.00	+37.20	+31.20	600.70
Peak	0.48	8.00	11.67	11.0	+10.0	7.33	7.30	725.70	+73.30	+65.30	634.80
"	2.05	5.00	9.54	7.2	+25.8	9.06	65.20	840.80	+234.00	+229.00	799.50
"	2.05	6.00	9.95	10.5	+30.6	7.94	83.00	1071.00	+242.00	+236.00	805.50
Crest	4.62	7.00	9.42	9.0	+28.5	4.80	43.20	436.80	+137.00	+130.00	699.50
Peak	4.52	6.00	7.48	23.2	+42.3	2.96	68.70	227.3	+125.20	+119.20	688.70
Crest	6.75	8.00	9.25	20.5	+40.4	2.50	51.20	198.8	+101.00	+93.80	662.70
GAP -	4.06	6.00	7.94	10.4	+30.5	3.88	40.40	347.60	+118.30	+112.30	681.80

$$\begin{array}{r} 6.54 \\ 3.47 \\ \hline 3.07 \\ 28.2 \\ \hline 278.0 \end{array}$$

$$\begin{array}{r} 6.94 \\ 3.06 \\ \hline 3.88 \end{array}$$

$$\begin{array}{r} 388 \\ 12.6 \\ \hline 375.4 \end{array}$$

$$\begin{array}{r} 6.66 \\ 5.34 \\ \hline 1.32 \end{array}$$

$$\begin{array}{r} 13.2 \\ 1.7 \\ \hline 11.5 \end{array}$$

$$\begin{array}{r} 7.50 \\ 4.51 \\ \hline 2.99 \end{array}$$

$$\begin{array}{r} 299 \\ 7.7 \\ \hline 291.3 \end{array}$$

$$\begin{array}{r} 700 \\ 3.6 \\ \hline 696.4 \end{array}$$

$$\begin{array}{r} 10.90 \\ 1.10 \\ \hline 9.80 \end{array}$$

$$\begin{array}{r} 8.5 \\ 1.5 \\ \hline 7.0 \\ 5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 7.28 \\ 2.73 \\ \hline 4.55 \end{array}$$

$$\begin{array}{r} 8.88 \\ 3.12 \\ \hline 5.76 \\ 2.88 \\ \hline 5.95 \end{array}$$

$$\begin{array}{r} 572 \\ 5.7 \\ \hline 570.3 \end{array}$$

$$\begin{array}{r} 1.000 \\ 10 \end{array}$$

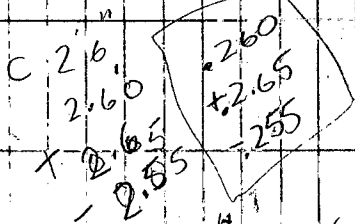
sin & cos  
sum

$$\begin{array}{r} 26 \\ 25 \\ \hline 01 \end{array}$$

5.000

$$2 \times (0.010)$$

$$\begin{array}{r} .005 \\ 2.55 \\ \hline 260 \end{array}$$



$$\begin{array}{r} 10.000 \\ 0.75 \\ \hline 9.925 \end{array}$$

$$\begin{array}{r} 5.00 \\ 33.47 \\ \hline 1.53 \end{array}$$



265 | 260 | 255 | (4.58) | 75 | -8.7 | 100 | 0.75 | 9.925 | -870 | 1.53

Gap	3.47	5.00	6.54	9.2	+29.00	3.07	28.20	278.80	+89.00	+84.00	653.50
Base Cliff	3.06	5.00	6.94	3.24	+17.8	3.88	12.60	375.40	+69.00	+64.00	633.50
"	5.34	6.00	6.64	18.9	+33.51	1.32	11.00	115.00	+44.20	+38.20	607.70
"	1.51	6.00	7.50	2.4	+15.2	2.99	7.70	291.30	+45.40	+39.40	608.90
											(658.50)
Outcrop from gap	1.10	6.00	10.90	1.8	-4.1	9.80	2.00	978.00	-40.20	-16.20	612.30
total slope	1.50	5.00	8.50	5.1	-7.1	7.00	31.57	696.40	-49.70	-54.70	603.80
total outcrop	2.73	5.00	7.28	9.0	+9.4	4.55	4.10	450.90	-12.80	-47.80	610.70
out/BLUE	3.12	6.00	8.88	9.9	+9.9	5.76	5.70	570.30	-57.00	-63.00	595.50

[500E on ridge crest.]

