

020587

LINE 2	W	HI	LO		DIFF	
STN	C	H	C	H	HI	LO
20 1/2 S	12	6	7			
101 + 1/2 N	-12	+6	-10	+6	-6	-4
103 + ↓	15	10	11	10	-5	-1
105 +	9	10	10	11	+1	+1
107 +	11	7	10	8	-4	-2
109 +	8	4	7	9	-4	-3
111 +	7	2	7	3	-5	-5
113 +	8	4	7	5	4	2
115 +	9	5	9	5	4	4
117 +	12	7	11	7	5	4
119 +	9	3	9	3	6	6
121 +	11	5	10	5	6	5
123 +	12	4	11	5	8	6
125 +	10	5	8	5	5	3

Crests

June 56 N

98 + 1/2 N	-8	+2	-6	+3	-6	-3
96 + ↓	8	2	7	3	6	4
99 +	8	3	6	3	5	3
92 +	8	12	7	2	6	5
	7	0	6	0	7	6
	5	2	-4	-1	-7	-5
	-8	0	-7	+1	-8	-6
	-11	-4	-7	-2	-15	-9
	-11	-10	-8	-3	-21	-11
	-12	-15	-7	-6	-27	-13
	-8	-20	-4	-12	-28	16
	-5	-26	0	-20	31	20
	0	-27	+6	-23	-27	-17
	+8	-34	+13	-26	-26	+3
	+13	-30	+17	-26	-17	9
	+15	-28	+18	-21	-13	3
	+15	-20	+16	-17	-5	-1

Poor NULS →

LINE#	STN	C	H	C	H	Diff	20
		+8	-15	+10	-15	-7	-5
		6	10	8	10	-4	-2
		0	-12	+3	-9	-12	-6
		-3	-5	-1	-1	-8	-2
		-13	-10	-6	0	-23	-6
		-10	-15	-5	-2	-25	-7
		-13	-15	-7	-5	-28	-12
		-14	-12	-6	-2	-26	-8
		-16	-14	-8	0	-30	-8
		19	10	9	0	-29	-9
		-18	-10	-9	0	-28	-9
		-20	-6	-10	+2	-26	-8
		-21	0	-13	+5	-21	-8
		-20	+6	-14	+8	-14	-6
		-17	+4	-12	+6	-13	-6
		-13	0	-10	+2	-13	-8
		-14	0	-10	+3	-14	-7
		-15	0	-12	+4	-15	-8
		-16	-2	-12	0	-18	-12
		-14	-3	-9	0	-17	-9
		-10	-2	-8	+2	-14	-6
		-8	-4	-5	0	-12	-5
		-9	-6	-6	-1	-15	-7

LINE #	4	H ₁	L ₀	Diff		
STN	C	H	C	H	H ₁	L ₀
10+ $\frac{1}{2}$ N	-17	+17	-17	+17	0	0
12+ \downarrow	10	11	10	11	+1	+1
14+	10	10	10	10	0	0
16+	16	16	16	16	0	0
18+	26	25	26	25	-1	-1
20+	38	38	38	38	0	0
22+	Granite outcropping					
26+ $\frac{1}{2}$ S	-11	+11	-11	+11	0	0
29+ \downarrow	-10	+11	-10	+11	+1	+1
22+	-12	+10	-12	+10	-2	-2
20+	16	15	16	15	-1	-1
18+	12	10	12	10	-2	-2
16+	12	11	12	11	-1	-1
14+	14	10	10	10	-5	0
13+	12	9	10	9	-3	-1
12+	11	8	9	8	-3	-1
11+	11	8	10	8	-3	-2
10+	11	10	10	10	-1	0

STN	O		HI		Lo		Slip	
	C	H	C	H	H	H	HI	Lo
18 $\frac{1}{2}$ N	-18	+18	-17	+18	+18		0	+1
16 $\frac{1}{2}$ ↓	20	20	20	20	20		0	0
14+	15	14	15	14	14		-1	-1
12+	12	13	12	13	13		+1	+1
10+	36	36	36	36	36		0	0
8+	30	29	30	29	29		-1	-1
6+	12	13	12	13	13		+1	+1
4+	10	11	10	11	11		+1	+1
2+	9	5	7	5	5		-2	-2
1+	5	3	5	3	3		-2	-2
B.L. $\frac{1}{2}$ N.	9 $\frac{1}{2}$	9	9 $\frac{1}{2}$	9	9		- $\frac{1}{2}$	- $\frac{1}{2}$
$\frac{1}{2}$ S	9	9	9	9	9		0	0
↓								
2+	14	14	14	14	14		0	0
4+	15	14	15	14	14		-1	-1
6+	12	12	12	12	12		0	0
8+	13	12	13	12	12		-1	-1
10+	14	13	13	13	13		-1	0
12+	14	13	13	13	13		+1	0
14+	14	13	14	13	13		-1	-1
16+	15	15	15	15	15		0	0
18+	15	14	15	14	14		-1	-1
20+	16	15	16	15	15		-1	-1
22+	14	14	14	14	14		0	0
24+	14	13	14	13	13		-1	-1
26+	13	13	13	13	13		0	0

LINE 20 HI ACE LO Diff

STN	C	H	C	H	Hi	Lo.
1+ $\frac{1}{2}$ N	-25	+11	-20	+13	-14	-7
2+ \downarrow	-20	0	-12	+4	-20	-8
3+	-18	-2	-12	+5	-20	-7
4+	-25	+6	+20	+15	-19	-5
5+	39	20	34	30	-19	-4
6+	44	28	41	36	-16	-5
7+	-45	+34	-43	+38	-11	-5
8+	-34	+24	-32	+28	-10	-4
9+	34	22	30	26	-12	-4
10+	30	19	24	22	-11	-2
11+ $\frac{1}{2}$	42	31	38	31	-11	-7
12+0	-40	33	-36	34	-7	-2
12+ $\frac{1}{2}$	36	31	34	32	-5	-2
13+0	32	28	28	28	-4	0
13+ $\frac{1}{2}$	30	27	28	28	-3	0
14+0	24	21	23	22	-3	-1
14+	17	16	16	16	-1	0
15+	13	12	12	12	-1	0
16+	10	10	10	10	0	0
17+	17	15	16	15	-2	-1
18+	23	19	22	19	-4	-3
19+	23	23	23	23	0	0
20+	16	8	13	11		

TOP OF HILL

LINE #24	HI		LO		Diff	
STN.	e	H	C	H	HI	LO
18+	$\frac{1}{2}N-18$	+6	-15	+10	-12	-5
19+	$\checkmark-19$	+10	-15	+13	-9	-2
20+	-26	+ 15 ⁸	-13	+11	-8	-2
21+	-16	+10	-13	+12	-6	1
17+	-20	+5	-15	+10	-15	-5
16+	-24	+9	-18	+14	-15	-4
15+	-28	+14	-23	+17	-14	-6
14+	-28	+12	-22	+16	-16	-6
13+	27	9	19	13	-18	-6
12+	-25	+5	-18	+10	-20	-8
11+	-30	+10	-22	-15	-20	-7
10+	-30	12	24	18	-18	-6
9+	30	10	23	17	-20	-6
8+	25	4	18	12	-19	-6
7+	-22	-2	-16	+6	-24	-10
6+	-25	0	+20	-12	-25	-8
5+	29	0	26	+16	-29	-10
4+	-26	+4	-26	+15	-22	-11
3+	-18	+3	-14	+5	-15	-9
2+	-12	-6	-7	0	-18	-7
1+	-11	-6	-7	0	-17	-7
	-24	-12	-26	0		
22+	9	8	9	10	-1	1
23+	15	13	14	13	-2	-1
24+	16	15	15	15	-1	0
25	21	20	21	20	-1	-1
26	13	13	13	13	0	0

LINE #32

H¹L₀

Diff

ST.N.	H ¹		L ₀		Diff	
	e	H	e	H	H ¹	L ₀
1+ ¹ N	-24	-10	-26	0	-34	-26
2+ ¹ ↓	-24	-10	-23	0	-34	-23
3+	-24	-8	-22	+4	-32	-18
4+	-26	-2	-23	+8	-28	-15
5+	-29	+6	-25	+14	-23	-11
6+	-29	+10	-25	+20	-19	-5
7+	-27	+10	-23	+16	-17	-7
8+	-20	+8	-19	+15	-12	-2
9+	-20	+9	-15	+11	-11	-4
10+	-25	+8	18	12	-17	-6
11+	-23	+4	-17	+10	-19	-7
12+	-21	+2	-14	+10	-19	-4
13+	-19	+4	-12	+8	-15	-4
14+	-19	5	-12	+8	-14	-4
15+	-18	4	-12	+8	-14	-4
16+	-15	0	-10	+5	-15	-5
17+	-13	-2	-8	+4	-15	-4
18+	-15	0	-10	+2	-15	-8
19+						
20+						
21						
22						
23						
24						
25						
26						
27						
28						

Shale

LINE #		H ₁		L ₀		Diff
STN	C	H	C	H	H ₁	-0
18 + 1/2 N	-23	0	-16	+8	-23	-8
17 + 1/2 ↓	-25	+2	-17	+10	-23	-9
15 +	-26	+6	-19	+12	-20	-7
13 +	-27	+8	-19	+14	-19	-5
11 +	-32	+10	-24	+18	-22	-6
9 +	-23	0	-18	+12	-23	-6
7 +	-23	-2	-17	+8	-25	-9
5 +	-21	+2	-15	+8	-19	-7
3 +	-19	+5	-15	+10	-14	-5
1 +	-25	+2	-18	+10	-23	-8

BASE-LINE (300' spacing)

29 + 1/2 N	33	5	33	16	-28	-17
31 +	-25	-8	-25	+4	-33	-21
33 +	-20	-10	-19	-4	-30	-23
35 +	-23	-12	-20	-2	-35	-24
37 +	-23	-4	-21	+2	-27	-19