Wednesday 27<sup>th</sup> Aug - 400, 800, 1200 Base line  
+ Koppes

$$\begin{array}{r} 2.46 \\ 73 \\ \hline 5.53 \end{array}$$

$$\begin{array}{r} 253 \\ 212 \\ \hline 231.8 \end{array}$$

$$\begin{array}{r} 11.73 \\ 10.60 \\ \hline 1.13 \\ \hline 226 \end{array}$$

$$\begin{array}{r} 16.5 \\ 10.6 \\ \hline 26.9 \end{array}$$

$$\begin{array}{r} 600.00 \\ 26.9 \\ \hline 573.1 \end{array}$$

$$\begin{array}{r} 7.68 \\ 2.32 \\ \hline 5.36 \end{array}$$

$$\begin{array}{r} 45 \\ 600 \\ 72 \\ \hline 527.9 \end{array}$$

$$\begin{array}{r} 11.29 \\ 8.8 \\ \hline 4.4 \end{array}$$

$$\begin{array}{r} 577.7 \\ 130.9 \\ \hline 446.8 \end{array}$$

$$\begin{array}{r} 440 \\ 36.6 \\ \hline 403.4 \end{array}$$

$$\begin{array}{r} 7.94 \\ 6.05 \\ \hline 1.89 \\ \hline .95 \\ 0 \end{array}$$

$$\begin{array}{r} 3.22 \\ 36.7 \\ \hline 285.8 \end{array}$$

$$\begin{array}{r} 9.36 \\ 6.67 \\ \hline 2.69 \end{array}$$

$$\begin{array}{r} 11.65 \\ 4.35 \\ \hline 7.30 \\ 3.65 \\ \hline 8.90 \end{array}$$

$$\begin{array}{r} 1.61 \\ 2 \\ \hline 3.22 \end{array}$$

$$\begin{array}{r} 1.61 \\ 10.39 \\ \hline \end{array}$$

$$\begin{array}{r} 189 \\ 45.4 \\ \hline 143.6 \end{array}$$

$$\begin{array}{r} 7.88 \\ 2.12 \\ \hline 5.76 \\ 2.88 \\ \hline 4.92 \end{array}$$

$$\begin{array}{r} 7.88 \\ 2.12 \\ \hline 5.76 \\ 2.88 \\ \hline 5.00 \end{array}$$

$$\begin{array}{r} 100.10 \\ 10.49 \\ \hline 89.7 \end{array}$$

$$\begin{array}{r} 269 \\ 41.9 \\ \hline 207.1 \end{array}$$

$$\begin{array}{r} 528.5 \\ 326.2 \\ \hline 202.3 \end{array}$$

$$\begin{array}{r} 8.44 \\ 3.57 \\ \hline 4.87 \end{array}$$

$$\begin{array}{r} 487 \\ 116.4 \\ \hline 370.6 \end{array}$$

$$\begin{array}{r} 528.50 \\ 213.60 \\ \hline 314.90 \end{array}$$

① N95°W / S7°E

$$\begin{array}{r} 730 \\ 186.1 \\ \hline 543.9 \end{array}$$

Hump	-79	2.00	3.26	8.4	+27.7	2.53	21.20	231.8	-70.10	-72.10	+600.00	527.90
Base outcrop	/	10.60	11.73	5.0	-7.12	2.26	1.00	225.00	-16.30	-26.90		513.10
Outcrop	6.80	9.00	11.20	8.3	-27.7	4.40	36.60	403.40	-121.90	-130.90	(577.70)	446.8
Δ												
4005/1000E	6.05	7.00	7.94	24.0	-42.7	1.89	45.40	143.6	-80.70	-87.70		490.00
Scop	2.12	5.00	7.88	7.0	-8.4	5.76	4.00	572.00	-48.40	-53.40		524.30
Knife edge	3.00	6.00	9.00	/	+3.4	6.00	-	600.00	+20.40	+14.40	(+528.50)	542.90
m	2.32	5.00	7.68	1.61	+7.9	5.36	3.00	533.00	+42.30	+37.30		565.80
n	/	(10.39)	0.00	10.9	+31.1	3.22	36.20	285.80	+100.10	+89.10		618.20
	6.67	8.00	9.36	23.0	+42.1	2.69	61.90	257.10	+113.20	+105.20		633.70
Δ												
8005/1000E	3.57	6.00	8.44	23.9	-42.6	4.87	116.40	370.60	-207.60	-213.60		314.90
Δ												
12003/1000E	4.35	8.00	11.65	25.5	-43.6	7.30	186.10	543.90	-318.20	-326.20		202.30
	2.1											

THURS 28<sup>th</sup> AUG - East Cirque + grid lines

$$\begin{array}{r} 11.47 \\ 4.57 \\ \hline 6.90 \\ 3.45 \\ \hline 8.05 \end{array}$$
$$\begin{array}{r} 11.17 \\ 4.83 \\ \hline 6.34 \\ 3.17 \\ \hline 8.0.0 \end{array}$$
$$\begin{array}{r} 634 \\ 157.1 \\ \hline 476.0 \end{array}$$
$$\begin{array}{r} 202.30 \\ 8.7 \\ \hline 206.0 \end{array}$$
$$\begin{array}{r} 9.12 \\ 2.80 \\ \hline 6.24 \end{array}$$
$$\begin{array}{r} 7.22 \\ 2.78 \\ \hline 4.44 \end{array}$$
$$\begin{array}{r} 338 \\ 12.6 \\ \hline 325.4 \end{array}$$
$$\begin{array}{r} 690 \\ 130.9 \\ \hline 559.1 \end{array}$$
$$\begin{array}{r} 9.68 \\ 2.32 \\ \hline 7.36 \end{array}$$
$$\begin{array}{r} 736 \\ 39.8 \\ \hline 696.2 \end{array}$$
$$\begin{array}{r} 6.00 \\ 2.62 \\ \hline 3.38 \end{array}$$
$$\begin{array}{r} 9.46 \\ 6.00 \\ \hline 3.46 \end{array}$$
$$\begin{array}{r} 8.39 \\ 1.61 \\ \hline 6.78 \\ 3.39 \\ \hline 5.00 \end{array}$$
$$\begin{array}{r} 678 \\ 102.5 \\ \hline 575.5 \end{array}$$
$$\begin{array}{r} 624 \\ 31.8 \\ \hline 592.2 \end{array}$$
$$\begin{array}{r} 206.0 \\ 18.8 \\ \hline 187.2 \end{array}$$
$$\begin{array}{r} 9.46 \\ 2.62 \\ \hline 7.84 \end{array}$$
$$\begin{array}{r} 392 \\ 6.54 \\ \hline \end{array}$$
$$\begin{array}{r} 9.46 \\ 2.62 \\ \hline 7.84 \end{array}$$
$$\begin{array}{r} 6.84 \\ 3.42 \\ \hline 6.04 \end{array}$$
$$\begin{array}{r} 11.90 \\ 2.10 \\ \hline 9.80 \\ 4.90 \\ \hline 7.00 \end{array}$$
$$\begin{array}{r} 206 \\ 176.90 \\ \hline 29.1 \end{array}$$
$$\begin{array}{r} 4.68 \\ 1.30 \\ \hline 3.38 \\ 1.69 \\ \hline 2.99 \end{array}$$
$$\begin{array}{r} 9.90 \\ 2.12 \\ \hline 7.78 \end{array}$$
$$\begin{array}{r} 684 \\ 45.8 \\ \hline 638.2 \end{array}$$
$$\begin{array}{r} 392 \\ 6.54 \\ \hline \end{array}$$
$$\begin{array}{r} 980 \\ 21.6 \\ \hline 958.4 \end{array}$$

DUF TOP	4.83	0.00	11.17	24.8	+43.2	6.34	157.10	476.90	+274.00	+266.00	472.00
"	4.57	8.00	11.47	19.1	+39.4	6.90	131.90	559.10	+272.00	+264.00	470.00
"	1.61	5.00	8.39	15.1	+35.8	6.78	102.50	575.50	+243.00	+238.00	444.00
"	2.88	6.00	9.12	5.1	+22.0	6.24	31.80	592.2	+137.10	+131.10	337.10
"	2.32	6.00	9.68	5.4	+22.6	7.36	39.80	696.20	+166.30	+160.30	366.30
Base Slope	2.78	5.00	7.22	/	-3.1	4.40	/	444.00	-13.80	-18.80	187.20
Δ 1600S/1000E	1.30	3.00	4.68	3.72	-19.0	3.38	12.60	325.40	-57.00	-60.00	146.00
Claim posts	2.52	6.00	9.46	6.70	-25.00	6.34	45.80	638.20	-170.90	-176.90	29.10
Δ 2000S/1000E	2.12	6.00	9.90	15.1	+7.2	7.78	4.00	774.00	+56.00	+50.00	256.00
Bulge	2.10	7.00	11.90	2.2	+4.1	9.80	21.60	958.40	+138.10	+131.10	337.10