STN	
29 + 1/2	28 - 23 = 5
31 + 1/2	33 - 25 = 8
33 + 1/2	30 - 24 = 6
35 + 1/2	35 - 19 1/2 = 15 1/2
37 + 1/2	27 - 16 = 11

5 | 45
9

Average = -9
Diff =

LINE 285	H _i	L ₀		Diff		
STN	@	H	C	H	H _i	L ₀
1+ ¹ / ₂ S - 25		0	-24	+6	-25	-18
2+ ↓ → 24		0	-23	+6	-24	-17
3+	-29	+2	-28	+12	-27	-16
5+	-37	+8	-34	18	-29	-16
7+	-37	+4	-36	18	-33	-18
9+	-30	+20	-32	20	-10	-12
8+	-33	-2	-35	+14	-35	21
9+0.	-32	+4	-35	16	-28	-19
10+0.	-28	+22	-28	+20	-6	-8
10+ ¹ / ₂ .	-27	+12	-23	+12	-9	-11
11+	-16	-4	-21	+8	-20	-13
12+	-27	-2	-23	+8	-29	-15
14+	-19	+2	-17	+8	-17	-9
15+	-21	+9	-17	+10	-12	-7
16+	-16	+9	-13	+10	-7	-3
17+	-11	+8	-11	+10	-3	-1
18+	10	10	10	10	0	0
20+	20	19	20	19	-1	-1
22+	24	24	23	22	0	-1
24+	14	14	14	14	0	0
26+	20	20	20	20	0	0
28+	22	22	21	22	0	+1
30+	23	23	23	23	0	0
32	20	26	20	20	0	0
34	24	25	24	25	+1	+1
36	26	25	26	25	-1	-1
38	28	28	28	28	0	0
40	30	30	30	30	0	0

LINE	325	H ₁		60	Diff	
STN	C	H	C	H	H ₁	60
22+ $\frac{1}{2}$ S	-22	+21	-22	+21	-1	-1
20+ \downarrow	-14	+16	-14	+16	+2	+2
18+	9	9	9	9	0	0
16+	-1	-2	-2	+4	-3	+2
15+	-1	-2	-1	-2	-3	-3
14+	-15	-1	-8	-1	-16	9
13+	-19	-10	-10	0	-29	-10
12+	-17	-10	-14	+5	-17	-9
11+	-15	-2	-15	+5	-17	-10
10+	-21	0	-21	+6	-21	-15
9+	-23	-7	-23	+3	-30	-20
8+	-21	-10	-21	+2	-31	-19
7+	-21	+2	-21	+5	-19	-16
6+	-28	0	-25	+6	-28	-19
5+	-30	-14	-27	+3	-44	24
4+	-25	-12	-25	+3	-37	-22
3+	-28	-8	-26	+6	-36	-20
2+	-28	-6	-27	+2	-34	-25
1+	-31	-10	-22	-6	-31	-28

LINE 40

H₁L₀

Diff

STN	C	H	C	H	H ₁	L ₀
14½N	-20	-6	-15	0	-26	-15
2+	-19	-14	-15	-2	-33	-17
3+	-17	-17	-14	-7	-34	-21
5+	-26	-6	-24	0	-32	-24
7+	-25	-7	-24	+4	-32	-20
9+	-21	-2	-17	+4	-23	-13
11+	-15	-4	-12	+4	-19	-8
13+	-14	-4	-9	+2	-18	-7
15+	-15	-5	-8	+5	-20	-3
17+	-18	-4	-10	+5	-22	-5

LINE #	H1	LO	diff
STN	C	H	C H. Lo
18+ $\frac{1}{2}$ N	-13	+4	-10 +5 -9 -5
16+ \downarrow	-15	0	-11 4 -15 -7
14+	-14	-7	-10 0 -21 -10
12+	-16	-10	-12 -4 -26 -16
10+	-17	-18	-14 -12 -35 -26
8+	-21	-10	-19 -4 -31 -23
6+	-18	-12	-15 -3 -30 -18
4+	-18	-10	-14 -3 -28 -17
2+	-19	-8	-14 -2 -27 -16
13+ $\frac{1}{2}$ N	-21	-7	-16 0 -28 -16
1+ $\frac{1}{2}$ S	-21	-6	-16 +4 -27 -12
3+ \downarrow	-20	+5	-15 +9 -15 -6
5+	-15	+10	NOISY -12 +10 -5 -2
6+	-16	+10	NOISE -12 +12 -6 0
7+	-16	+10	NOISE -12 +10 -6 -1
8+	-15	+10	-12 +10 -5 -2
9+	-13	+10	-10 +13 -3 0
10+	-10	+9	-10 +9 -1 -1
12+	-12	+11	-12 +10 -1 -2
14+	-10	+9	-10 +9 -1 -1
16+	8	8	8 8 0 0
18+	8	8	8 8 0 0
20+	7	8	7 8 +1 +1
22+	9	9	9 9 0 0