THURS 28<sup>th</sup> AUG - EAST CIRQUE S GRID LINES

$$\begin{array}{r}
 3.98 \\
 2.03 \\
 \hline
 1.95 \\
 9.80 \\
 \hline
 4.85 \\
 5.60
 \end{array}$$

$$\begin{array}{r}
 6.03 \\
 3.95 \\
 \hline
 2.08 \\
 1.54 \\
 \hline
 1.04 \\
 1.99
 \end{array}$$

$$\begin{array}{r}
 6.03 \\
 3.95 \\
 \hline
 2.08 \\
 1.04 \\
 \hline
 4.99
 \end{array}$$

$$\begin{array}{r}
 9.27 \\
 6.77 \\
 \hline
 2.56
 \end{array}$$

$$\begin{array}{r}
 10.55 \\
 3.45 \\
 \hline
 7.10 \\
 3.55 \\
 7
 \end{array}$$

$$\begin{array}{r}
 7.08 \\
 4.90 \\
 \hline
 2.16 \\
 7.10 \\
 4.9 \\
 \hline
 668.1
 \end{array}$$

$$\begin{array}{r}
 537.70 \\
 4.70 \\
 \hline
 341.80
 \end{array}$$

Bulge	2:03	3.00	3.98	$\frac{1.6}{1.50}$	+12.5	1.95	3.00	192.00	+24.4	+23.40	363.20
2400s/1000E	2:45	5.00	6.03	3.72	+19.0	2.08	8.00	200.00	+39.60	+34.60	<del>327.20</del> 376.40
Ridge	3:45	7.00	10.55	5.9	+23.5	7.10	41.90	668.10	+166.90	+159.90	501.70
Creek	4:20	7.00	9.80	4.48	+26.9	5.60	25.00	535.00	+117.00	+110.00	+51.80
2400s/800E	4:42	6.00	7.08	3.06	+17.2	2.16	7.00	209.00	+37.20	+31.20	373.00
Creek	6:11	8.00	9.27	/	-4.7	2.56	/	256.00	-12.10	-20.10	321.70

(+341.80)

TURNS 28<sup>1/2</sup> AVG - EAST CIRCUE  $\frac{1}{2}$  GRID LINES

$$\begin{array}{r} 5.62 \\ 4.37 \\ \hline 1.25 \end{array}$$

$$\begin{array}{r} 9.82 \\ 6.16 \\ \hline 3.66 \end{array}$$

$$\begin{array}{r} 366 \\ 82.4 \\ \hline 283.6 \end{array}$$

$$\begin{array}{r} 601.70 \\ 161.10 \\ \hline 440.6 \end{array}$$

$$\begin{array}{r} 11.74 \\ 10.26 \\ \hline 1.48 \end{array}$$

$$\begin{array}{r} 597.70 \\ 4 \\ \hline 594.70 \end{array}$$

$$\begin{array}{r} 7.82 \\ 6.18 \\ \hline 1.64 \end{array}$$

$$\begin{array}{r} 164 \\ 36.6 \\ \hline 127.4 \end{array}$$

$$\begin{array}{r} 268 \\ 48.5 \\ \hline 219.5 \end{array}$$

$$\begin{array}{r} 10.33 \\ 7.65 \\ \hline 2.68 \\ 1.34 \\ \hline 3.99 \end{array}$$

$$\begin{array}{r} 695.8 \\ 4.2 \\ \hline 700.0 \end{array}$$

$$\begin{array}{r} 745.8 \\ 5.0 \\ \hline 770.8 \\ 92 \\ \hline 678.8 \end{array}$$

$$\begin{array}{r} 6.32 \\ 5.68 \\ \hline .64 \end{array}$$

$$\begin{array}{r} 2.92 \\ 1.07 \\ \hline 1.85 \end{array}$$

$$\begin{array}{r} 185 \\ 72 \\ \hline 113 \end{array}$$

$$\begin{array}{r} 7.05 \\ 4.95 \\ \hline 2.10 \end{array}$$

$$\begin{array}{r} 210 \\ 17.8 \\ \hline 192.2 \end{array}$$

$$\begin{array}{r} 4.57 \\ 1.37 \\ \hline 3.20 \\ 60 \\ \hline 297 \end{array}$$

$$\begin{array}{r} 320 \\ 40.8 \\ \hline 279.2 \end{array}$$

$$\begin{array}{r} 710.8 \\ 114 \\ \hline 596.8 \end{array}$$

$$\begin{array}{r} 710.8 \\ 172.2 \\ \hline 538.6 \end{array}$$

$$\begin{array}{r} 9.30 \\ .68 \\ \hline 8.62 \\ 43 \\ \hline 49 \end{array}$$

$$\begin{array}{r} 5.45 \\ .51 \\ \hline 4.94 \\ 2.47 \\ \hline 2.47 \\ 198 \end{array}$$

$$\begin{array}{r} 494 \\ 71.1 \\ \hline 422.9 \end{array}$$

$$\begin{array}{r} 710.8 \\ 329 \\ \hline 381.8 \end{array}$$

$$\begin{array}{r} 862 \\ 146.6 \\ \hline 715.4 \end{array}$$



KITCHEN.

4 slabs bacon  
 4 cases eggs.  
 1 case milk  
 1 bail coffee (24)  
 1 plunger washer.  
 1 wash tub.

1 case grape fruit pieces  
 1 case paper-cups.  
 Butcher twine  
 Spices  
 2 Cases small apple juice  
 2 Cases small orange crush  
 2 Cases trio instant potato  
 2 Case peaches  
 " cherries  
 " pears

NAILS

1 2 lbs 4" nails  
 2 1/2 lbs 1 1/4"  
 1 2 lbs 2"

2 cases Cola cola.  
 Chocolate bars  
 Bakers semi-sweet choc  
 Fresh fruit  
 Canned vegetables.

SAM MCCLOUD 1 carton players filter.  
 CHARLIE OLIE 2 carton Export A filter  
 LIVINGSTON JOHNSON 1 pair large leather gloves.  
 - 1 sack knife  
 LEE TURNER - 1 can export cig tobacco  
 3 Vogue papers  
 2 Cartons No 7 large cigs.

2 swede saws.  
 8 bars hand soap.  
 3 5gal cans naphtha  
 1 10 x 12 fly  
 1 14 x 16 fly.  
 6 machetes.

Coleman lamp mantles. & Tbb generator  
 8 wooden cots & foamies.  
 6 cases orange flagging  
 Couple of compasses.  
 2 axes  
 1 box files  
 3 camp stoves  
 200ft rope  
 Speed sew

Casino  
Airstrip

11.15 - 11.30 am

John Brock  
Gordon Davis

Sam McLeod

Livingston Johnson

→ Peter Foy

Charlie Olie

→ Lee Turner

- 2 Bottles Dutch Cleaners
- 1 can Vogue Tobacco - A Gray
- 1 sack Potatoes
- 6 Shaker cans Salt
- 1 case Strawberries
- 1 case Cherries
- 1 case Peaches
- 6 Bottles Ketchup
- 4 Boxes Crackers
- 1 gallon Mayola oil

The Minstrels sing of an English King  
Who lived long years ago.  
He ruled his land with an Iron hand  
But his mind was mighty slow.  
He was very fond of hunting  
Out in the Royal Wood.  
And very fond of pulling  
Of pulling his Royal Hood.  
Oh God how he pulled his hood  
All the clothes he wore was a  
woolen under-shirt  
with which he tried to hide the  
hide  
But he couldn't hide the shirt.  
Now the Queen of Spain was  
a spiffy old dame  
and the spiffy old dame was  
she  
She loved to fool with a  
master's tool  
From far across the sea,  
She sent a royal message  
with a Royal messenger  
Inviting the King of England  
To spend a month with her.  
Now Philip of France when he  
heard the news.  
He said to his Royal Court

I guess she ~~is~~ prefers my  
rival

Because my horn is short.

So he sent the Duke of York  
to give the queen a dose of clap  
that would cripple ~~the~~ dear old  
England.

When the news of this foul  
deed was noised

around Westminster halls,

The king he swore by the shirt  
he wore,

He would have that Frenchman's  
balls.

So he offered half his kingdom  
and the whole of the Royal Hostens

to any loyal Englishman  
who would meet the King of France

Then the loyal Duke of Essex

Retook himself to France

He swore he was a fakir

so the king took down his pa

about his doing he place a

thing.

Then Merivie Murrity galloped  
Along.

Back to the throne of England  
The king threw up his breakfast  
And he bit right on the  
floor.

For in that ride the Lurchman  
Pride

Had stretched a yard or more.