SWAMP

LINE	#28N H	Lo			Diff	
STN	C	H	C	H	H	Lo
20+ $\frac{1}{2}$ N	-19	-7	-11	+13	-26	-8
21+ \downarrow	-15	-7	-7	+2	-22	-5
22+	-13	-10	-6	0	-23	-6
23+	-13	-8	-6	-2	-21	-8
24+	-12	-7	-5	-2	-19	-7
25+	-9	-6	+4	0	-15	-4
26+	-9	-2	-4	0	-11	-4
27+	6	-3	-2	0	-9	-2
28+	-5	-4	-1	0	-9	-1
29+	-6	-5	-1	-1	-11	-2
30+	-8	0	-5	+3	-8	-2
31+	-9	+3	-6	5	-6	-1
32+	11	4	7	5	-7	-2
33+	6	3	3	3	-3	0
34+	-3	+2	-3	+3	-1	0
35+	9	2	3	2	-2	-1
36+	3	2	1	2	-1	+1
37+	-1	+3	-1	+3	+2	+2
38+	6	4	4	4	-2	0
39+	8	5	7	5	-3	-2
40+	6	5	6	5	-1	-1
41+	6	4	5	4	-2	-1
42+	6	2	3	2	-4	-1
43+	5	2	3	3	-3	0
44+	8	2	4	3	-6	-1
45+	7	0	2	1	-7	-1
46+	8	0	3	1	-8	+2

LINE	40	H1	L0		L1	
STN	C	H	C	H	H1	L1
22+ $\frac{1}{2}$ S	-13	+14	-13	+14	+1	+1
20+ ↓	11	12	11	12	+1	+1
18+	10	9	10	9	-1	-1
16+	10	9	10	9	-1	-1
15+	-13	+2	-13	+6	-11	-7
14+	-17	+3	-15	+3	-14	-12
	-15	+2	-13	6		
13+	-13	+5	-13	+5	-8	-8
12+	-12	0	-15	+5	-12	-10
10+	-17	-8	-19	-2	-25	-21
8+	-23	-4	-20	+4	-27	-16
6+	-26	-3	-20	+8	-29	-1
4+	-24	+2	-19	+10	-22	-9
2+	-24	+2	-18	+6	-22	-12
BL+ $\frac{1}{2}$ S	-22	-6	-14	+4	-28	-18

LINE 28N cont'd

47+	-8	-1	-3	-1	-9	-4
48+	7	0	-1	0	-7	-1
49+	-6	-6	0	-2	-12	-2
50+	-7	-7	-2	-2	-14	-4
51+	-9	-8	-4	-2	-17	-6
52+	11	6	4	2	17	6
53+	-13	-5	-6	0	-18	-6
54+	-11	-10	-4	-3	-21	-
55+	12	-8	-5	-2	20	-
56+	11	-10	-2	-2	-21	-4
57+	-4	-10	+2	-4	-14	-
58+	8	-14	+6	-8	14	-

INE 64	H	LO	Diff
STN	C	H	C H H ₁ L ₀
1+50'S	-1	0	-1 0 -1 -1
3+ ↓	-2	+3	-3 +2 +1 -1
5+	6	5	6 5 -1 -1
7+	9	10	10 10 +1 0
9+	14	13	14 13 -1 -1
11+	14	14	14 14 0 0
13+	11	11	11 11 0 0
15+	8	8	8 8 0 0
17+	10	9	9 9 -1 0
19+	9	9	9 9 0 0
21+	4	4	4 4 0 0
23+	1	3	1 3 +2 +2
25+	4	3	4 3 -1 -1
27+	5	5	5 5 0 0
29+	5	3	5 3 -2 -2
30+	3	3	3 3 0 0
31+	4	3	4 3 -1 -1
33+	3	3	4 3 0 -1
35+	4	4	4 4 0 0
37+	5	5	5 5 0 0
39+	7	6	7 6 -1 -1
41	7	8	7 8 +1 +1
43	12	11	12 11 -1 -1
45	14	14	14 14 0 0
47	12	12	12 12 0 0

LINE	#56	H1	20		Diff	
STN	C	H	C	H	H1	
46 $\frac{1}{2}$ S	-12	+12	-12	+12	0	0
44 \downarrow	-10	+9	-10	+9	-1	-1
42+	7	7	7	7	0	0
40+	6	6	6	6	0	0
38+	5	5	5	5	0	0
36+	-3	+2	-3	+2	-1	-1
34+	3	3	3	3	0	0
32+	5	5	5	5	0	0
30+	4	4	4	4	0	0
28+	5	4	5	4	-1	-1
26+	6	6	6	6	0	0
24+	9	10	9	10	+1	+1
22+	9	10	9	10	+1	+1
20+	8	8	8	8	0	0
18+	7	6	7	6	-1	-1
16+	8	9	9	9	+1	0
14+	9	9	9	9	0	0
12+	8	8	8	8	0	0
10+	8	8	8	8	0	0
8+	7	7	7	7	0	0
6+	6	6	6	6	0	0
4+	5	5	5	5	0	0
2+	5	5	5	5	0	0
B.L+ $\frac{1}{2}$ S	4	4	4	4	0	0
1+ $\frac{1}{2}$ N	5	4	5	4	-1	-1
3 \downarrow	5	5	5	5	0	0

LINE #56	H		L0		diff	
STN	C	H	C	H	H1	L0
5+N	6	4	5	4	-2	-1
7+	-7	-2	-6	+2	-9	-4
8+	-15	+3	-10	+3	-12	-7
9+	-21	-2	-16	+2	-23	-14
10+	-25	-10	-20	0	-35	-20
11+	-22	-10	-19	0	-32	-19
12+	-20	-10	-15	0	-30	-15
13+	-20	-6	-15	0	-26	-16
14+	-18	-6	-15	0	-24	-15
15+	-17	-10	14	0	-27	-14
16+	-15	-8	-12	-4	-23	-16
17+	-15	-8	-11	-2	-23	-13
18+	-13	-5	-9	0	-18	-9
19+	-12	-5	8	0	-17	-8
20+	-10	-4	-6	-2	-14	-8