And all the ladies of London

town

Said "To hell with the British  
Crown

So Phillip of France usurped  
The throne of England.

0 10 20 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23

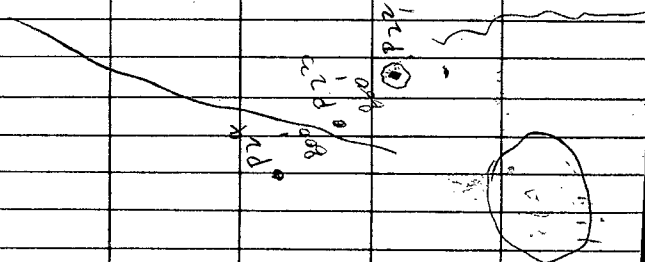
$$\begin{array}{r} 9 \\ \hline 9 \\ \hline 5 \\ \hline 2 \\ \hline 1 \end{array}$$

Camp 1 (Dog)

Sample

11.12  
3.30  
2.5  
2.5

16.04  
16.15  
16.30  
16.45



Qtz/bio sch

Qtz/bio sch  
(mit/br skarn) .02

Qtz/bio sch

plastic bag 0-5

SKARN 1.05

SKARN .12

SKARN .24  
gossan

Backsack 5-10

SKARN 1.47

SKARN .09

SKARN .09