→ 14¹/₂N 0 0 0 0 0 0

LINE #64						
18+	0	-3	+1	-3	-3	-2
17+	+1	-3	+1	-3	-2	-2
16+	0	0	0	0	0	0
15+	0	+1	0	+1	+1	+1
13+	-3	+2	-3	+2	-1	-1
11+	-3	+2	-3	+2	-1	-1
9+	-2	+1	-2	+1	-1	-1
7+	-1	+2	-1	+2	+1	+1
5+	-1	+2	-1	+2	+1	+1
3+	3	2	2	2	-1	0

LINE #	72	H ₁	L ₀		L ₁	
STN	C	H	C	H	H ₁	L ₀
1+ ¹ / ₂ 8	-2	+2	-2	+2	0	0
3+ W	7	7	7	7	0	0
5+	15	16	15	16	+1	+1
7+	16	16	16	16	0	0
9+	17	16	16	16	-1	0
11+	15	15	15	15	0	0
13+	9	9	9	9	0	0
15+	9	5	9	5	+1	+1
17	3	4	3	4	+1	+1
19	9	3	9	3	-1	-1
21	9	9	9	9	0	0
23	9	9	9	9	0	0
25	5	5	5	5	0	0
27	5	5	5	5	0	0
29	9	3	9	3	-1	-1
31	9	9	9	9	0	0
33	9	9	9	9	0	0
35	5	5	5	5	0	0
37	5	5	5	5	0	0
39	6	6	6	6	0	0
41	8	7	8	7	-1	-1
43	8	7	8	7	-1	-1
45	5	5	5	5	0	0
47	6	5	6	5	-1	-1

Swamp

NE 80

H₁

L₀

Diff

STN	C	H	C	H	H ₁	L ₀
47 ^{1/2} S	5	5	5	5	0	0
45+	4	4	4	4	0	0
43+	4	4	4	4	0	0
41	5	5	5	5	0	0
39	6	7	6	7	+1	+1
37	6	5	6	5	-1	-1
35	6	6	6	6	0	0
33	5	5	5	5	0	0
31	4	4	4	4	0	0
29	4	3	4	3	-1	-1
27	-3	+1	-3	+1	-2	-2
25	-2	+1	-2	+1	-1	-1
23	5	5	5	5	0	0
21	6	5	6	5	-1	-1
19	3	3	3	3	0	0
17	3	3	3	3	0	0
15	3	3	3	3	0	0

14. Claim Posts. ACE #56 Post 1; #55; #54; #53

13+	3	3	3	3	0	0
11+	8	7	7	7	-1	0
9+	11	12	11	12	+1	+1
7+	12	11	12	11	-1	-1
5+	7	7	7	7	0	0
3+	11	12	12	12	+1	0
1+	5	5	5	5	0	0

LINE # 8 ON		Hi		Lo		diff	
STN	C	H	C	H	H ₁	Lo	
B.L. + 1/2 N	5	5	5	5	0	0	
2 + 1/2 V	6	6	6	6	0	0	
4 +	6	6	6	6	0	0	
6 +	6	5	6	5	-1	-1	
8 +	4	4	4	4	0	0	
10 +	4	3	4	3	-1	-1	
12 +	2	2	2	2	0	0	
14 +	0	0	0	0	0	0	
16 +	+1	-1	+1	-1	0	0	
18 +	+2	-4	+3	-4	-2	-1	

LINE # 72 N

18 + 20 V	+3	-4	+3	-4	-1	-1	
16 + V	+1	-2	+1	-2	-1	-1	
14 +	+2	-2	+2	-2	0	0	
12 +	0	-1	0	-1	-1	-1	
10 +	-1	0	-1	0	-1	-1	
11	50' W CLAIM POSTS,		16, 15; 17, 18 W Barclay				
8 +	0	0	0	0	0	0	
6 +	-1	+1	-1	+1	0	0	
4 +	-3	+1	-2	+1	-2	-1	
2 +	0	0	0	0	0	0	
B.L. + 1/2 N	0	0	0	0	0	0	

Corner of airstrip

NE#	88	H ₁		20		Diff	
STN	C	H		C	H	H	LO
+ ¹ / ₂ S	-7	+5		-7	+5	-2	-2
x ↓	4	4		5	4	0	-1
5+	8	7		8	7	-1	-1
7+	10	7		10	7	-3	-3
9+	12	12		12	12	0	0
0+	5	4		5	4	-1	-1
2+	0	-1		0	-1	-1	-1
AIM LINE							
14+	6	5		6	5	-1	-1
16+	5	7		6	7	+2	+1
18+	8	7		8	7	-1	-1
20+	3	3		3	3	0	0
22+	-3	+1		-3	+1	-2	-2
24+	1	2		2	2	+1	0
26+	3	3		4	3	0	-1
28+	4	4		4	4	0	0
30+	3	3		3	3	0	0
32+	3	3		3	3	0	0
34+	6	4		5	4	-2	-1
36+	4	5		4	5	+1	+1
38+	4	4		5	4	0	-1
40+	6	5 NOISE		6	5 NOISE	-1	-1
41+	5	6		5	6	+1	+1
43+	6	4		5	4	-2	-1
45+	5	3		5	3	-2	-2
47+	5	3		5	3	-2	-2
49+	6	5		6	5	-1	-1
50+	6	5		6	6	+1	0