Back Pocket 10-15

SKARN .04

SKARN .87

SKARN .11  
gossan

Red Side pocket 15-20

Quartzite .02

gossan

SKARN .05

SKARN .31

Other side pocket 20-25

SKARN .02

100N

GD

7505

Jacket 25-30

SKARN .02

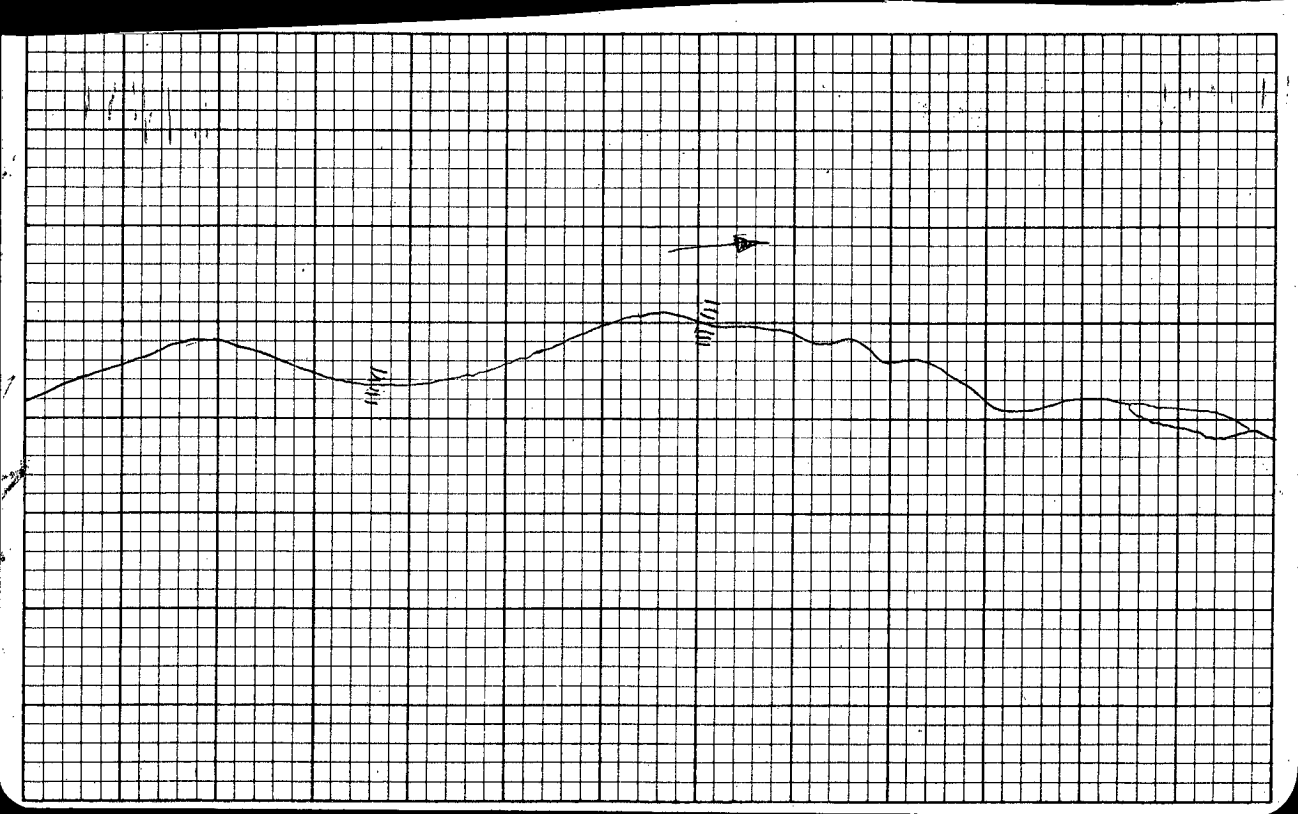
GD

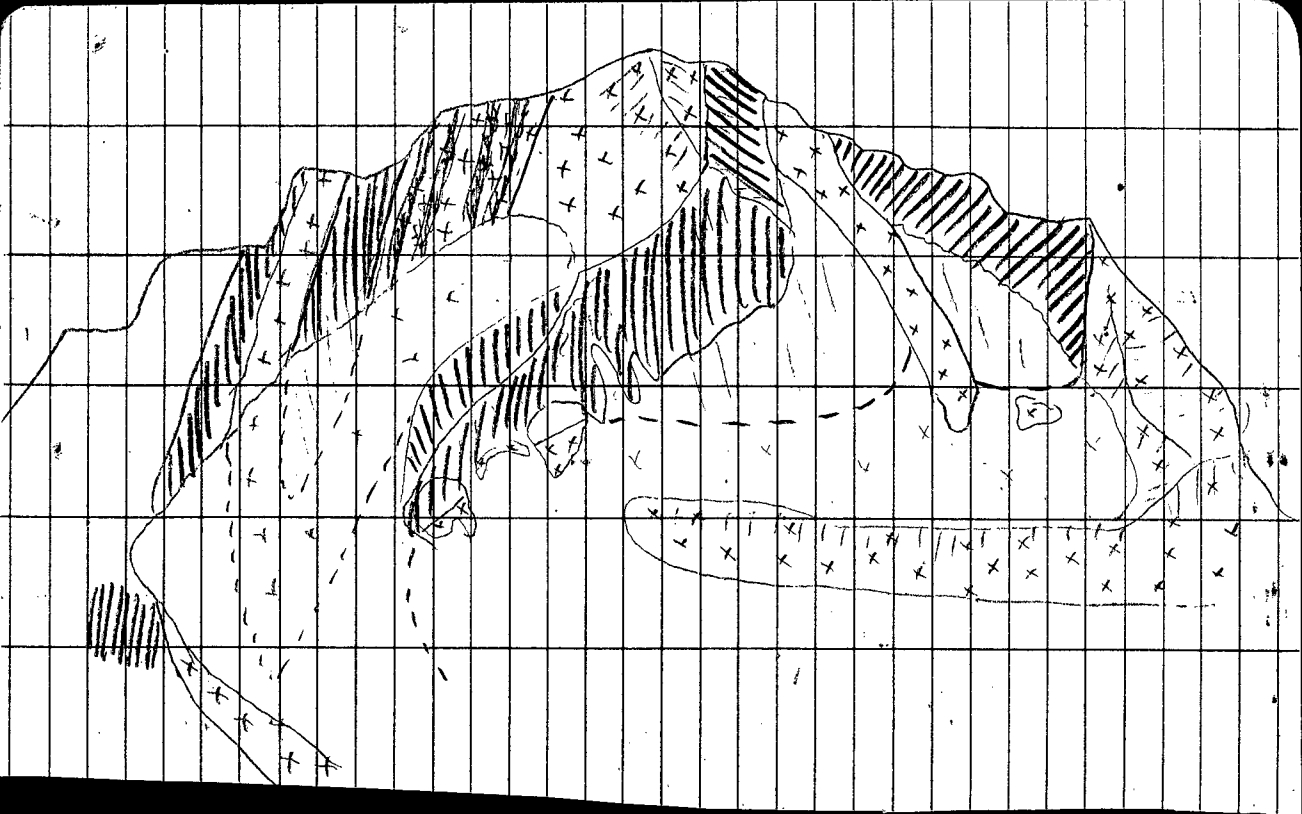
1300

Bottom

2400 N

- ① 5' heavy gossan + fq dissemin sch. middle of 15' gossaned  
bio/qtz sch.
- ② 2' heavy gossan + fq dissemin sch. 2' limestone band  
below, 4' gossaned bio/qtz sch above
- ③ 1' heavy gossan + fq dissemin sch. 3' gossaned  
Skarn above, GD contact below