LINE # 96⁺ H1 L0 diff

STN	C	H	C	H	H1	L0
48+ ² S	-8	+8	-8	+8	0	0
46+ ⁺ ↓	9	9	9	9	0	0
44+	9	10	9	10	+1	+1
42+	9	7	9	7	-2	+2
40+	7	6	7	6	-1	-1
38+	8	7	8	7	-1	-1
36+	10	9	10	9	-1	-1
34+	8	6	8	6	-2	-2
32+	7	6	7	6	-1	-1
30+	4	4	4	4	0	0
28+	2	2	2	2	0	0
26+	2	1	2	1	-1	-1
24+	+1	-2	+1	-2	-1	-1
22+	0	0	0	0	0	0
20+	+1	-1	+1	-1	0	0
18+	+2	-2	+1	-2	-1	-1
16+	-2	+1	-2	+1	-1	-1
14+	-6	+5	-6	+5	-1	-1
12+	-2	+3	-2	+3	+1	+1
10+	-2	+2	-2	+2	0	0
Swampy	+1	+2	-2	+2	0	0
RUST	6	+9	-8	+9	+1	+1
4+	-15	+15	-15	+15	0	0
2+	15	14	15	14	-1	-1
BL+ ² S	9	11	9	11	+2	+2

CLAIM LIN

LINE 96	H ₁		L ₀		diff	
STN	C	H	C	H	H ₁	L ₀
1 1/2 N	-9	+8	-9	+8	-1	-1
3 + ↓	6	6	6	6	0	0
5 +	7	7	7	7	0	0
7 +	8	8	8	8	0	0
9 +	8	6	8	6	-2	-2
LIM LINE 11 +	6	6	6	6	0	0
13 +	0	+1	0	+1	+1	+1
15 +	+2	-1	+2	-1	+1	+1
17 +	+3	-4	+3	-4	-1	-1

LINE 104

17 1/2 N	-1	+1	-1	+1	0	0
15 + ↓	3	3	3	3	0	0
13 +	4	5	4	5	+1	+1
11 +	6 1/2	6	6 1/2	6	-1/2	-1/2
LIM LINE 9 +	8	8	8	8	0	0
7 +	12	12	12	12	0	0
5 +	15	16	15	16	+1	+1
3 +	16	16	16	16	0	0
1 +	15	15	15	15	0	0
BL 1/2 S	18	19	18	19	+1	+1
2 + ↓	10	10	10	10	0	0
4 +	4	3	4	3	-1	-1
6 +	8	8	8	8	0	0
8 +	-2	+2	-2	+2	0	0
10 +	+2	-2	+2	-2	0	0
12 +	+5	-4	+5	-4	+1	+1
13 +	+8	-7	+8	-7	+1	+1

LINE#	109	H1	LO		Diff	
STN.	C	H	C	H	H1	LO
16+ ¹ / ₂ S	+4	-4	+4	-4	0	0
18+ $\sqrt{\ominus}$	-	-2	0	-2	-2	-2
20+	0	0	0	0	0	0
22+	-2	+2	-2	+2	0	0
24+	+2	-3	+2	-3	-1	-1
26+	+3	-3	+3	-3	0	0
28+	-1	+1	-1	+1	0	0
30+	-2	+3	-2	+3	+1	+1
32+	-5	+4	-5	+4	-1	-1
34+	-7	+5	-7	+5	-2	-2
36+	9	8	9	8	-1	-1
38+	8	9	8	9	+1	+1
40+	9	9	9	9	0	0
42+	12	11	12	11	-1	-1
44+	13	13	13	13	0	0
46+	10	10	10	10	0	0
48+	12	12	12	12	0	0

L28N

59+	-18	+3	-10	+9	-15	-1
60+	+3	-20	+11	-14	-17	3
61+	-26	+9	-20	+14	22	6
62+	0	-32	+18	-22	-32	-6
63+	+3	-40	+18	26	-37	-8
64+	+3	-38	+18	-26	35	8
65+	+3	-35	+12	-26	32	14
66+	-3	-30	+6	-25	33	19
67+	-7	-35	+2	-24	42	22

STN	C	H	C	H	H ₁	L ₀
18+ ¹² S	+12	-13	+12	-13	-1	-1
16+ ¹² V	0	0	0	0	0	0
14+	+5	+5	+5	-4	0	+1
12+	+8	-8	+8	-7	0	+1
10+	+12	-12	+12	-12	0	0
8+	+14	+14	+14	-14	0	0
6+	+15	-15	+15	-15	0	0
4+	+15	-15	+15	-14	0	+1
2+	+16	-16	+16	-16	0	0
18+	+18	-18	+18	-18	0	0
16+	+18	-18	+18	-18	0	0
14+	+15	-15	+15	-15	0	0
12+	+15	-15	+15	-15	0	0
10+	+17	-17	+17	-17	0	0
8+	+18	-18	+18	-18	0	0
6+	+17	-17	+17	-17	0	0
4+	+17	-17	+17	-17	0	0
2+	+19	-20	+19	-20	-1	-1
18+	+19	-20	+19	-20	-1	-1
16+	+23	-22	+23	-22	+1	+1
14+	+27	-28	+27	-28	-1	-1
12+	+26	-27	+26	-27	-1	-1
10+	+30	-32	+30	-32	-2	-2
8+	+29	-30	+29	-30	-1	-1
6+	+5	+5	+5	+5	+1	+1

LINE#	120	H1	L0		Diff	
STN	C	H	C	H	H1	L0
1+50 N	-3	+2	-3	+2	-1	-1
3+ ↓	-3	+2	-3	+2	-1	-1
5+	+6	-7	+6	-7	-1	-1
7+	+8	-8	+8	-8	0	0
9+	+3	-3	+3	-3	0	0
11+	-6	+5	-6	+5	-1	-1
13+	-5	+5	-5	+5	0	0
15+	-9	+3	-9	+3	-1	-1
17+	-3	+3	-3	+3	0	0
19+	+3	+3	-3	+3	0	0

Line# 112

19+50 N	+9	-9	+9	-9	0	0
17+ ↓	+9	-9	+9	-9	0	0
15+	+9	-9	+9	-9	0	0
13+	+7	-7	+7	-7	0	0
11+	+5	-5	+5	-5	0	0
9+	+1	-1	+1	-1	0	0
7+	-1	0	-1	0	-1	-1
5+	-5	+4	-5	+4	-1	-1
3+	-13	+12	-13	+12	-1	-1
1+	-6	+6	-6	+6	0	0
11+50 S	+2	-3	+2	-3	-1	-1
3+ ↓	+14	-15	+14	-15	-1	-1

LINE #	112 H ₁		Lo		Diff	
	STN	C	H	C	H	H ₁ Lo.
5+	+17	-17	+17	- 17	0	0
7+	+20	-22	+20	-22	-2	-2
9+	+26	-27	+26	-27	-1	-1
11+	+21	-21	+21	-21	0	0
13+	+19	-17	+19	-17	+2	+2
15+	+17	-17	+17	-17	0	0
17+	+17	-17	+17	-17	0	0
19+	+16	-15	+16	-15	+1	+1
21+	+17	-17	+17	-17	0	0
23+	+15	-15	+15	-15	0	0
25+	+15	-14	+15	-14	+1	+1
27+	+17	-16	+17	-16	+1	+1
29+	+17	-16	+17	-16	+1	+1
31+	+19	-12	+14	-12	+2	+2
33+	+10	-9	+10	-9	+1	+1
35+	+12	-10	+12	-10	+2	+2
37+	+11	-9	+11	-9	+2	+2
39+	+9	-8	+9	-8	+1	+1
41+	+6	-7	+6	-7	-1	-1
43+	+5	-5	+5	-5	0	0
45+	+5	-5	+5	-5	0	0
47+	+5	-4	+5	-4	+1	+1
49+						
50+						

2 stations 43's

ST LINE	H ₁	Lo	Diff			
STN	C	H	C	H	H ₁	Lo
1+ $\frac{1}{2}$ S	21	13	18	16	-8	-2
2+ ↓	21	12	17	15	-9	-2
3+	24	16	20	18	-8	-2
4+	18	16	17	16	-2	-1
5+	16	11	13	13	-5	0
6+	10	8	10	10	-2	0
7+	13	10	11	10	-3	-1
8+	12	12	12	12	0	0
9+	12	11	11	11	-1	0
10+	11	11	11	11	0	0
1+ $\frac{1}{2}$ N	18	9	14	11	-9	3
2+ ↓	22	13	17	15	-9	-2
3+	24	15	19	19	9	0
4+	23	17	18	17	6	1
5+	27	22	25	23	5	-2
6+	25	26	25	26	+1	+1
7+	28	28	27	28	+1	+1
8+	19	21	19	20	+2	+2
9+	18	19	18	20	+1	+2
10+	17	17	17	17	0	0
11+	16	16	16	16	0	0

LINE#	12	H ₁	L ₀		Diff	
STN	C	H	C	H	H ₁	L ₀
1 1/2 S	34	10	29	19	24	10
2+ ↓	35	17	30	20	28	10
3+	34	16	28	22	16	8
4+	29	16	24	18	-13	-6
5+	27	18	23	18	-9	-5
6+	27	18	24	18	-9	-6
7+	25	16	22	16	9	6
8+	22	12	19	14	10	5
9+	20	10	19	14	10	5
10+	25	14	22	16	11	6
11+	24	12	23	14	12	9
12+	26	10	23	14	16	9
13+	23	8	21	13	15	8
14+	23	9	21	14	14	7
15+	21	10	19	12	11	7
16+	19	12	17	14	-7	-3
17+	17	14	16	14	-3	-2
18+	13	13	12	13	0	+1
19+	10	11	11	11	+1	0
20+	10	10	10	10	0	0
1 1/2 N	22	5	23	14	-17	9
2+ ↓	33	20	33	25	-13	-8
3+	43	32	39	35	-11	-4
4+	43	41	41	40	-2	-1
5+	51	49	49	49	-2	0
6+	51	50	51	50	-1	-1
7+	52	50	52	50	+2	-2