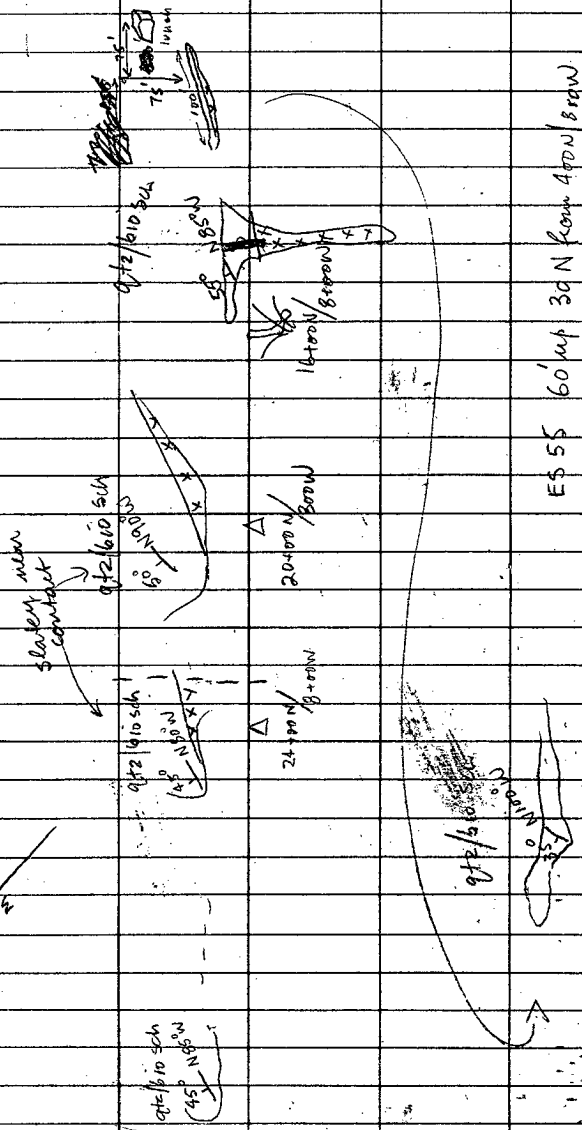
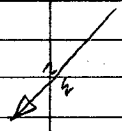


# GEOLOGY NOTES (bedding wye MN)

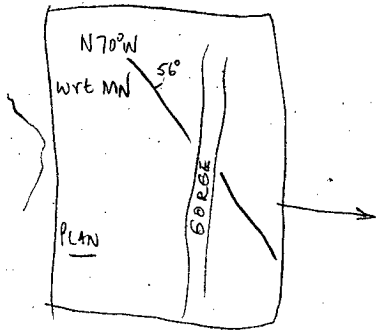
No 1 Orebody Gossan/Sch-diorite Contact N20°W

TUES 19<sup>th</sup> Aug 1969

W.Y.E. Magnetic North



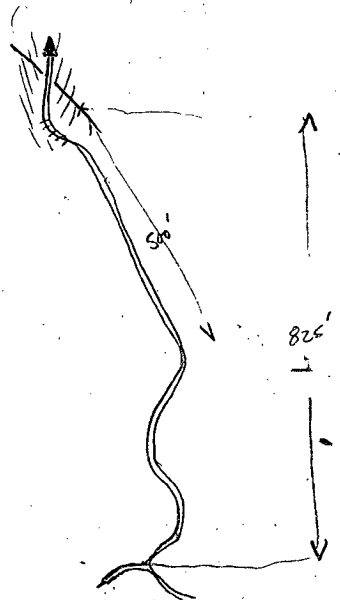
ES 55 60' up 30N from 400N/800W



$\frac{3165}{825}$



$$\begin{aligned}
 x &= 70 - 35 \\
 &= N 35^\circ W \text{ wrt. TN} \\
 &= 360 - 35 \\
 &= 325 (-180) \\
 &= \underline{\underline{145^\circ}}
 \end{aligned}$$



Charlie Wicks 2<sup>nd</sup> July to 22<sup>nd</sup> Aug.

Ray Wells 25<sup>th</sup> to 31<sup>st</sup> Aug

Harry Atkinson 31<sup>st</sup> Aug to