LINE#	12	H ₁	Lo	Stiff
STN	C	H	C	H H ₁ Lo
8+	-48	+46	-46	146 -2 0
9+	41	42	40	42 +1 +2
10+	32	35	33	35 +3 +2
11+	31	33	32	33 +2 +1
12+	30	30	30	30 0 0
13+	23	25	24	25 +2 +1
14+	20	23	21	23 +3 +2
15+	20	21	20	21 +1 +1
16+	16	16	16	16 0 0
17+	13	14	13	14 +1 +1
18+	15	15	15	15 0 0

128N (cont'd)

68+	-2	-35	+6	-25 -37 -19
69+	-2	-37	+6	-29 39 23
70+	-2	-34	+4	-26 -36 22
71+	-4	-30	+2	-25 -36 23
72+	-3	-28	+5	-20 -31 15
73+	+2	-35	+9	-27 -33 -18
74+	+2	-34	+8	-25 32 -17
75+	-3	-30	+5	-23 33 18
76+	-8	-30	0	-20 -38 -20
77+	-2	-30	+4	-20 32 -16
78+	-4	-31	+5	-22 35 -15
79+	0	-30	+5	-22 30 -19
80+	+9	-35	+12	-26 -26 14
81+	+9	-30	+13	-26 -21 -12
82+	-2	-30	+8	24 -32 -14

LINE # 28N (continued) Lo Diff

STN	C	H	C	H	H ₁	Lo
83+	0	-30	+5	-20	-30	-15
84+	+3	-26	+7	-20	-23	-13
85+	+4	-26	10	20	-22	-10
86+	+7	-30	+14	-22	-23	-8
87+	+8	-24	+12	-18	-16	-6
88+	+4	-16	+7	-12	-12	-5
^{bottom} 89+	+2	-12	+4	-9	-10	-5
90+	-3	-7	0	-5	-10	-5
91+	-6	-3	-4	0	-9	-4
92+	-9	+3	-7	+3	-6	-4
93+	-12	+7	-10	+7	-5	-3
94+	-13	+8	+2	+9	-5	-3
95+	-13	+6	-12	+6	-7	-6
96+	-8	+4	-7	+5	-4	-2
97+	-8	+3	-6	+3	-5	-3
98+	-8	+4	-8	+4	-4	-4
99+	-11	+6	-10	+6	-5	-4
100+	-12	+6	-10	+6	-6	-4
101+	-11	+6	-10	+6	-5	-4
102+	-14	+8	-12	+9	-6	-3

LINE#	20	H1	20	H	Diff	H1	20
STN	C	H	C	H			
1+ ¹ / ₂ S	-26	+4	-27	+10	-22	-17	
2+ ↓	25	-2	-25	+9	-27	-21	
3+	-26	0	-27	+6	-26	-21	
4+	-30	+5	-31	+12	-25	-19	
5+	-32	+13	-33	+18	-19	-15	
6+	-31	+13	-32	+20	-18	-12	
7+	-36	+15	-37	+26	-21	-11	
8+	-42	+26N	-40N	+28N	-16	-12	
9+	-39	+29	-38	+33	-10	-5	
10+	-37	+25	-35	+28	-12	-7	
11+	33	22	31	25	11	6	
12+	33	20	31	20	13	11	
13+	30	17	29	20	13	9	
14+	31	19	31	24	12	7	
15+	38	22	36	30	16	6	
16+	39	23	31	25	11	4	
17+	26	21	24	21	-5	-3	
18+	28	16	26	16	-12	10	
19+	20	19	20	19	-1	-1	
20+	19	18	19	18	-1	-1	
21+	18	18	18	18	0	0	
22+	17	16	16	16	-1	0	
23+	14	13	13	13	-1	0	
24	13	13	13	13	0	0	

Check

LINE # 24 H _i			L ₀		Diff	
STN.	C	H	C	H	H _i	L ₀
21 + $\frac{1}{2}$ S	-21	+21	-21	+21	0	0
20 + ↓	-19	+19	19	19	0	0
19 +	-16	+16	16	16	0	0
18 +	-18	+16	18	16	-2	-2
17 +	-20	+15N-20N	+20N	-6	0	
16 +	-29	+20N	-26	+22N	-9	-4
15 +	-33	+16N-28N	+22N	-17	-6	
14 +	-32	+16N	-30N	+22N	-16	-8
13 +	-32	+15	28	20	-17	-8
12 +	-29	+6	-30	+17	-23	-13
11 +	-24	+8	-25	+15	-16	-10
10 +	-30	+20	30	20	-10	-10
9 +	-38	+15	39	24	-23	-15
8 +	-45	+16	45	30	-21	-15
7 +	-45	+23	45	32	-22	-13
6 +	-46	+25	45	36	-21	-9
5 +	-43	+22	-43	+30	-21	-13
4 +	-41	+20	-41	30	-21	-11
3 +	-30	+12	32	16	-18	-16
2 +	-27	+8	27	14	-19	-13
1 +	-24	+7	24	13	-17	-11
0	-22	+4	22	9	-18	-13